

Thermodynamics and phase transitions in magnetic materials

Lecture 2

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Outline of Lecture 2

- More on the theory of tricritical transitions (see blackboard)
- An introduction to magnetic cooling (to be continued in Lecture 3)

Critical exponents: experiment vs theory for $d=3$

Transition type	Material	α	β	γ	ν
		$C \sim t ^{-\alpha}$	$\langle m \rangle \sim t ^\beta$	$\chi \sim t ^{-\gamma}$	$\xi \sim t ^{-\nu}$
Ferromag. ($n = 3$)	Fe, Ni	-0.1	0.34	1.4	0.7
Superfluid ($n = 2$)	He ⁴	0	0.3	1.3	0.7
Liquid-gas ($n = 1$)	CO ₂ , Xe	0.11	0.32	1.24	0.63
Superconductors		0	1/2	1	1/2
Mean-field		0	1/2	1	1/2

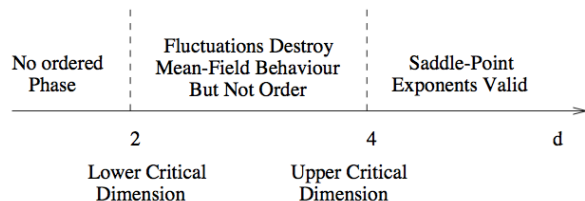
Here " t " is proportional to $T - T_c$

Table from Ben Simons' lectures on Phase Transitions and Collective Phenomena, U. Cambridge.

More comparisons

	Ising	X-Y	Heisenberg
d=1	No ordering!	No ordering!	No ordering!
d=2	$\beta=1/8$; $\gamma=7/4$	Special case!	No ordering!
d=3	$\beta=0.32$; $\gamma=1$	$\beta=0.35$; $\gamma=1$	$\beta=0.36$; $\gamma=1.39$
Mean field	$\beta=1/2$; $\gamma=1$		

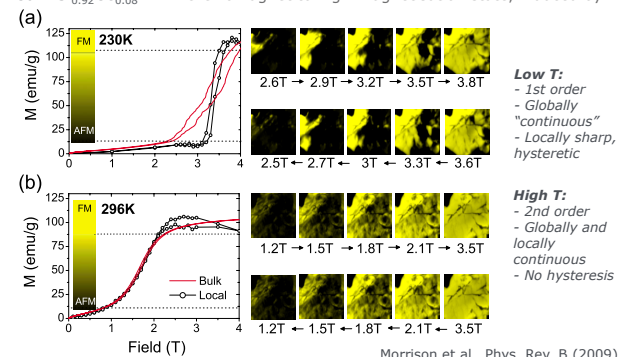
A phase diagram of the Ginzburg-Landau Hamiltonian



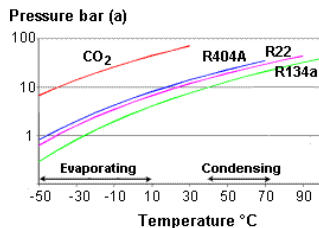
This diagram is from Ben Simons' lectures on Phase Transitions and Collective Phenomena, U. Cambridge.

CoMnSi: imaging tricriticality using a Hall probe

CoMnSi_{0.92}Ge_{0.08} Antiferromagnet to high-magnetisation state, induced by field



Vapour compression refrigeration



Refrigerant	Critical temp.	Critical pressure
CO ₂	31 °C	7.38 MPa
R22	96.2 °C	4.99 MPa
R134a	101 °C	4.06 MPa

Gas compression refrigeration works in *sub-critical* regime

The efficiency of the refrigerant is directly related to the critical temperature.

Tuning the *critical point* and the *pressure-temperature* phase line gradient are very important

Solid-state cooling at room temperature

**Ferroic cooling,
including magnetic
cooling**

Magnetic refrigeration: a growing area of interest

$$dG = -SdT - MdH_M + \sum_l^{m=l} K_l^m(H_M) d(Y_l^m(\Omega_M)) + Vdp + \dots$$



Ferroc Cooling

Project

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About This Site

Caloric Effects in Ferroc Materials: New Concepts for Cooling

DFG Priority Programme 1599

Project

Ratification is one of the main drives of the German and European electricity consumption and accordingly contributes to worldwide CO₂ emissions. High reduction potentials are envisaged if caloric effects in solid materials are utilized. The recent discovery of giant entropy changes associated with ferromagnetic phase transformations promises higher efficiency. Ferroc materials enhance the entropy change of magnetic, electro-thermo and electro-caloric effects. Furthermore, because the magnetocaloric effect is a solid state technology, it completely eliminates the need for high global-warming potential refrigeration refrigerants. The smaller footprint for operation and the scalable mechanism open up further applications such as cooling of microsystems. While the principal feasibility of magnetocaloric refrigeration is already evident, the requirement of a large magnetic field (> 2 T) hampers wide industrial and commercial applications. It is expected that this obstacle can be overcome by materials with lower hysteresis and by utilizing other types of field (stress, electric).

In order to accelerate research on ferroc cooling DFG decided to establish the priority program SPP 1599 in April 2011. This SPP will address the following major challenges for introducing ferroc materials in practical cooling applications: Understanding of the underlying mechanisms, energy efficiency, effect size, fatigue, and system integration.

Project proposals are required to cover one of the following "ferroc-caloric" material classes or combinations thereof: ferromagnetic, ferroelectric and ferroelastic materials. Proposals have to focus on basic or applied aspects of solid state cooling processes.

In detail, the research programme of the priority programme will focus on four key problems related to ferroc cooling:

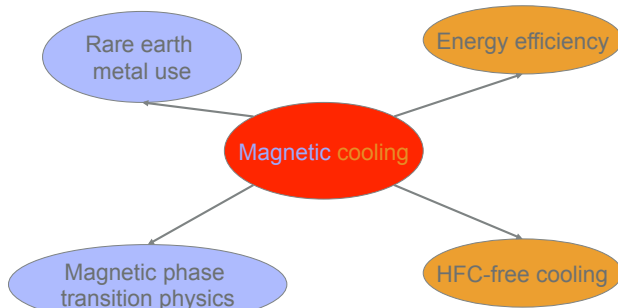
Magnetic cooling: the future

Cambridge

A careful system-wide cost and efficiency analysis revealed the benefit of magnetic cooling at low powers (< 500 Watt).

	Thermodynamic Ideal	Current Solution (Butane)	Magnetic A+++ Solution (no vacuum panels)
Target Cooling Power (W)	30	30	30
External Temperature (°C)	25	40	35
Internal Temperature (°C)	5	-15	0
Cooling Engine Power (W)	30	150	30
Technology Efficiency (%)	100%	43%	50%
Running Time (%)	100%	20%	100%
Carnot COP	14	2	4
Relative Efficiency	100%	14%	28%
Energy Consumption (W)	2.2	15	7.5

A research frontier



Magnetocaloric principles

Apply magnetic field adiabatically

$$S_{\text{total}} = S_{\text{magnetic}} + S_{\text{lattice}} + S_{\text{electronic}}$$

S_{magnetic} high
 S_{lattice} low

S_{magnetic} low
 S_{lattice} high

$$\Delta T_{\text{ad}}(H, T) = \frac{T \Delta S}{C_p}$$

Can also be described in terms of isothermal entropy change, ΔS :

$$\Delta S_{\text{total}}(H, T) = \int_0^H \left(\frac{\partial M(T, H')}{\partial T} \right)_H dH'$$

Maxwell relation for continuous $M(T, H)$

$$\Delta S_{\text{total}}(H, T) = -\Delta M \frac{dH_c}{dT}$$

Clausius-Clapeyron eqn. for 1st order transition in M

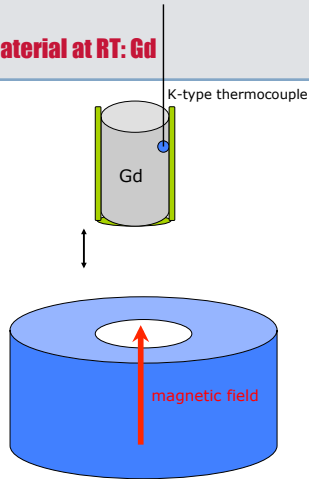
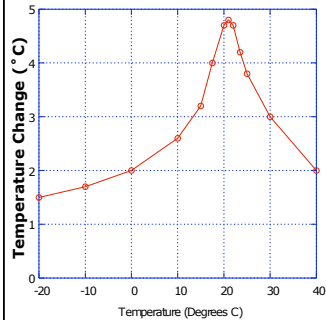
So the material (usually) heats in an applied field ($\Delta T_{\text{ad}} > 0$)

The effect is maximal at a (magnetic) phase transition

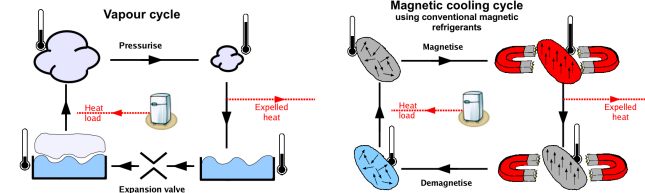
The sign of (dM/dT) is crucial and yields two possibilities for the MCE

Magnetocaloric benchmark material at RT: Gd

Adiabatic Magnetocaloric Effect in Gd (0-2T)



The cycle



K. G. Sandeman, Mag. Tech. Int. 1 30-32 (2011)

State of the art (2010)



Review

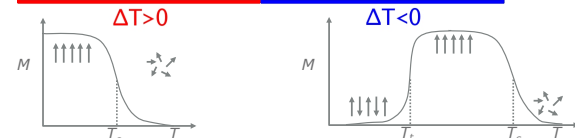
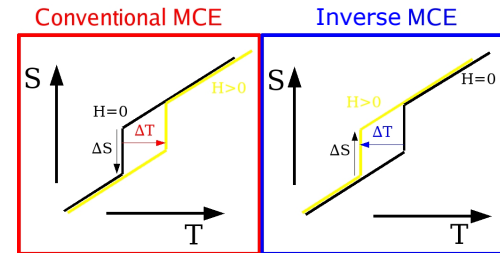
A review of magnetic refrigerator and heat pump prototypes built before the year 2010

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^b University of Applied Sciences of Western Switzerland, Institute of Thermal Sciences, CH-1401 Yverdon-les-Bains, Switzerland

Lists 41 prototypes to 2010.
 Most used Gd as refrigerant at that time.
 No clear example of end-user integration at that time.
 The situation has already changed in the 3 years since...

Magnetocaloric principles



What makes a good magnetic refrigerant?

Cheap
d-metal magnetism



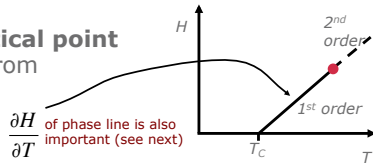
First order transition

because ΔT_{ad} of second order transition is too low (if d-metal alloy)

$$\Delta T_{ad}(H, T) = \frac{T \Delta S}{C_p}$$

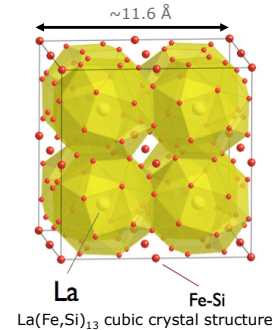
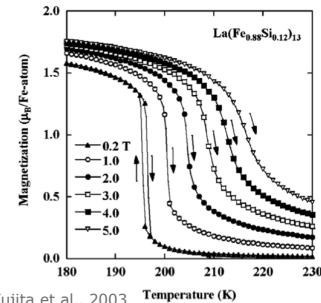
Proximity to (tri)critical point

Minimise energy loss from hysteresis



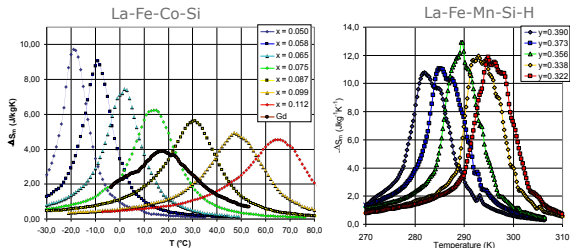
Single phase refrigerants

A candidate magnetic refrigerant at room temperature: La(Fe,Si)_{13}



Fujita et al., 2003

Tuning transition temperature



Magnetic entropy change as a function of temperature of: $\text{La(Fe}_{0.915}\text{Co}_{0.085}\text{Si}_{0.002})_{13}$ (left) and five $\text{LaFe}_{1.174}\text{Mn}_y\text{Si}_{1.28}\text{H}_{1.53}$ alloys with different y (right) for a magnetic field change of 1.6 T. The entropy change is higher than that seen in gadolinium (Gd, left plot only).