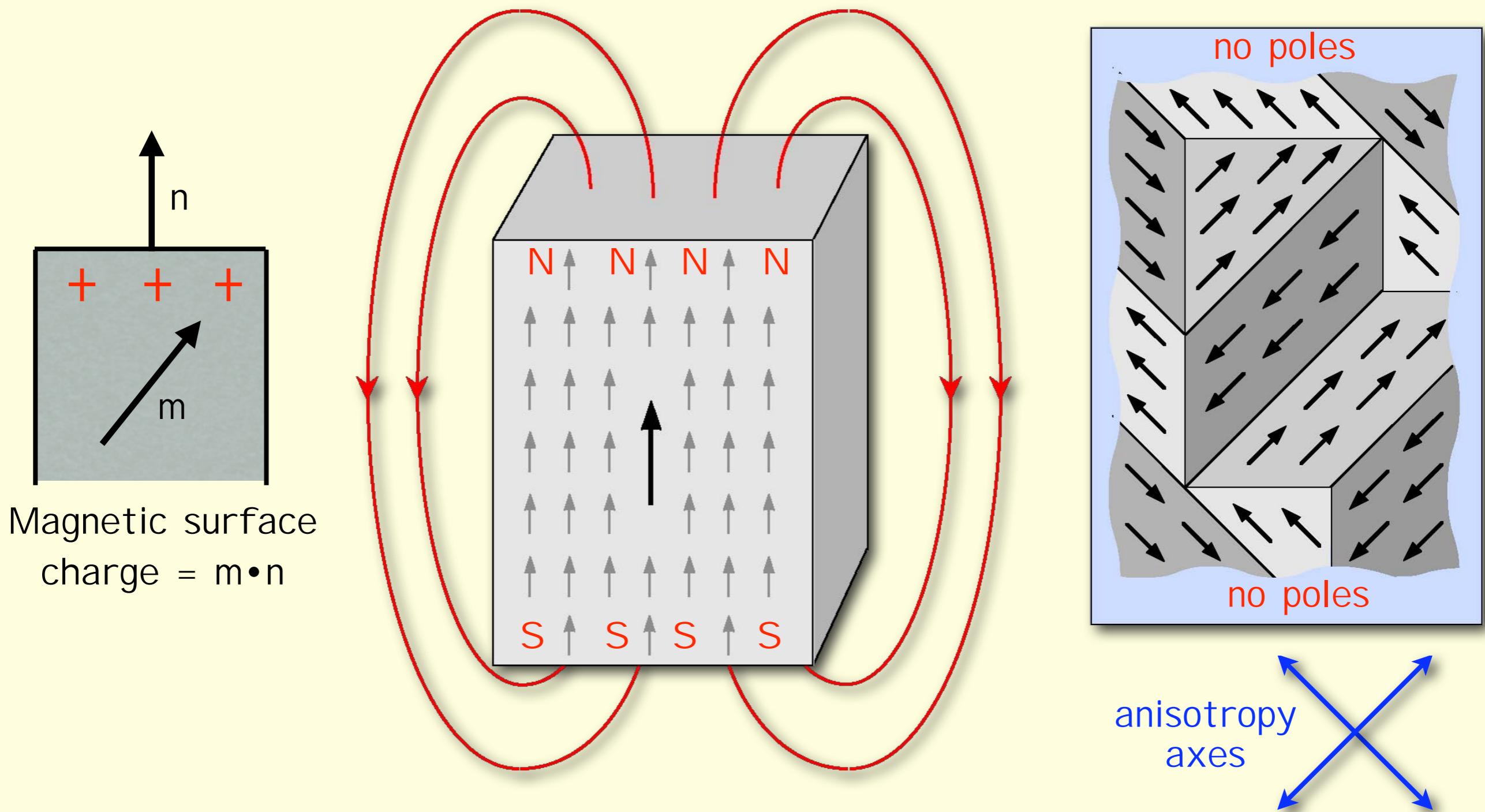

The Magnetic Microstructure of Nanostructured Materials

Magnetic Microstructure: Magnetic Domains



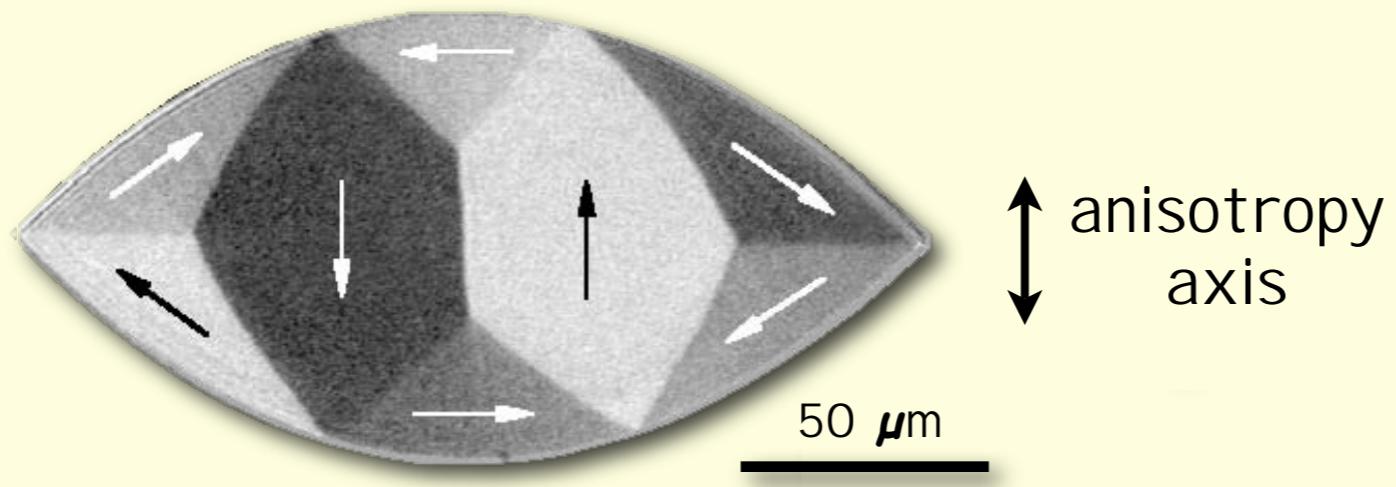
Magnetic Domains:
Areas of different magnetization direction,
but equal magnetization strength (M_s)

Quality factor Q

Character of magnetic domains is determined by quality factor Q
 (= material parameter)

$$Q = \frac{\text{Anisotropy constant } K}{\text{Stray-field energy coefficient } (K_d = \mu_0 M_s^2 / 2)}$$

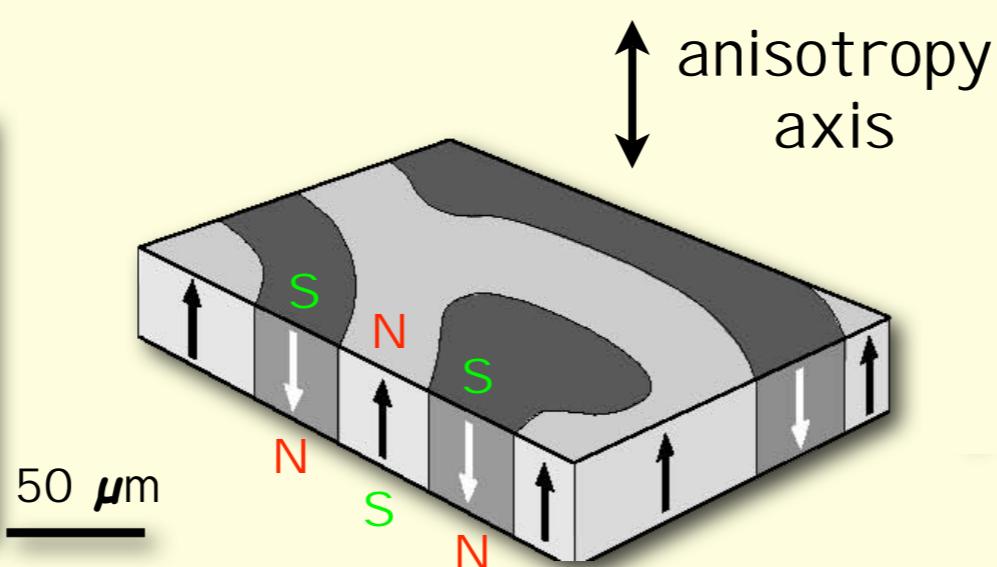
NiFe film element



$Q < 1$:

- stray field energy dominates
- flux-closed magnetization
- soft magnets

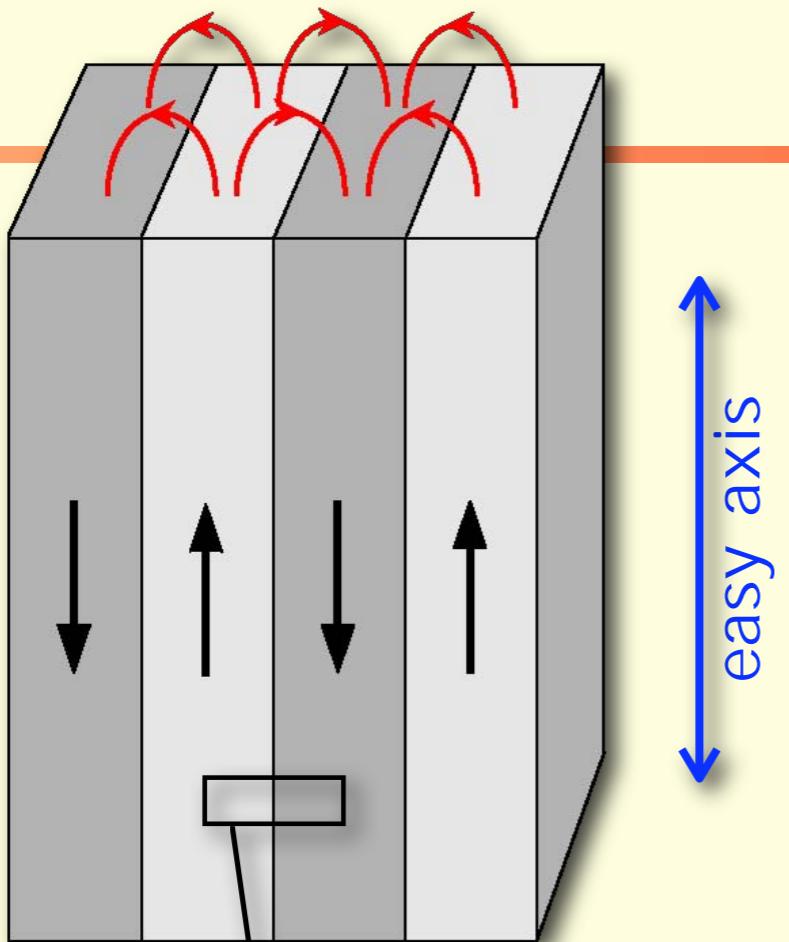
Garnet film



$Q > 1$:

- anisotropy energy dominates
- „open“ magnetization
- hard magnets

Domain wall

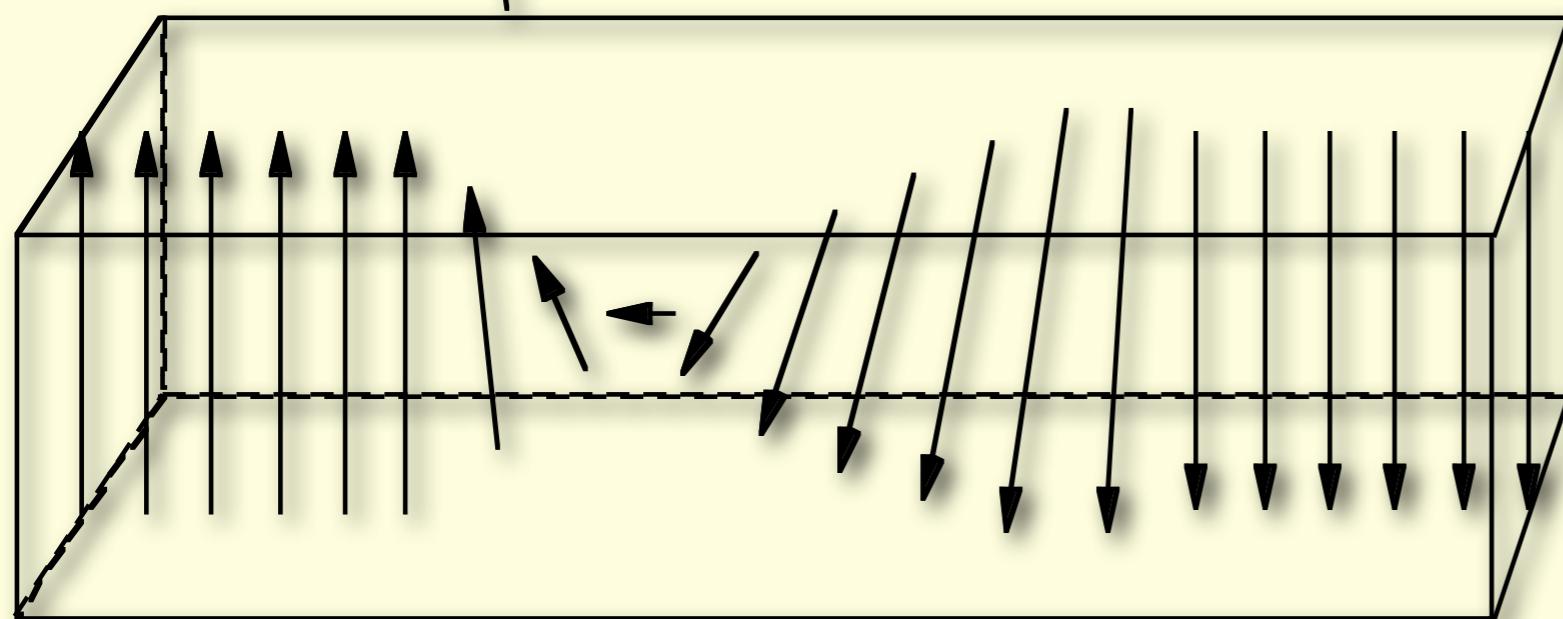


Bloch wall width:

$$\sim \sqrt{A/K}$$

A: exchange constant

K: anisotropy constant

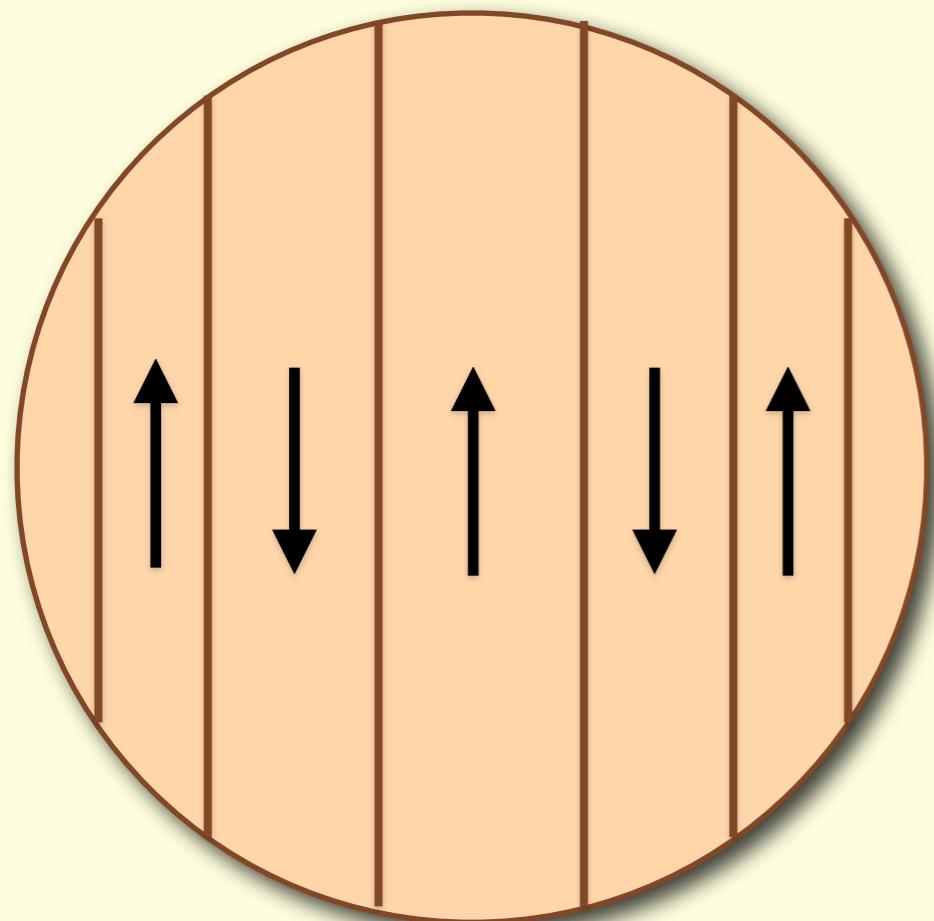


domain

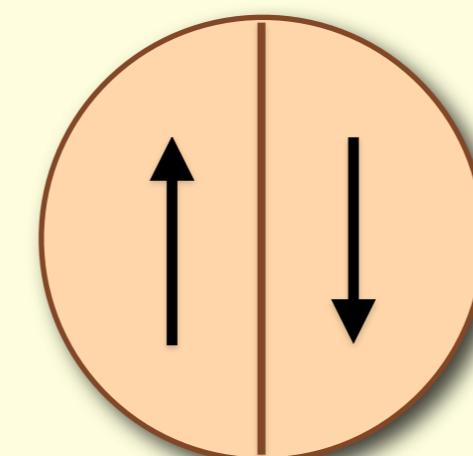
Bloch wall

domain

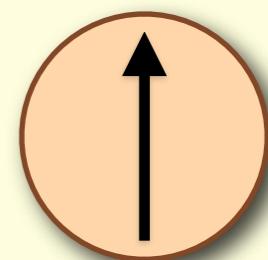
Single domain particle



Multi-domain
sample

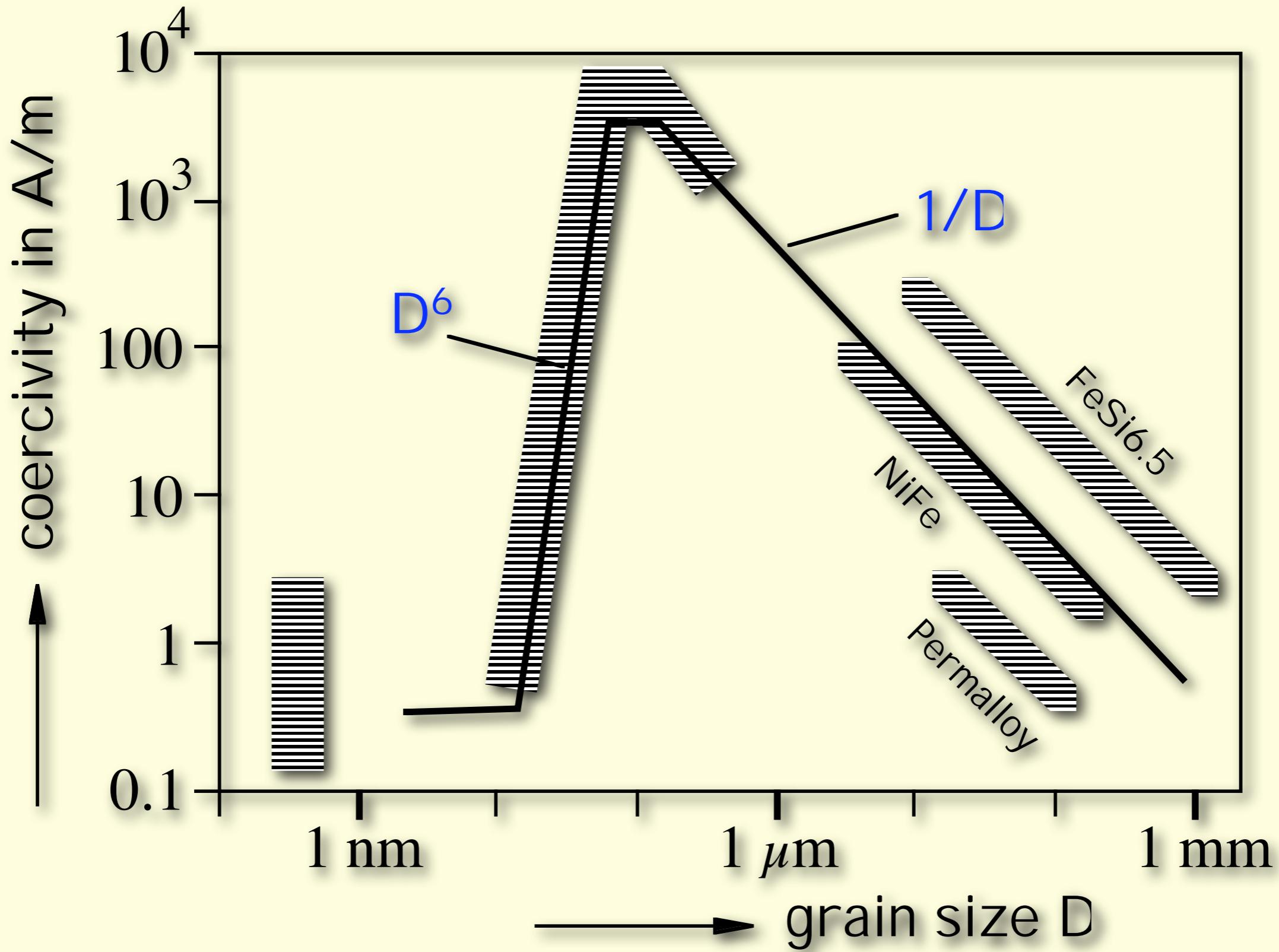


Multi-domain
particle

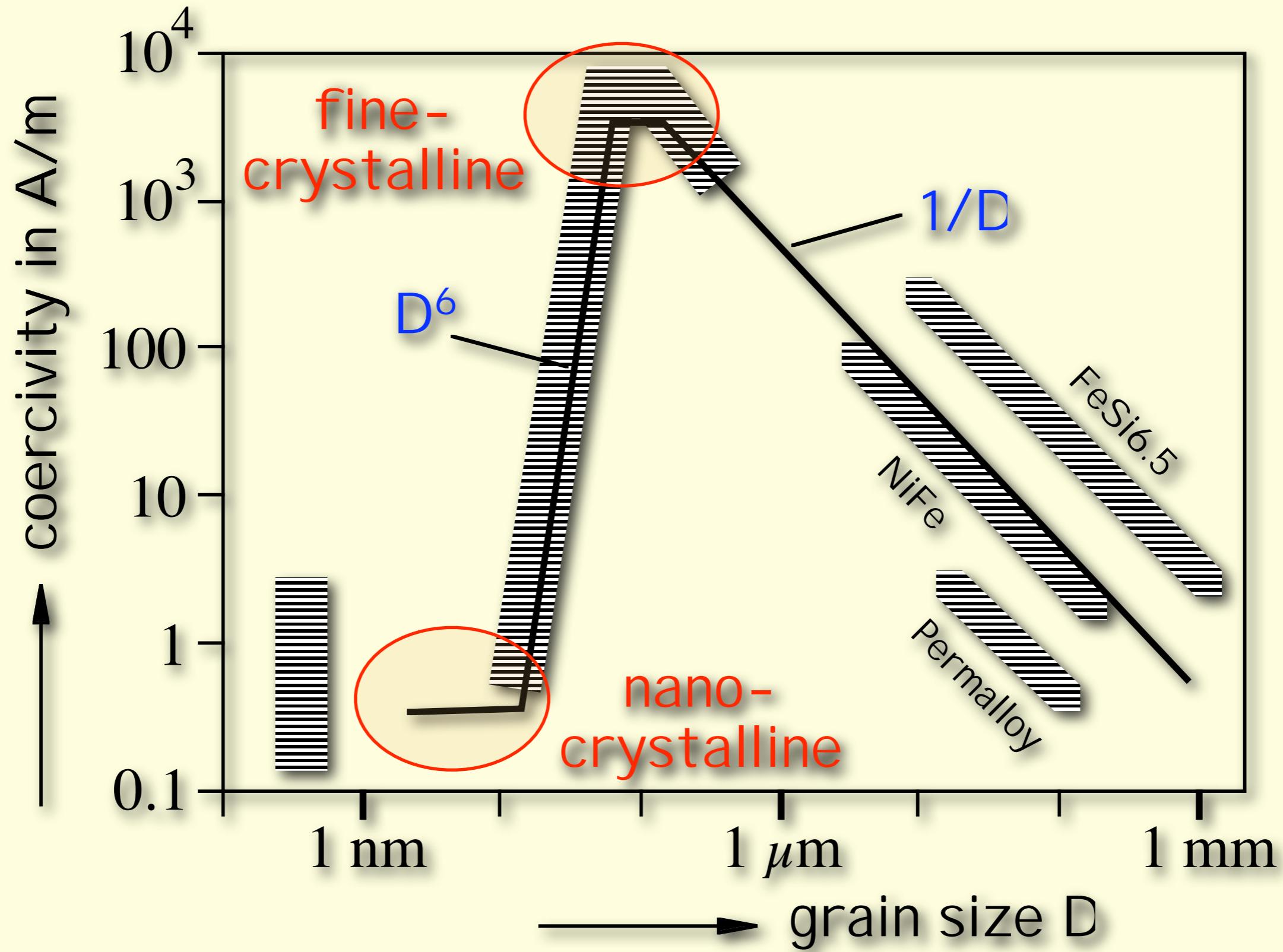


Single-domain
particle

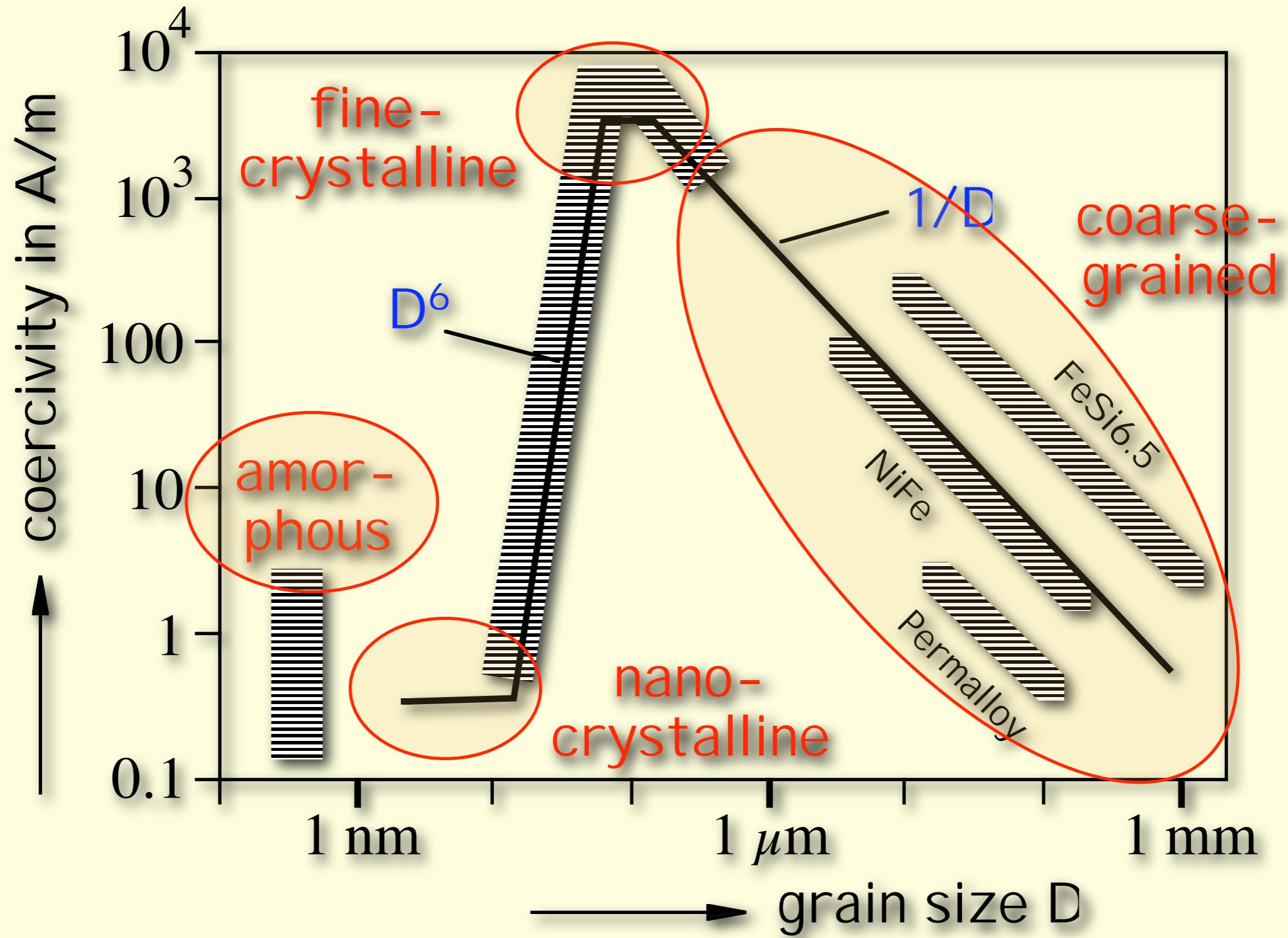
Coercivity and grain size



Coercivity and grain size



Coercivity and grain size



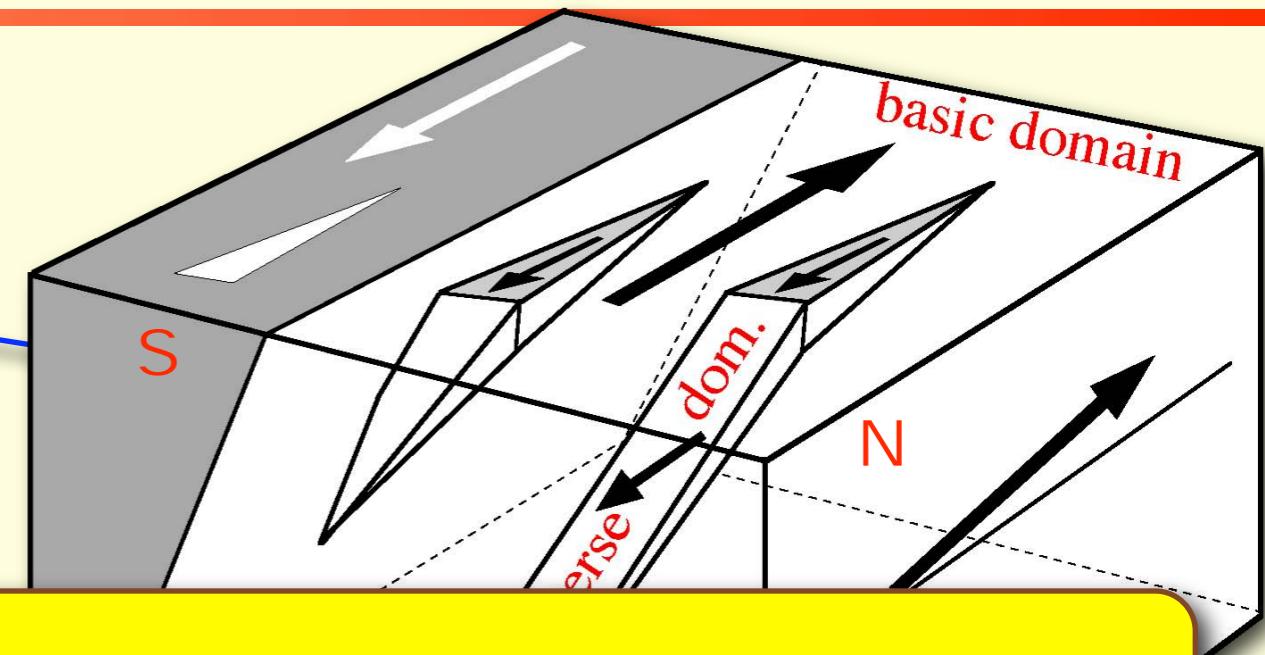
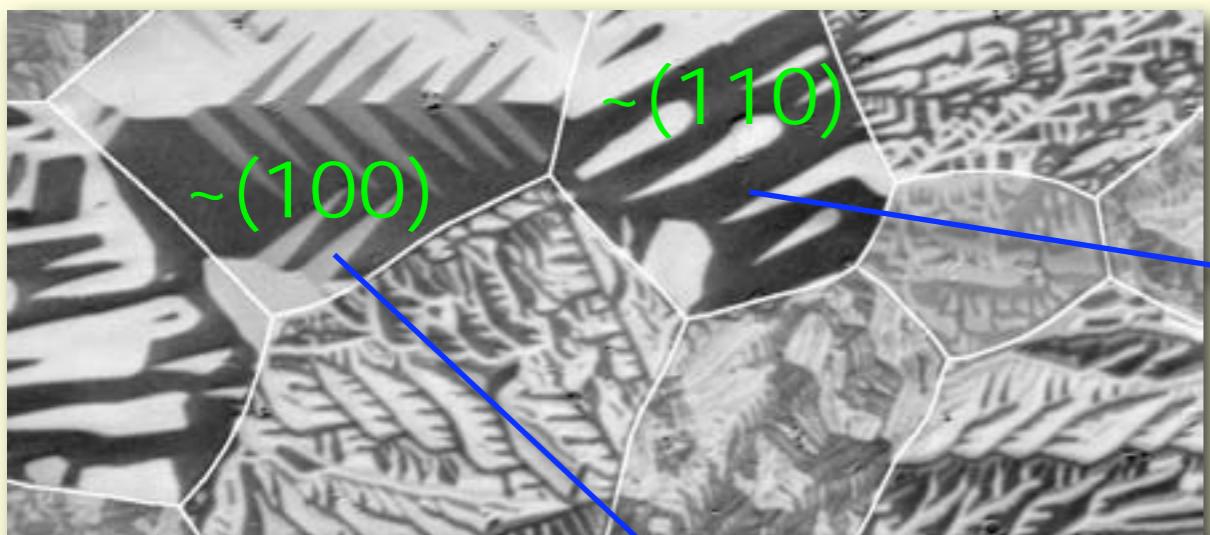
Overview

1. Domains in coarse-grained material
2. Domains in amorphous material
3. Domains in nanocrystalline,
soft magnetic ($Q \ll 1$) materials
4. Domains in fine- and nanostructured,
permanent magnetic ($Q > 1$) materials

Overview

1. Domains in coarse-grained material
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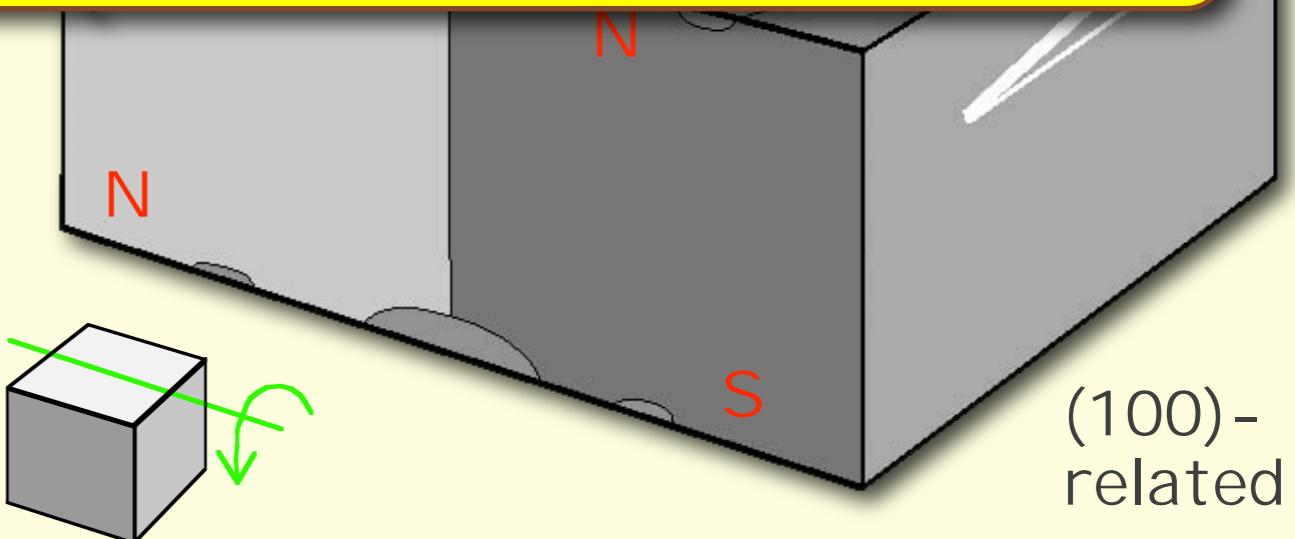
Non-oriented electrical steel



Domain character is determined by
surface orientation
of individual grains

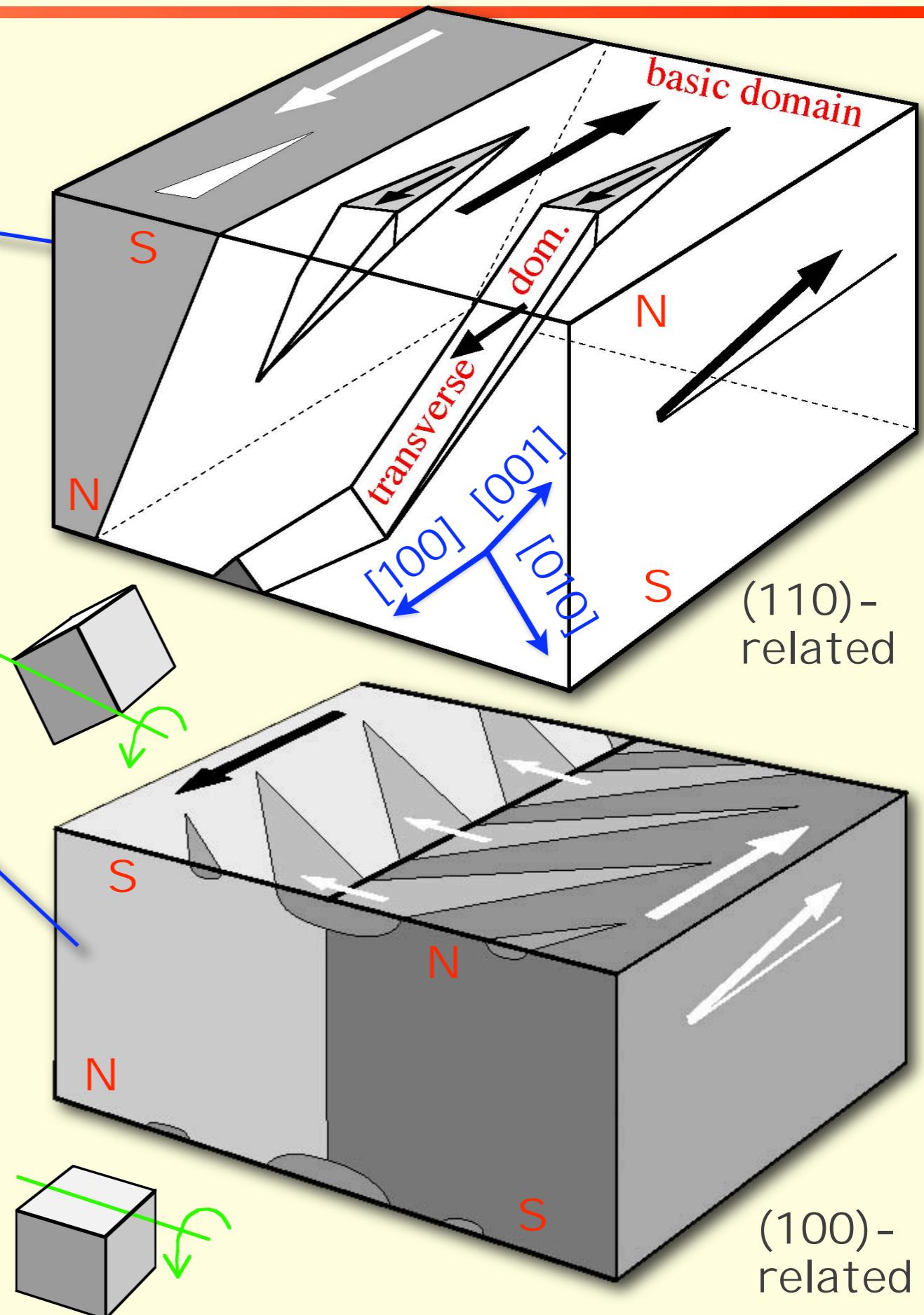
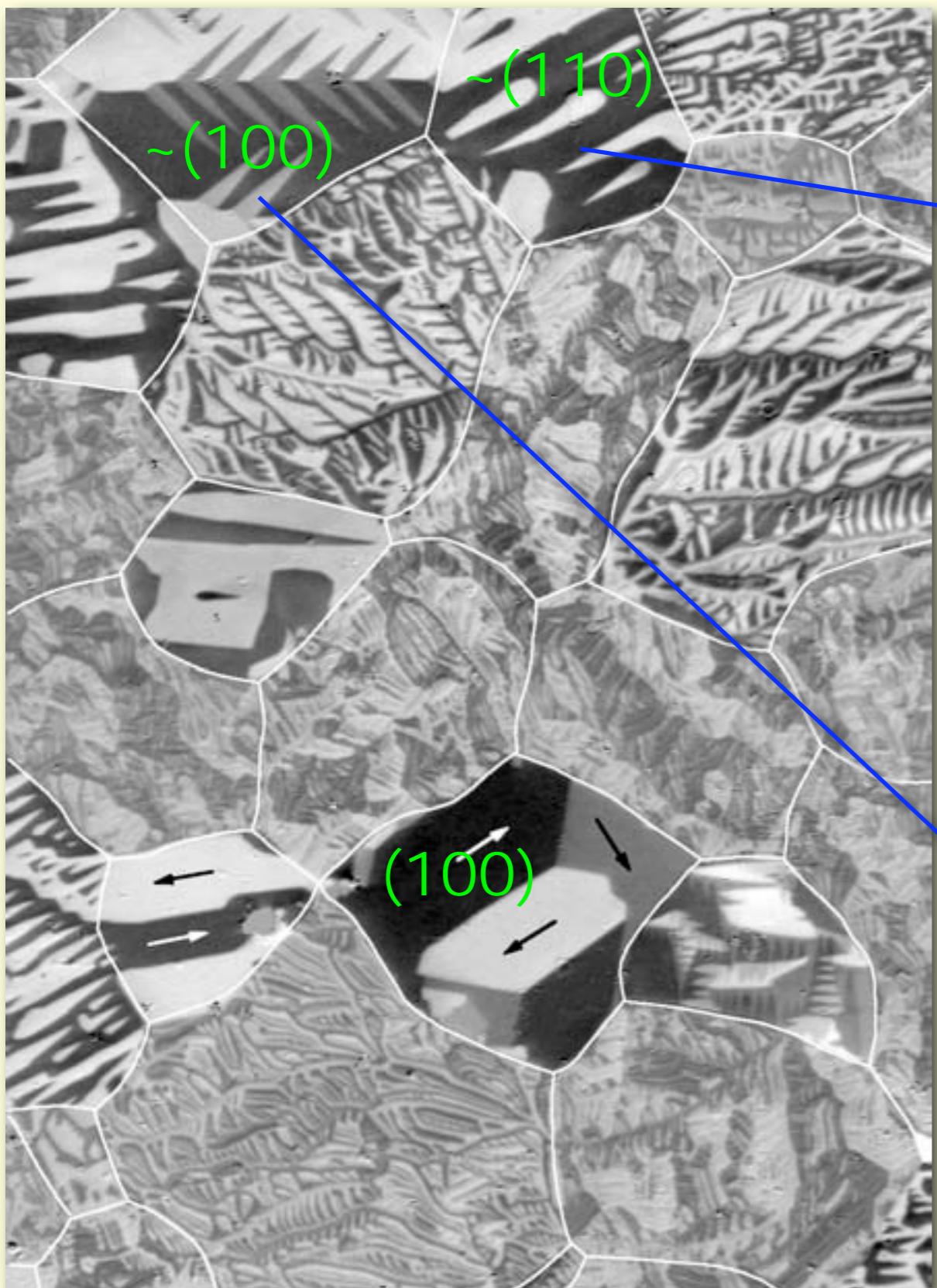


0.5 mm

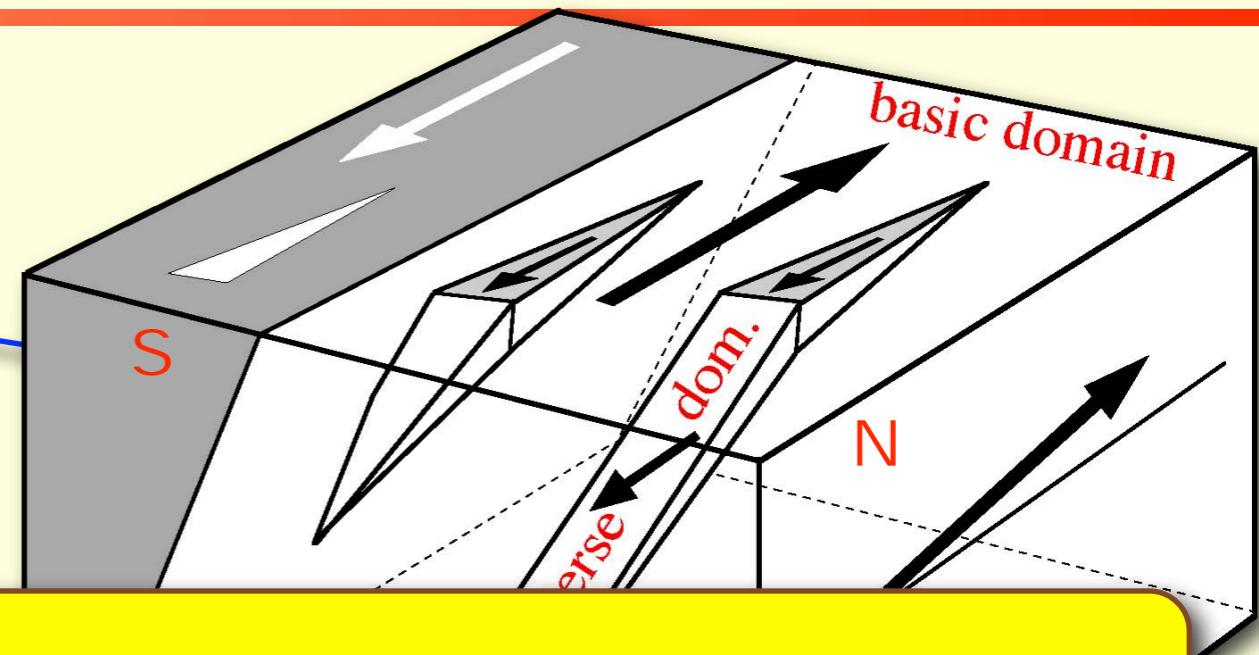
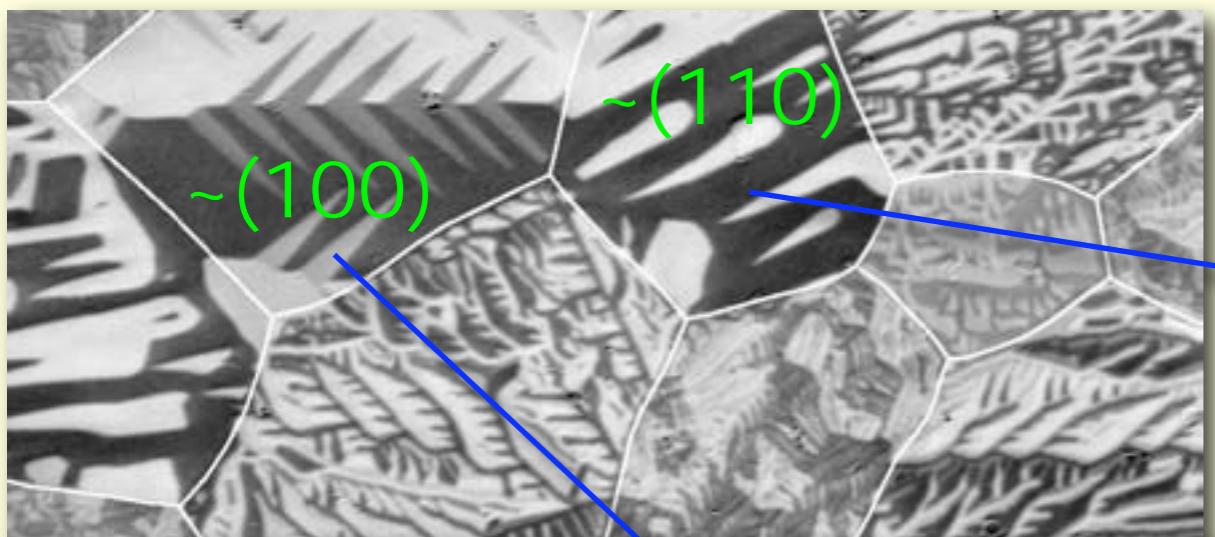


Coarse-grained
materials

Non-oriented electrical steel



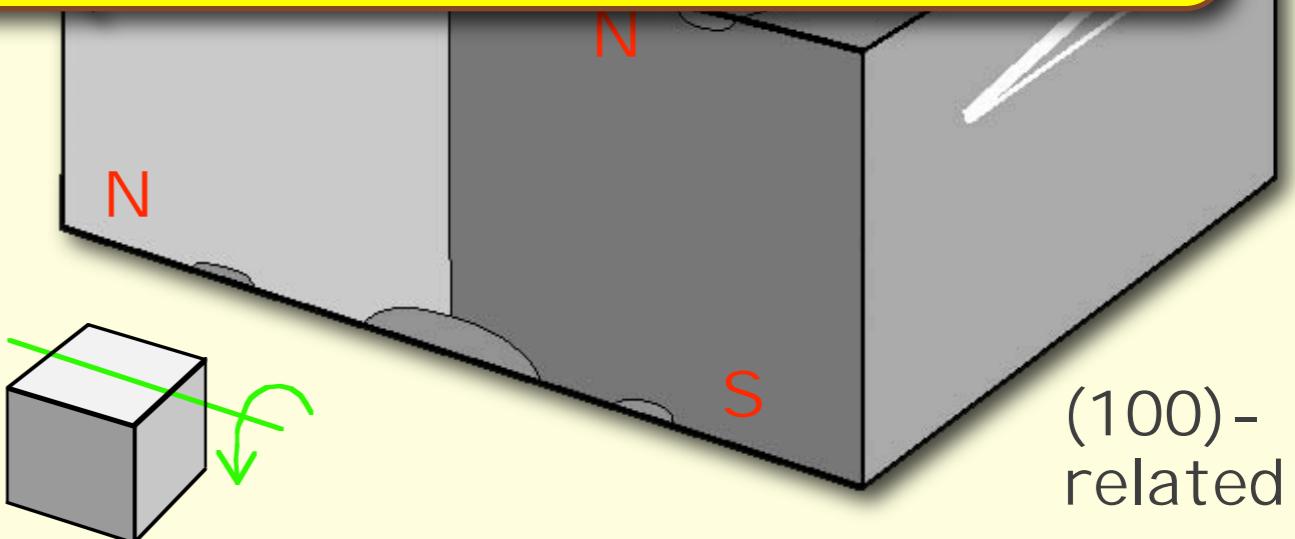
Non-oriented electrical steel



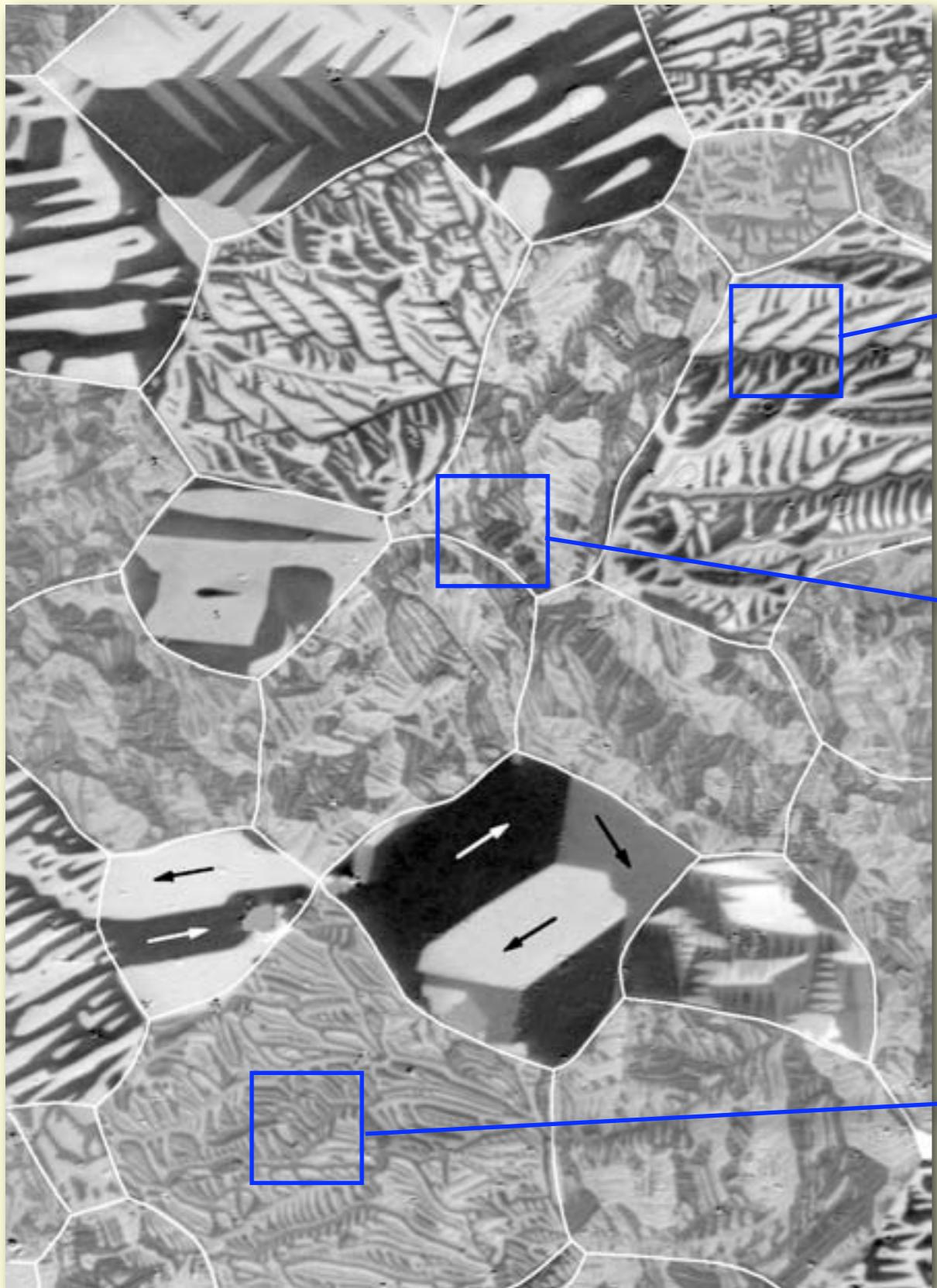
Weak misorientation:
Refinement of surface domain width
by supplementary domains



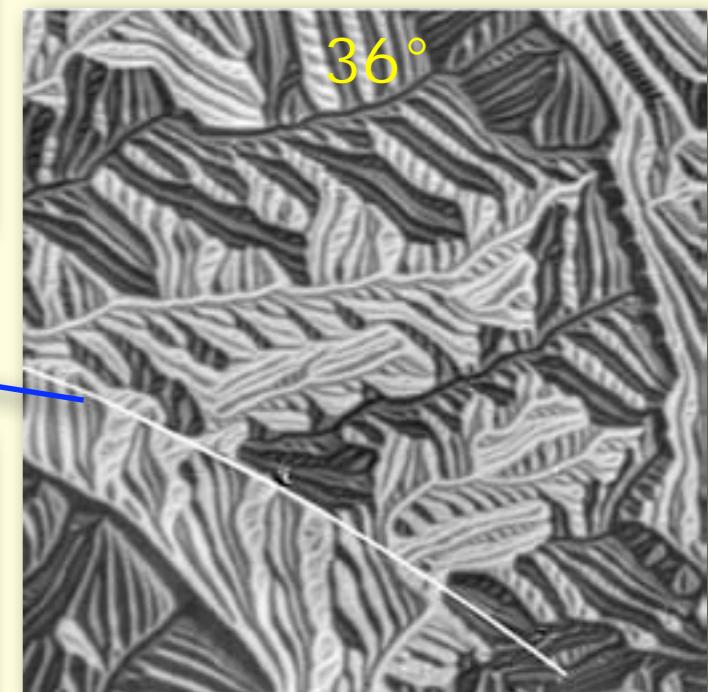
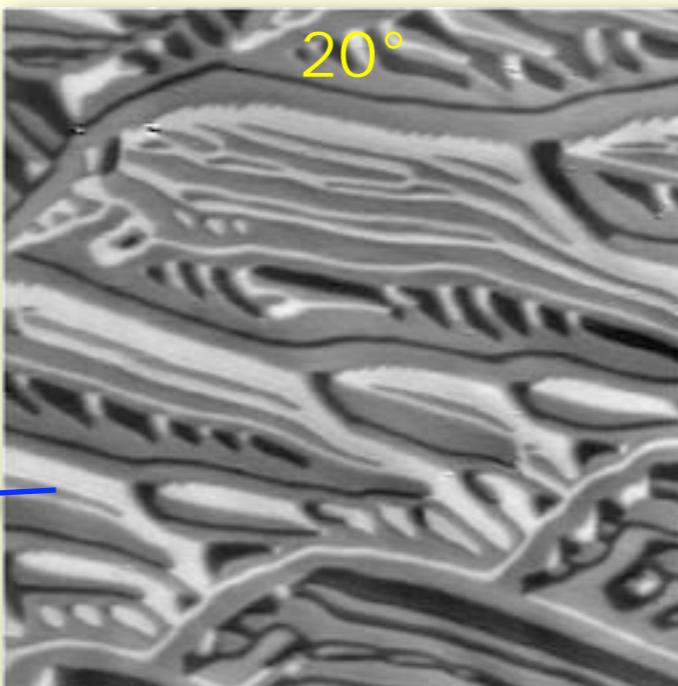
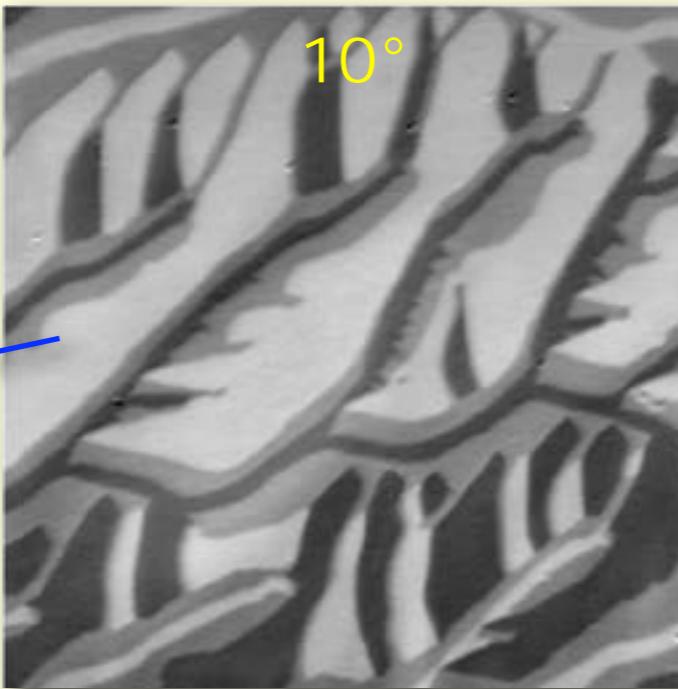
0.5 mm



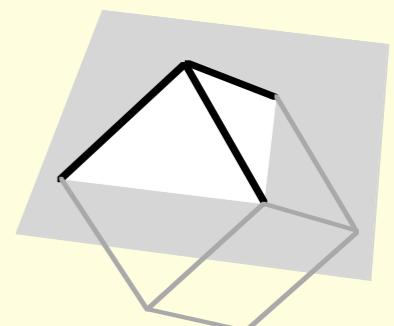
Non-oriented electrical steel



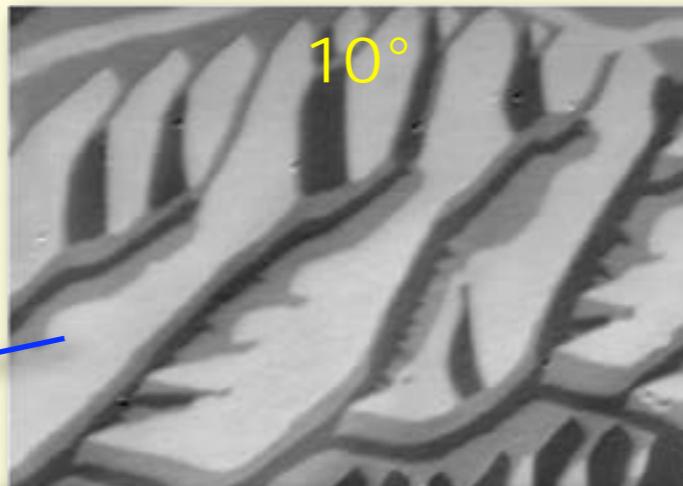
0.5 mm



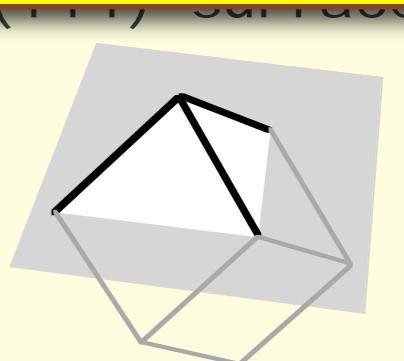
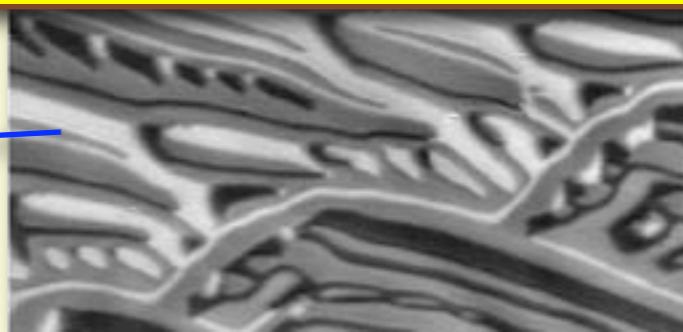
(111)-surface



Non-oriented electrical steel

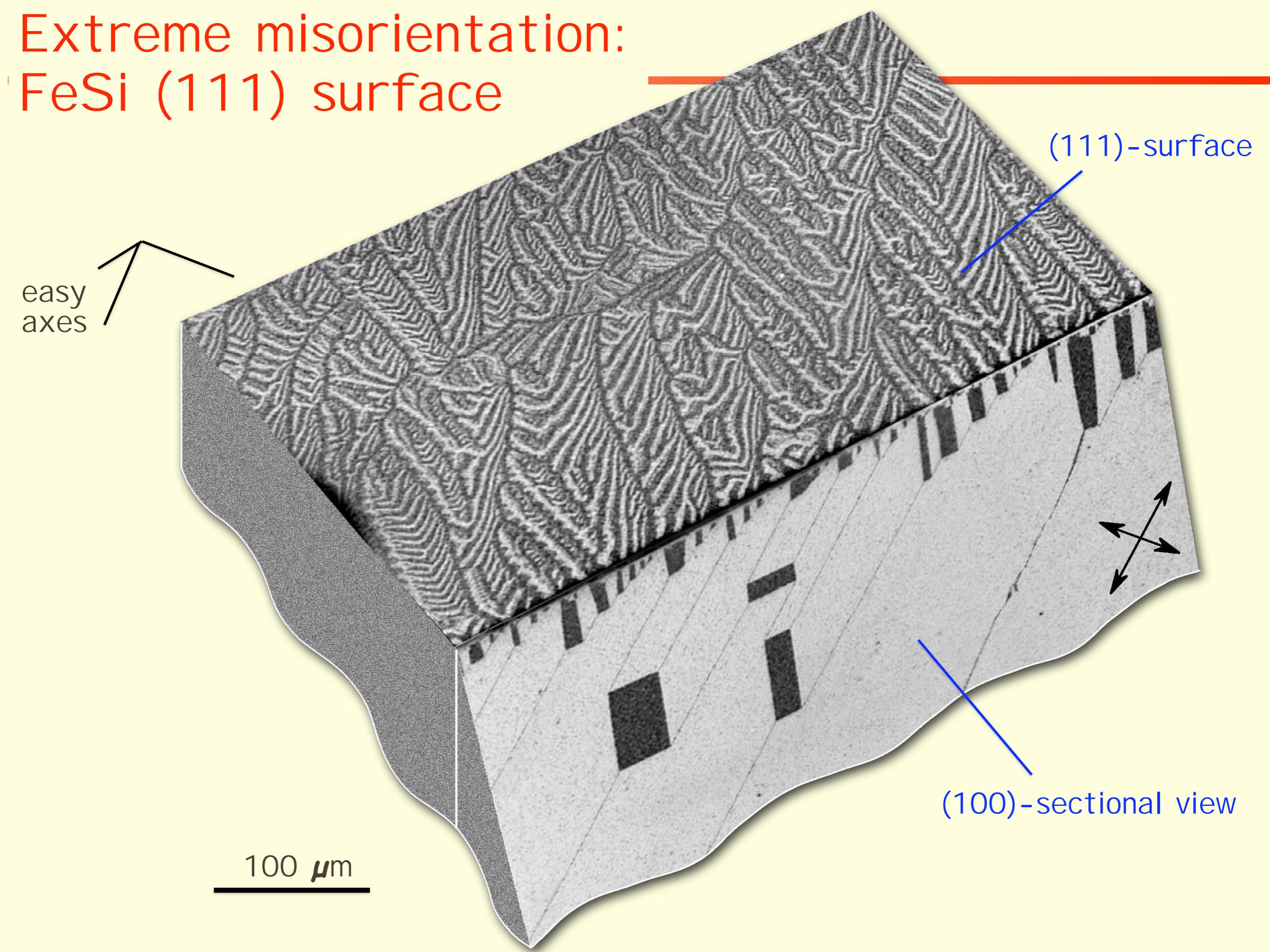


Increasing misorientation:
Domain complexity increases

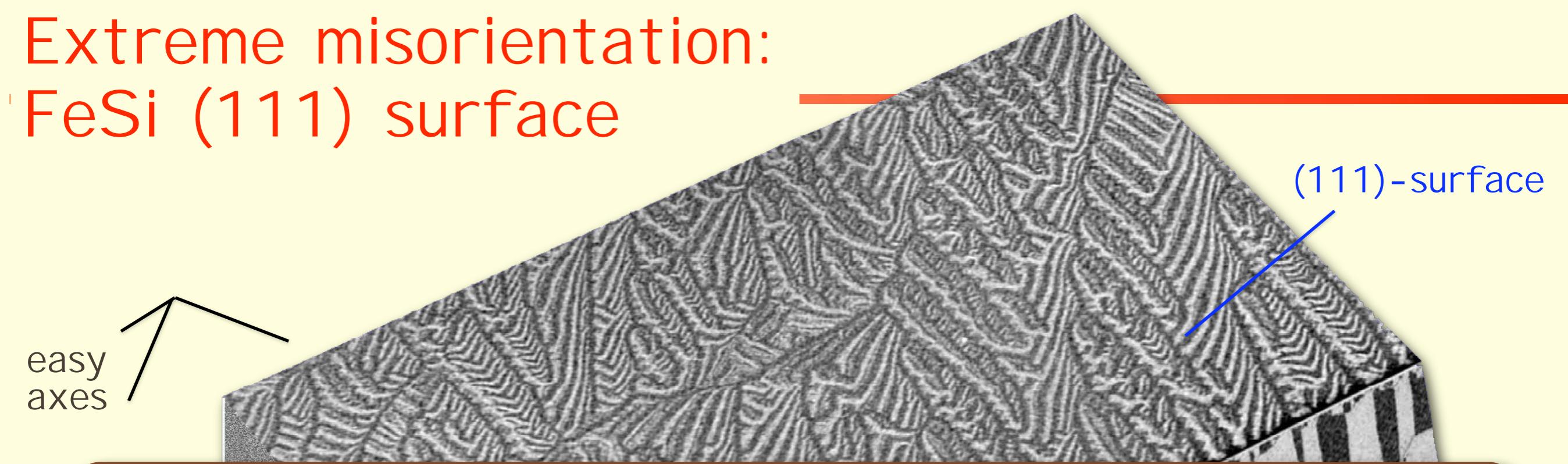


0.5 mm

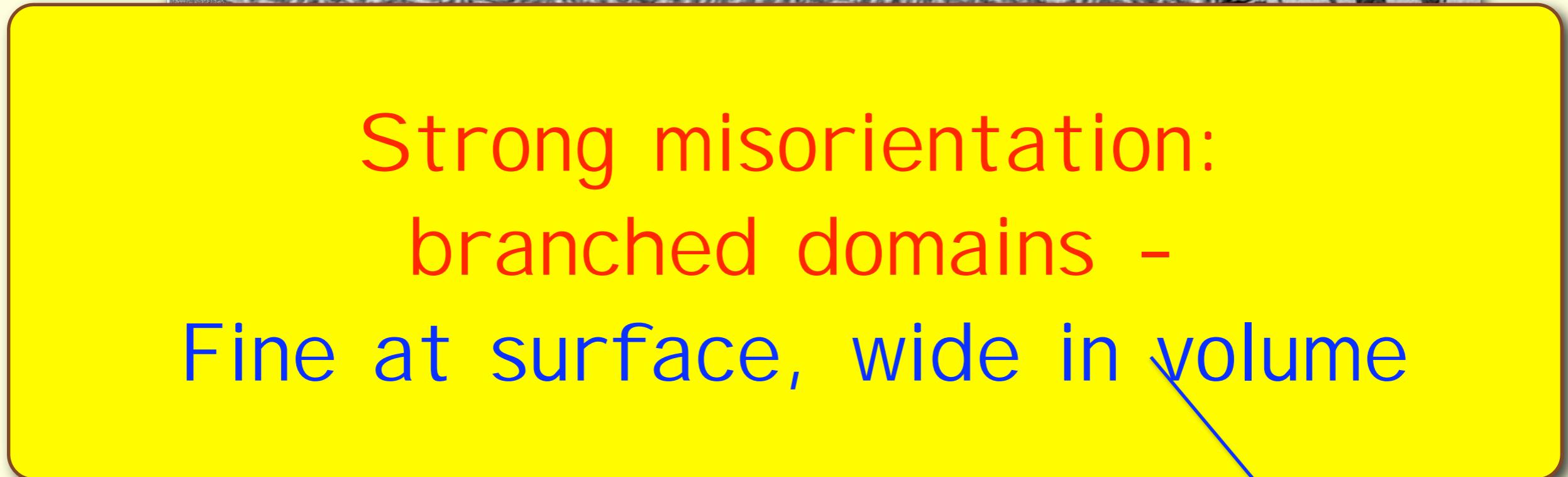
Extreme misorientation: FeSi (111) surface



Extreme misorientation: FeSi (111) surface



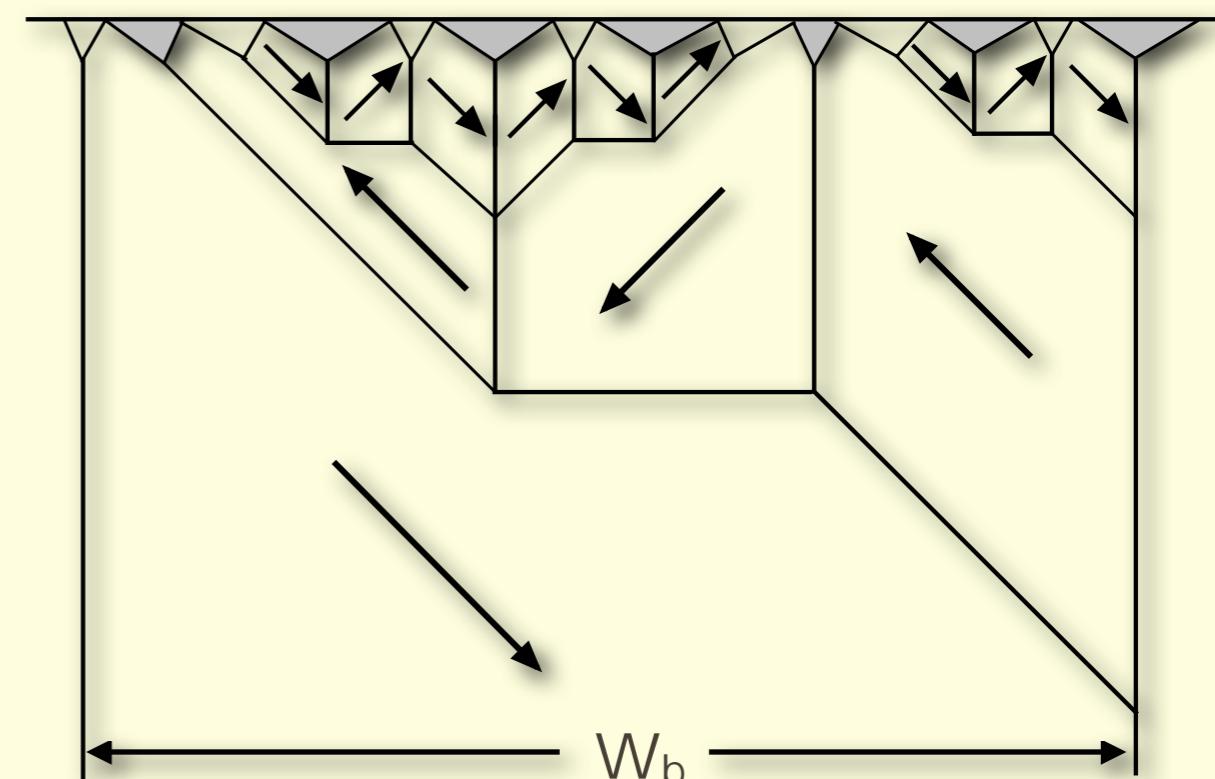
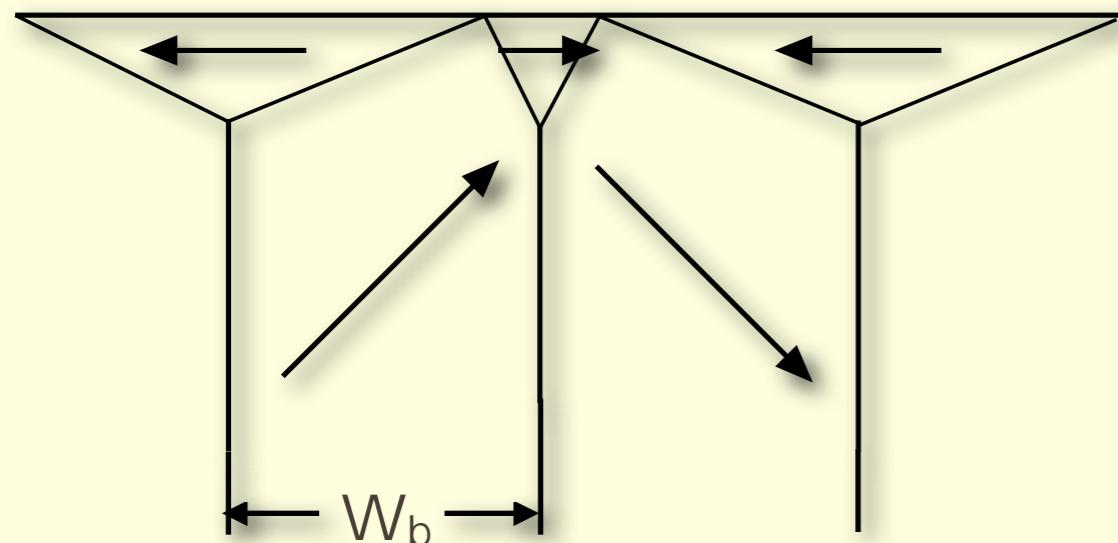
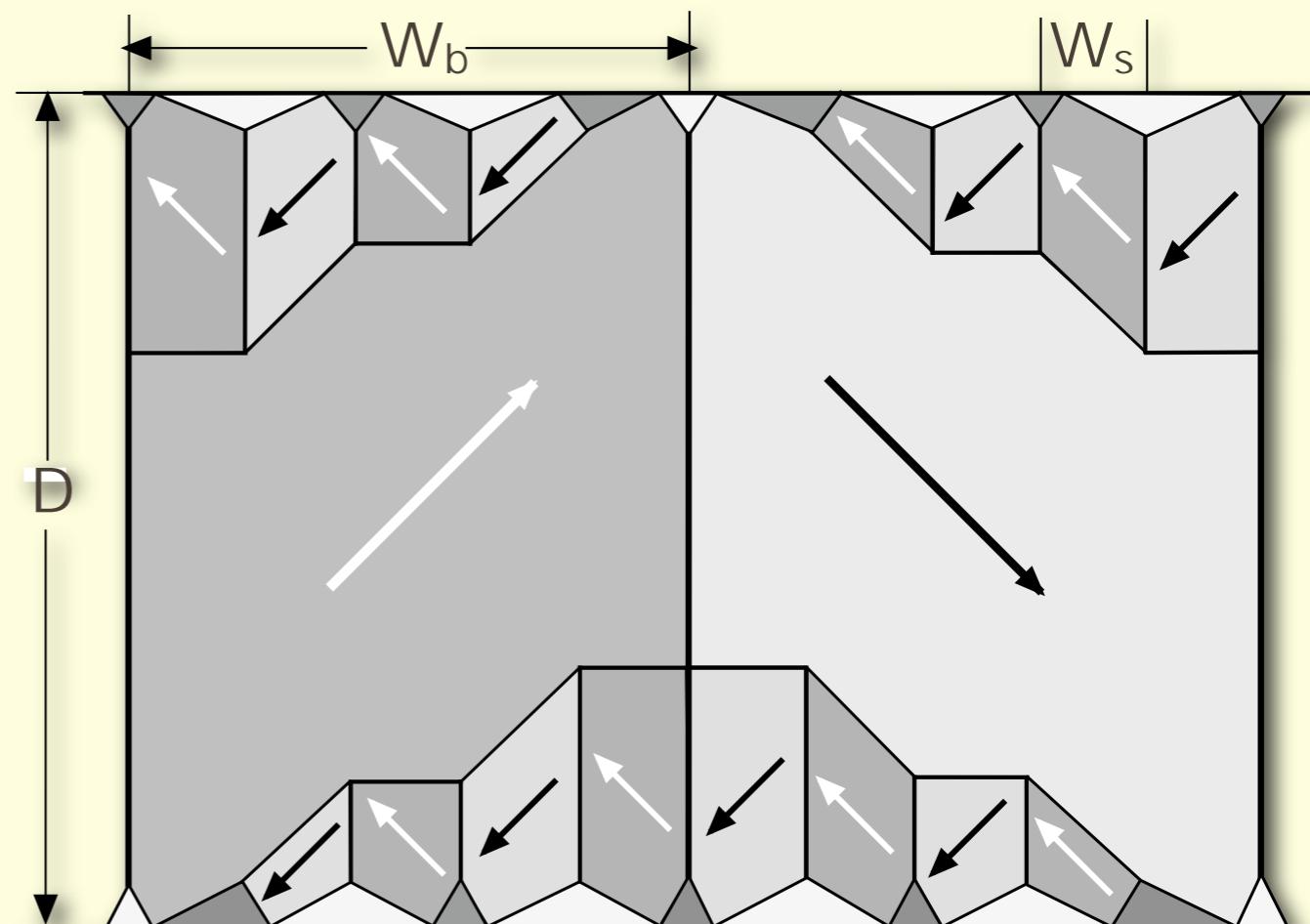
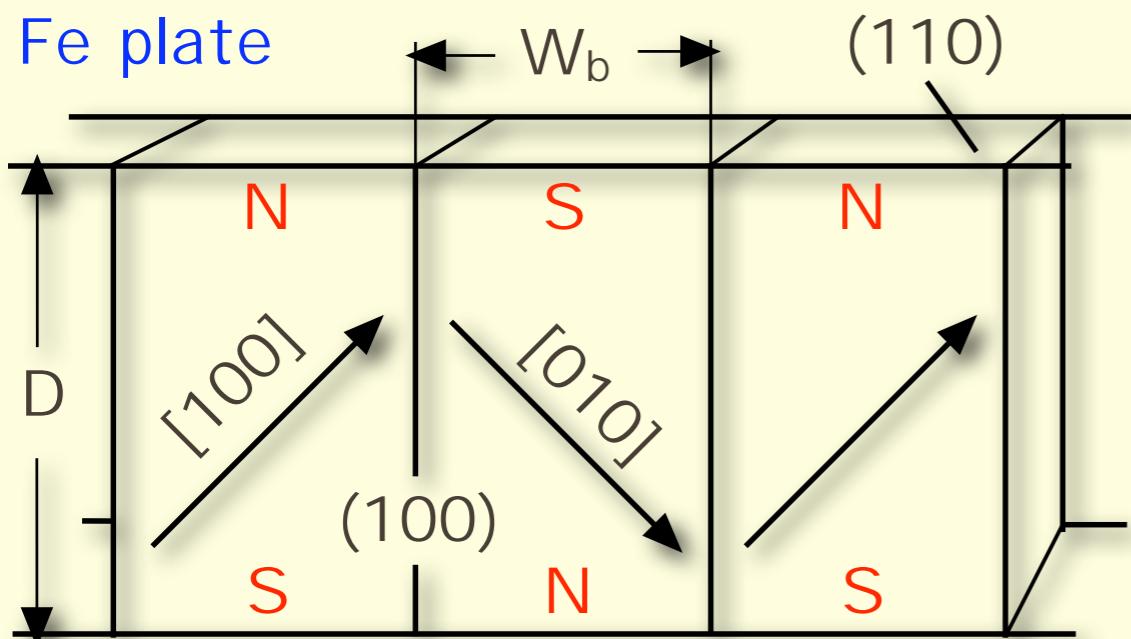
Strong misorientation:
branched domains -
Fine at surface, wide in volume



(100)-sectional view

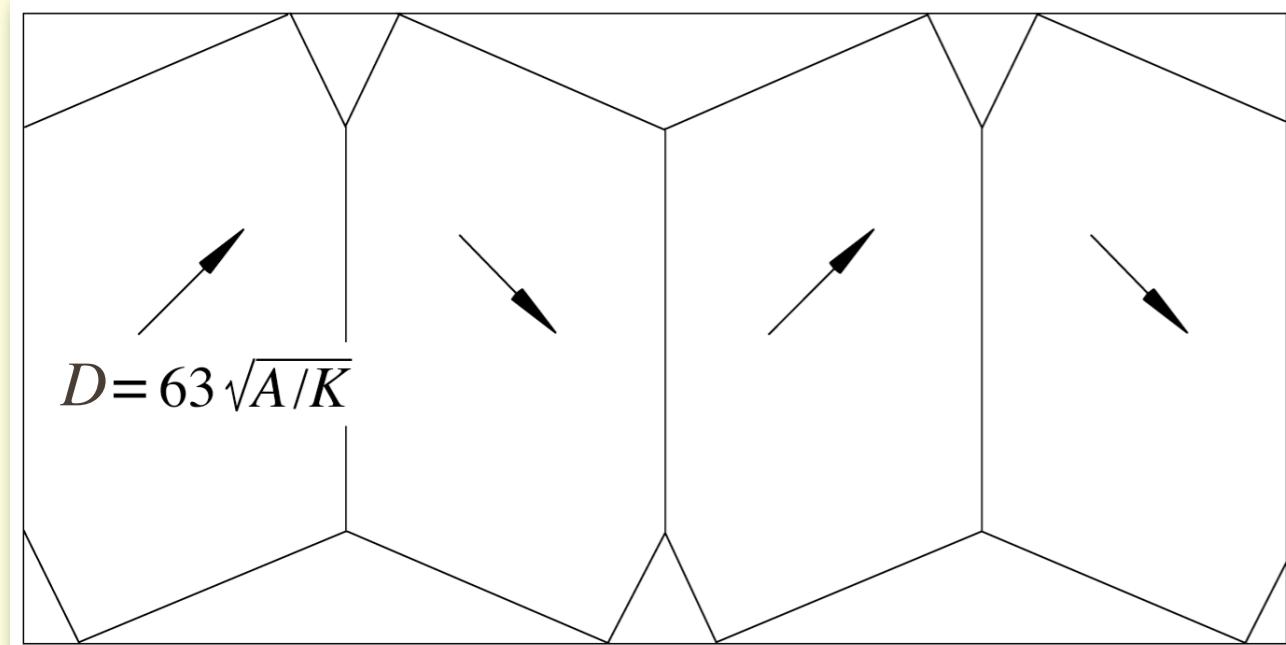
Extreme misorientation: 2-dim. model

Four-phase branching:
the echelon pattern

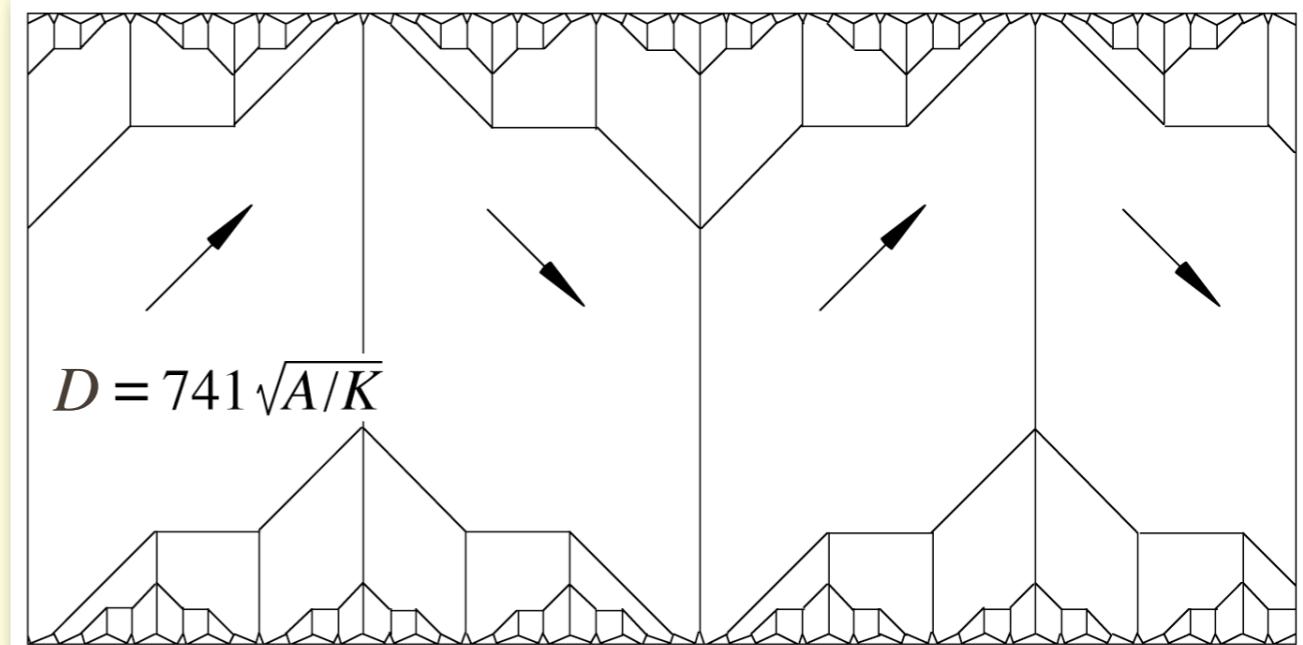


$$W_b \sim \sqrt{D}$$

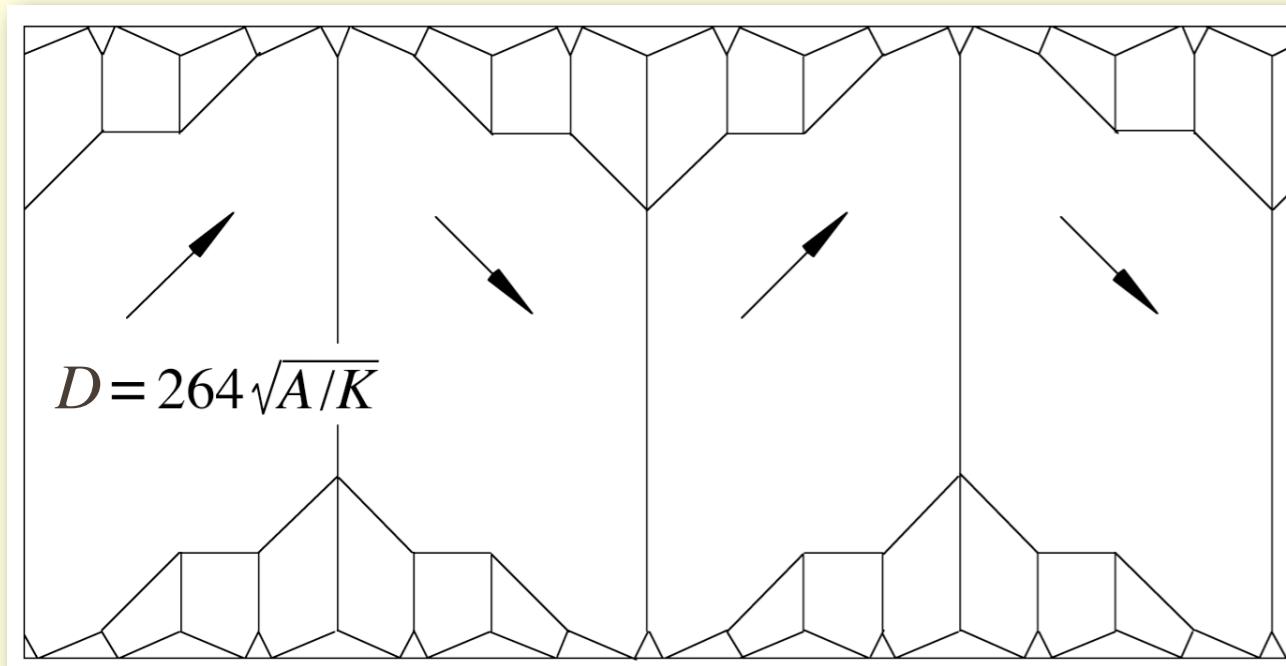
Extreme misorientation: 2-dim. model



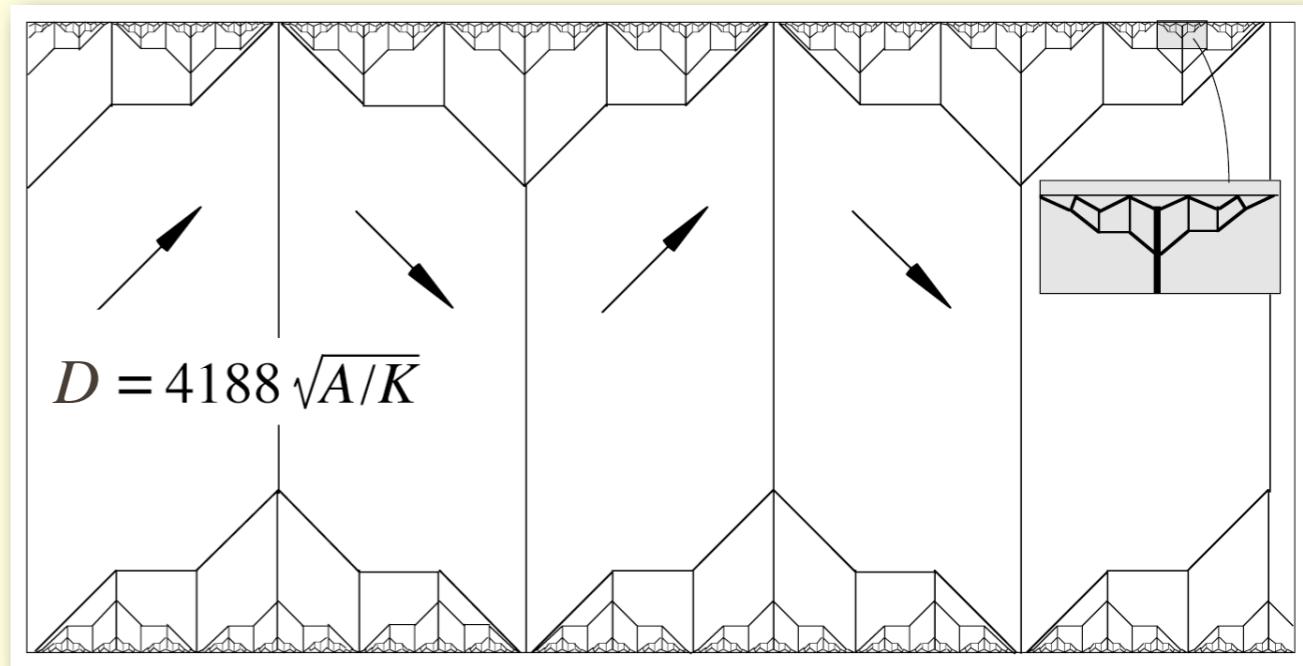
no branching



two generations

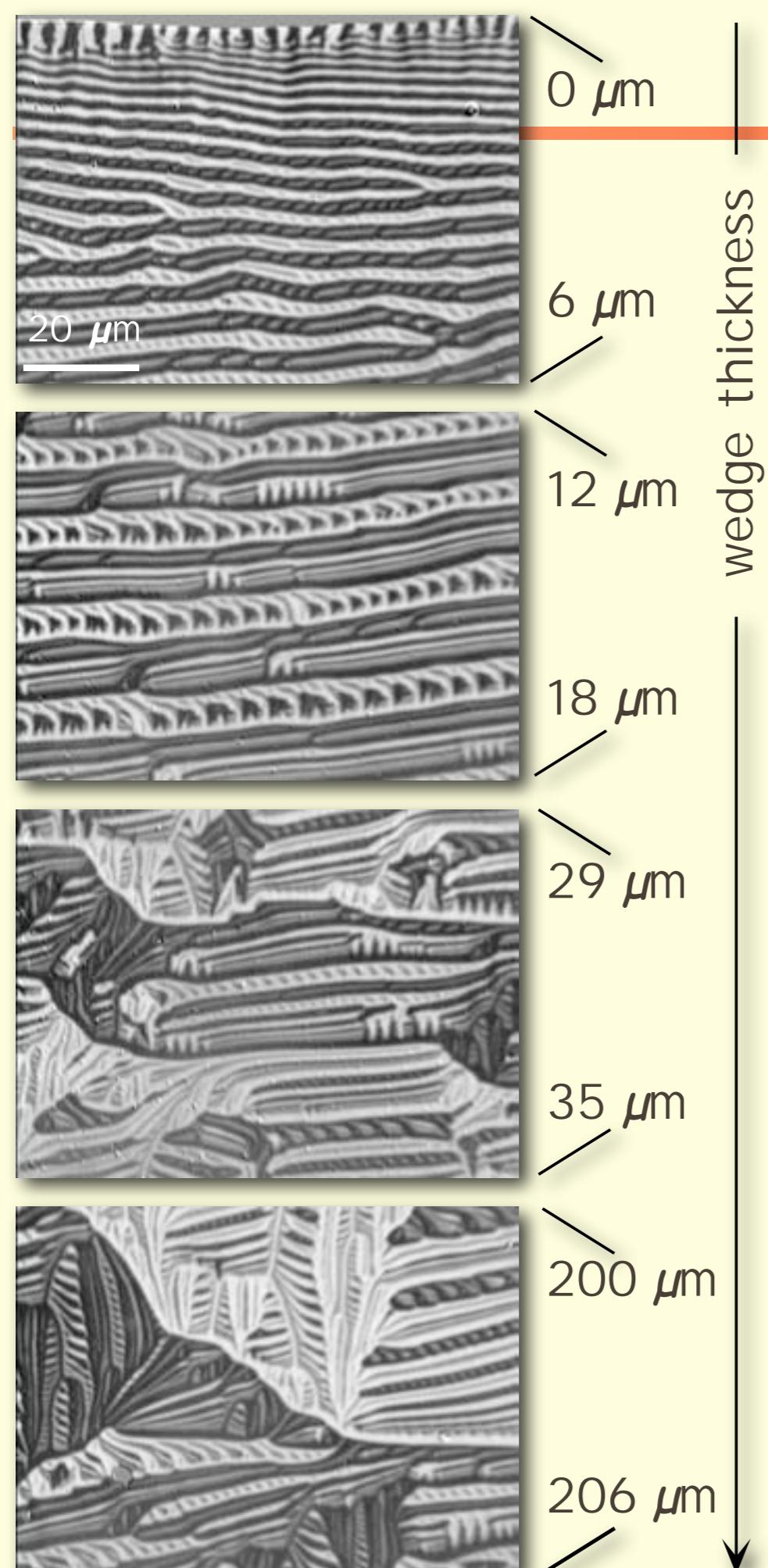


one generation

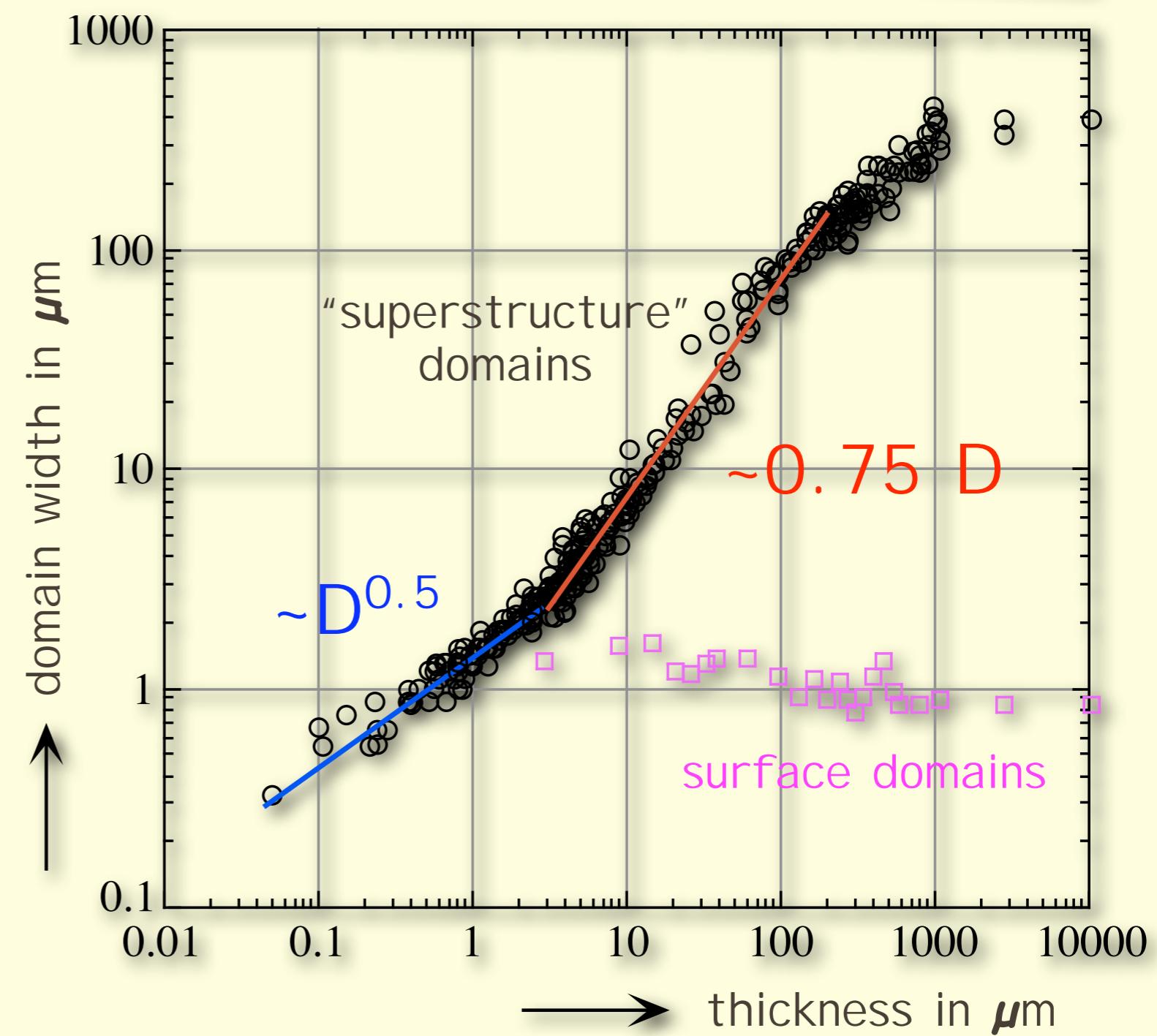


three generations

Multi-phase branching



Experiment: Fe 12.8at%Si



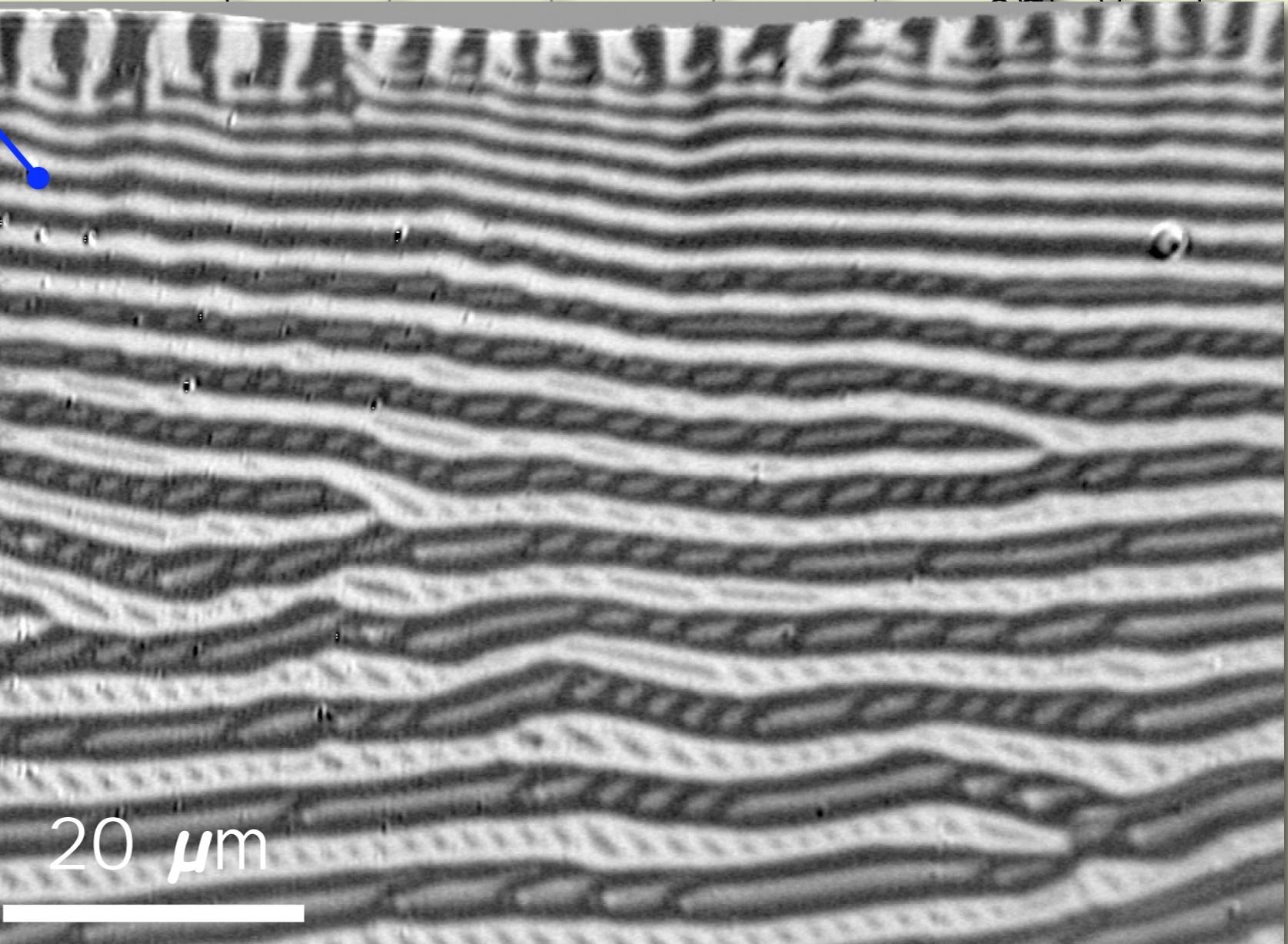
Multi-phase branching

Experiment: Fe 12.8at%Si

(111) surface

FeSi wedge

1000



0 μm

6 μm

12 μm

18 μm

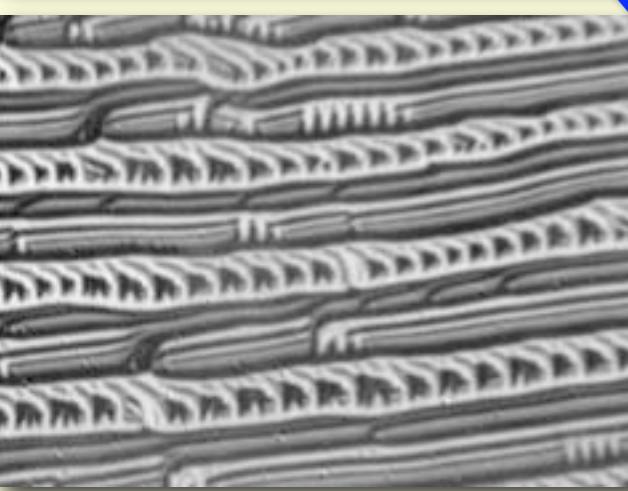
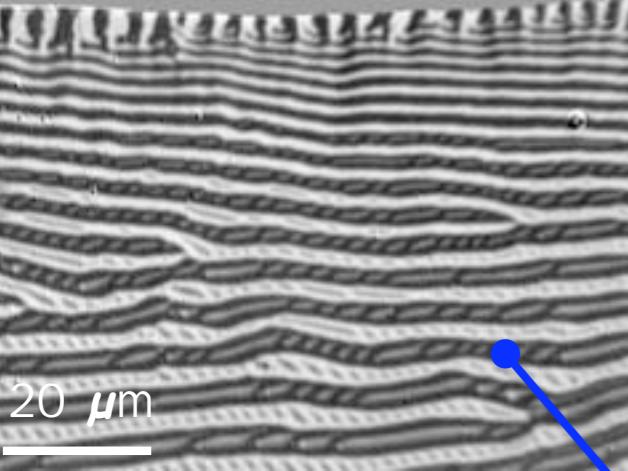
29 μm

35 μm

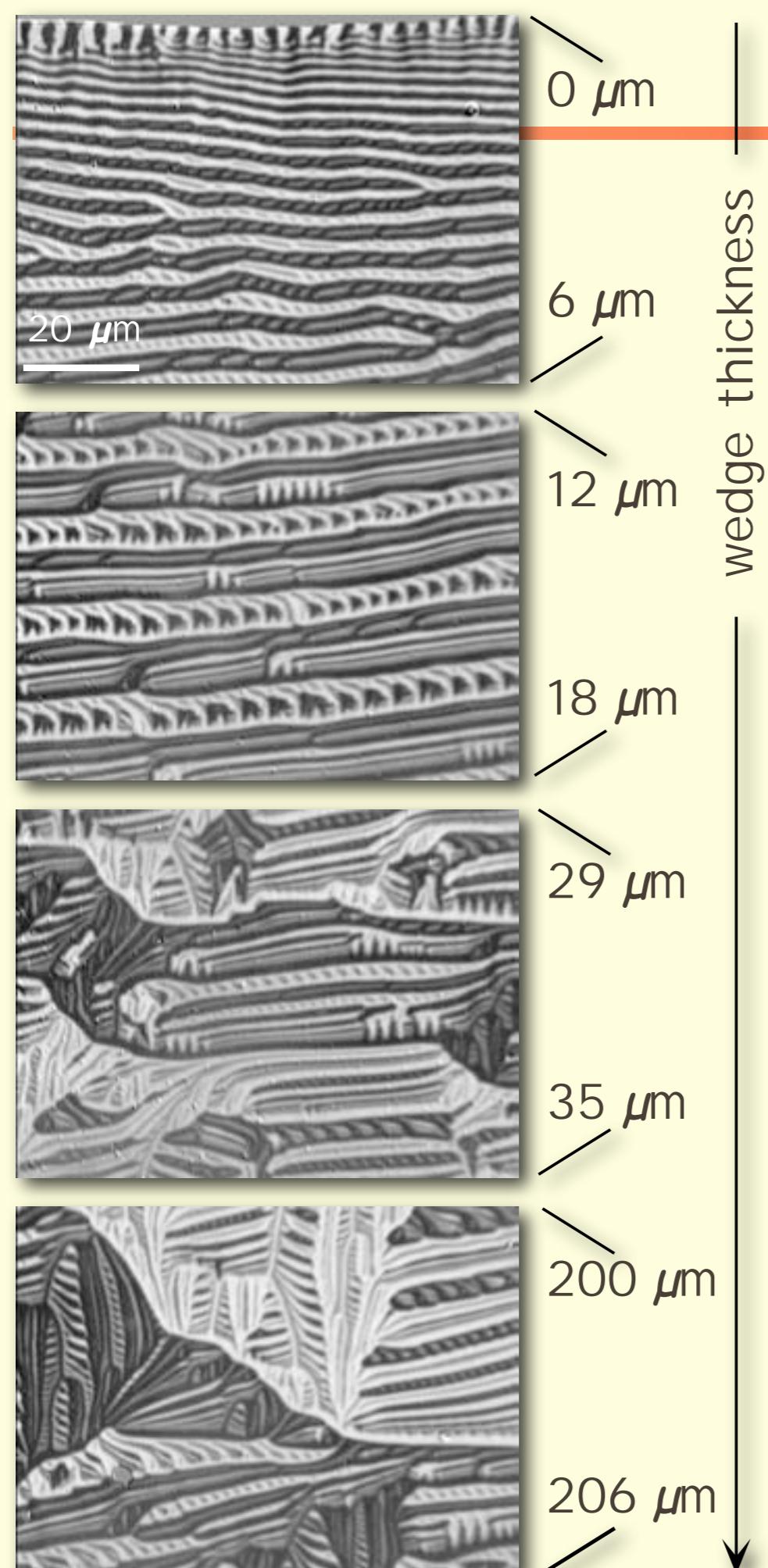
200 μm

206 μm

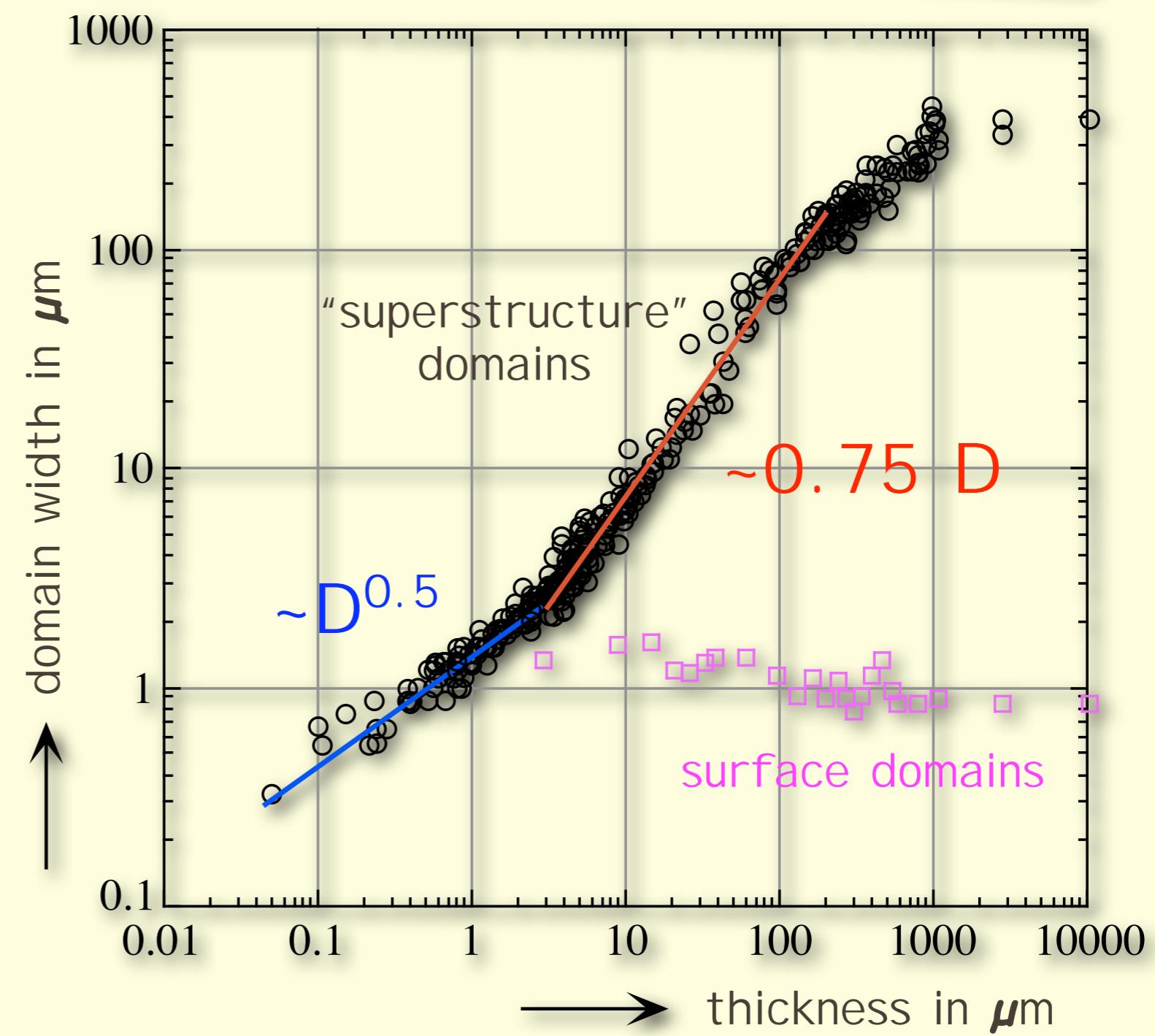
wedge thickness



Multi-phase branching



Experiment: Fe 12.8at%Si



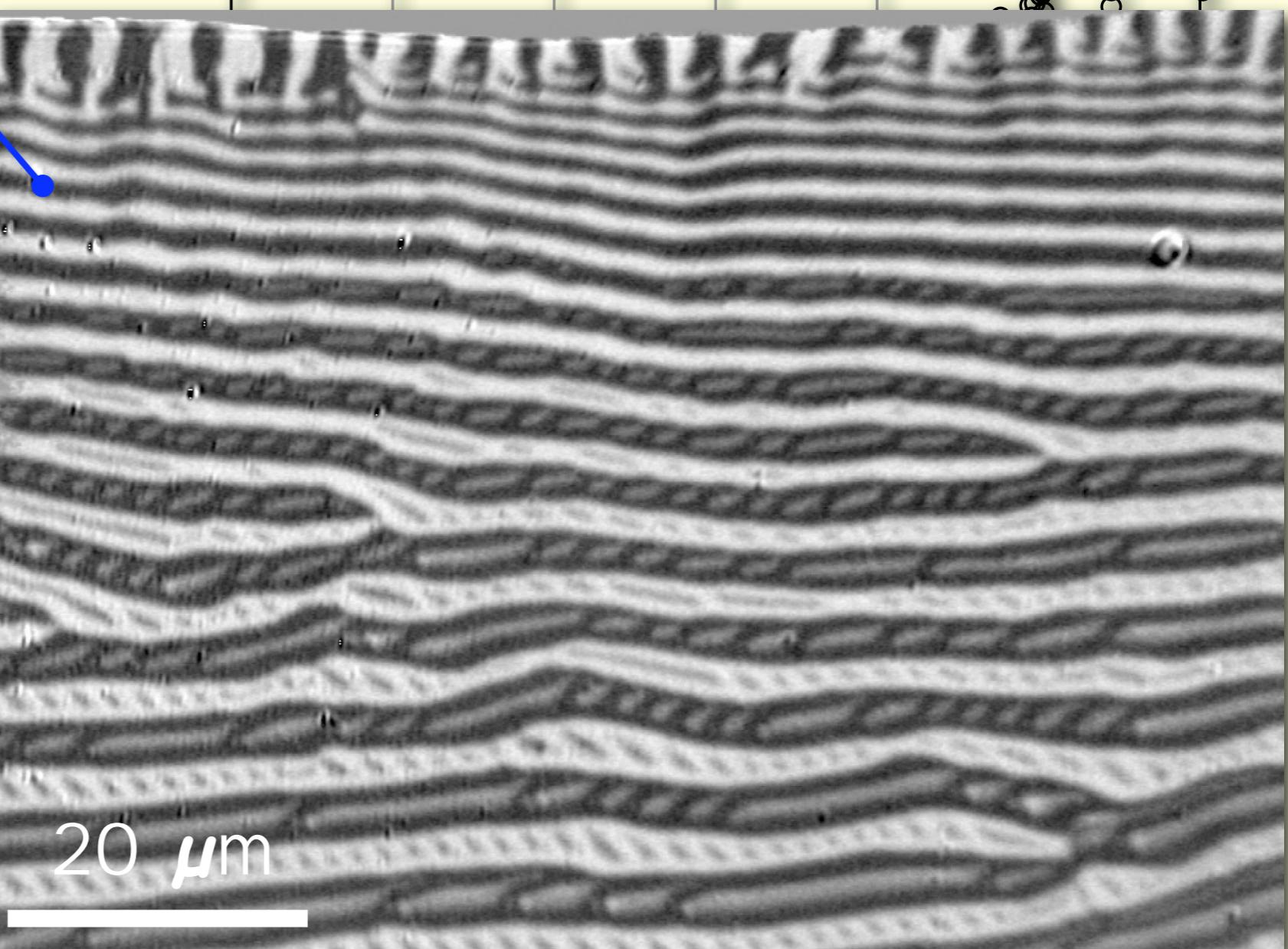
Multi-phase branching

Experiment: Fe 12.8at%Si

(111) surface

FeSi wedge

1000



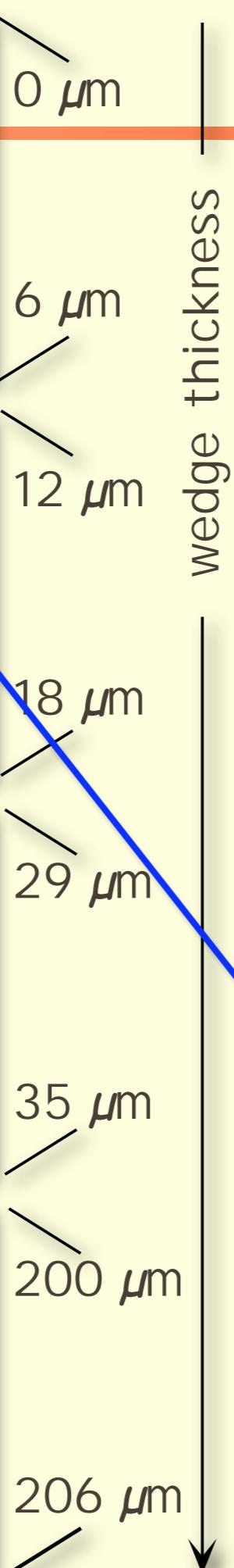
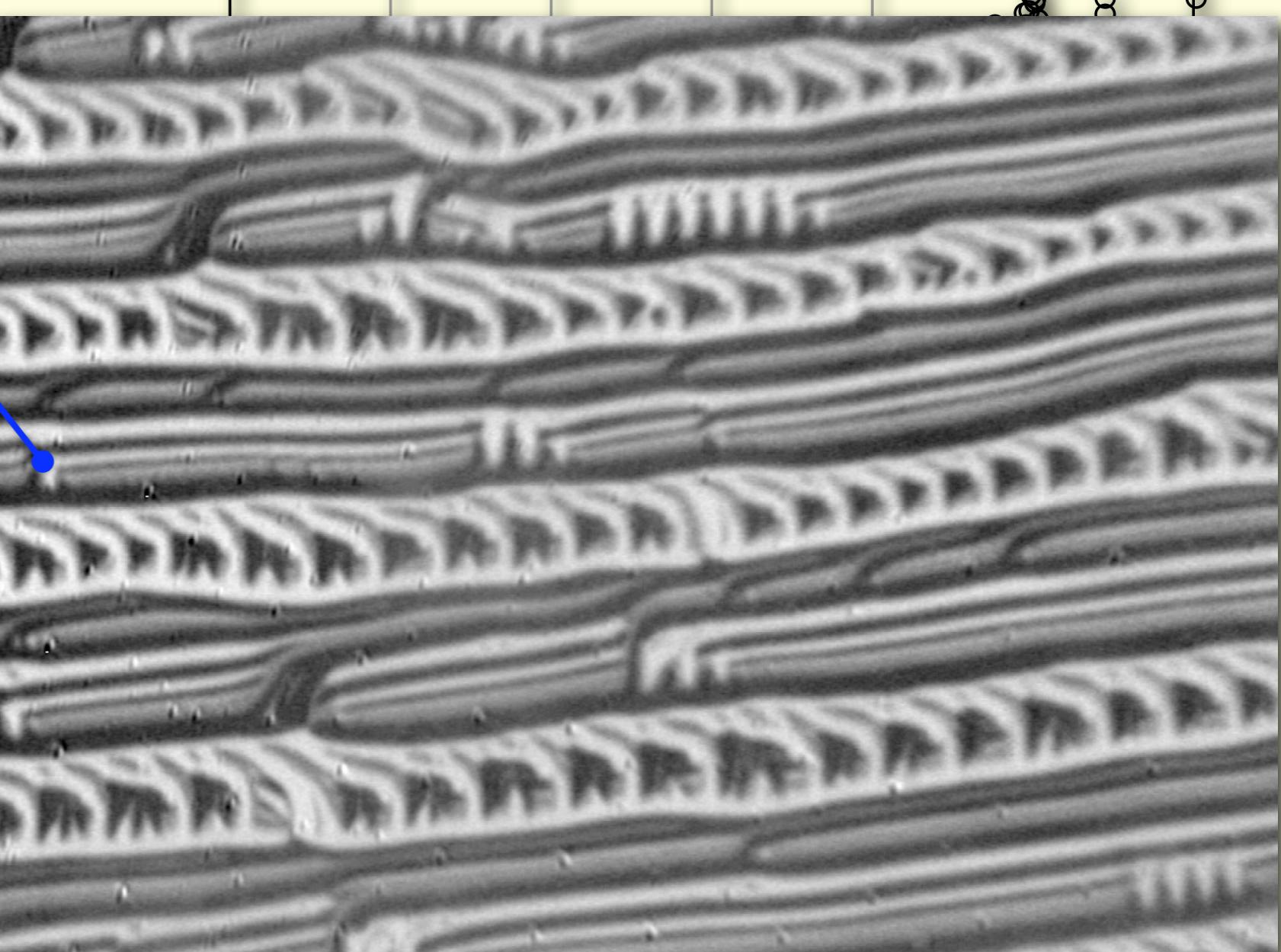
Multi-phase branching

Experiment: Fe 12.8at%Si

(111) surface

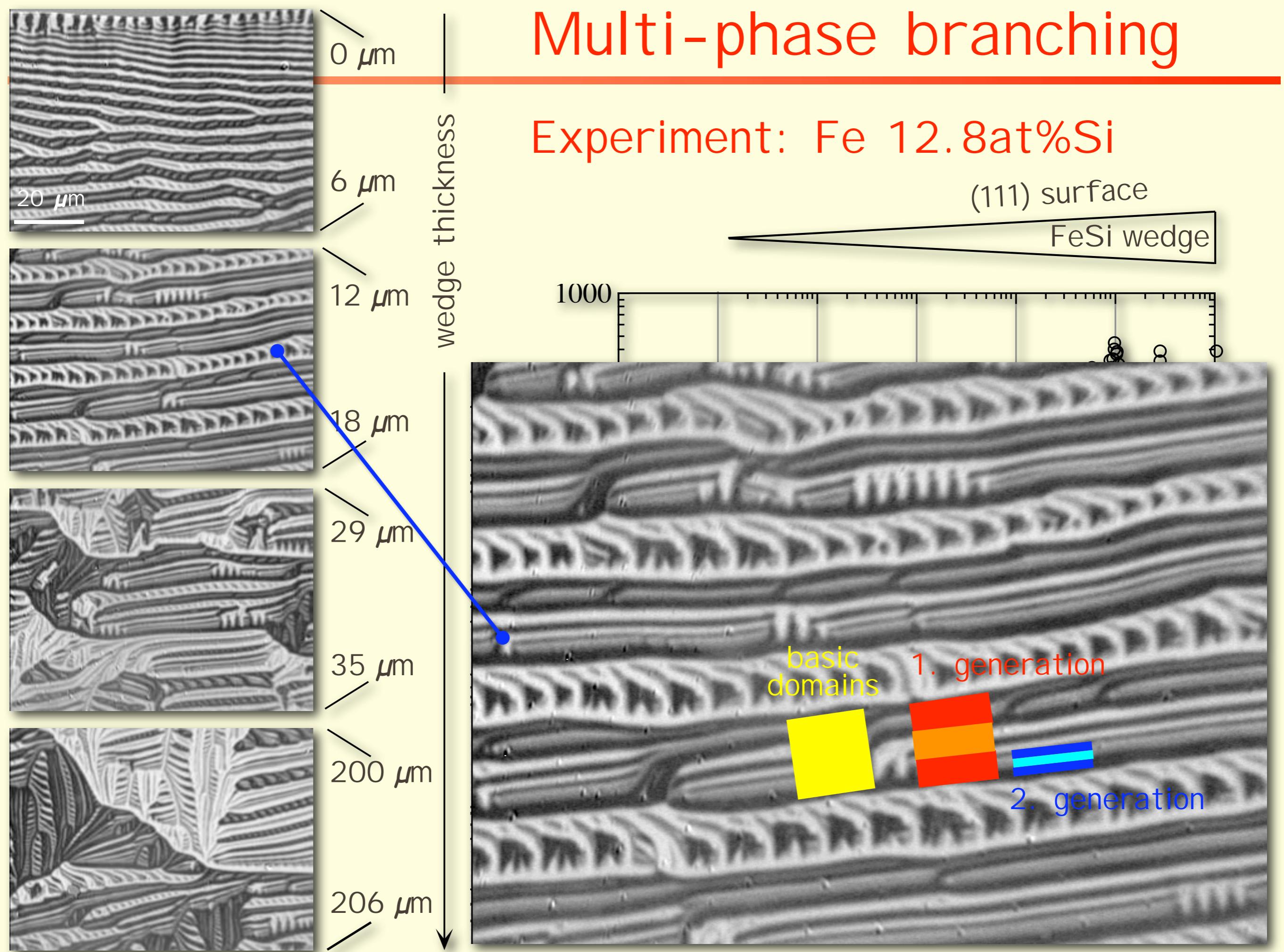
FeSi wedge

1000



Multi-phase branching

Experiment: Fe 12.8at%Si

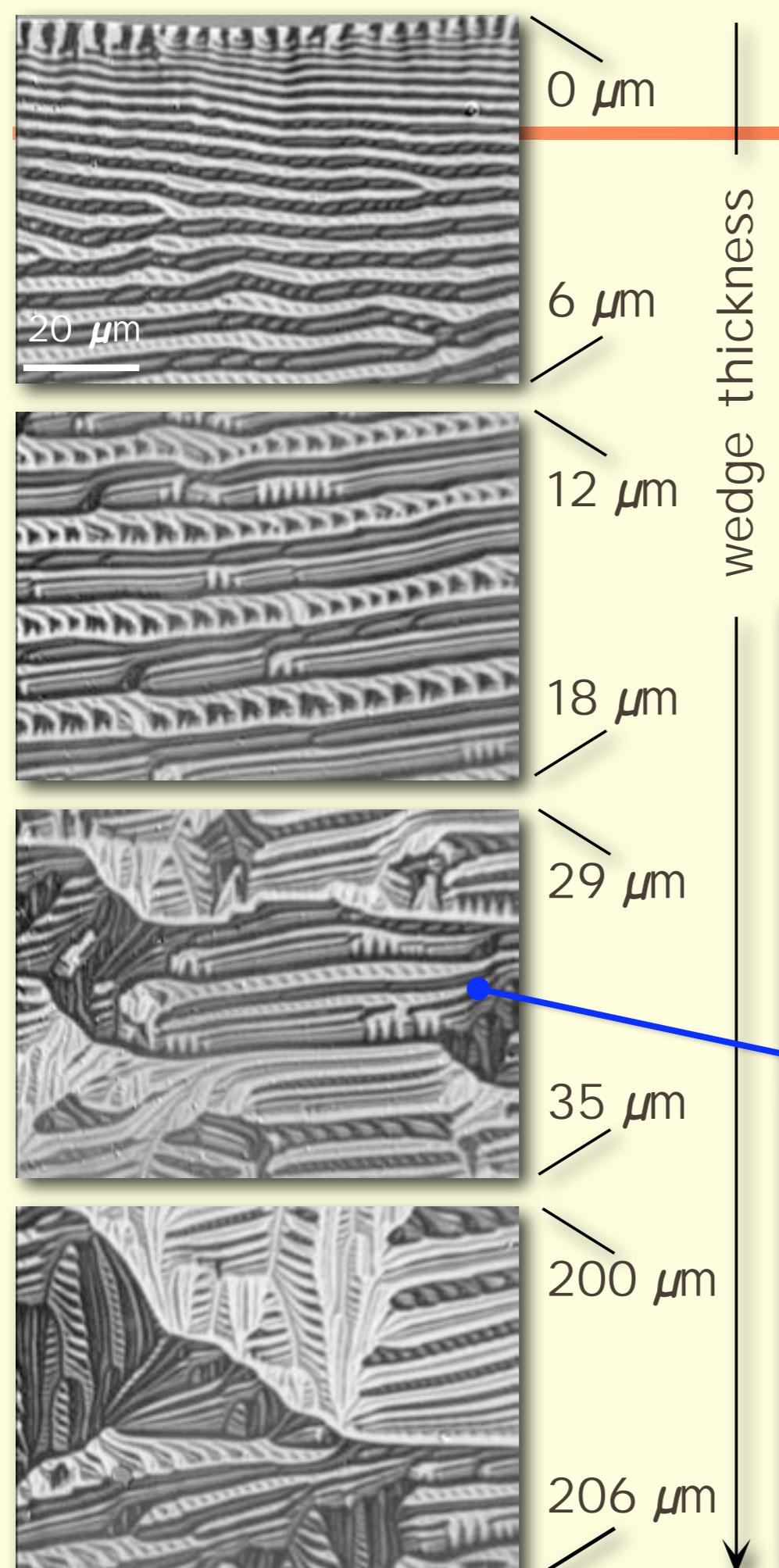
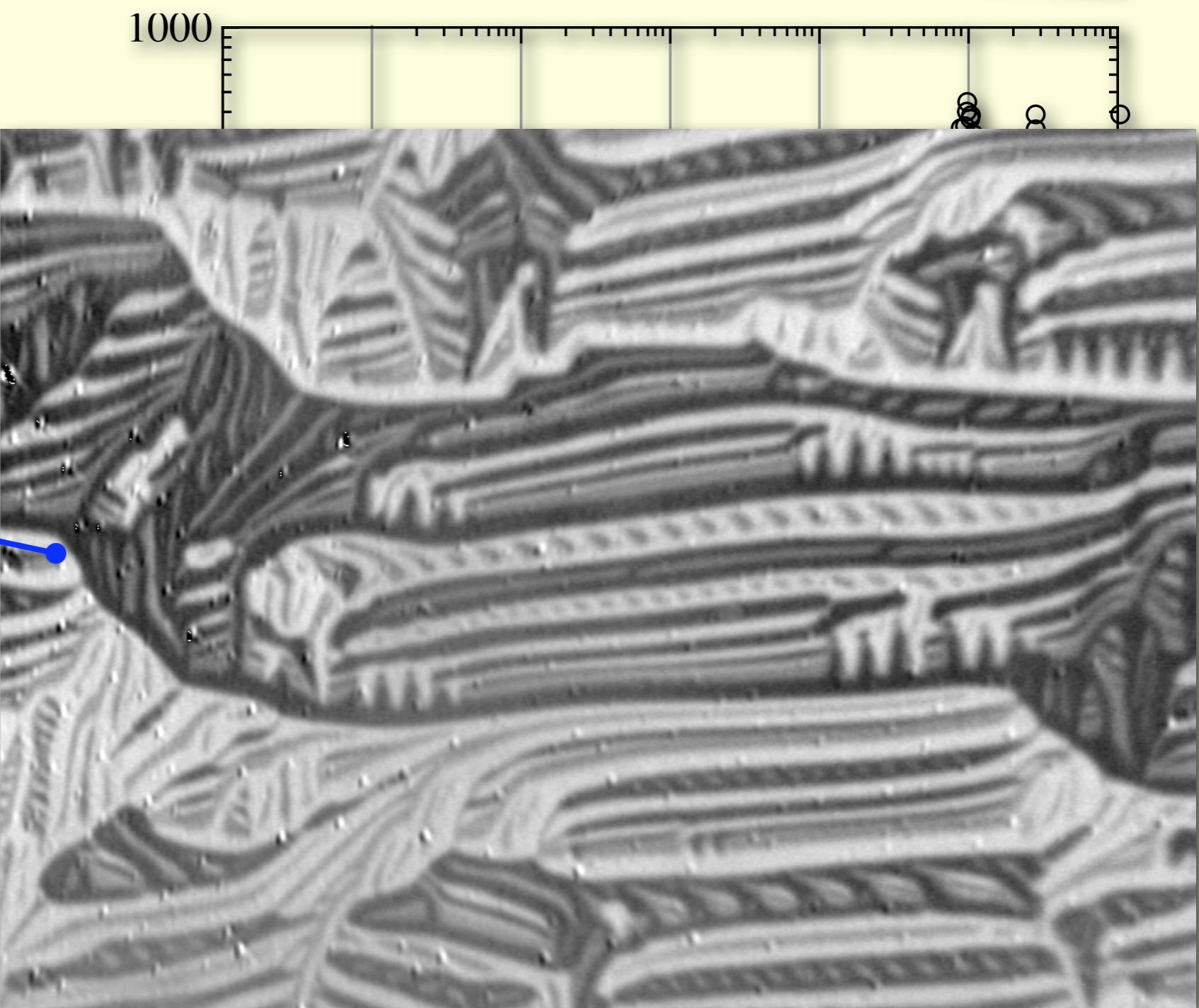


Multi-phase branching

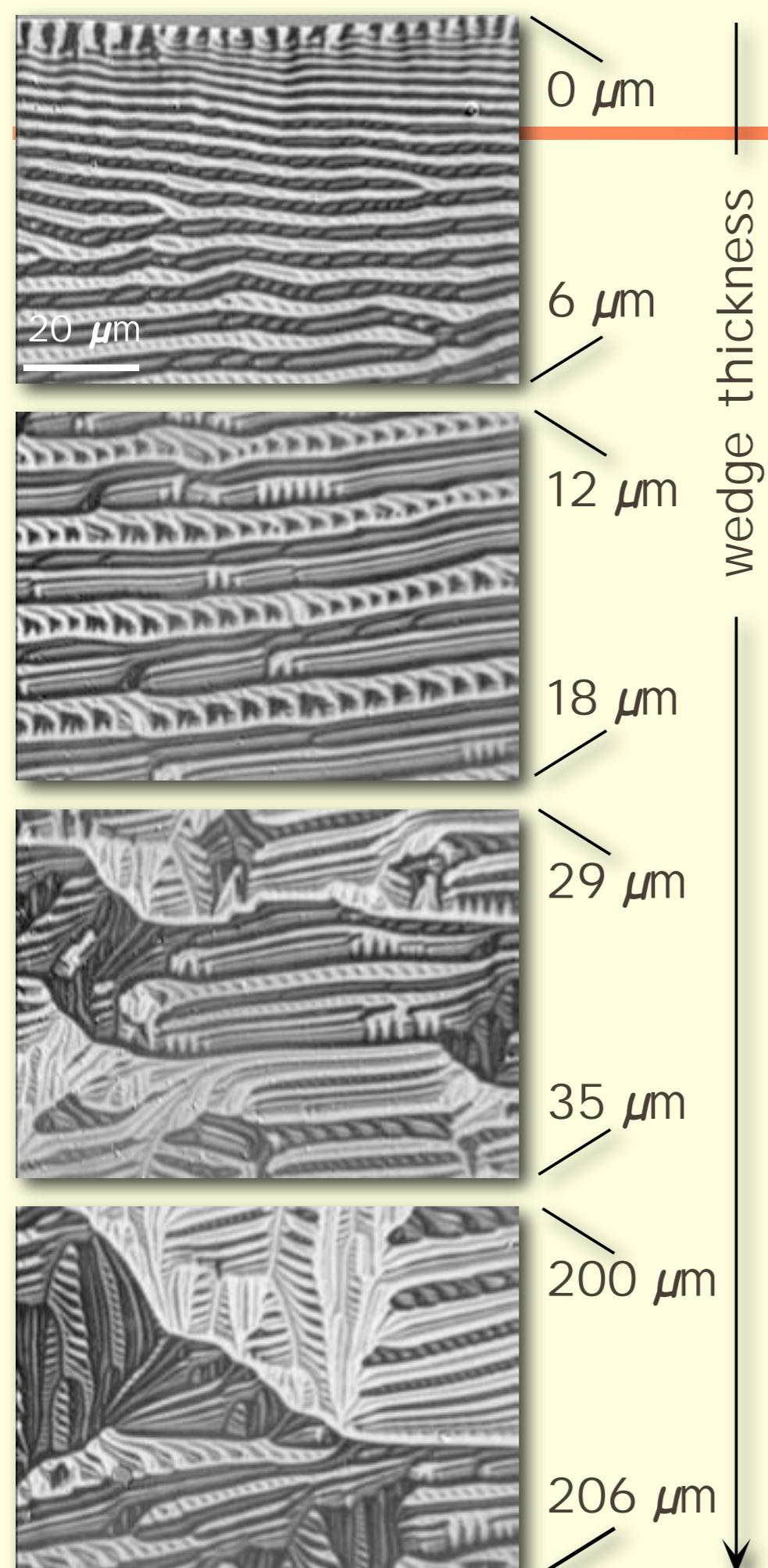
Experiment: Fe 12.8at%Si

(111) surface

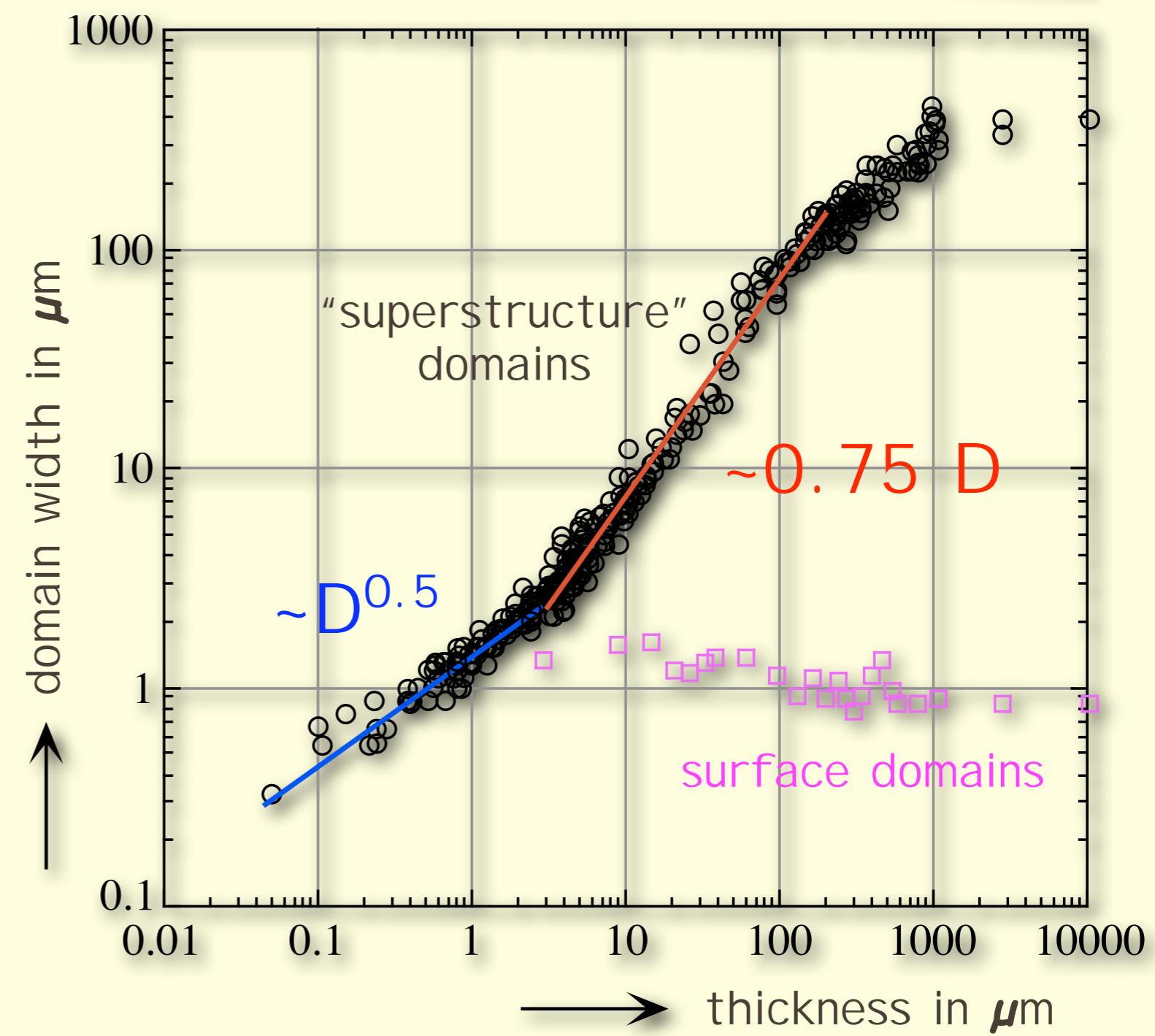
FeSi wedge



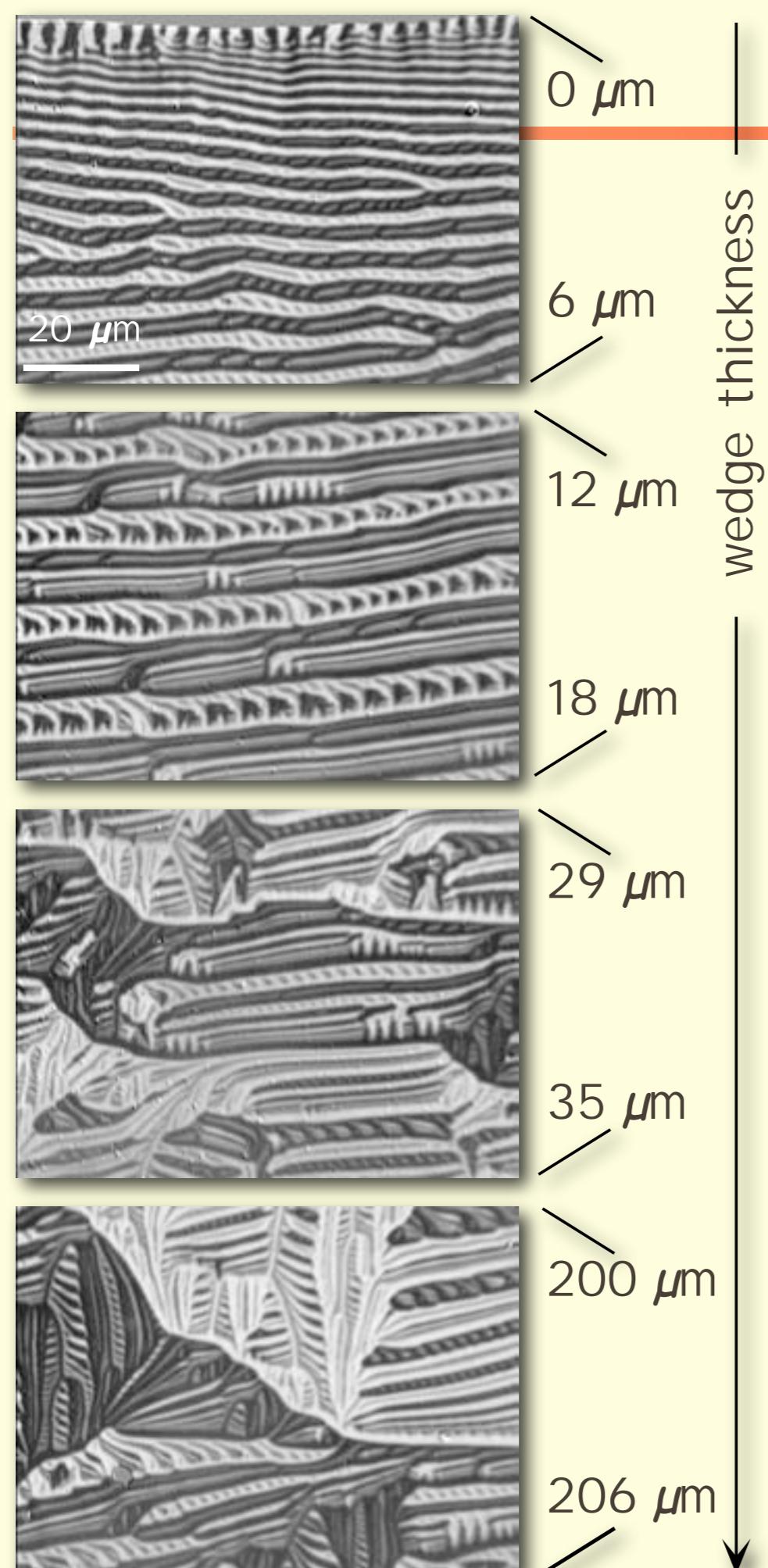
Multi-phase branching



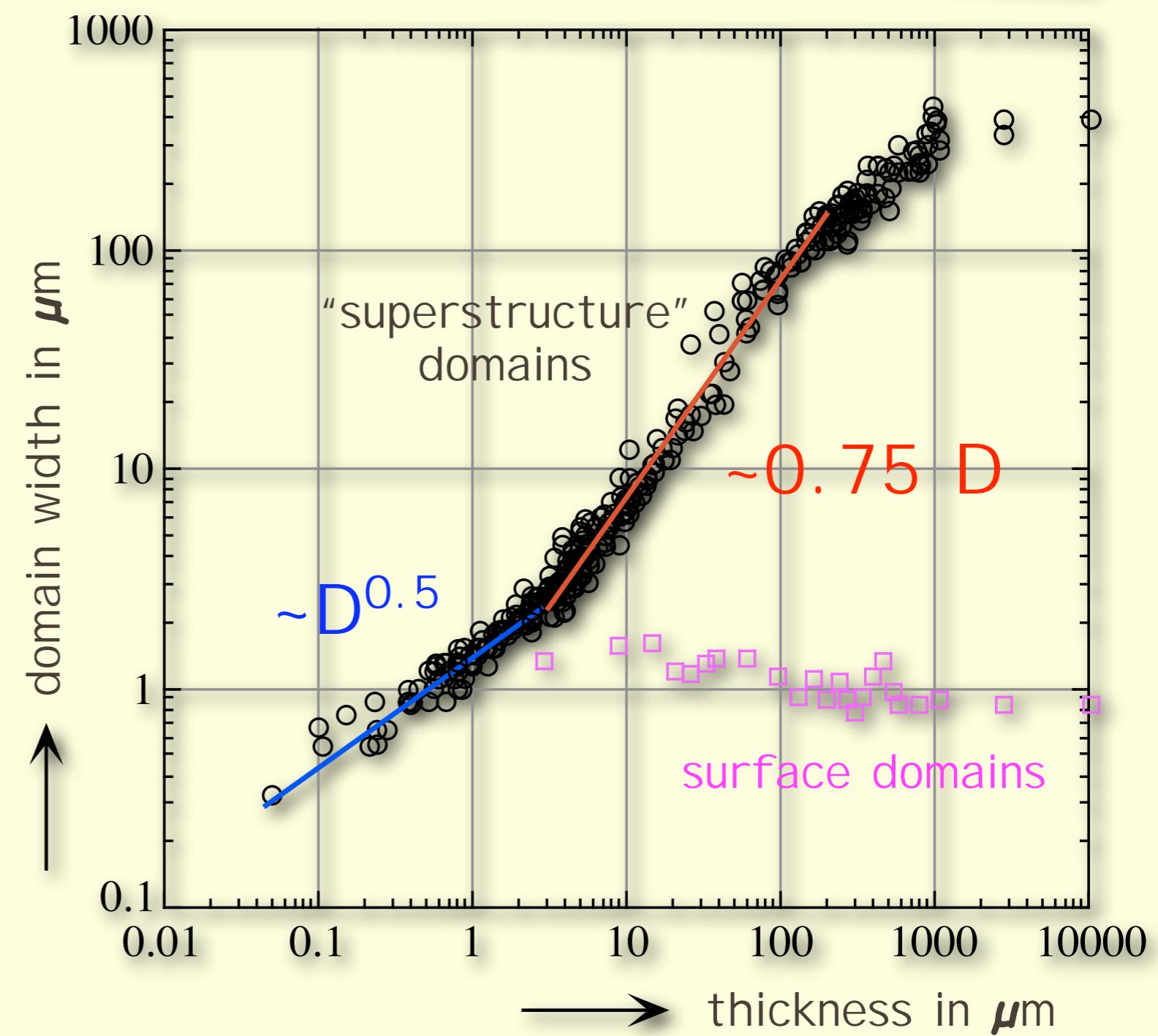
Experiment: Fe 12.8at%Si



Multi-phase branching



Experiment: Fe 12.8at%Si



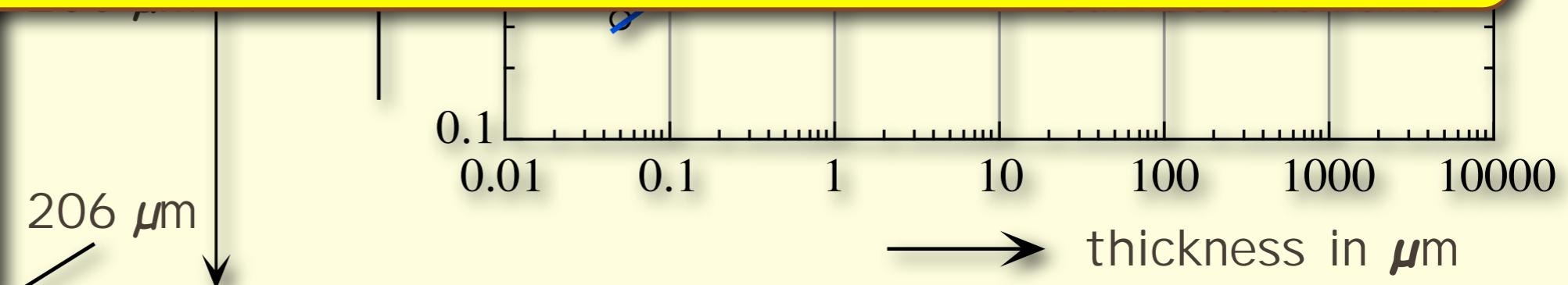
Multi-phase branching

Experiment: Fe 12.8at%Si

(111) surface

Strong misorientation:
branched domains -

Volume domain width scales linearly
with thickness,
i.e. it also scales linearly
with grain size



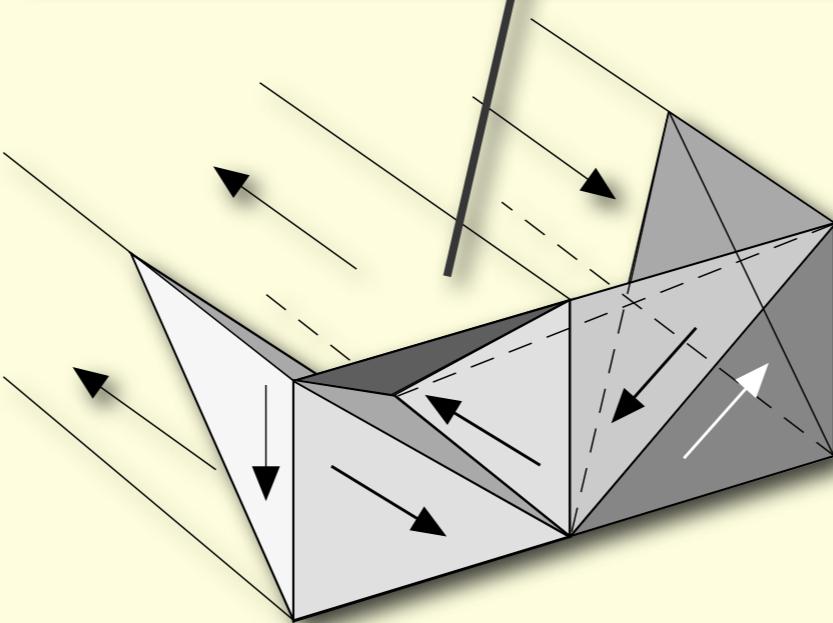
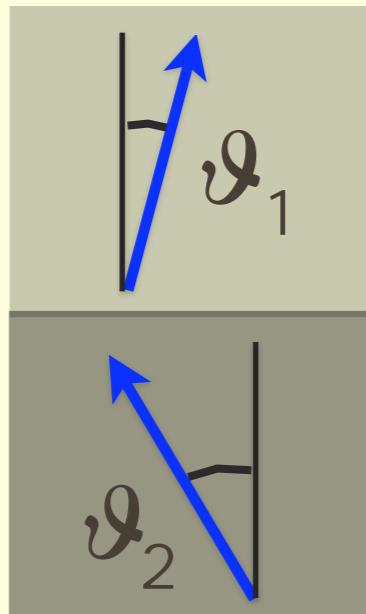
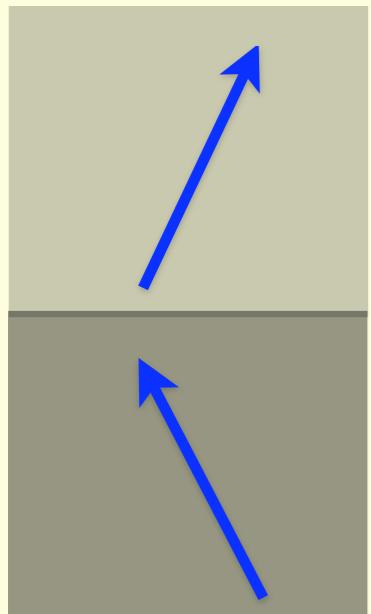
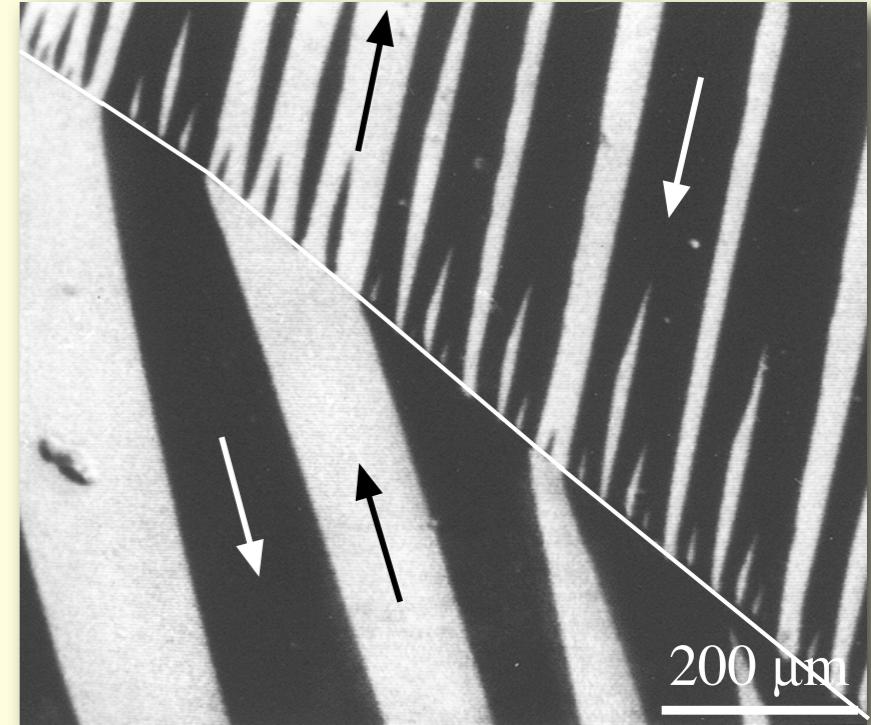
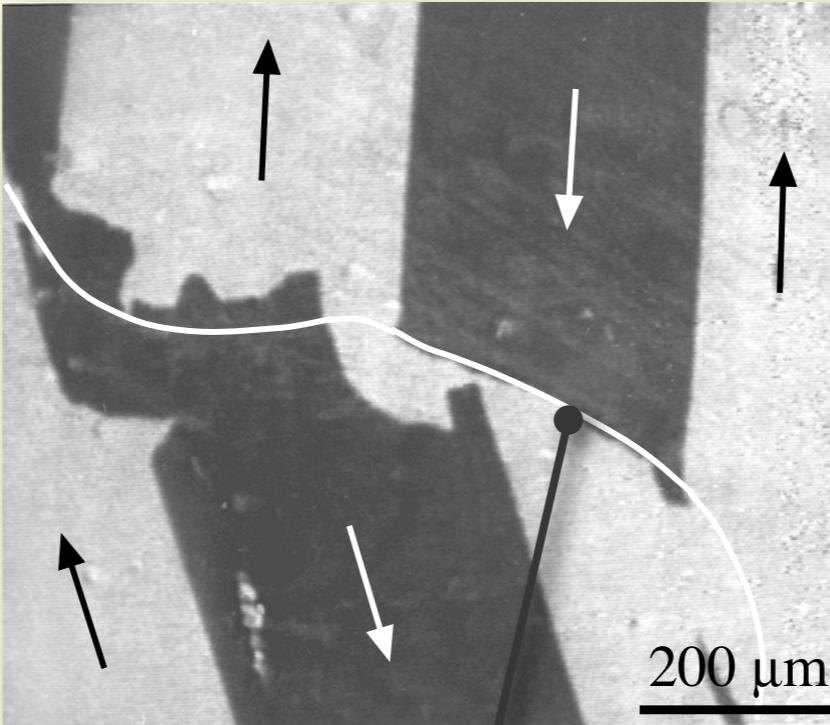
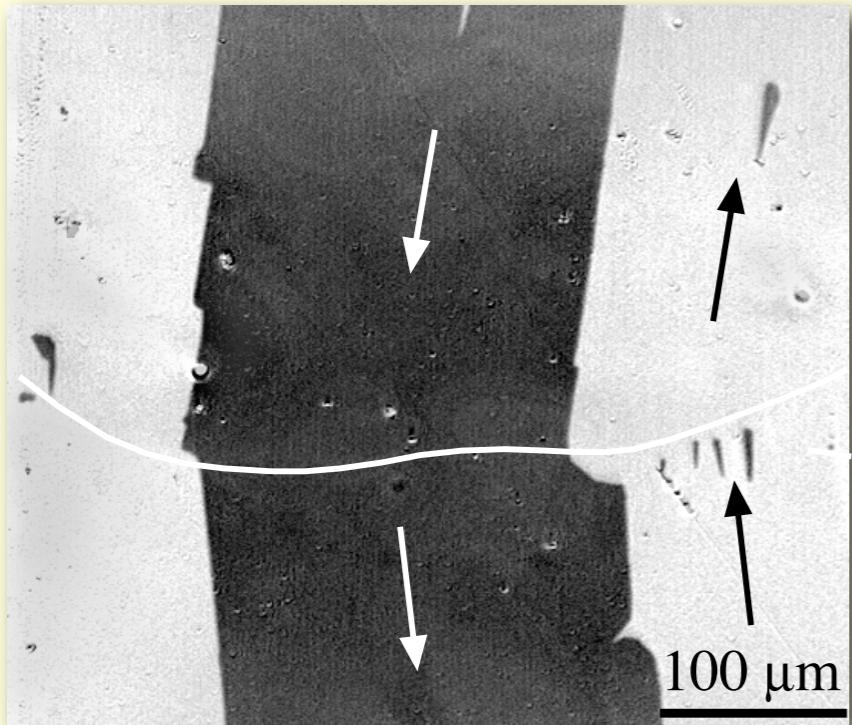
With decreasing grain size
the domains get finer.

With decreasing grain size
the domains get finer.

How is coercivity related
to grain size?

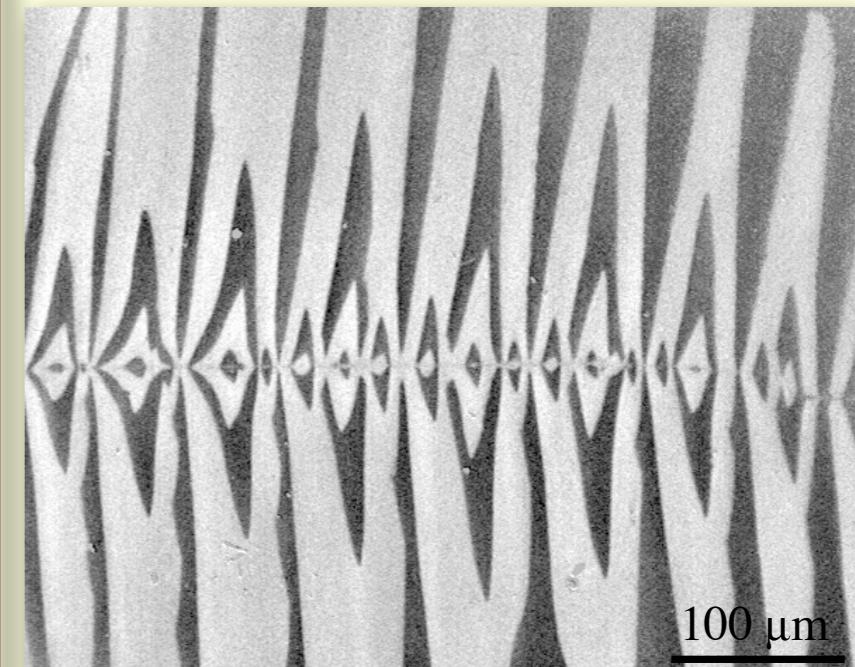
Grain boundary domains

Goss sheets



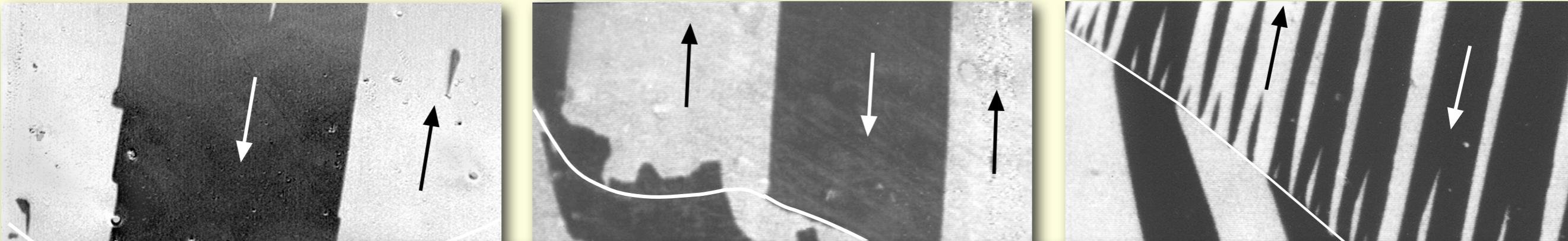
interface charge
 $= \cos \varphi_1 - \cos \varphi_2$

Ni(55%)Fe

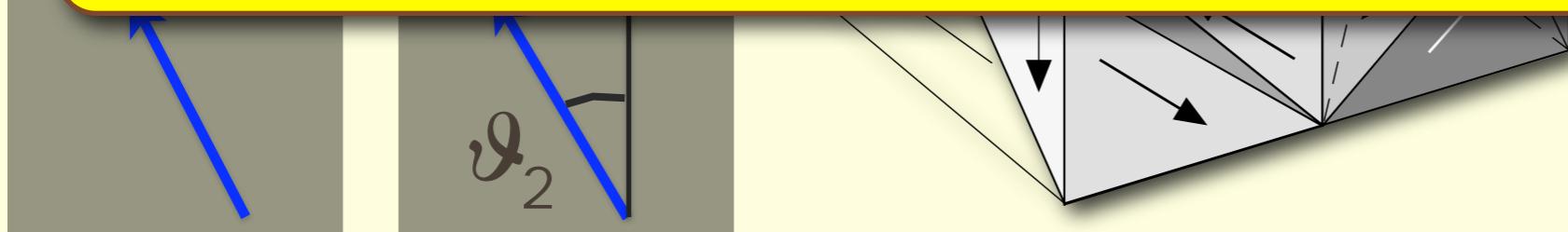


Grain boundary domains

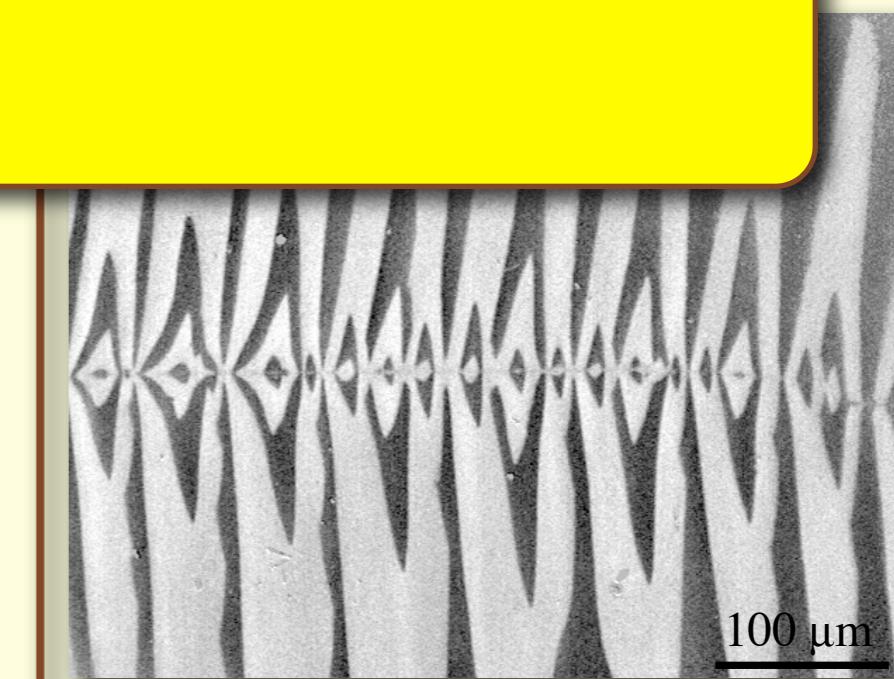
Goss sheets



Grain boundary domains:
avoid (reduce) magnetic charges

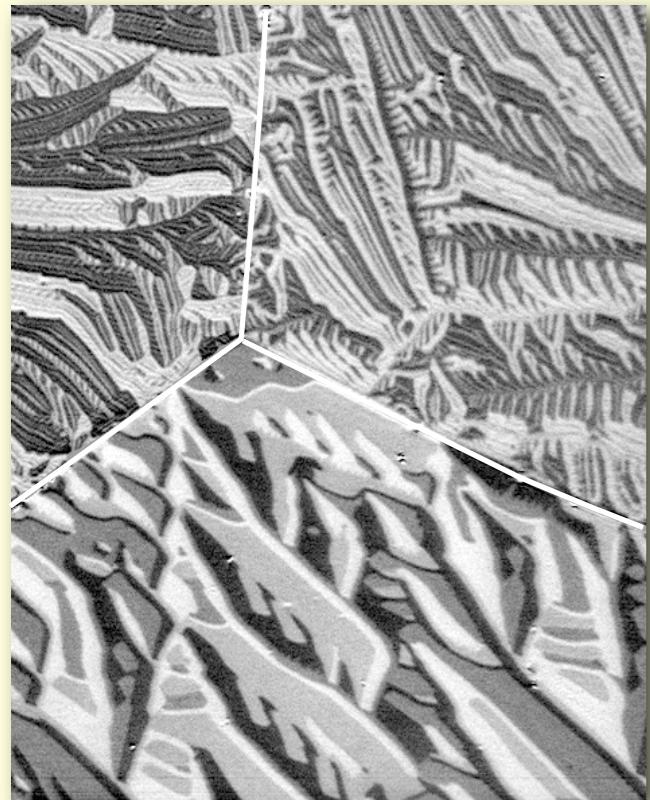


interface charge
 $= \cos \vartheta_1 - \cos \vartheta_2$

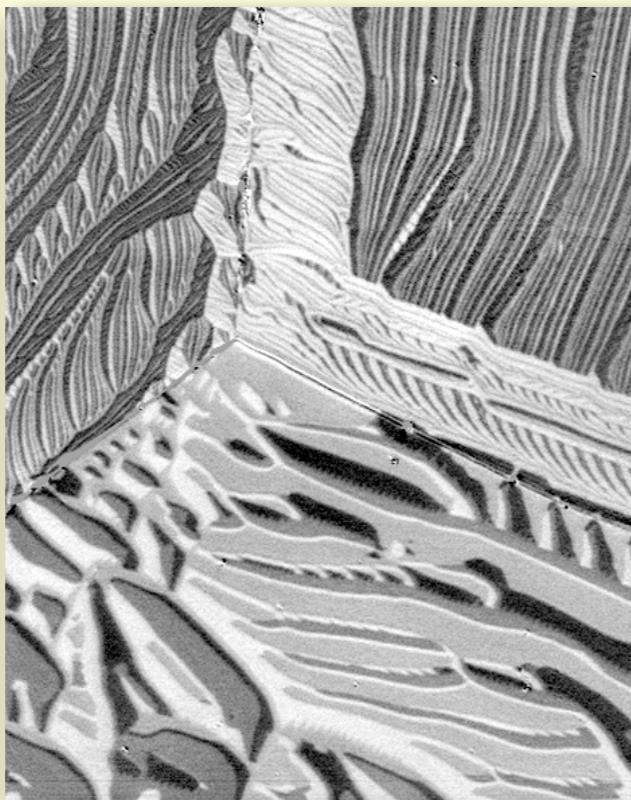


Grain boundary domains

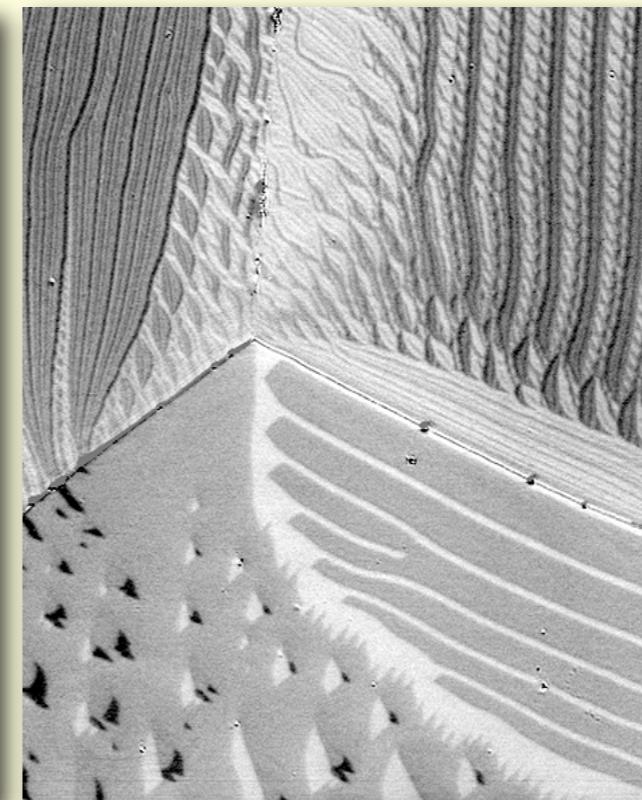
FeSi non-oriented sheet



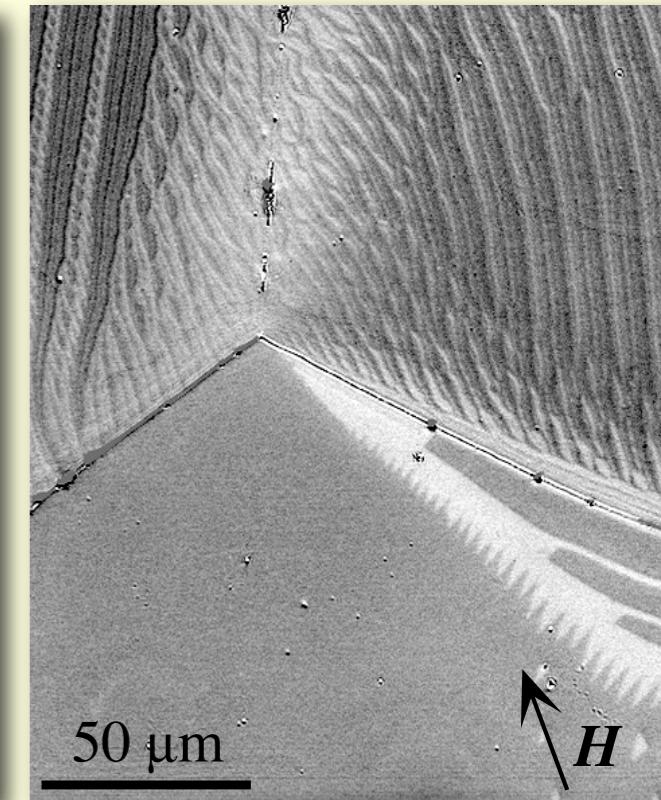
demagnetized



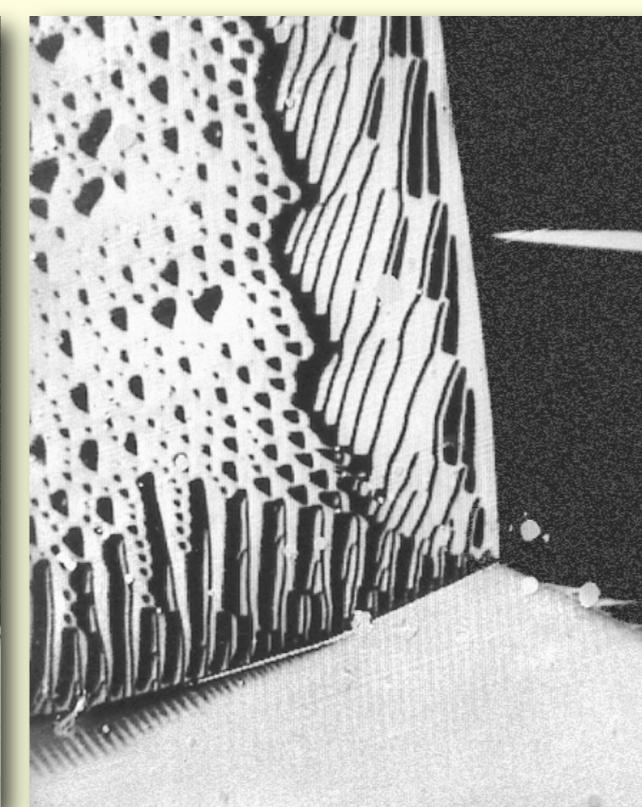
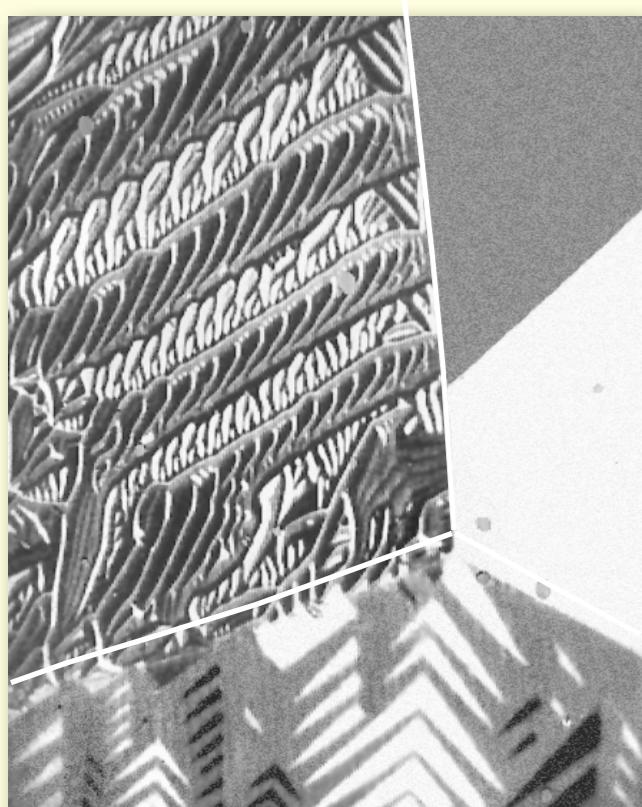
$0.17 M_S$



$0.26 M_S$



$0.34 M_S$

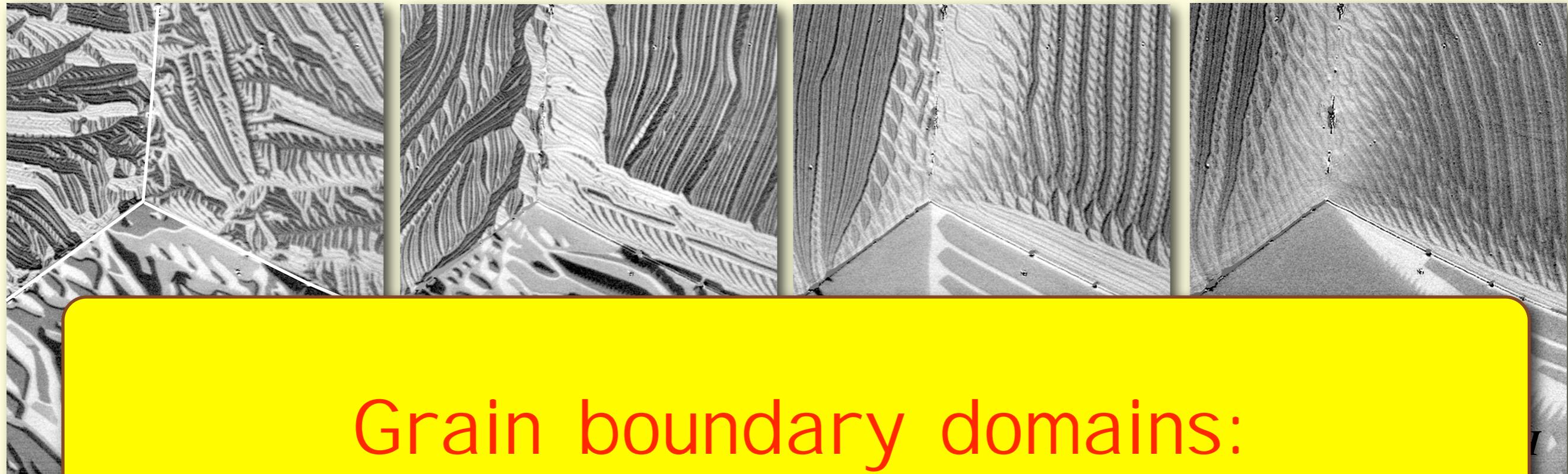


$100 \mu m$

H

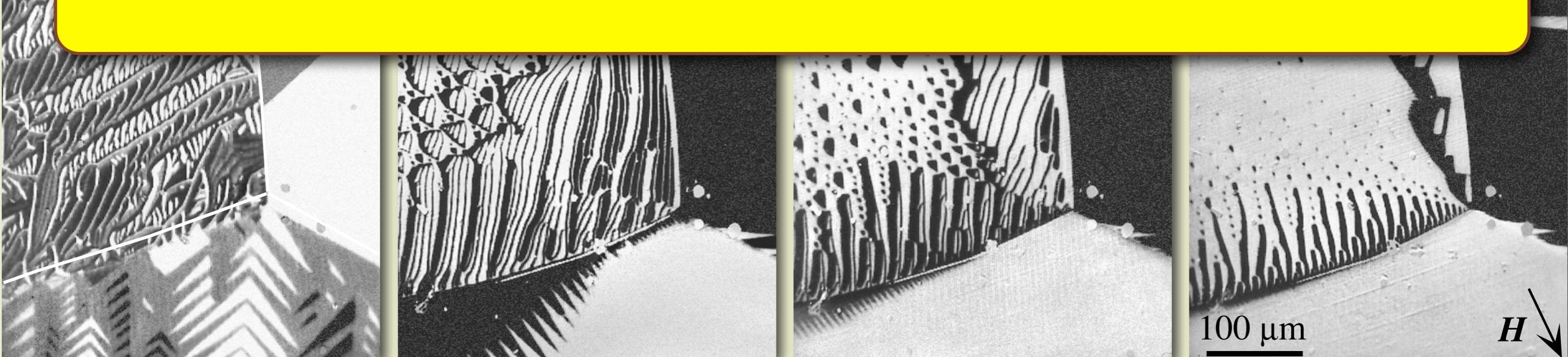
Grain boundary domains

FeSi non-oriented sheet



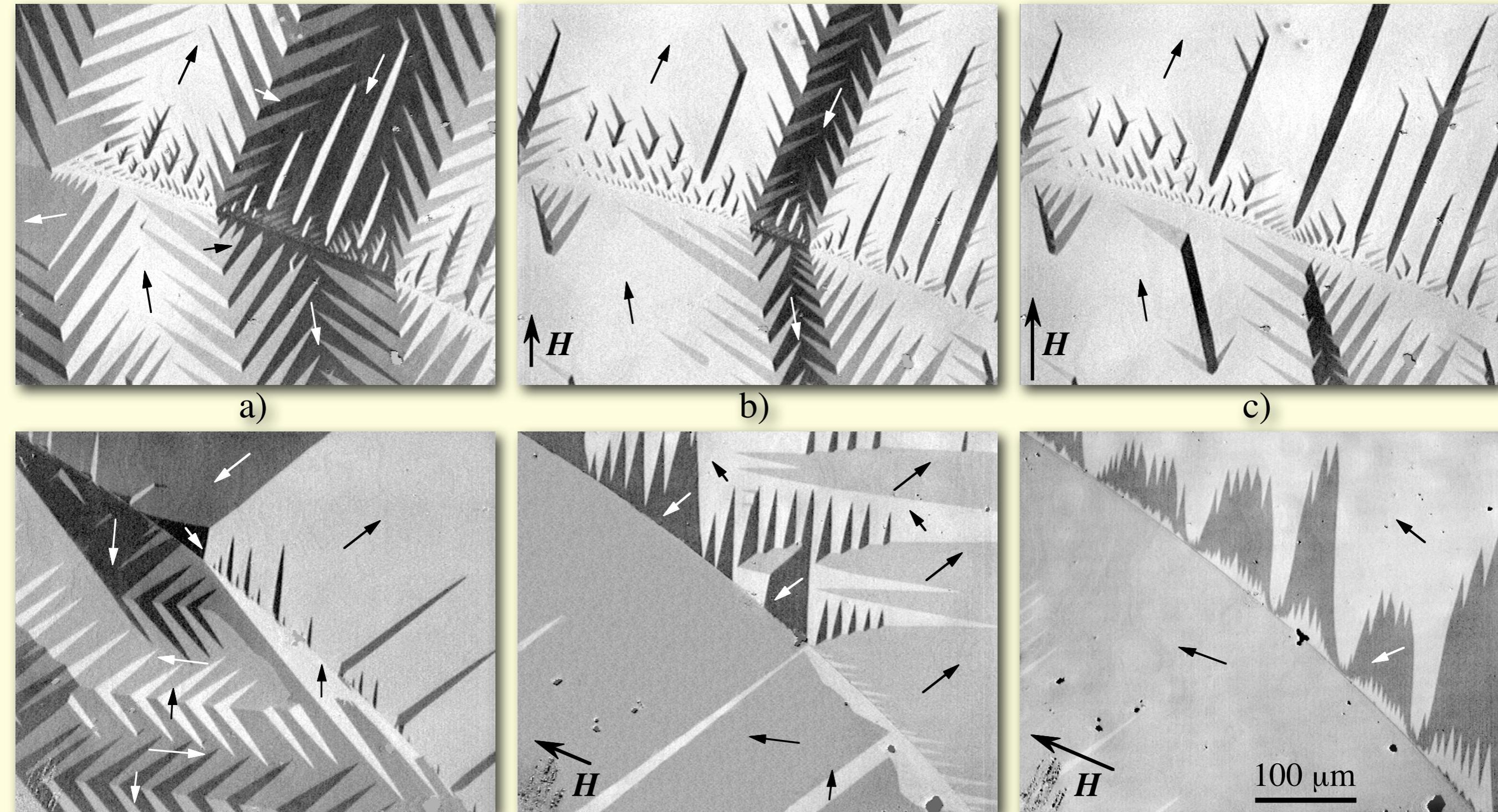
Grain boundary domains:

extend 50 - 100 μm into grains



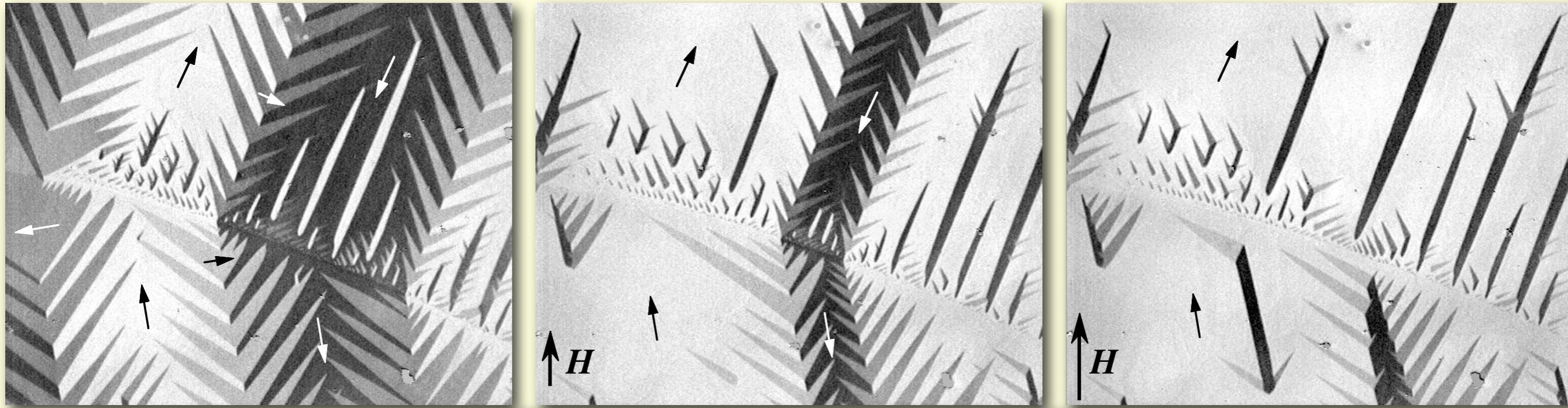
Grain boundary domains

FeSi non-oriented sheet



Grain boundary domains

FeSi non-oriented sheet



Grain boundary domains:
Their reorganization in magnetic
field costs energy



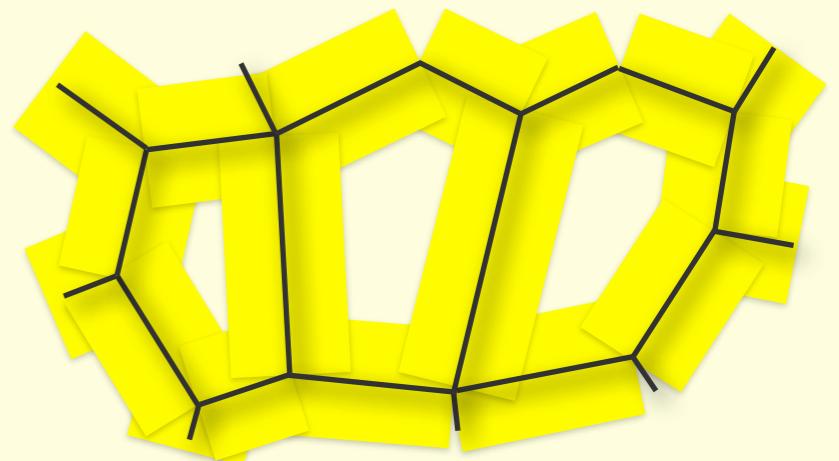
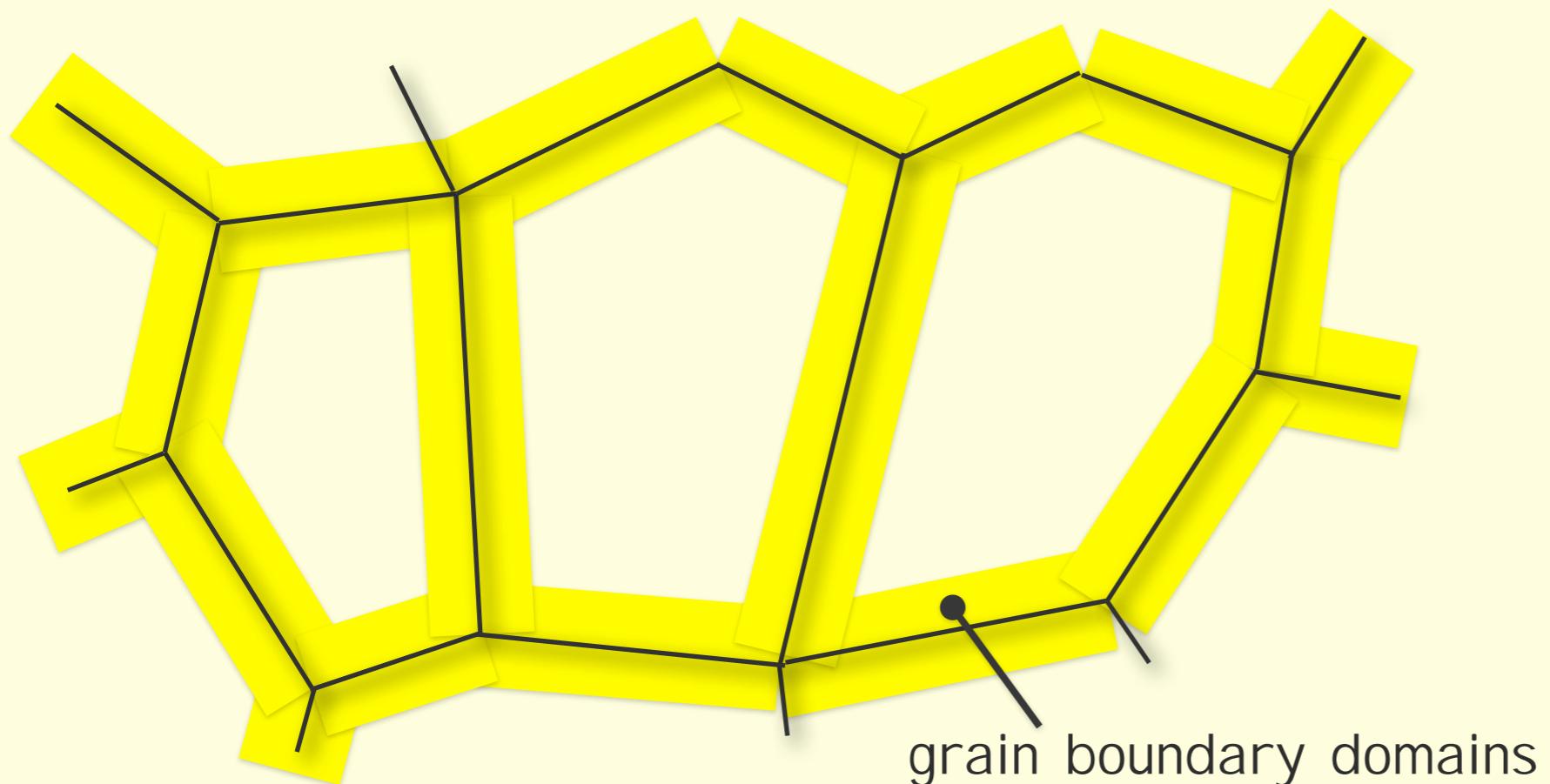
They are responsible for coercivity.

Grain boundary domains

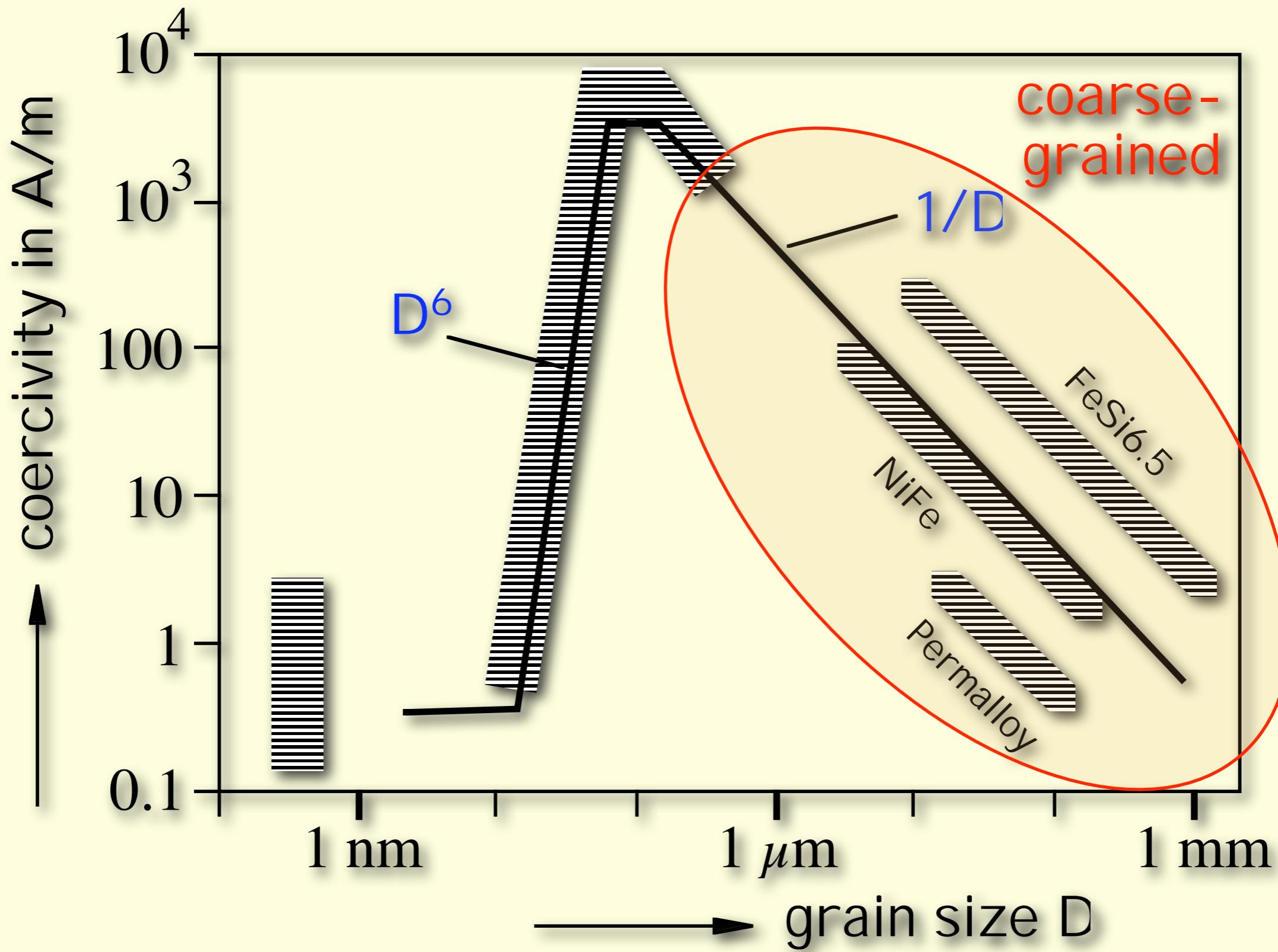
Their relative volume increases with decreasing grain size



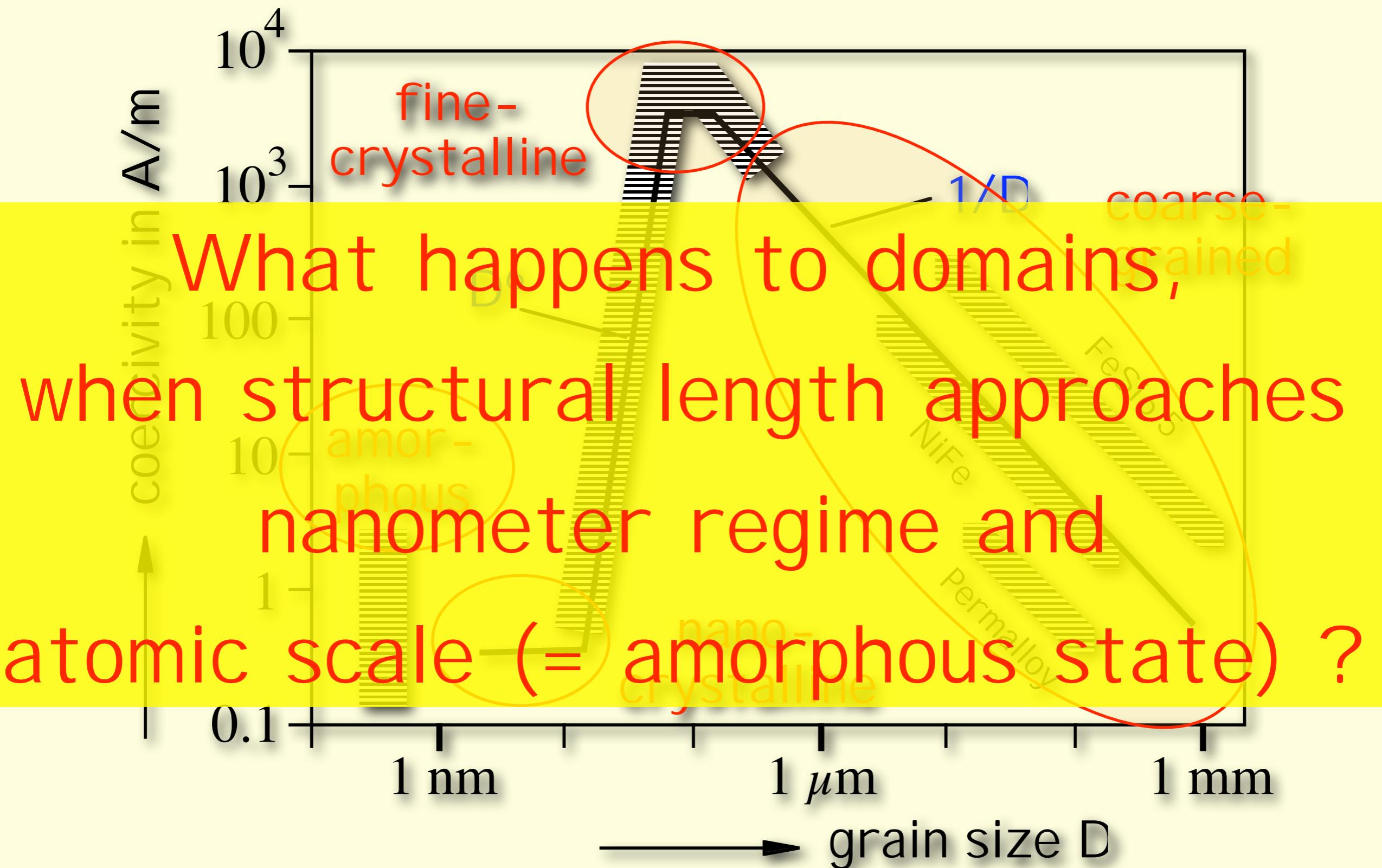
Coercivity increases with decreasing grain size



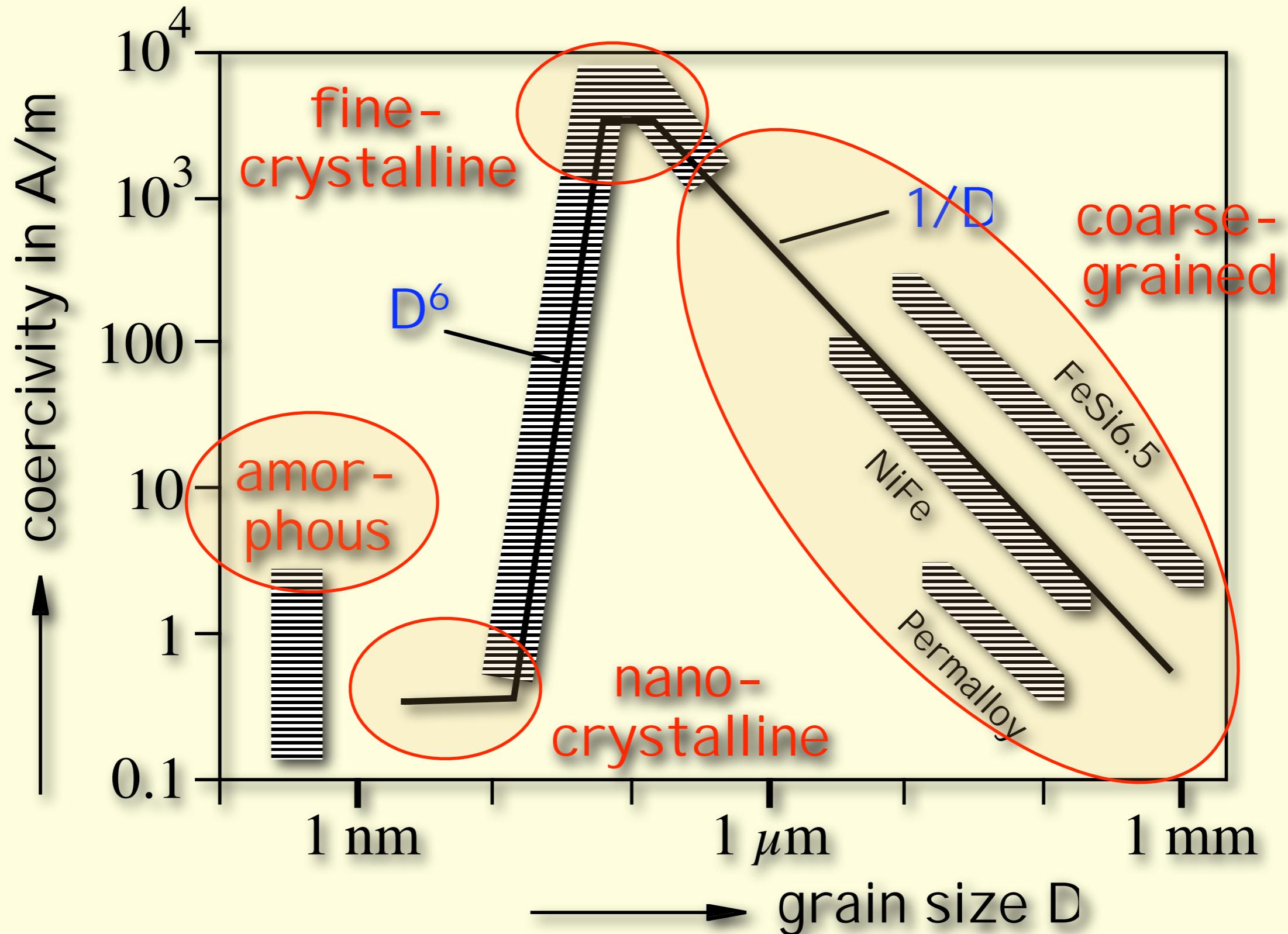
Coercivity and grain size



Coercivity and grain size



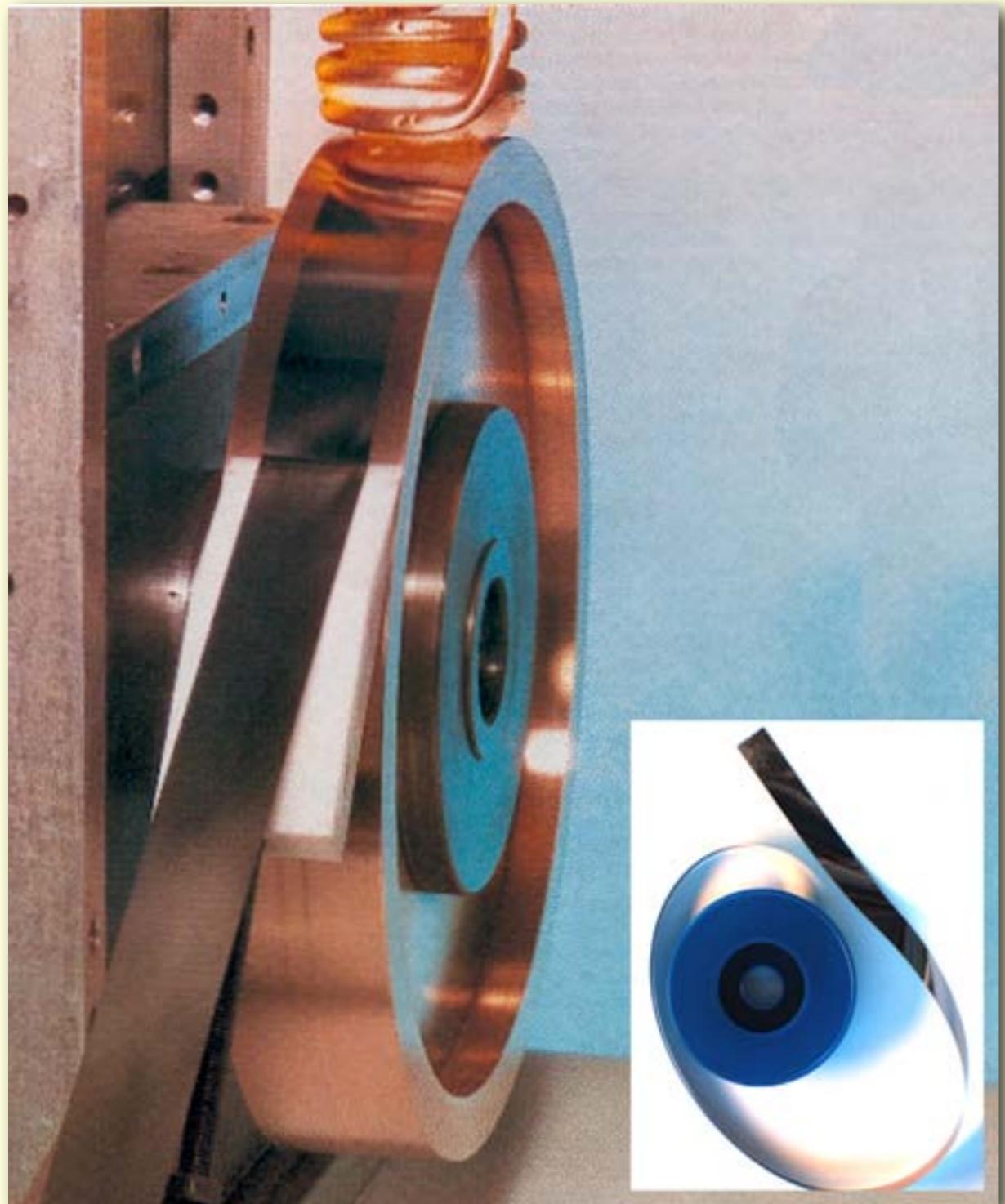
Coercivity and grain size



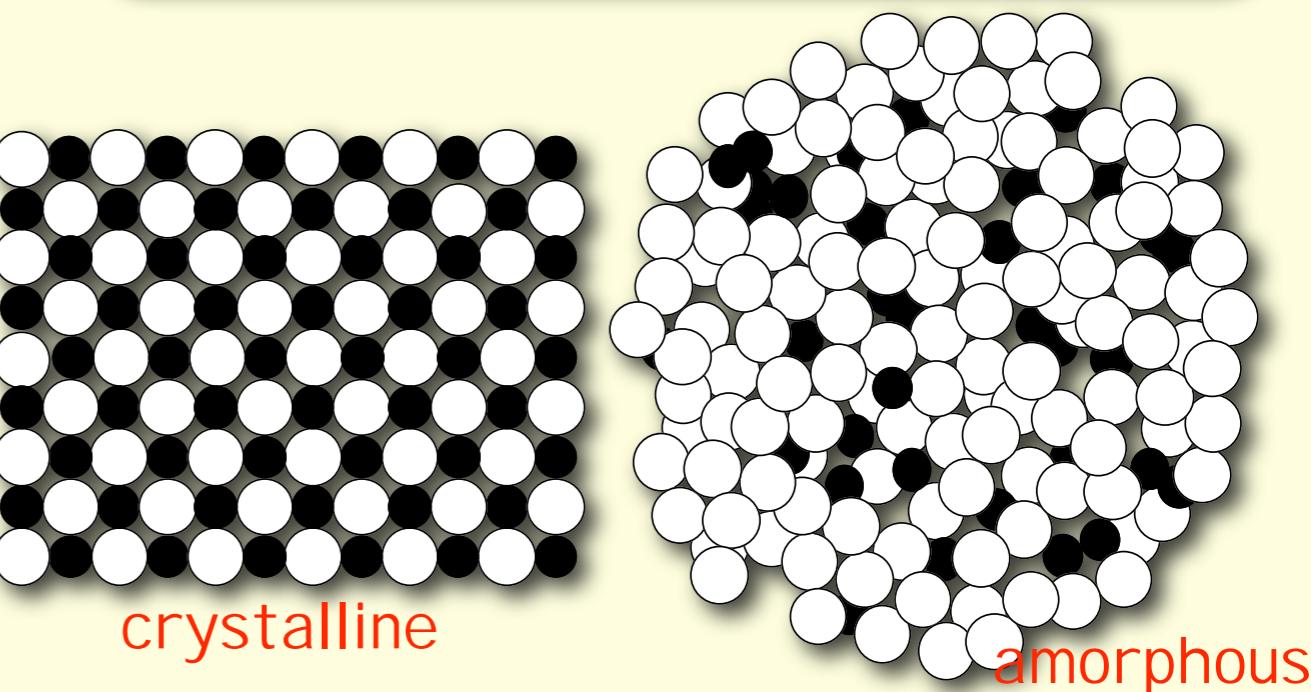
Overview

1. Domains in coarse-grained material
2. Domains in amorphous material
3. Domains in nanocrystalline,
soft magnetic ($Q \ll 1$) materials
4. Domains in fine- and nanostructured,
permanent magnetic ($Q > 1$) materials

Rapidly quenched amorphous ribbons

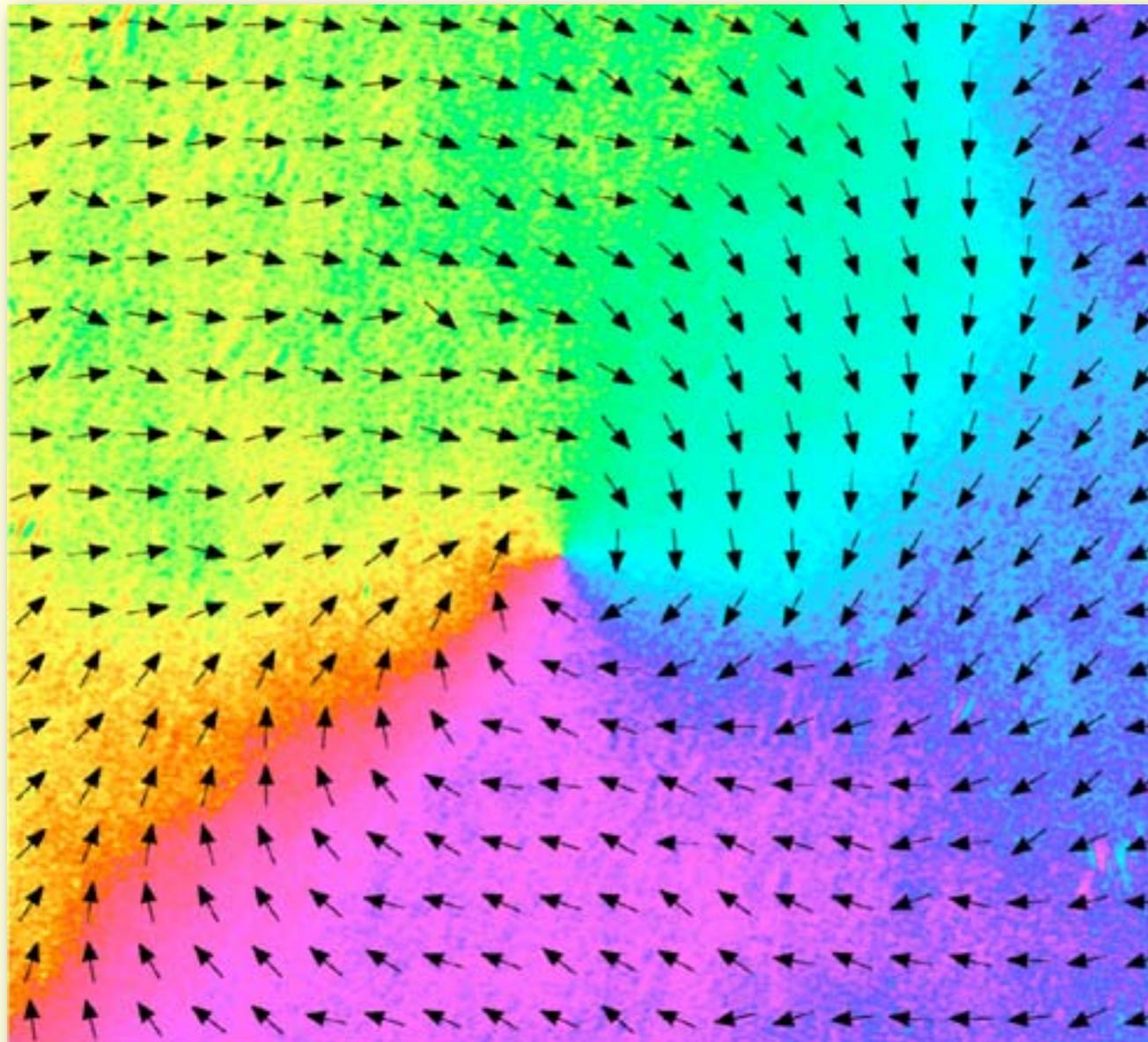


- thickness $20 \mu\text{m}$
 - ferromagnetic
(with Fe, Ni, Co)
 - $T_{75-83} M_{25-17}$
 $T = \text{Fe, Co, Ni}$
 $M = \text{P, C, B, Si, Al, ...}$
- no magnetocrystalline anisotropy

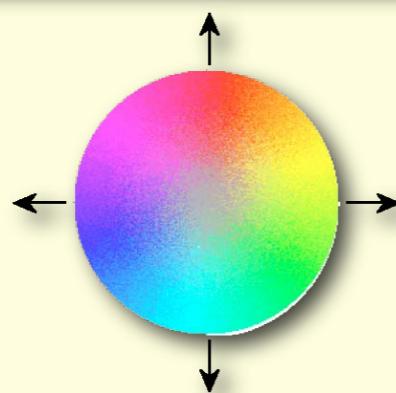
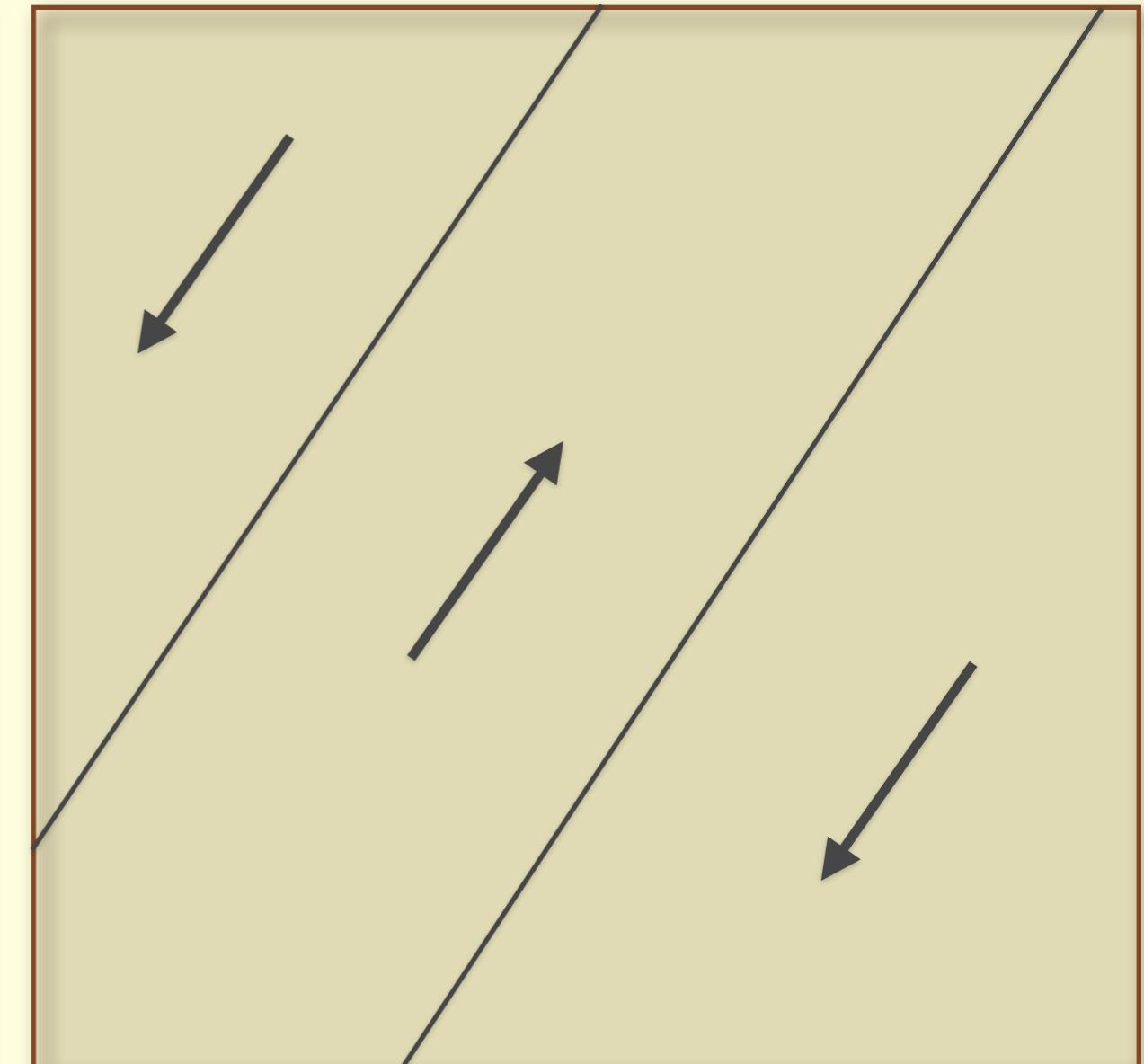


Magnetic microstructure of amorphous ribbons

$m(r)$ continuously flowing ?



or regular domains ?



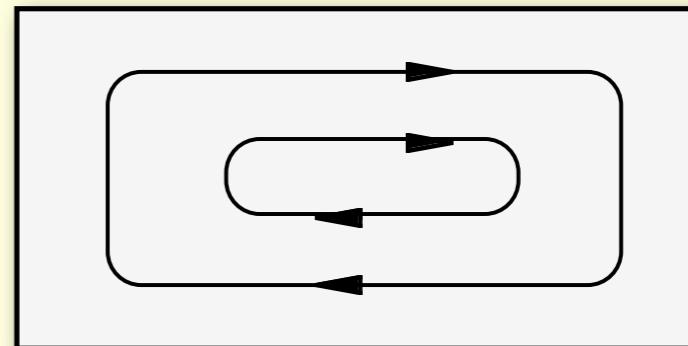
Excursion:

Some general considerations
on anisotropy and domains

Van den Berg Concept

[H.A.M. van den Berg, 1986]

- Assumption: anisotropy-free film element



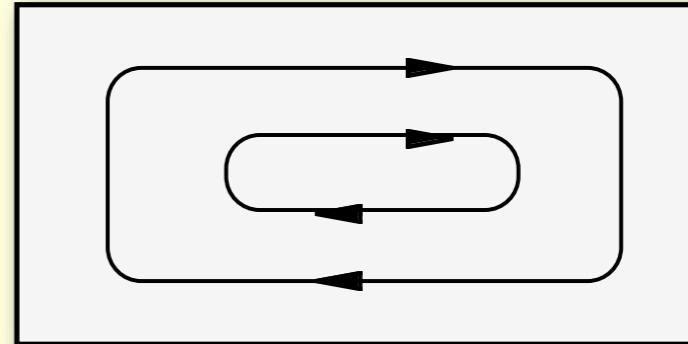
expect: continuously flowing $m(r)$

Van den Berg Concept

[H.A.M. van den Berg, 1986]

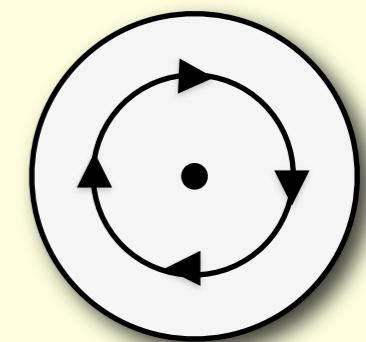
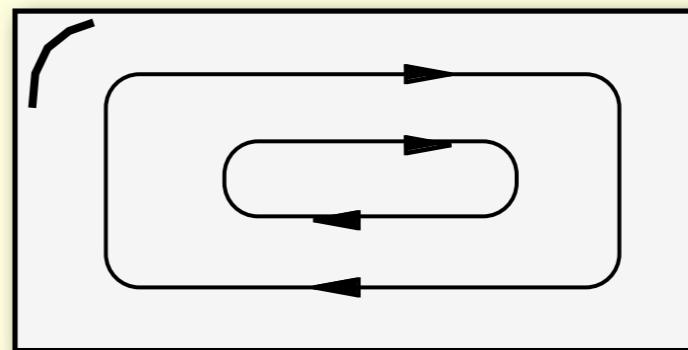
- Assumption: anisotropy-free film element
- Stray-field freedom requires:

- $\text{div } \mathbf{m} = 0$
- $\mathbf{m}(x,y) \parallel \text{sample edge}$
- $\mathbf{m}(x,y) \parallel \text{film plane}$
- $|\mathbf{m}| = 1$



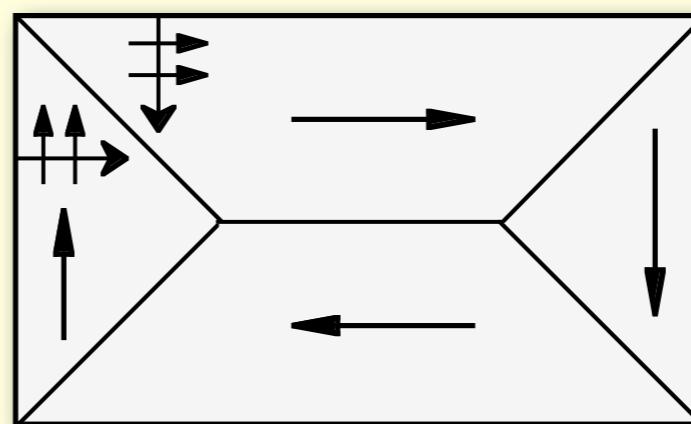
expect: continuously flowing $\mathbf{m}(r)$

Conditions cannot be met by
continuous pattern
(exception: circular element)

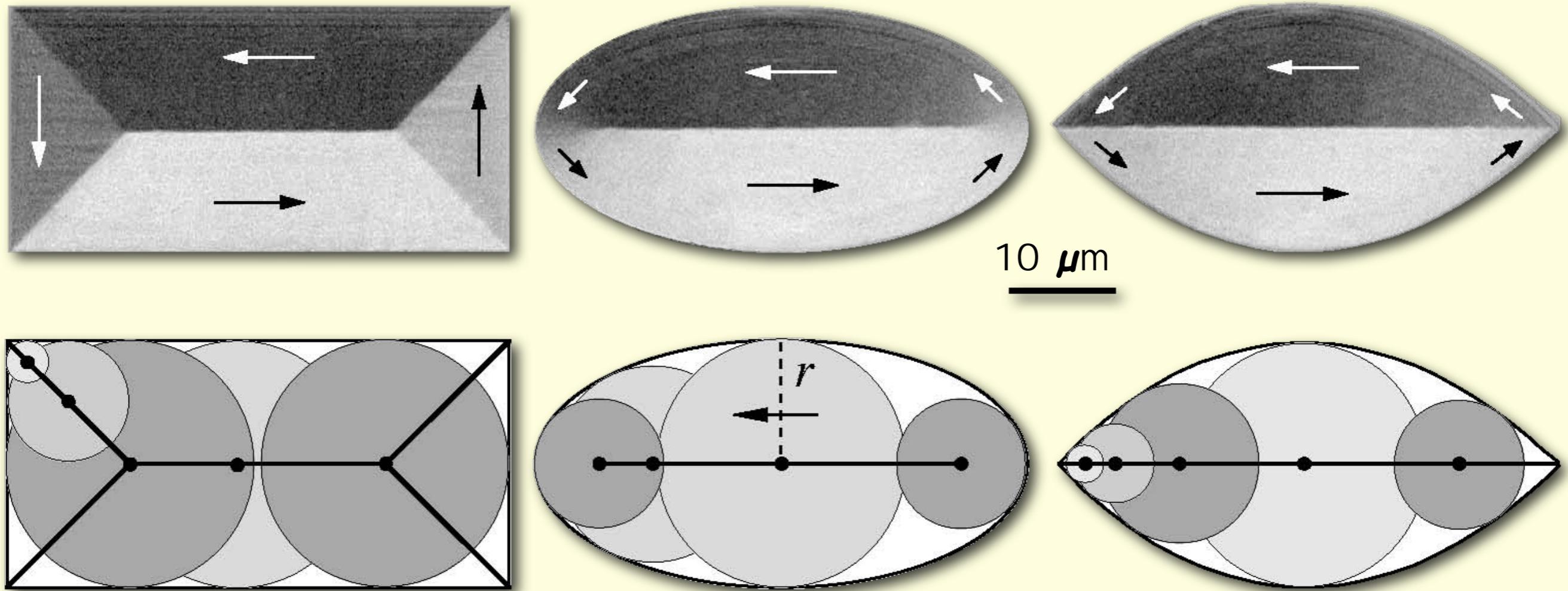


Consequence:

Regular domain pattern with
discontinuities (domain walls),
enforced by element shape to
avoid magnetic poles

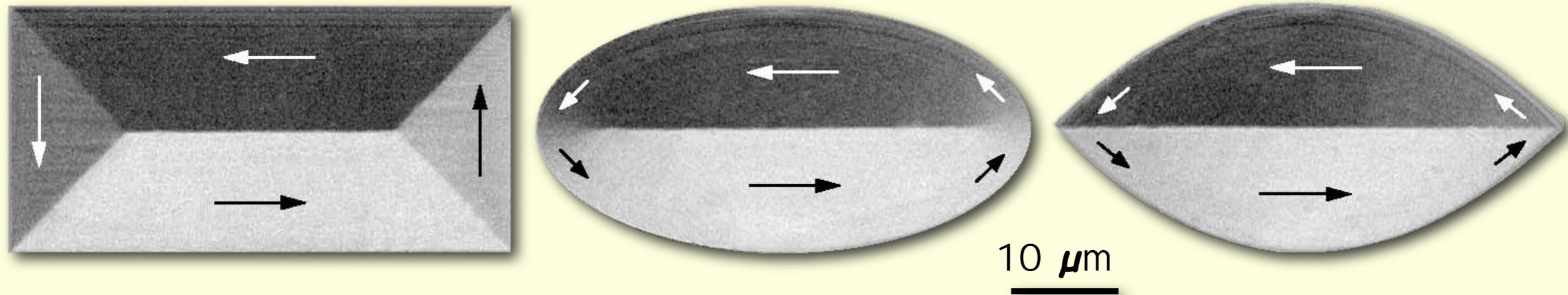


Van den Berg Construction



- Take circles that touch edge at two or more points.
Centers of circles form walls
- In every circle the magnetization direction must be perpendicular to each touching radius
- If a circle touches edge in more than 2 points: its center forms wall junction
- If touching points fall together: wall ends at center of circle = zone of concentric rotation
- Acute corner: boundary runs into corner

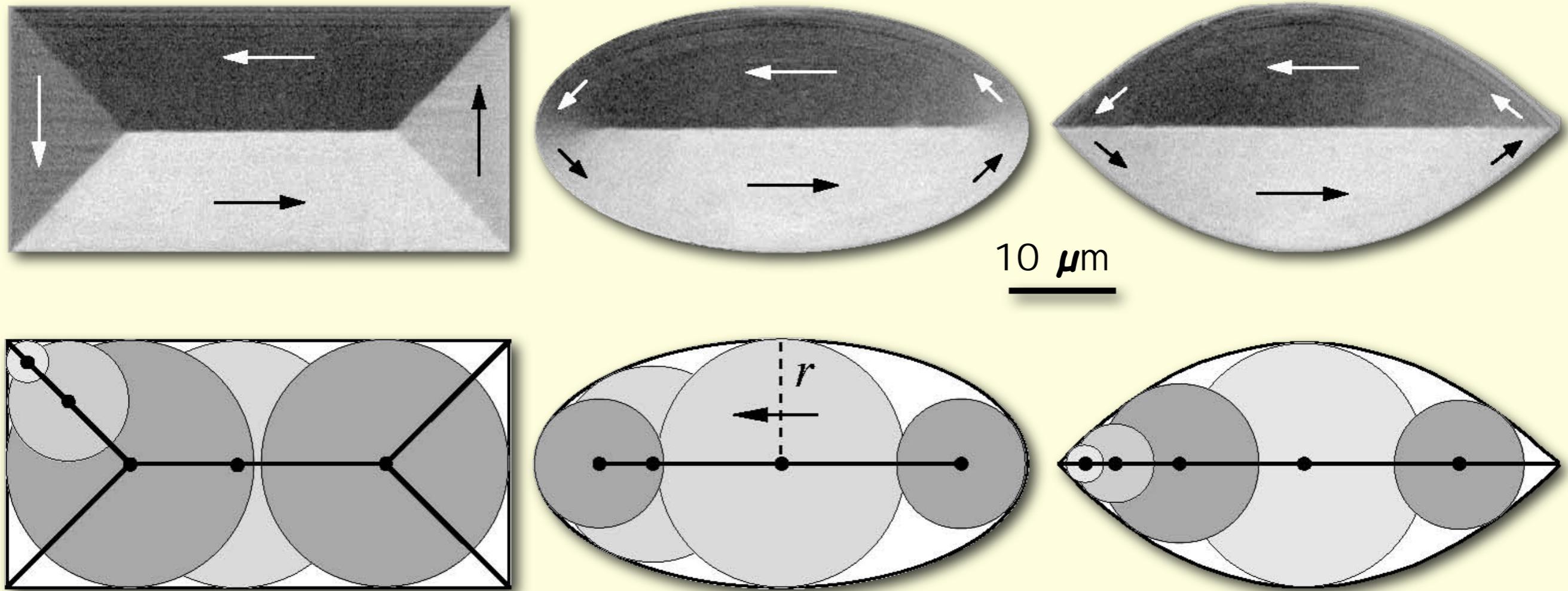
Van den Berg Construction



Anisotropy-free film element:

- Curved domain walls
- Domain walls and rotation areas,
- formed by requirement of stray-field freedom
- Acute corner: boundary runs into corner

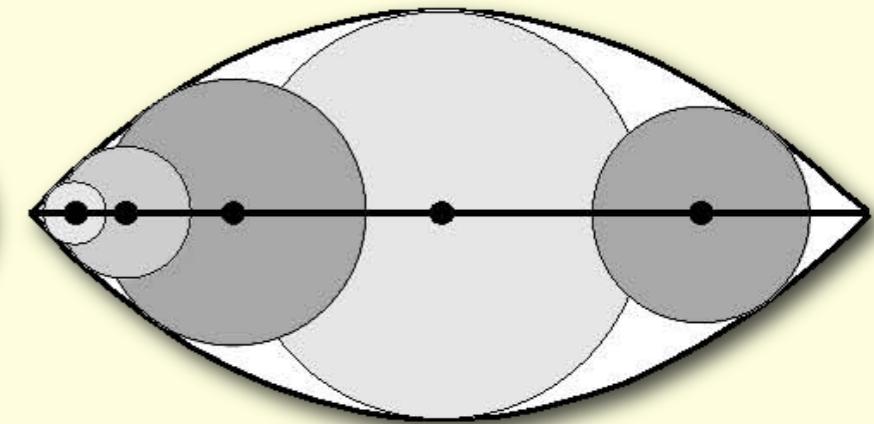
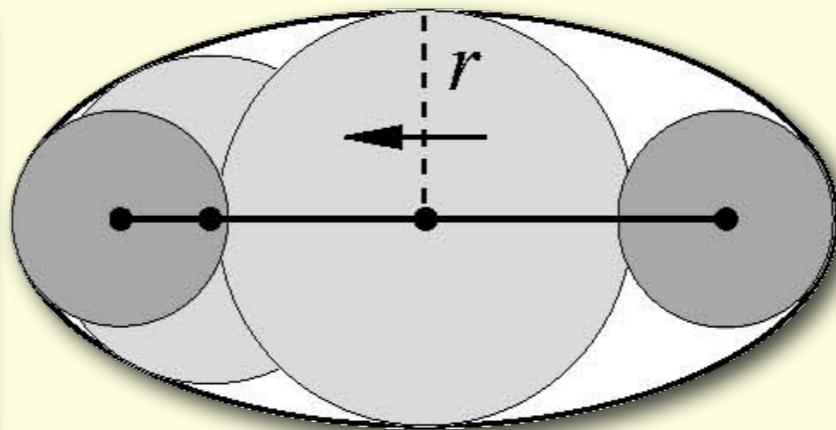
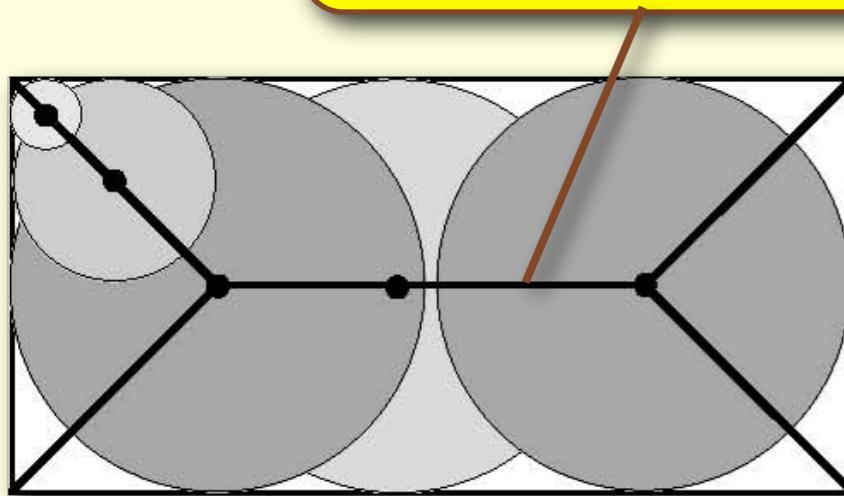
Van den Berg Construction



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- Acute corner: boundary runs into corner

Van den Berg Construction

van den Berg discontinuities
are in reality domain walls



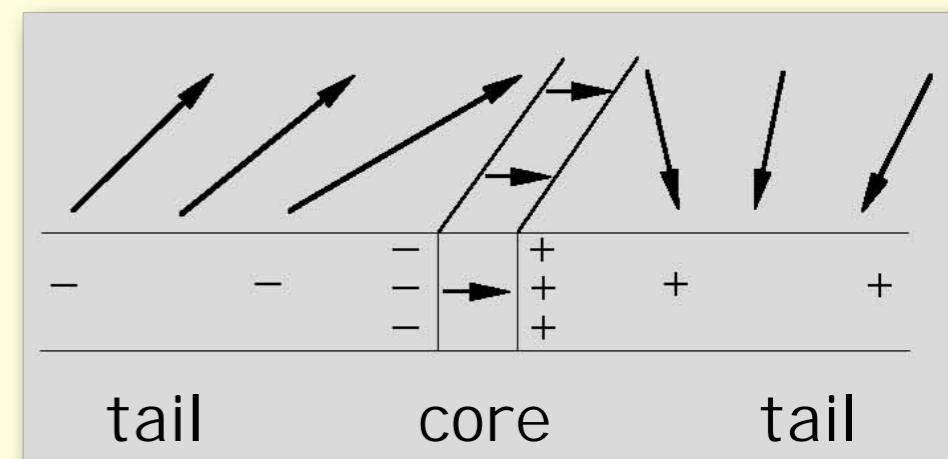
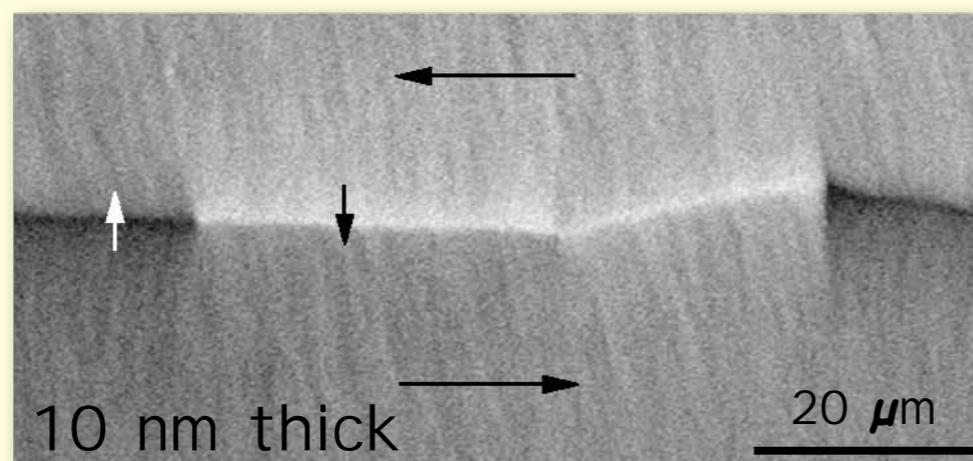
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- Acute corner: boundary runs into corner

180° wall types in soft magnetic films

Néel wall

film thickness
 < 100 nm

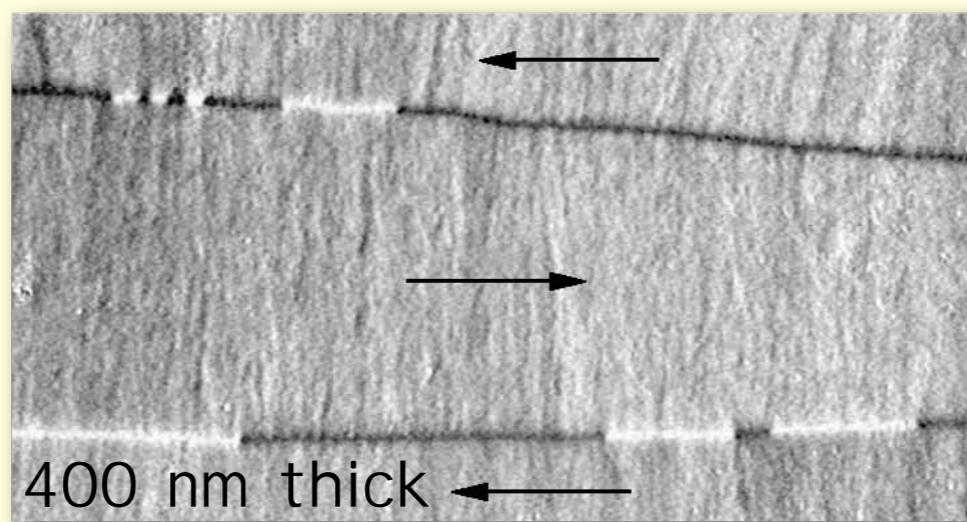
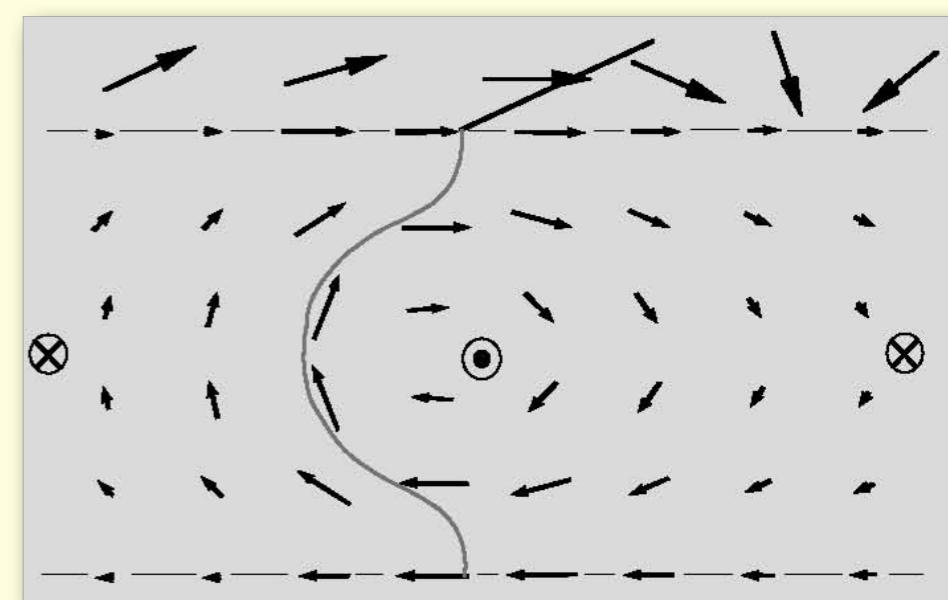
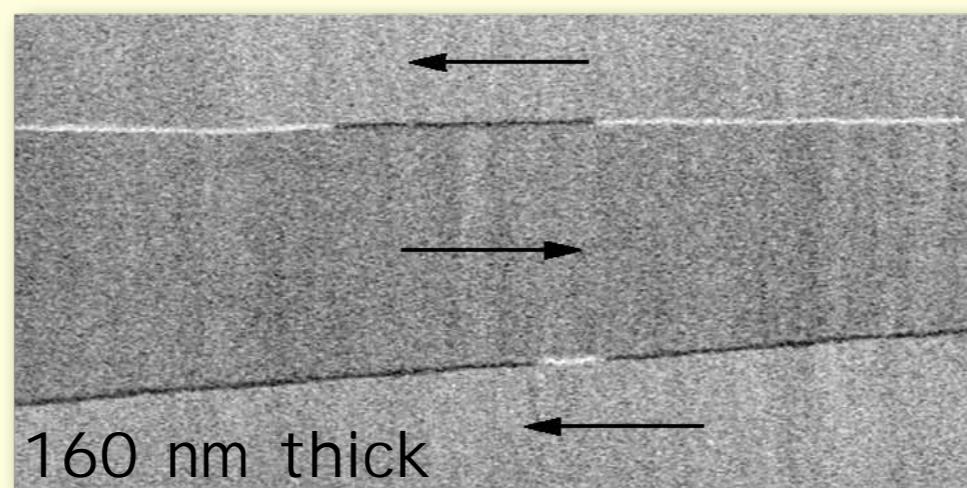
scales with $\sqrt{A/K_d}$



Asymmetric
Bloch wall

film thickness
 > 100 nm

scales with
thickness



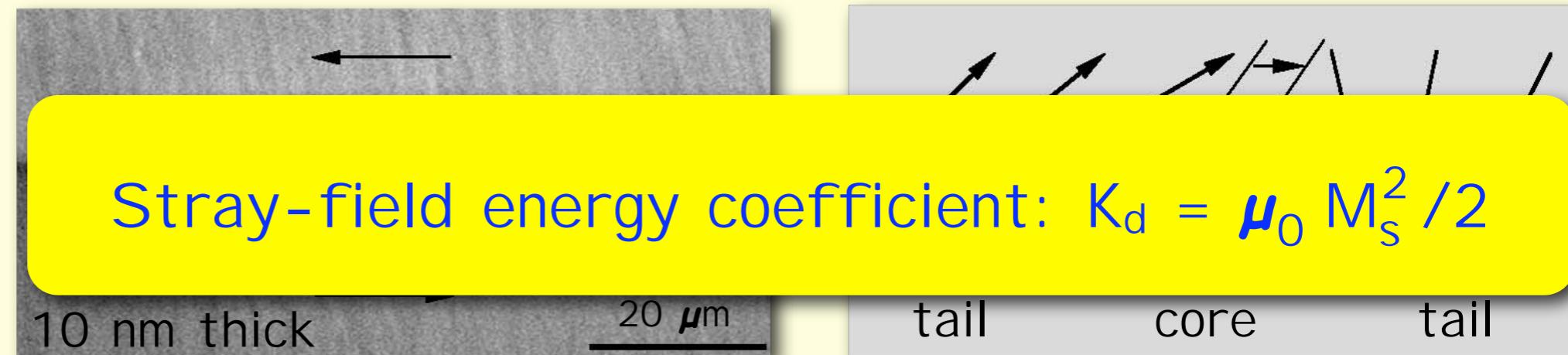
Permalloy
(NiFe)

180° wall types in soft magnetic films

Néel wall

film thickness
 $< 100 \text{ nm}$

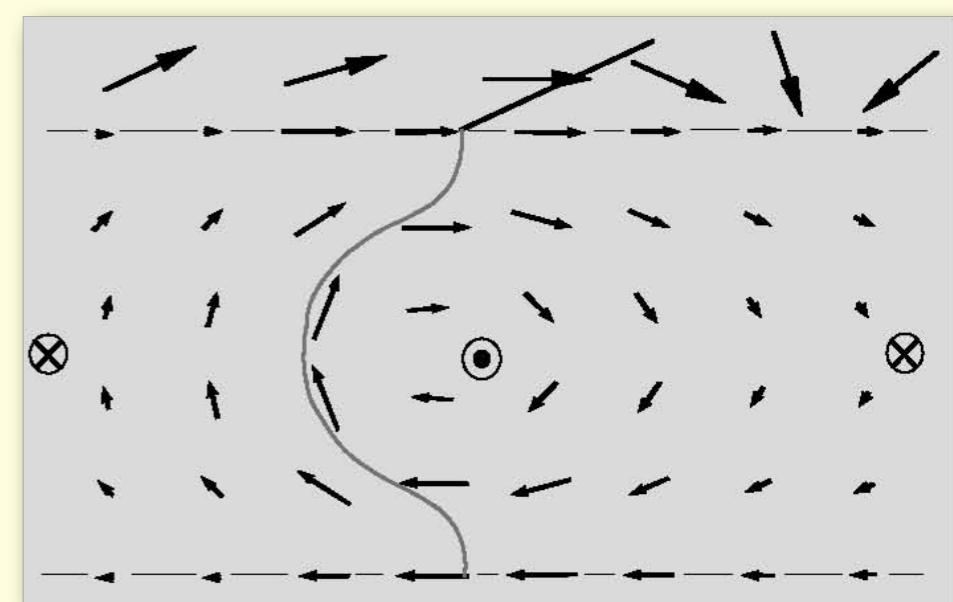
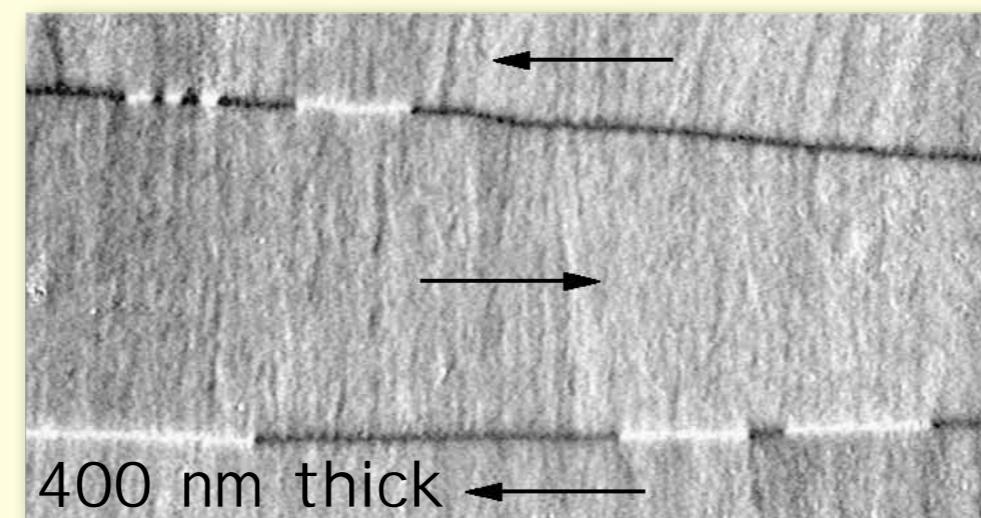
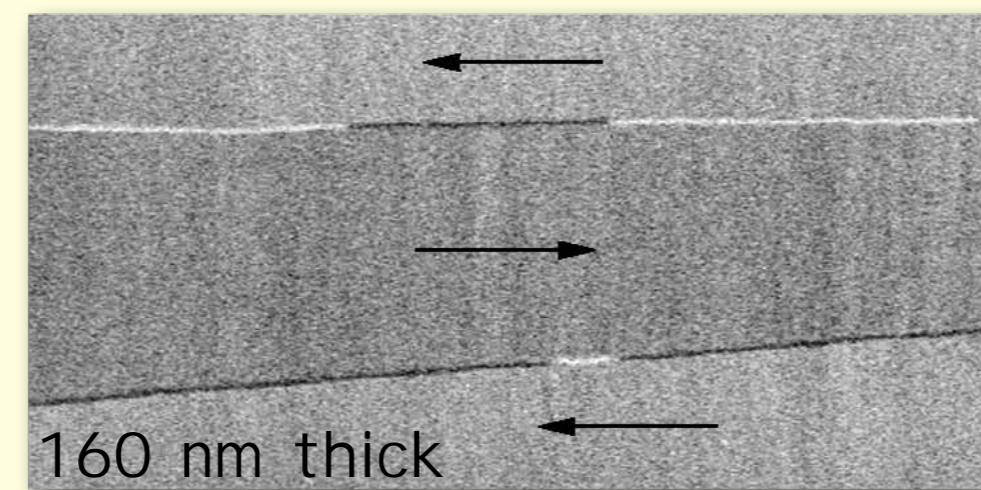
scales with $\sqrt{A/K_d}$



Asymmetric
Bloch wall

film thickness
 $> 100 \text{ nm}$

scales with
thickness



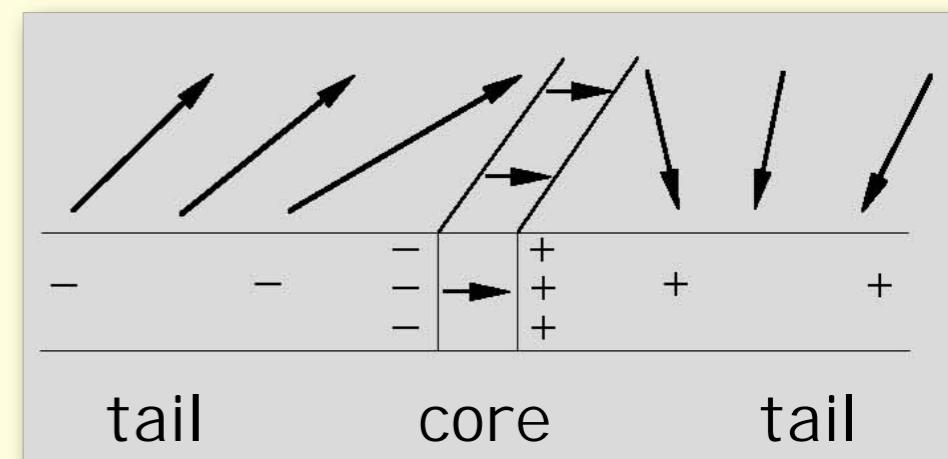
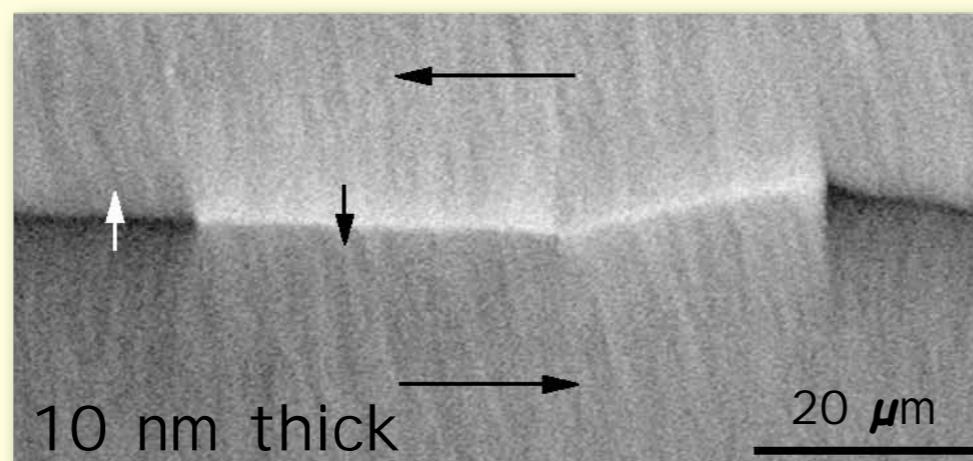
Permalloy
(NiFe)

180° wall types in soft magnetic films

Néel wall

film thickness
 < 100 nm

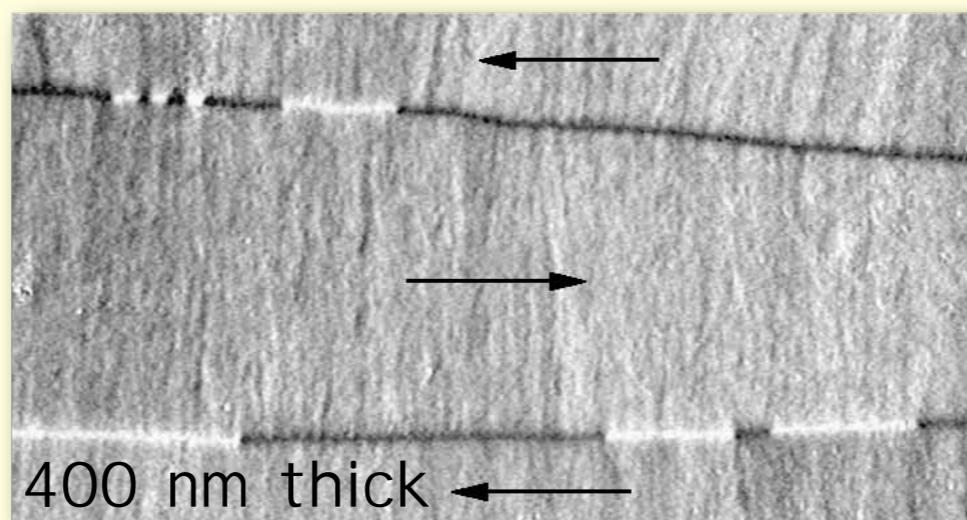
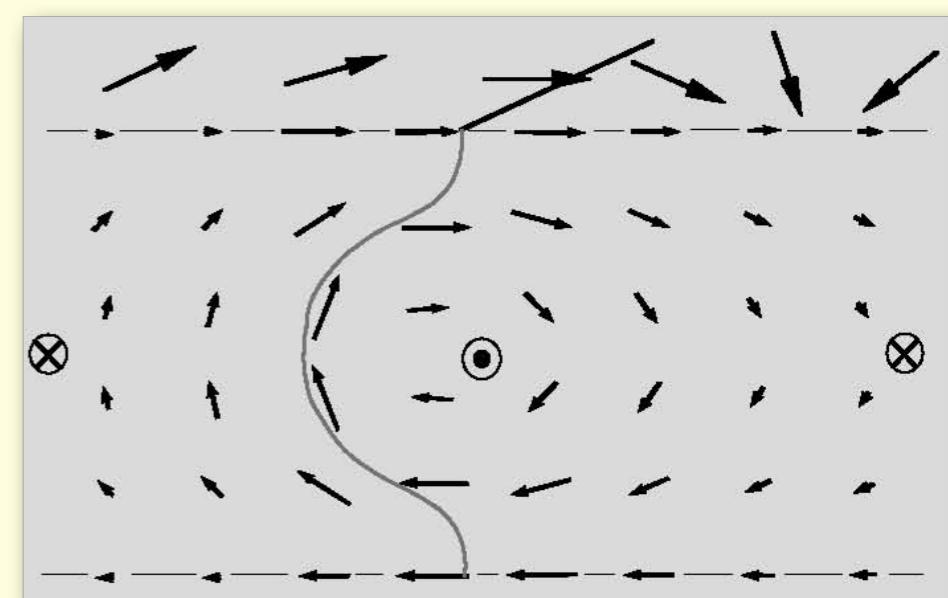
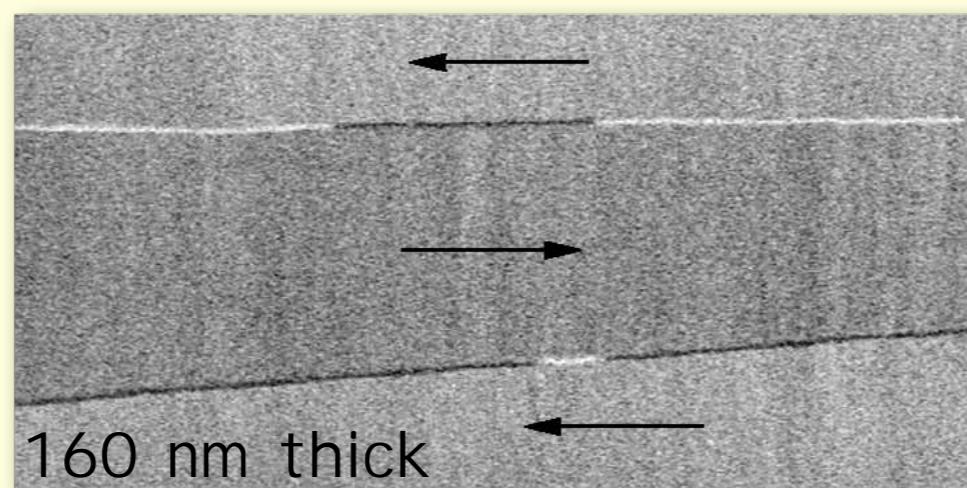
scales with $\sqrt{A/K_d}$



Asymmetric
Bloch wall

film thickness
 > 100 nm

scales with
thickness



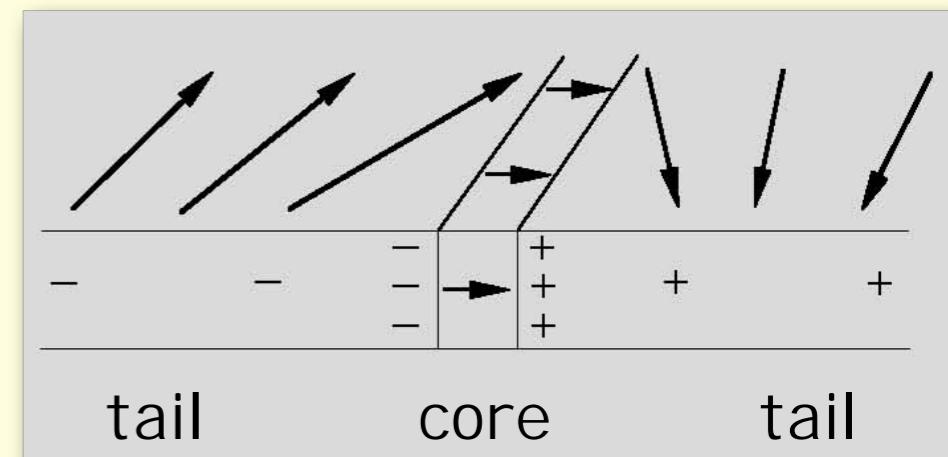
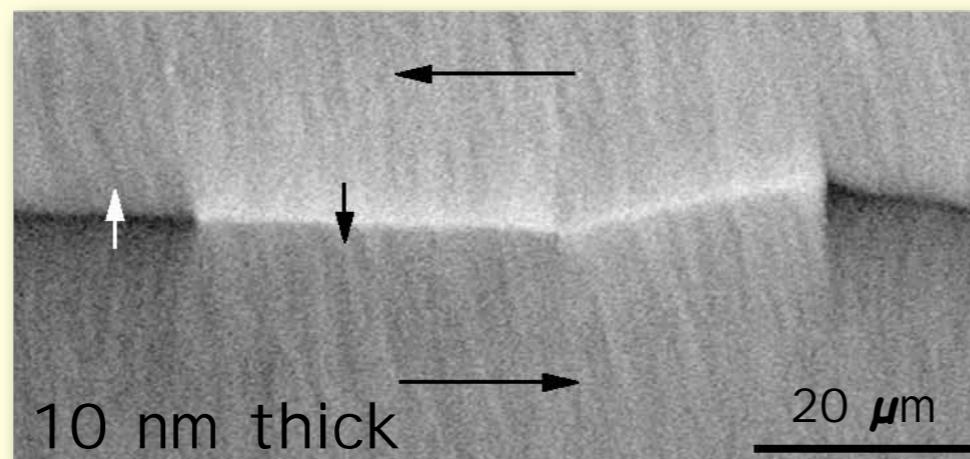
Permalloy
(NiFe)

180° wall types in soft magnetic films

Néel wall

film thickness
 < 100 nm

scales with $\sqrt{A/K_d}$



Asymmetries

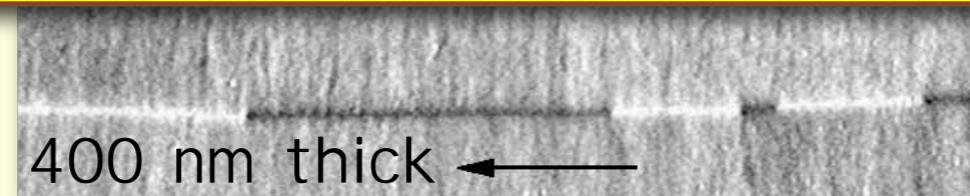
Bloch

film
 > 1

scale
thickness

Anisotropy-free film element:

Existence of real domain walls
does not change van den Berg theory

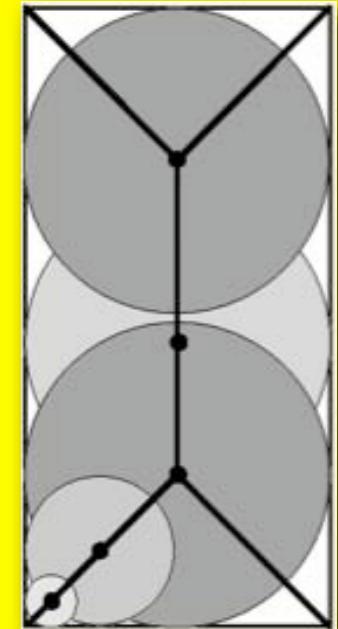


ferromagnetic
(NiFe)

Van den Berg Construction

Transition to three-dimensional bodies
(i.e. bulk materials):

Replace touching circles
by touching spheres



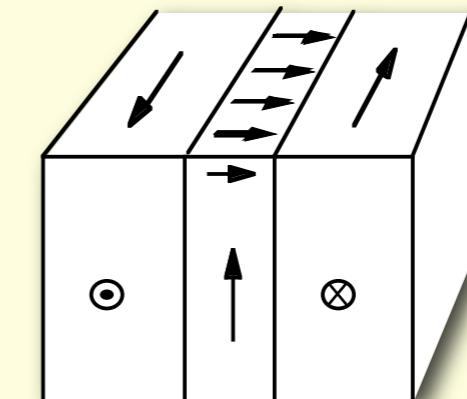
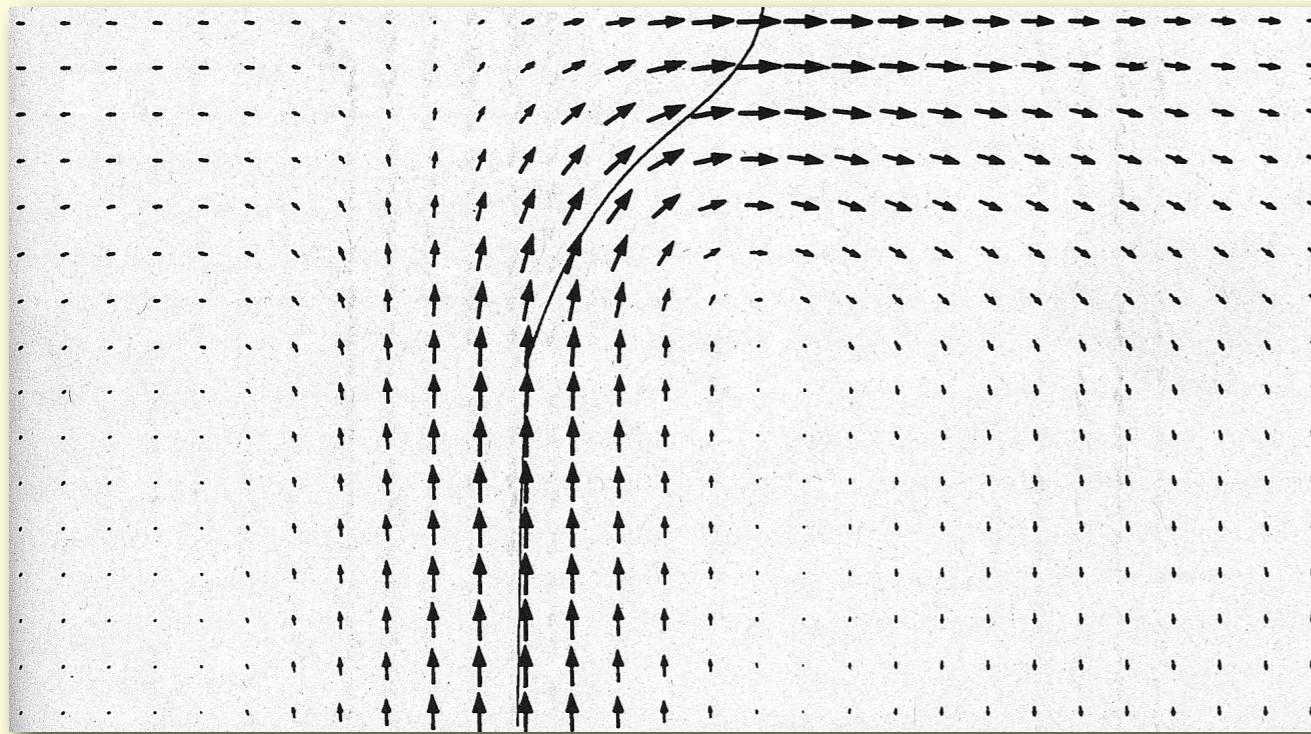
Centers of spheres define position of
domain walls



Expect regular domains with defined walls
also in anisotropy-free bulk materials

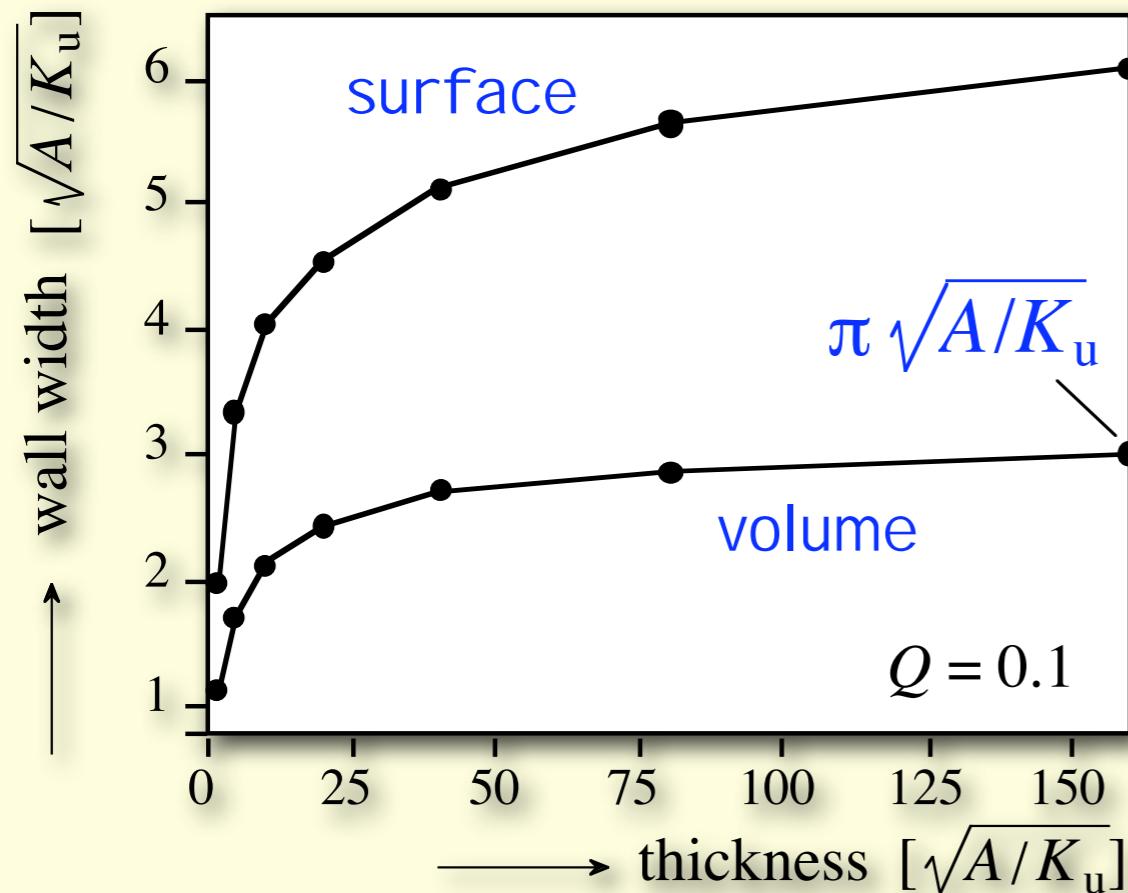
180° wall types in soft magnetic films

Thickness $> 5 \sqrt{A/K_u}$: vortex restricted to surface, Bloch-character in volume



Fe (100) wall,
thickness 200 nm

A. Aharoni, J. P. Jakubovics
Phys. Rev. B 43 (1991) 1290



Wall width at surface
increases steadily with thickness

Wall width in volume
approaches classical value

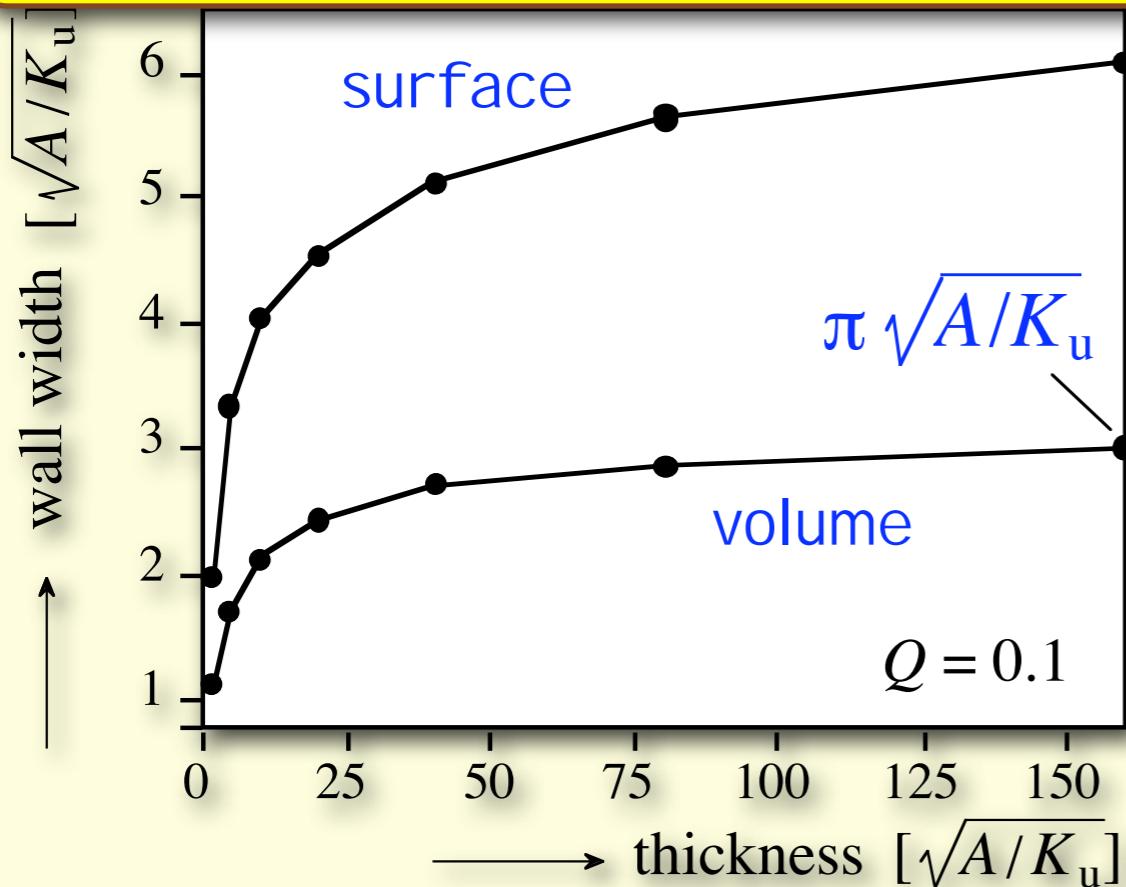
W. Rave and A. Hubert
JMMM 184 (1998) 179

180° wall types in soft magnetic films

Thickness $> 5 \sqrt{A/K_d}$: vortex restricted to surface, Bloch-character in volume

Bulk low-anisotropy materials:

Domain walls required (van den Berg),
Wall width scales with $\sqrt{A/K}$



Wall width at surface
increases steadily with thickness

Wall width in volume
approaches classical value

W. Rave and A. Hubert
JMMM 184 (1998) 179

180° wall types in soft magnetic films

Thickness > $5 \sqrt{A/K_d}$: vortex restricted to surface, Bloch-character in volume

Bulk low-anisotropy materials:

Domain walls required (van den Berg),
Wall width scales with $\sqrt{A/K}$



Bulk anisotropy-free materials:

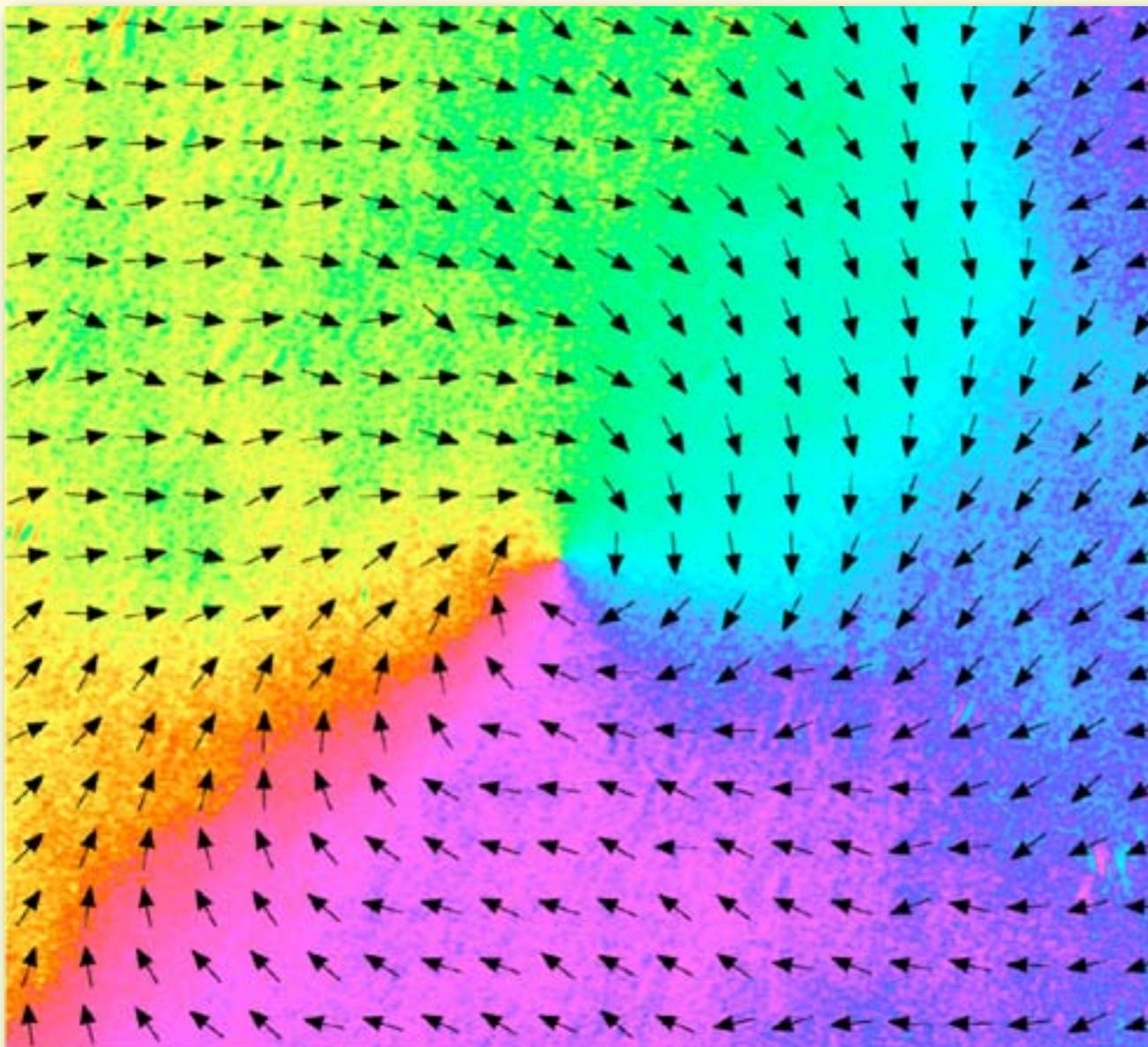
Domain walls are not defined
anymore

Consequence

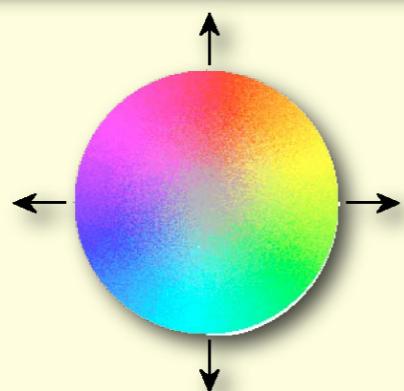
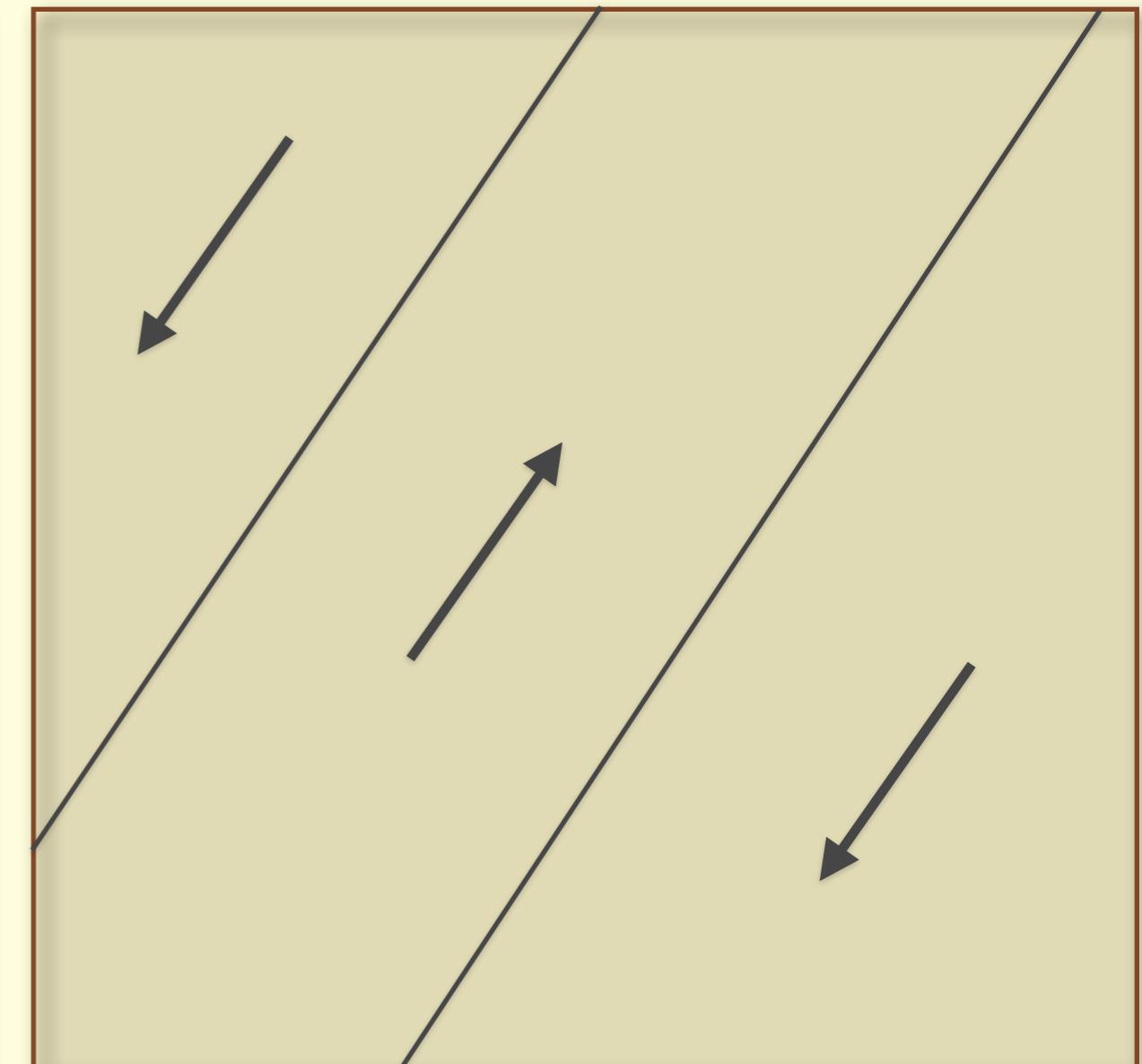
In bulk materials with vanishing anisotropy we do no expect regular, homogeneously magnetized domains with well defined walls, but continuous patterns

Magnetic microstructure of amorphous ribbons

$m(r)$ continuously flowing ?



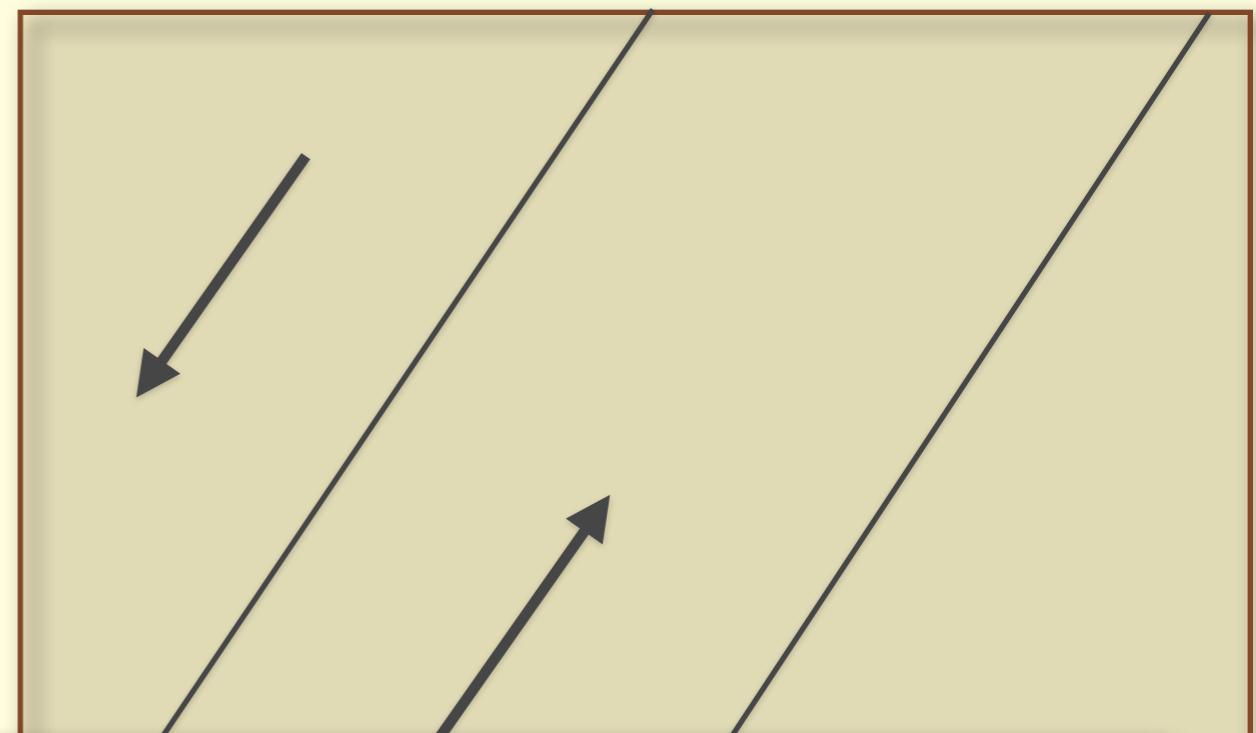
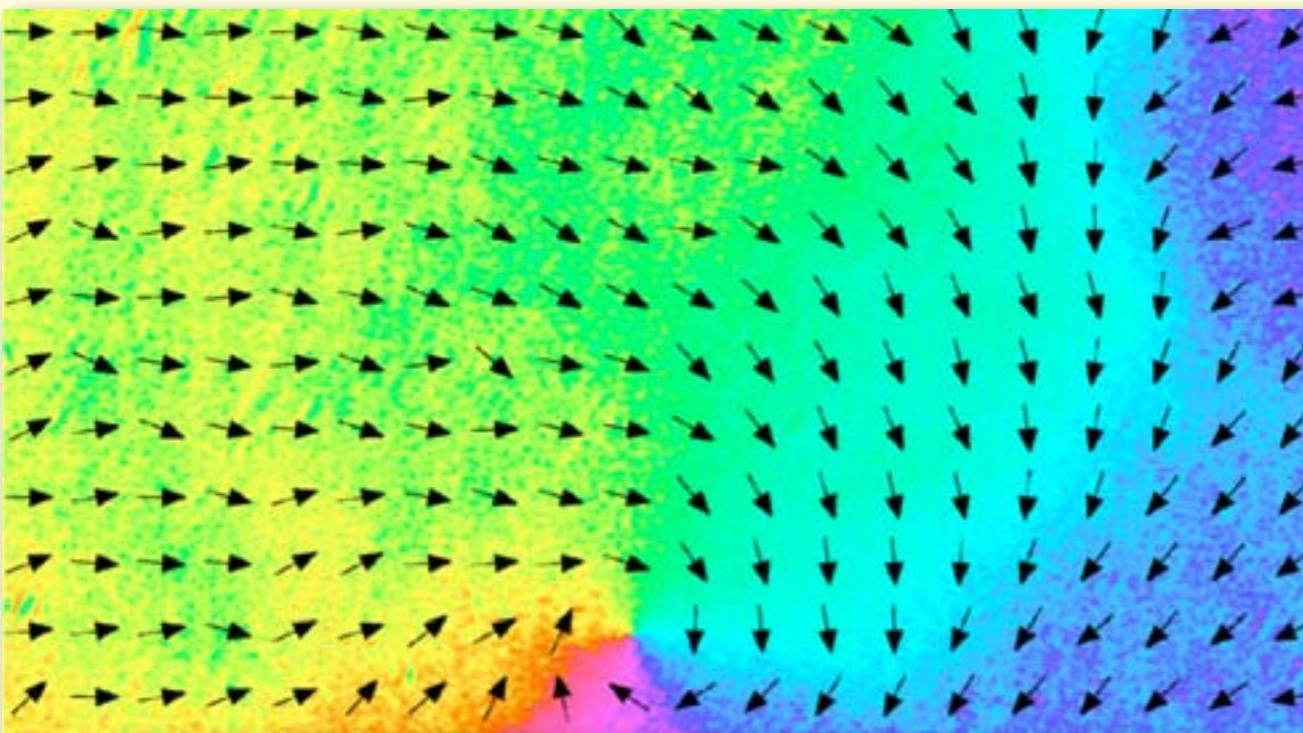
or regular domains ?



Magnetic microstructure of amorphous ribbons

$m(r)$ continuously flowing ?

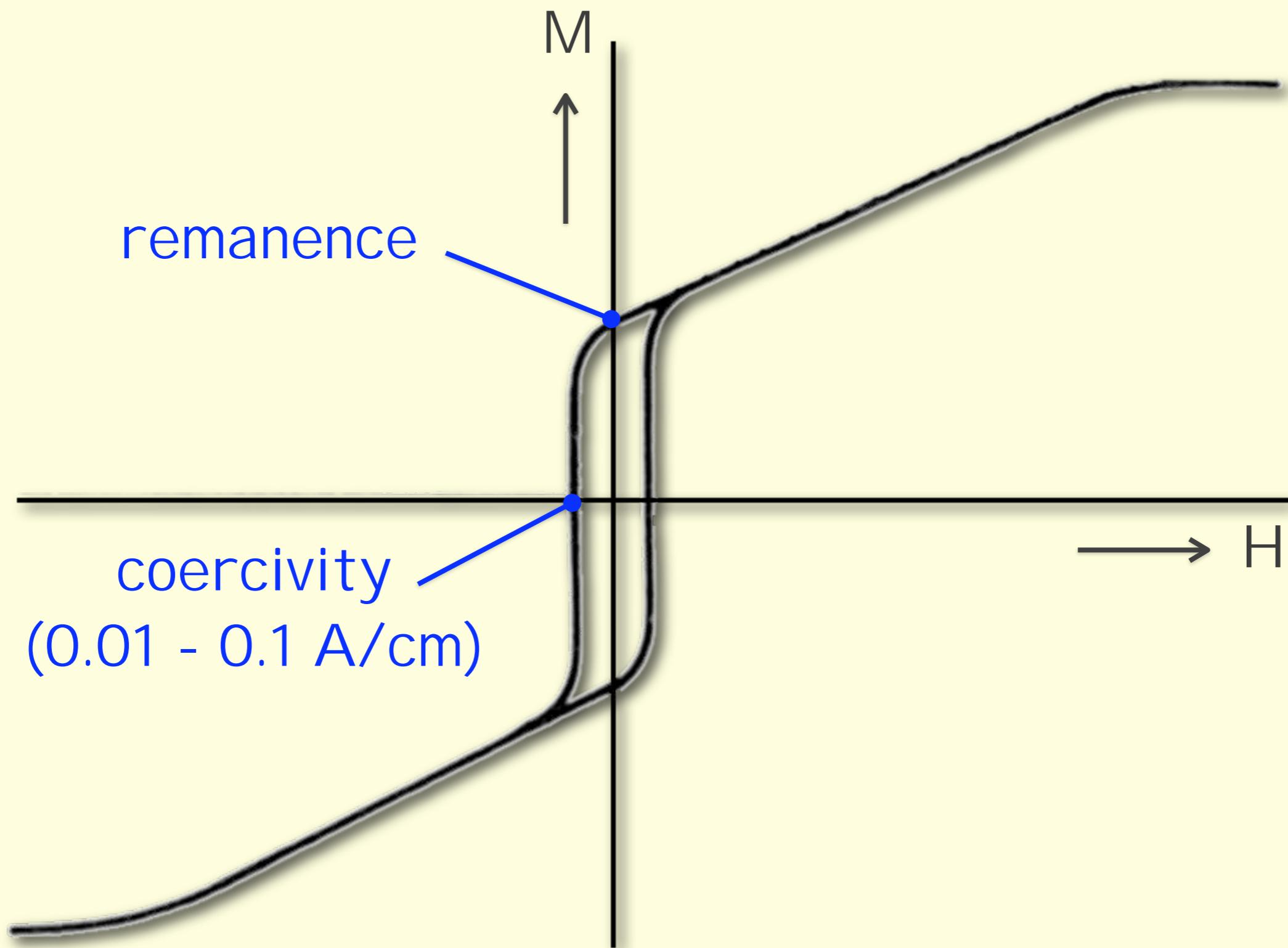
or regular domains ?



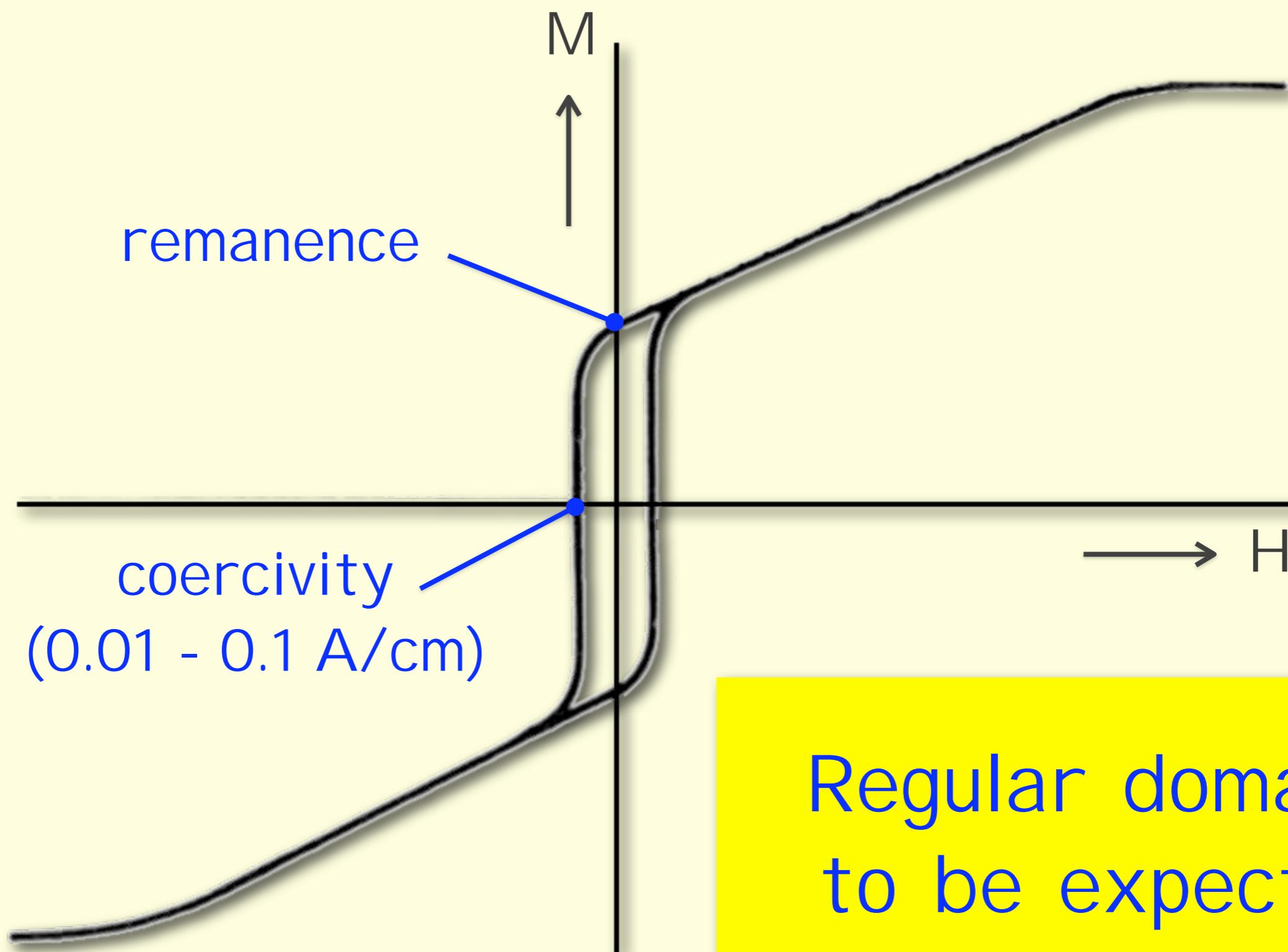
In amorphous material:

Continuously flowing magnetization
expected rather than regular domains

Amorphous ribbon (as-quenched): hysteresis loop



Amorphous ribbon (as-quenched): hysteresis loop

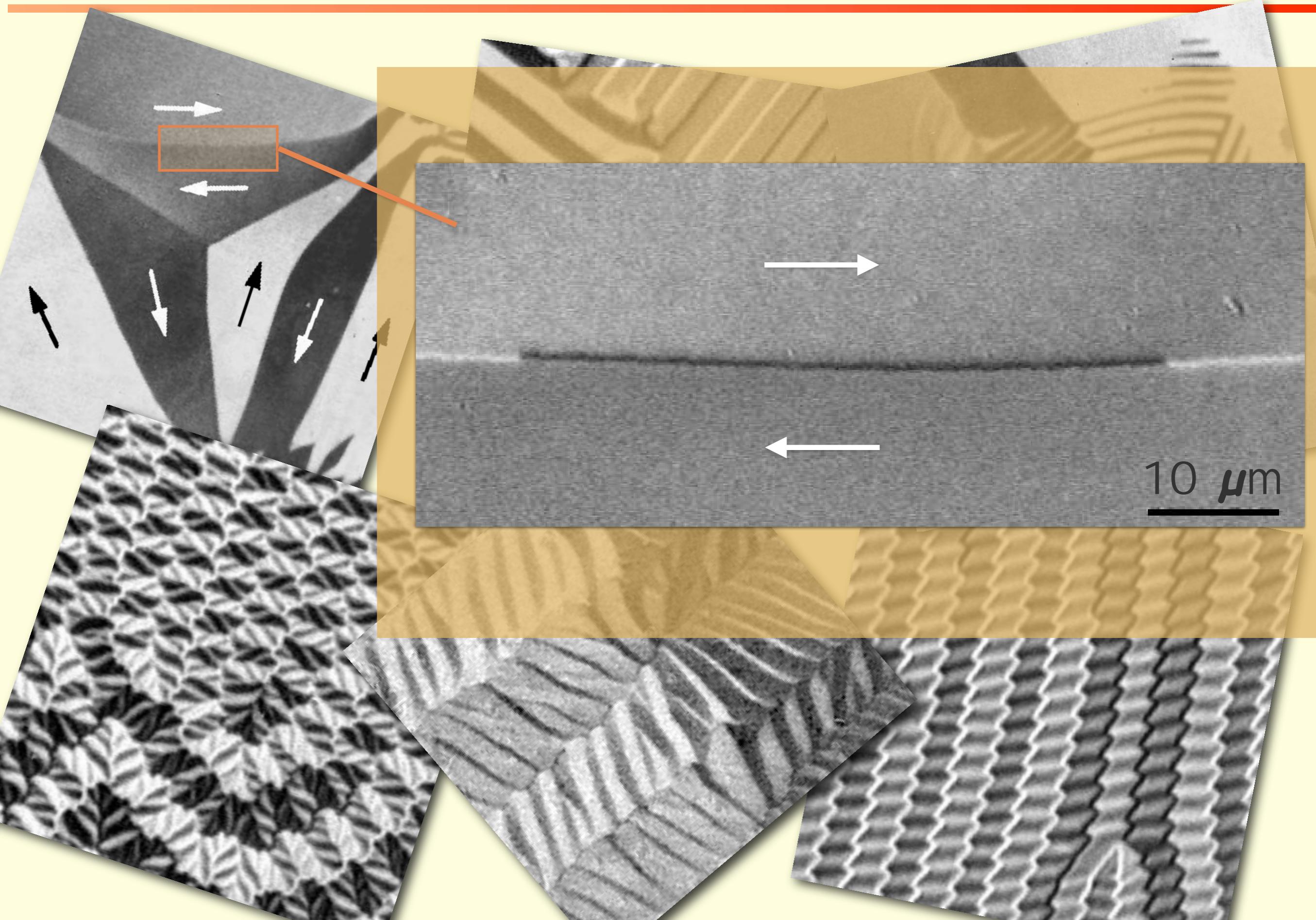


Regular domains
to be expected

“Regular domains” in amorphous ribbons

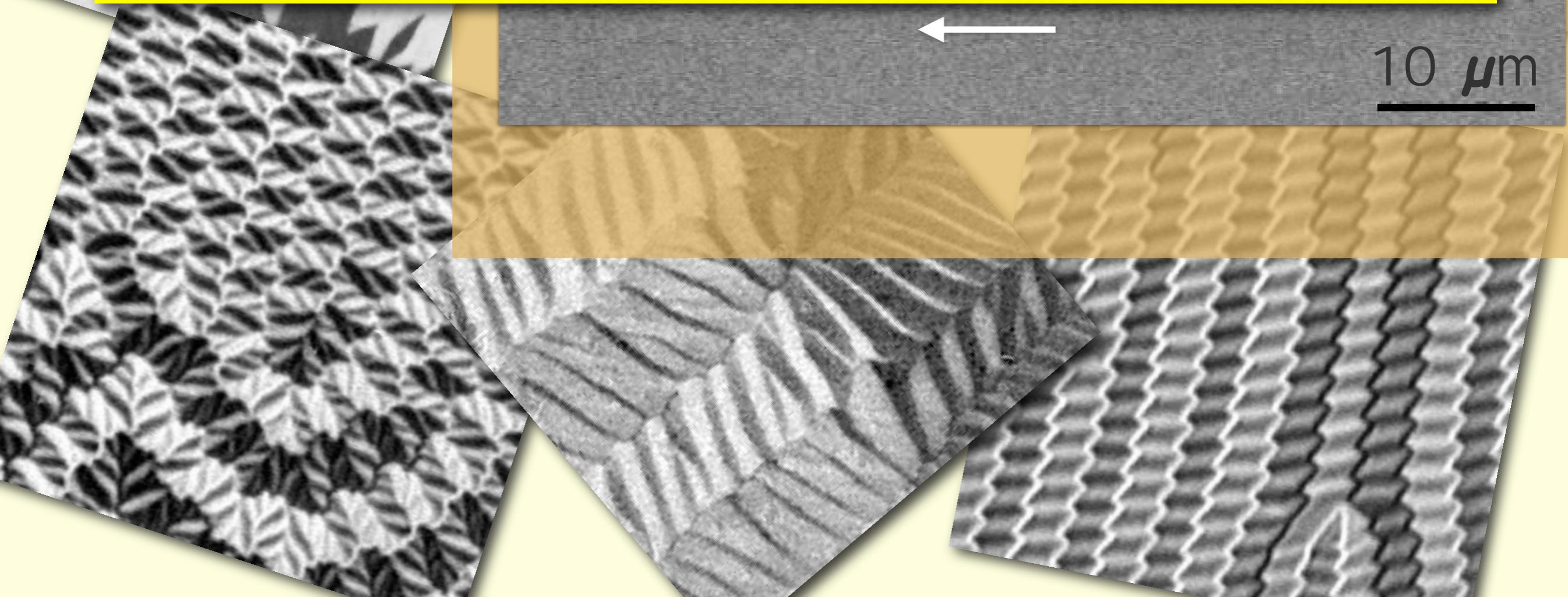


"Regular domains" in amorphous ribbons



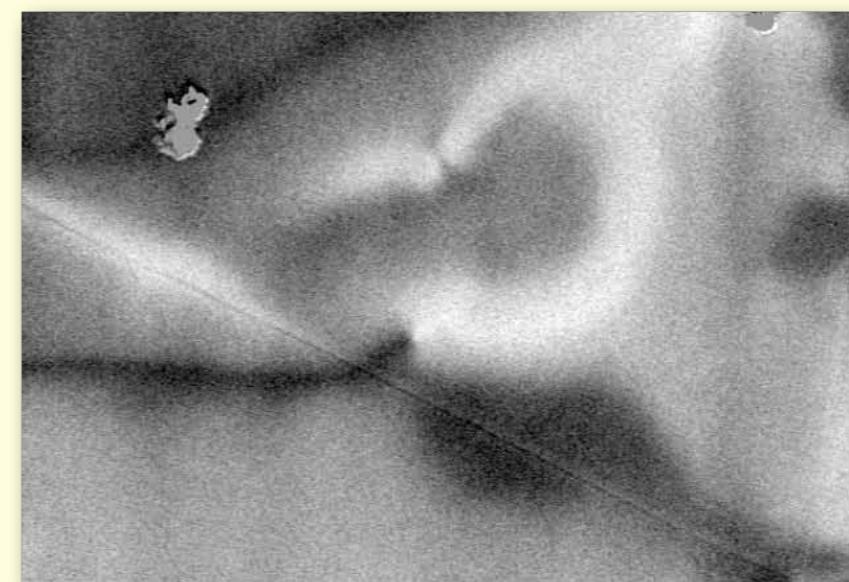
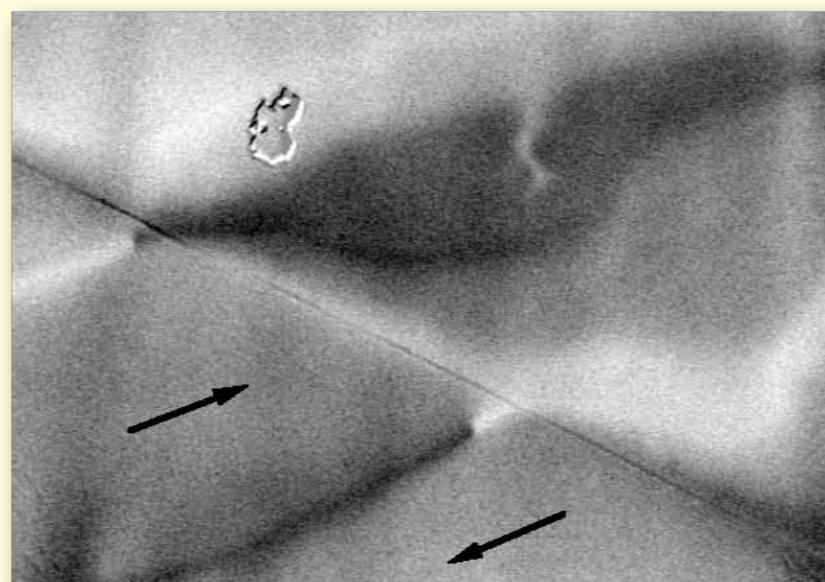
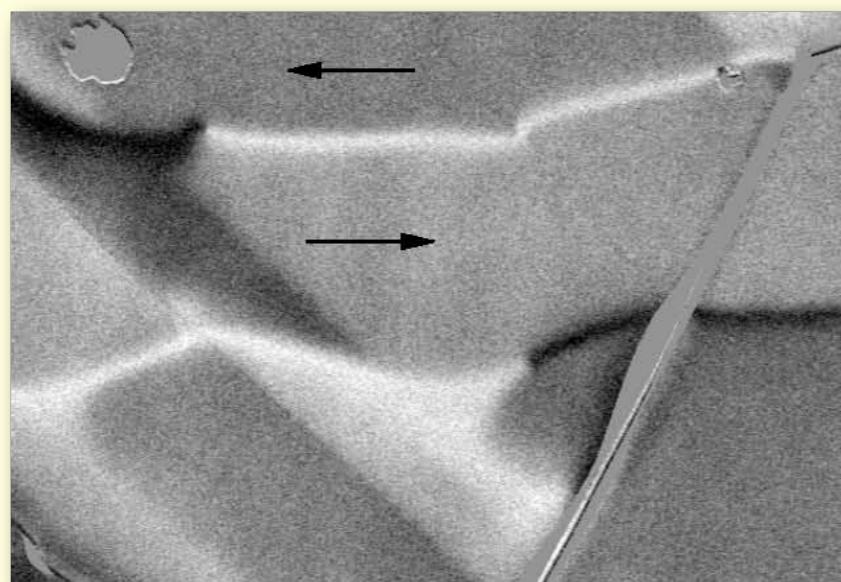
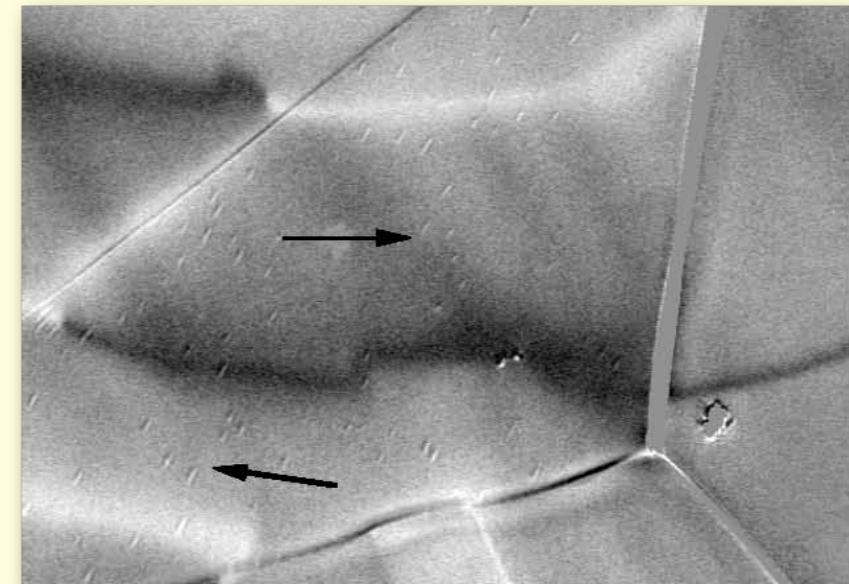
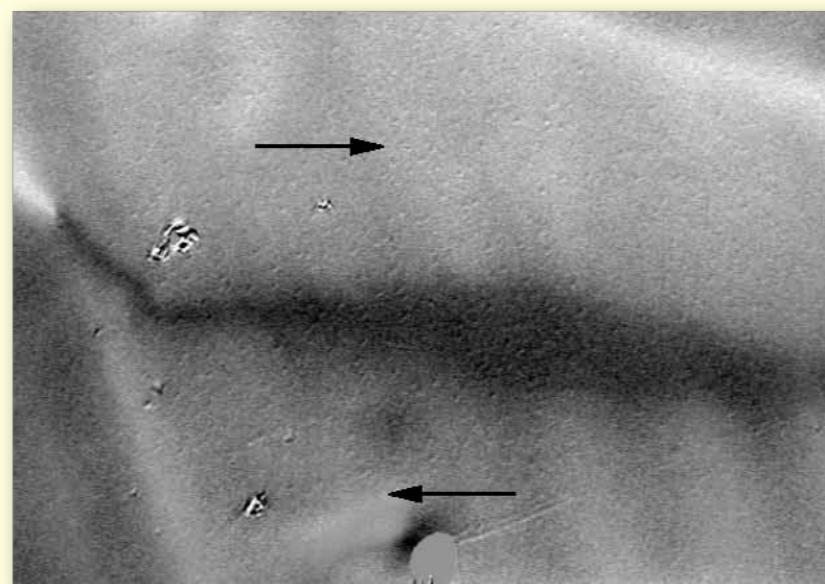
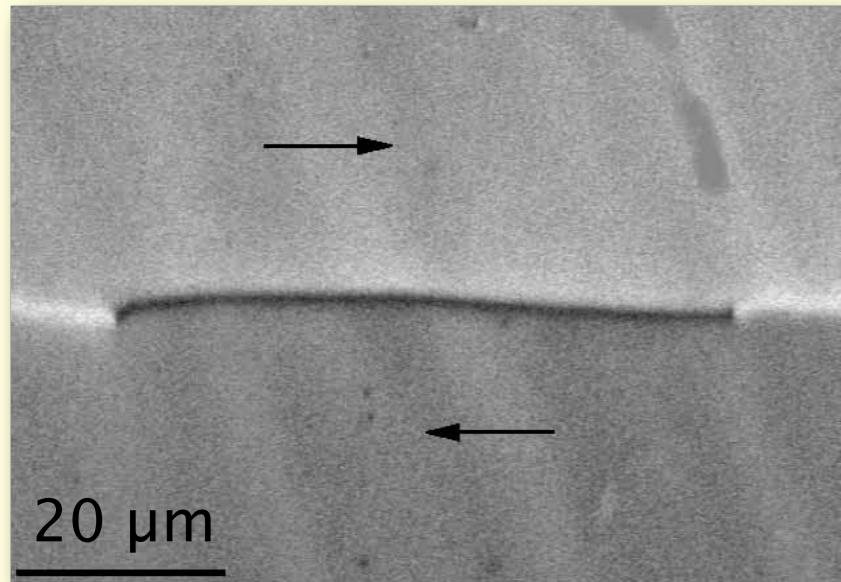
“Regular domains” in amorphous ribbons

Amorphous ribbons show
regular domains and walls
(rather than „flowing“ patterns)



Walls in high-permeable Permalloy cores

(sheets: 50 μm thick)



Also Permalloy shows (more or less)
regular domains walls

“Regular domains” in amorphous ribbons

Amorphous ribbons show
regular domains
(rather than „flowing“ patterns)

“Regular domains” in amorphous ribbons

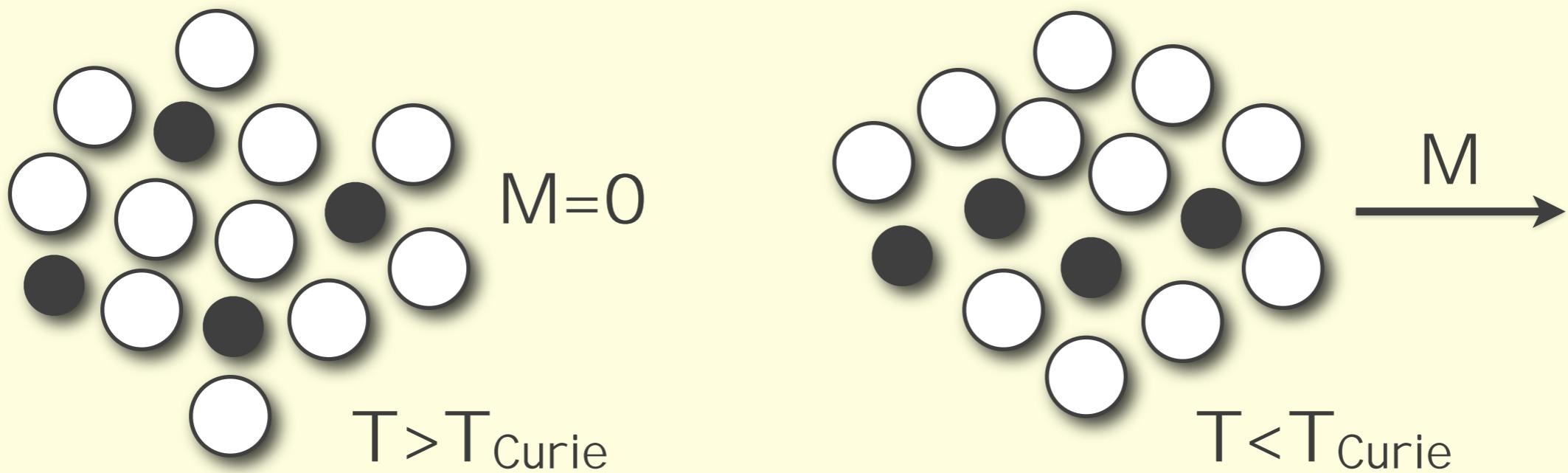
Amorphous ribbons show
regular domains
(rather than „flowing“ patterns)

Reason:

Residual anisotropies

Residual anisotropies in amorphous ribbons

- magnetization-induced minute deviations from random pair ordering



- stress-induced internal mechanical stress,
e.g. due to differences in quenching speed

Stress-induced anisotropy

magnetoelastic coupling energy

$$e_{me} = \frac{3}{2} \lambda_s \sigma \sin^2 \theta$$

magnetostriction
constant

mechanical
stress

angle between
M and stress σ

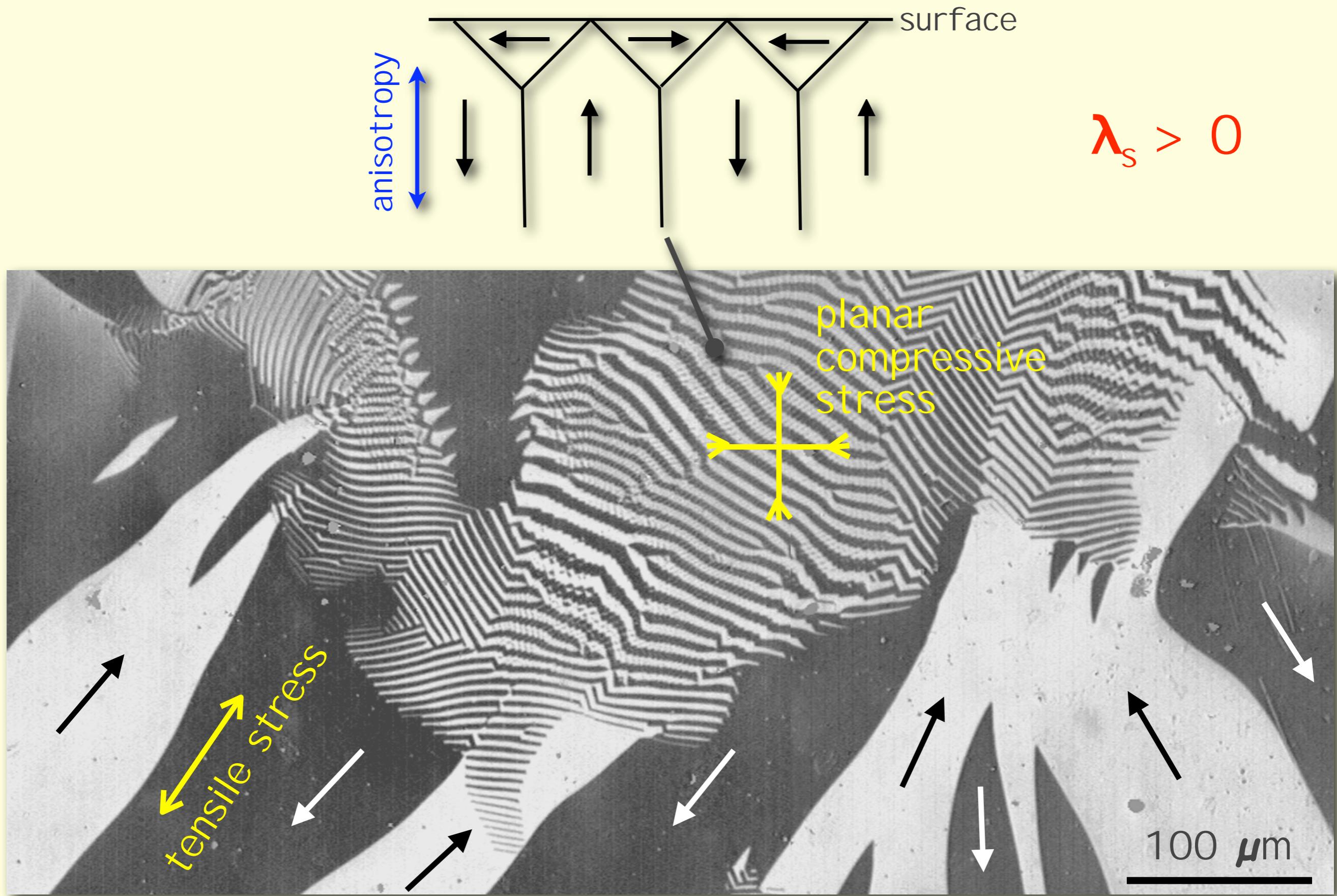
$$\lambda_s > 0, \sigma > 0 : \quad \leftarrow \quad \rightarrow \quad M \quad \sigma$$

$$\sigma < 0 : \quad \rightarrow \quad \uparrow \quad \downarrow \quad M \quad \leftarrow \sigma$$

$$\sigma < 0 : \quad \rightarrow \quad \downarrow \quad \uparrow \quad M \quad \leftarrow \sigma$$

(planar)

As-quenched Fe₇₈Si₁₃B₉ amorphous ribbon

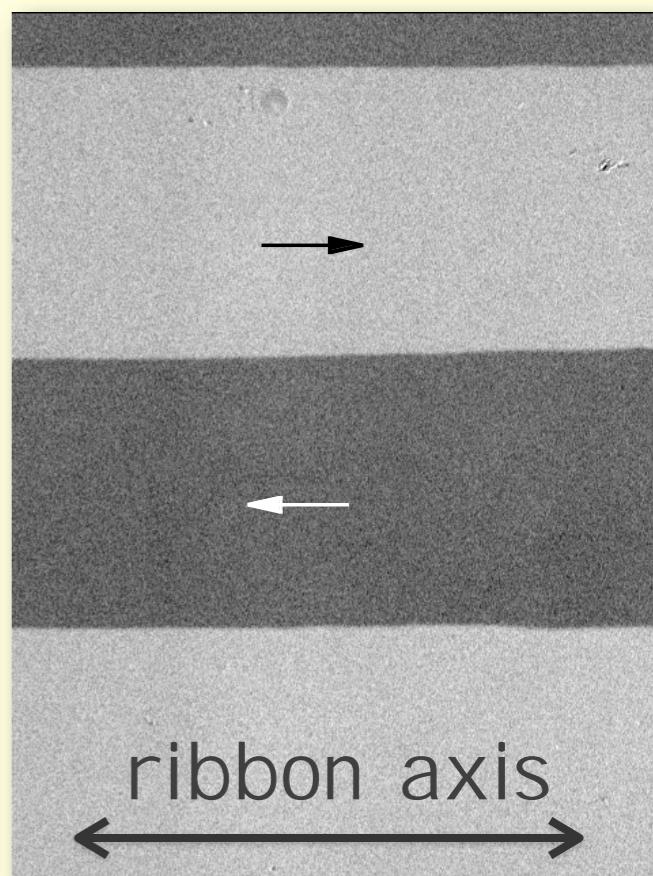
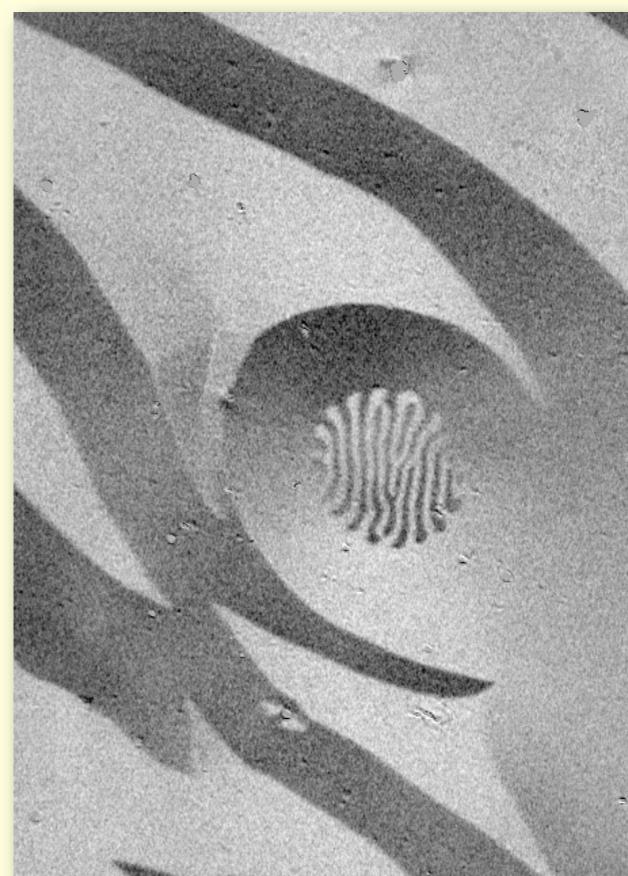
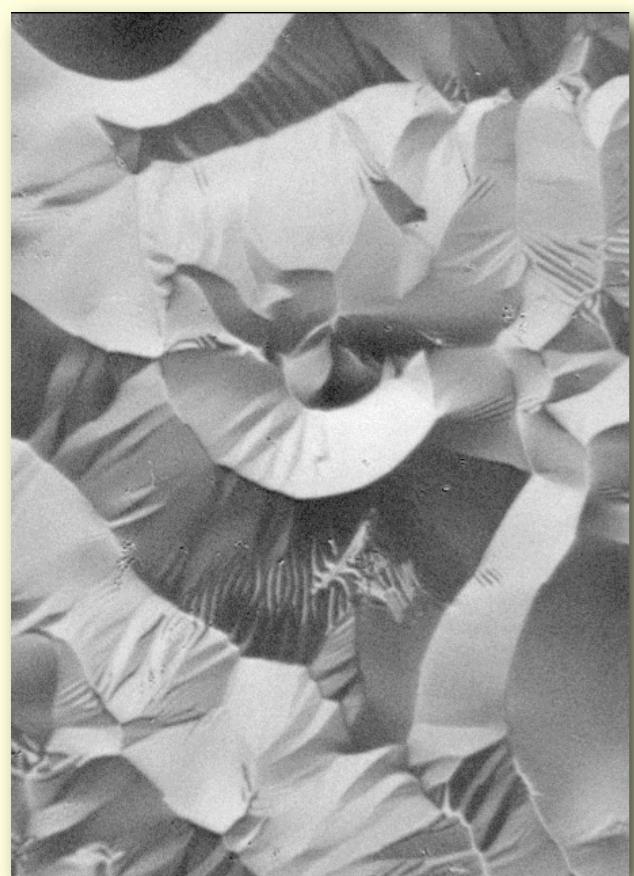


Amorphous ribbons: Magnetostriction & domains

$$e_{me} = \frac{3}{2} \lambda_s \sigma \sin^2 \theta$$

magnetostriction constant mechanical stress angle between M and stress σ

same location, independently demagnetized \rightarrow local anisotropy



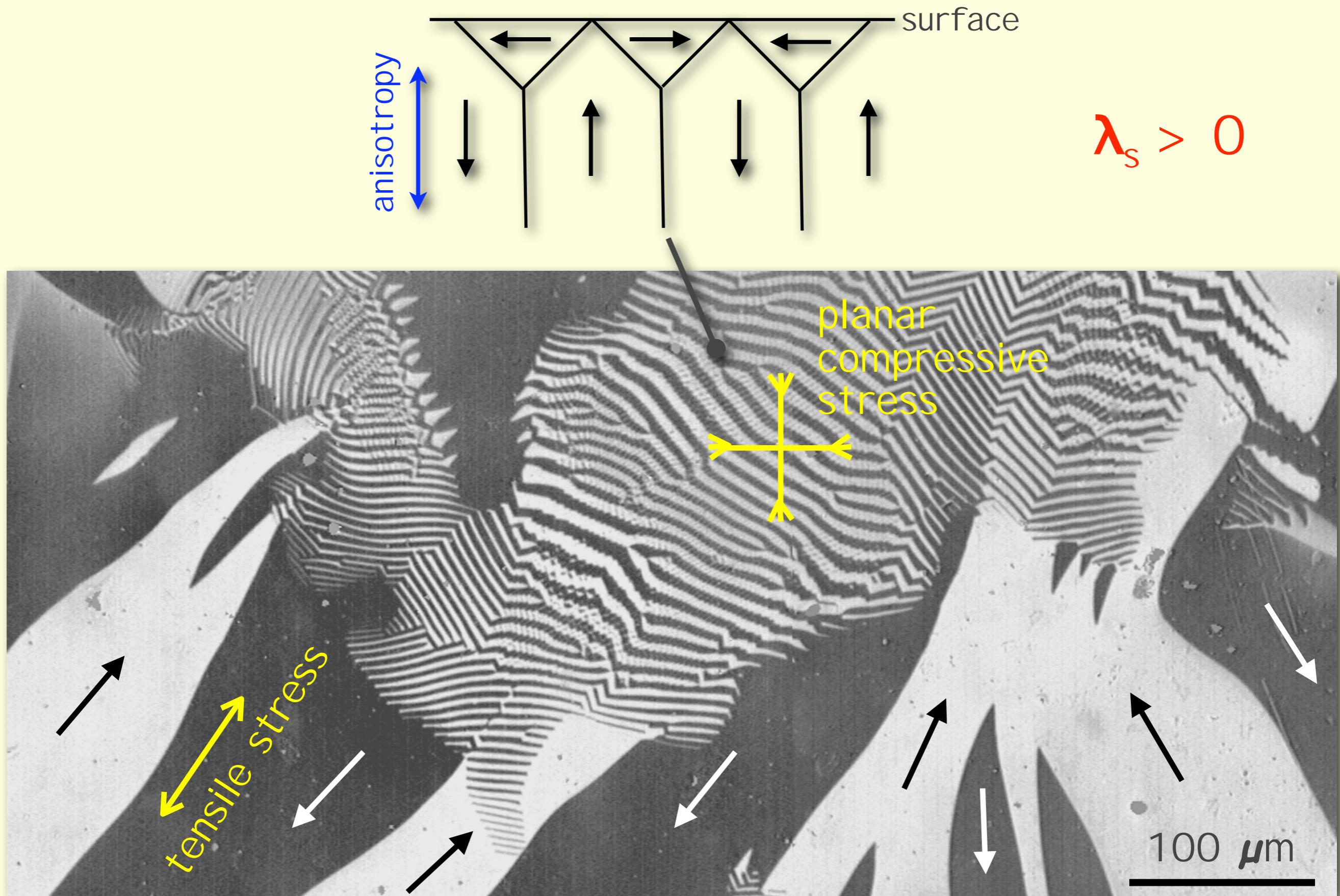
$\lambda_s = +35 \cdot 10^{-6}$
 $(\text{FeCo})_{83}(\text{Si, B})_{17}$

$\lambda_s = +24 \cdot 10^{-6}$
 $\text{Fe}_{76}(\text{Si, B})_{24}$

$\lambda_s = +8 \cdot 10^{-6}$
 $\text{Ni}_{39}\text{Fe}_{39}(\text{Si, B, C})_{22}$

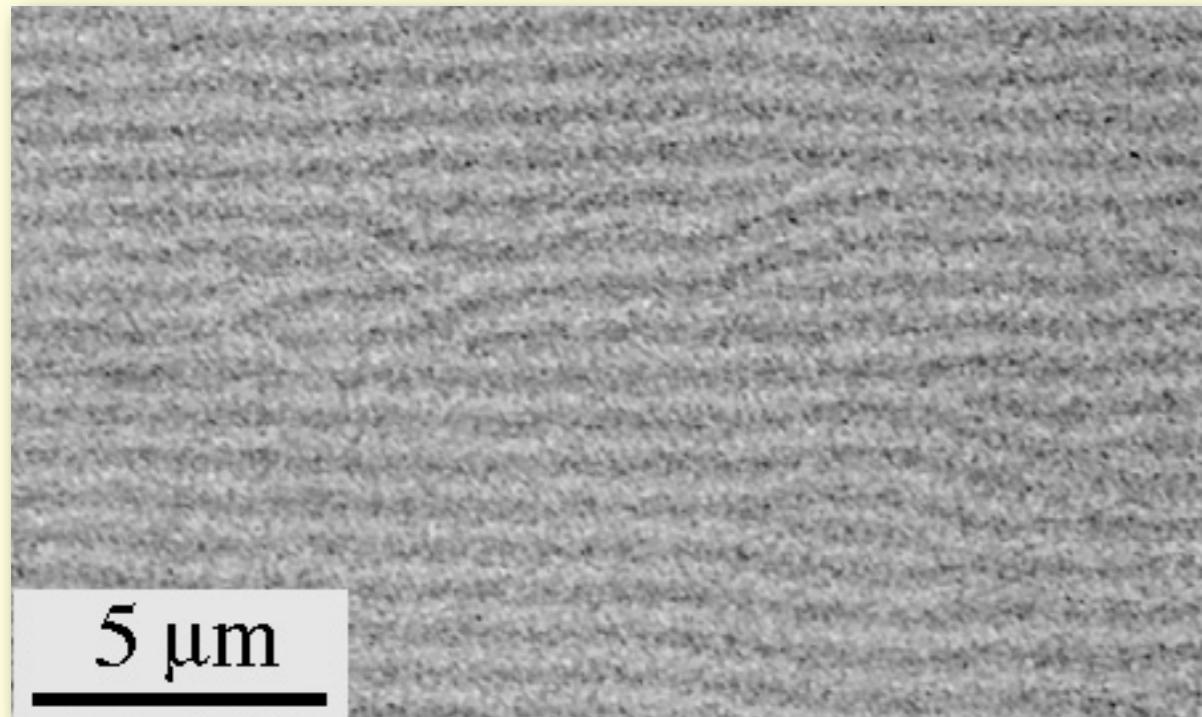
$\lambda_s < 0.2 \cdot 10^{-6}$
 $(\text{Co, Fe, Mn, Mo})_{77}(\text{Si, B})_{23}$

As-quenched Fe₇₈Si₁₃B₉ amorphous ribbon

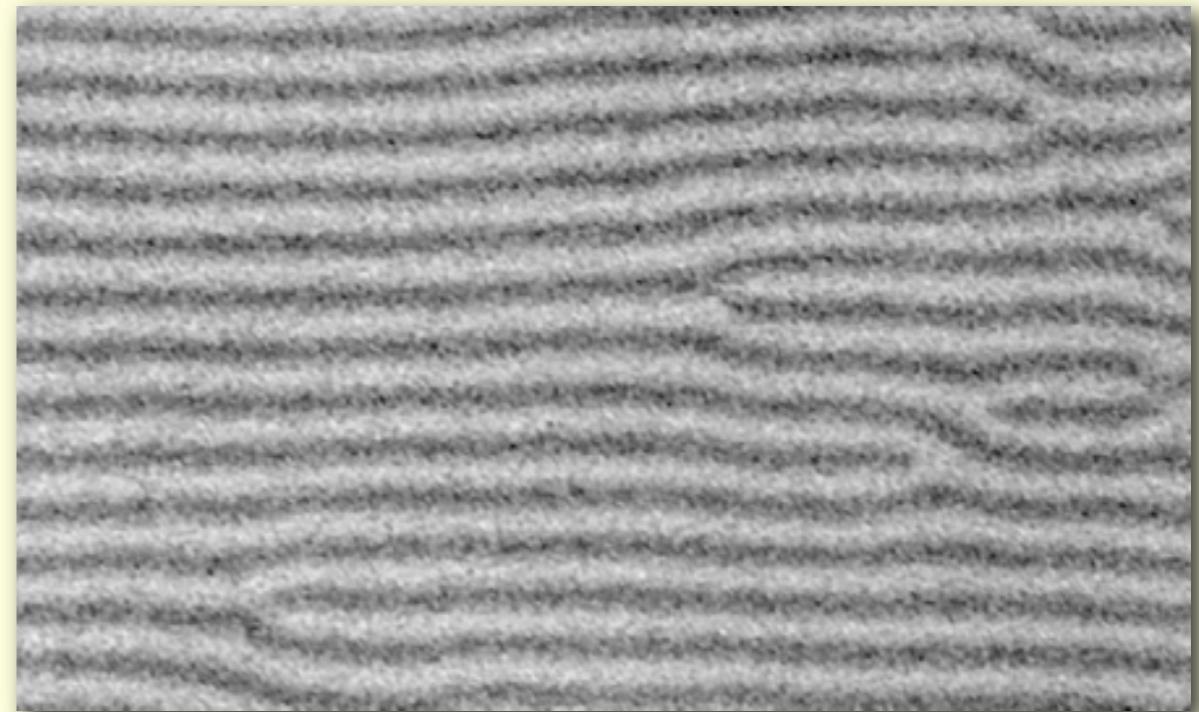


Compare: stripe domains in magnetic films

FeSiBCuNb amorphous film (2 μm thick)



$\leftarrow \text{H}$



$\text{H} = 0$

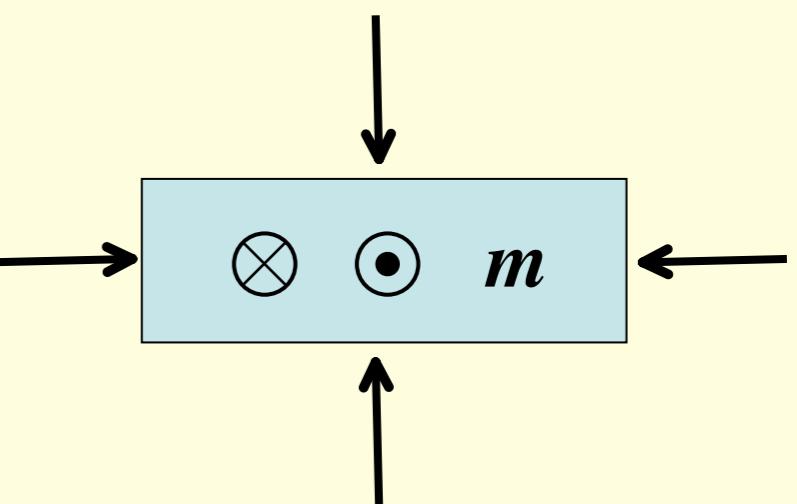
reason: planar compressive stress σ_p

$$e_{me} = \frac{3}{2} \lambda_s \sigma_p \sin^2 \theta$$

$\lambda_s > 0, \sigma_p < 0 :$

θ : angle between \mathbf{m} and σ_p

→ perpendicular anisotropy

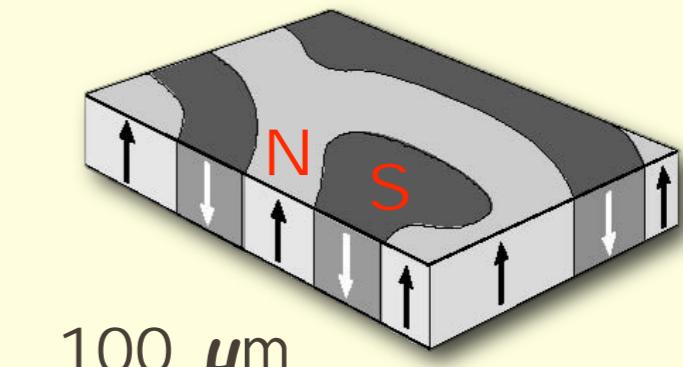
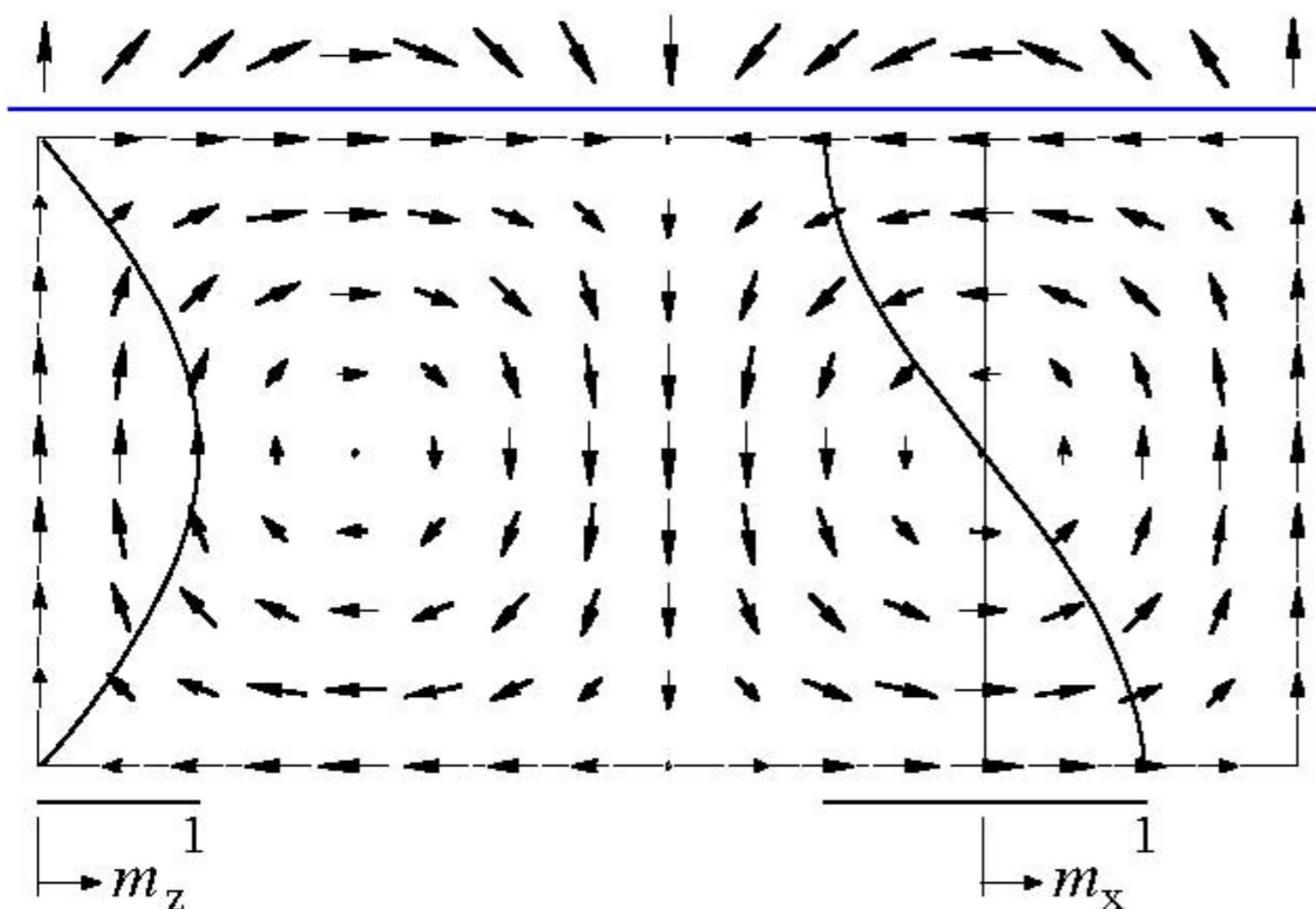


Compare: stripe domains in magnetic films

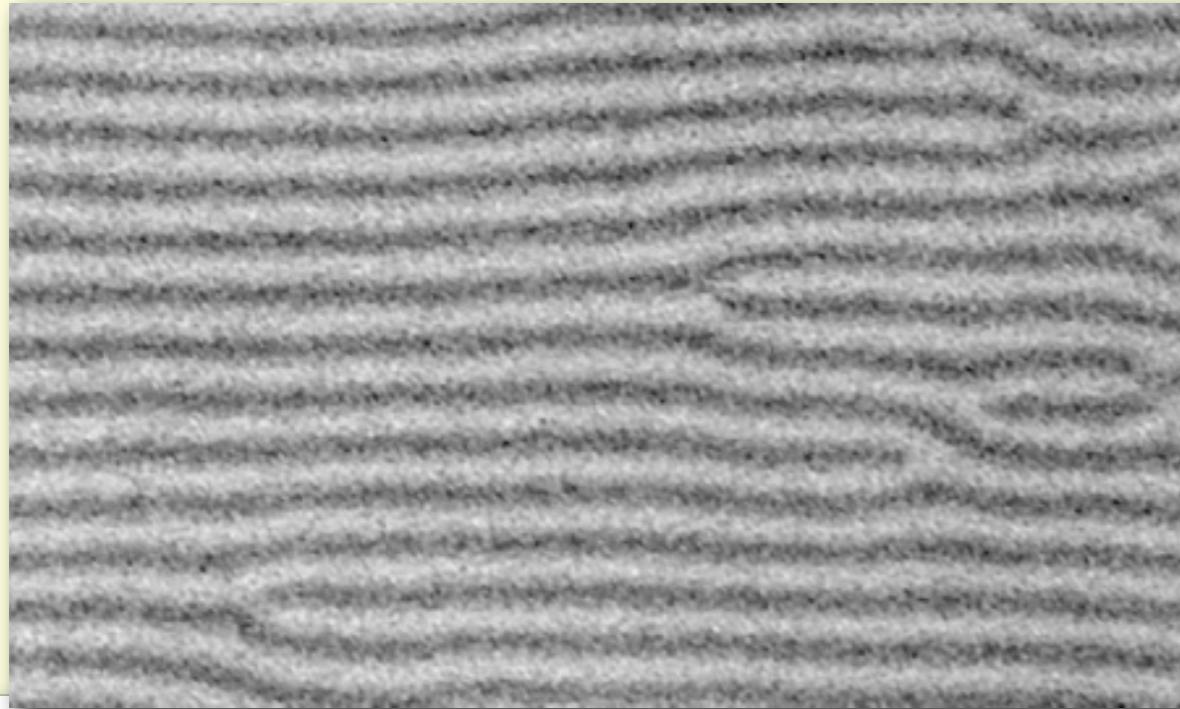
↔ anisotropy

low anisotropy
(i.e. $Q \ll 1$) film
→ dense stripe domains

for comparison:
high anisotropy film
(garnet, $Q > 1$)

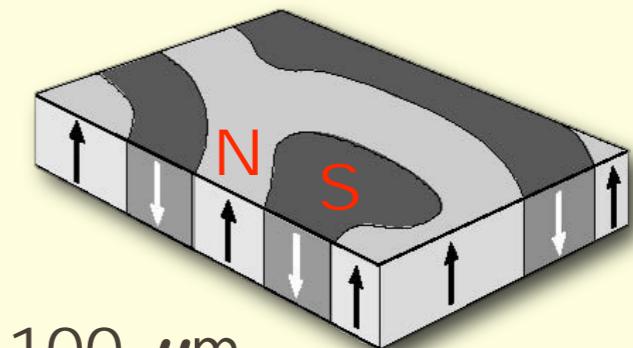
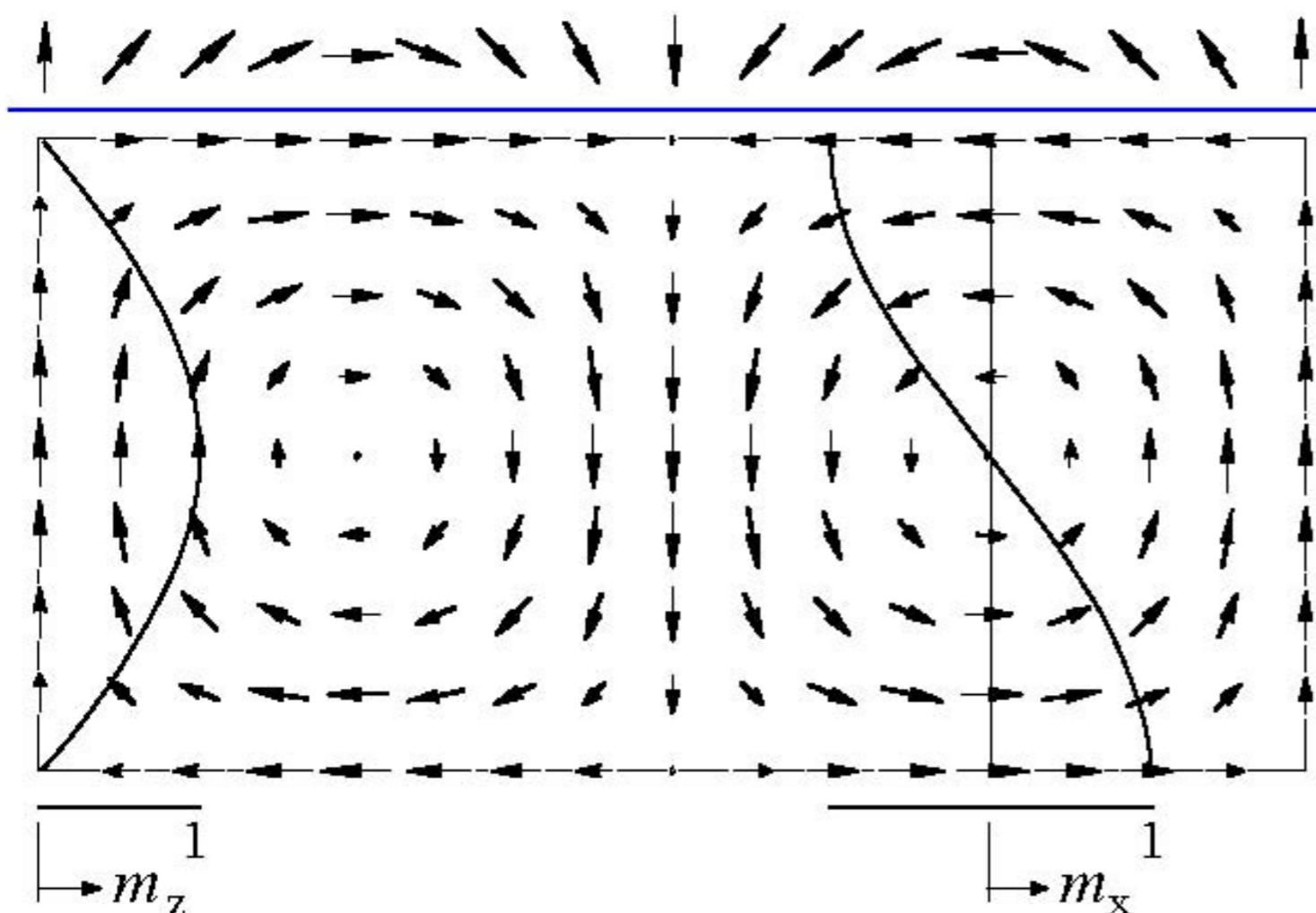


Compare: stripe domains in magnetic films



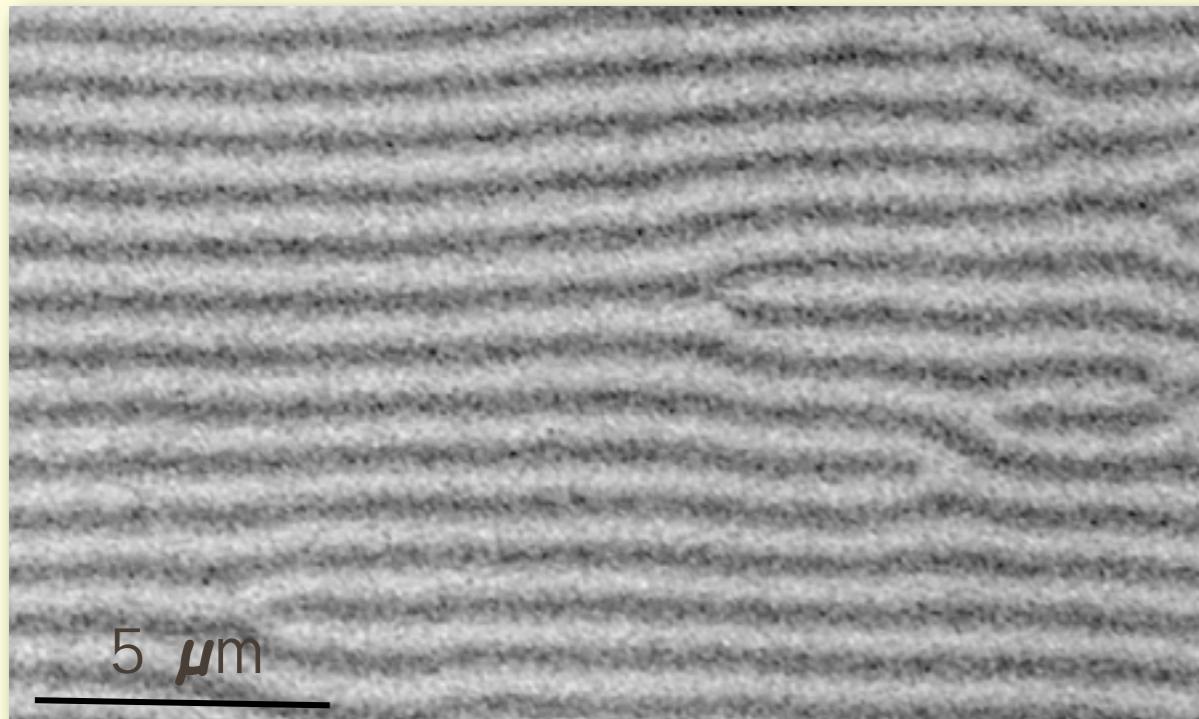
copy

for comparison:
high anisotropy film
(garnet, $Q>1$)

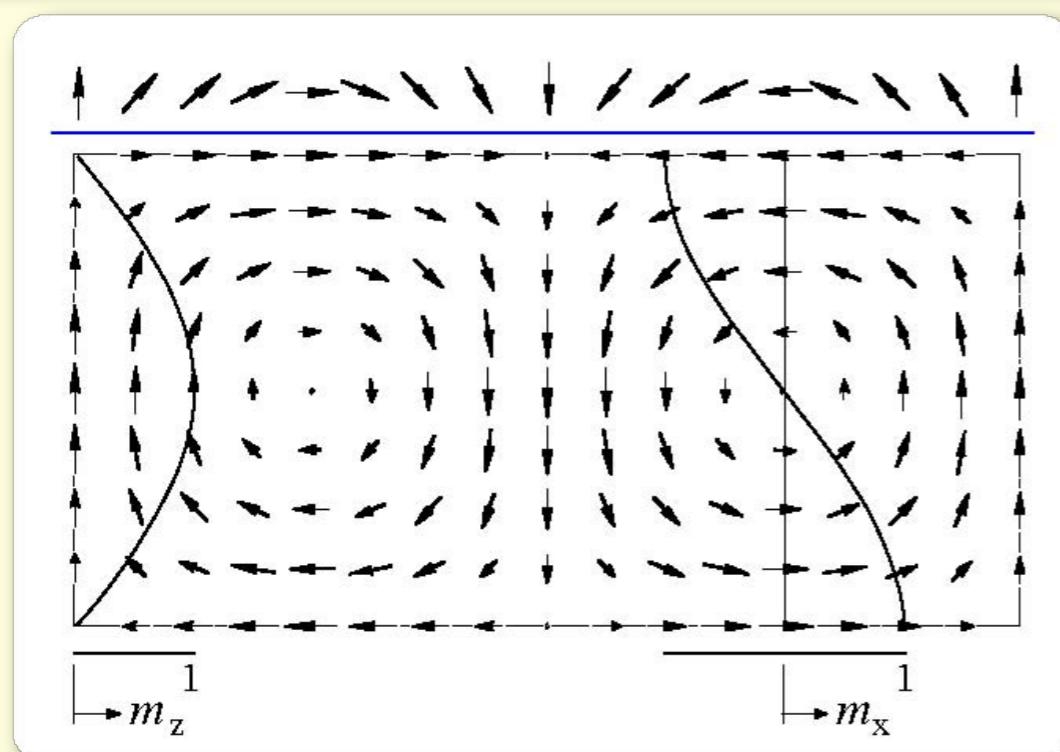
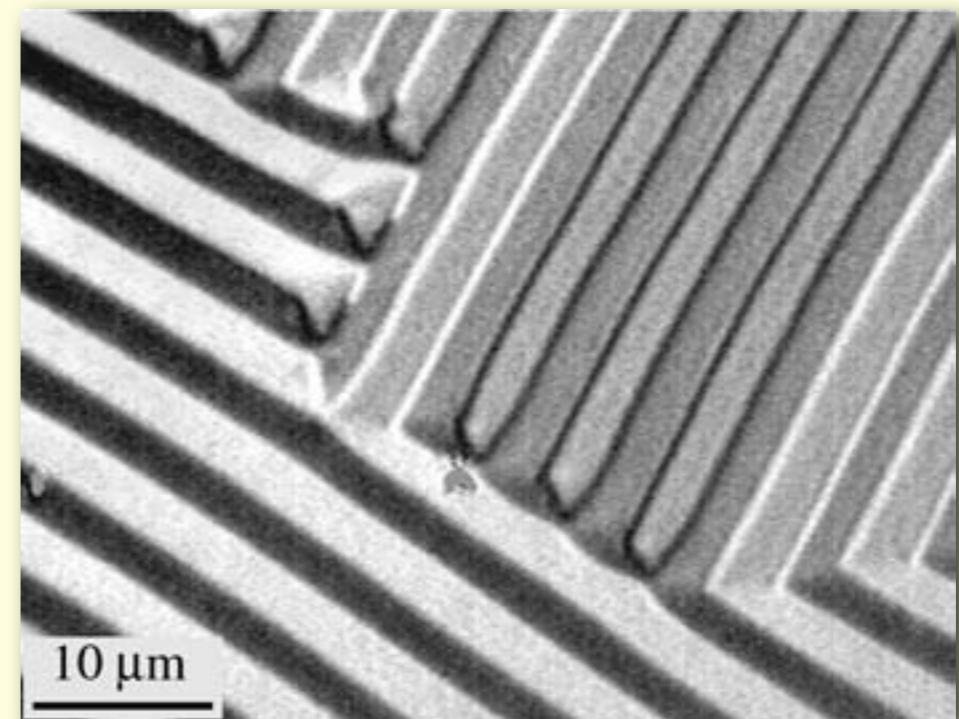


Compare: stripe domains in magnetic films

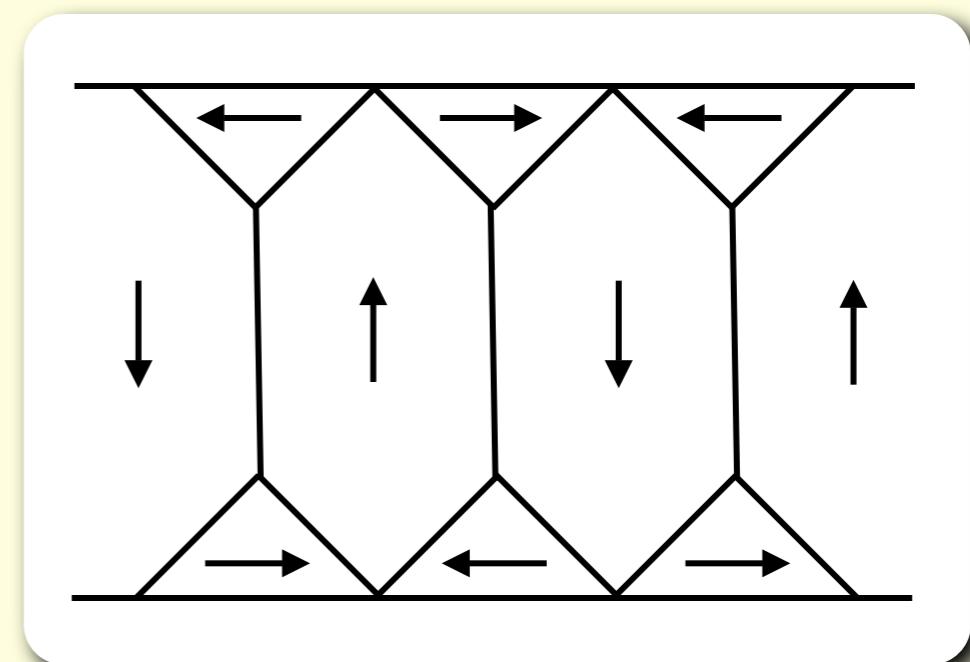
amorphous thin film
(2 μm thick)



amorphous ribbon
(20 μm thick)

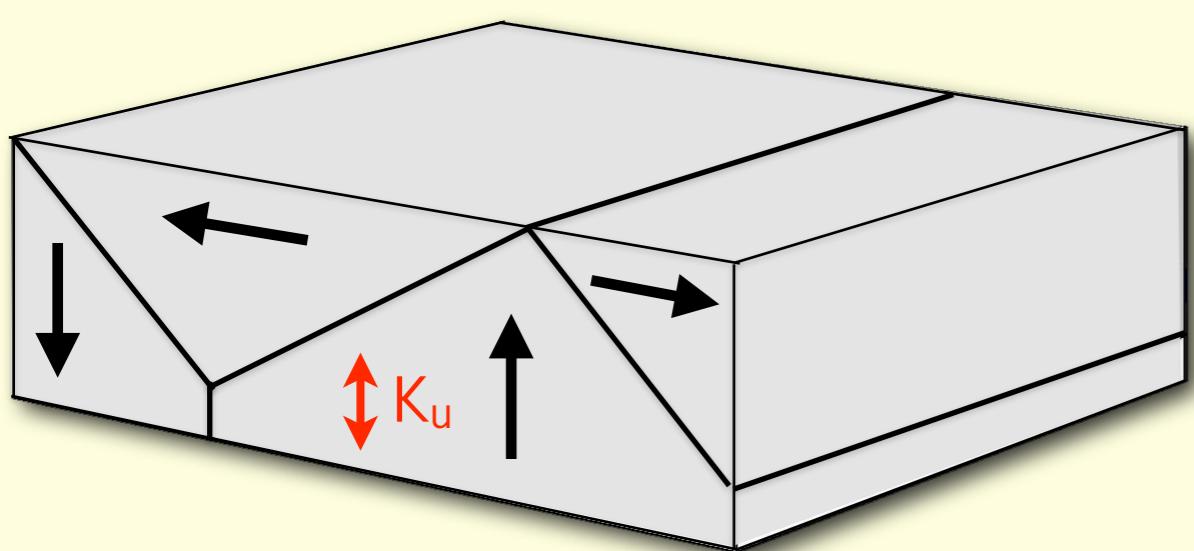
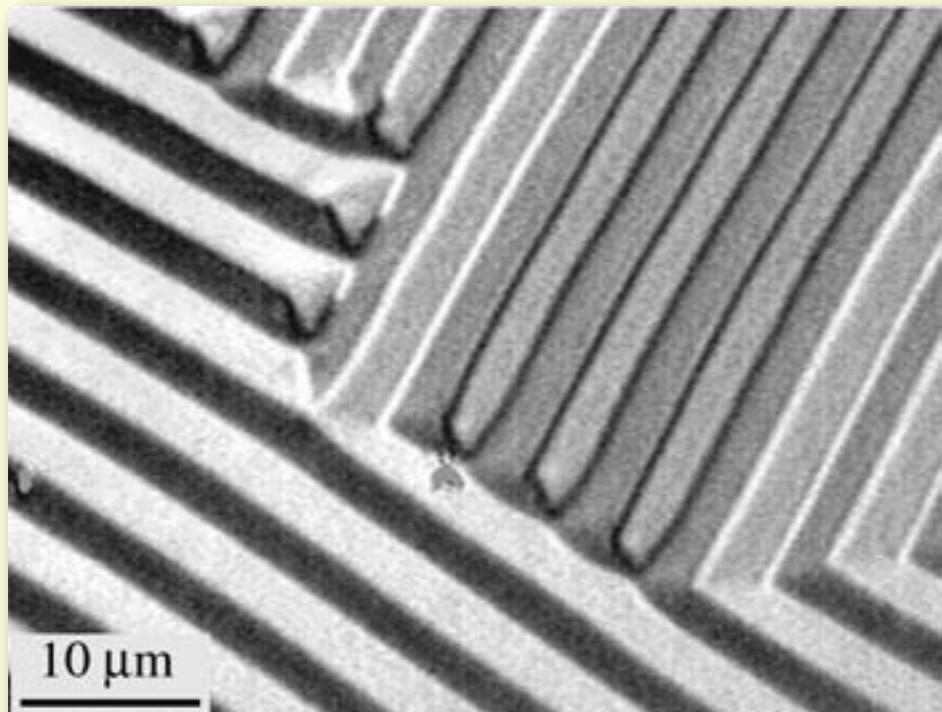


↔
anisotropy



Branched domains in amorphous ribbons

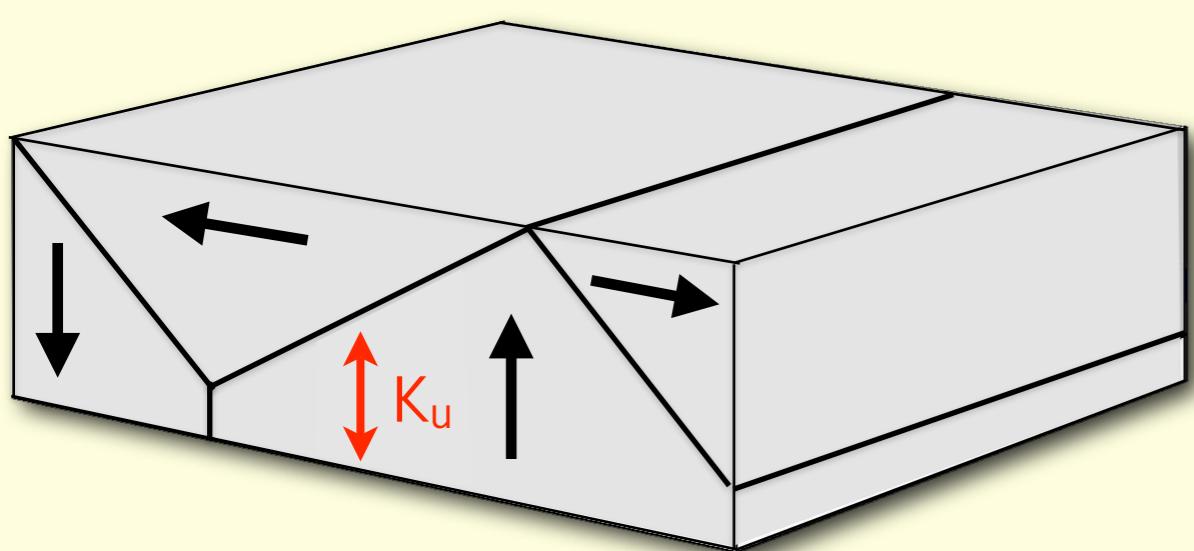
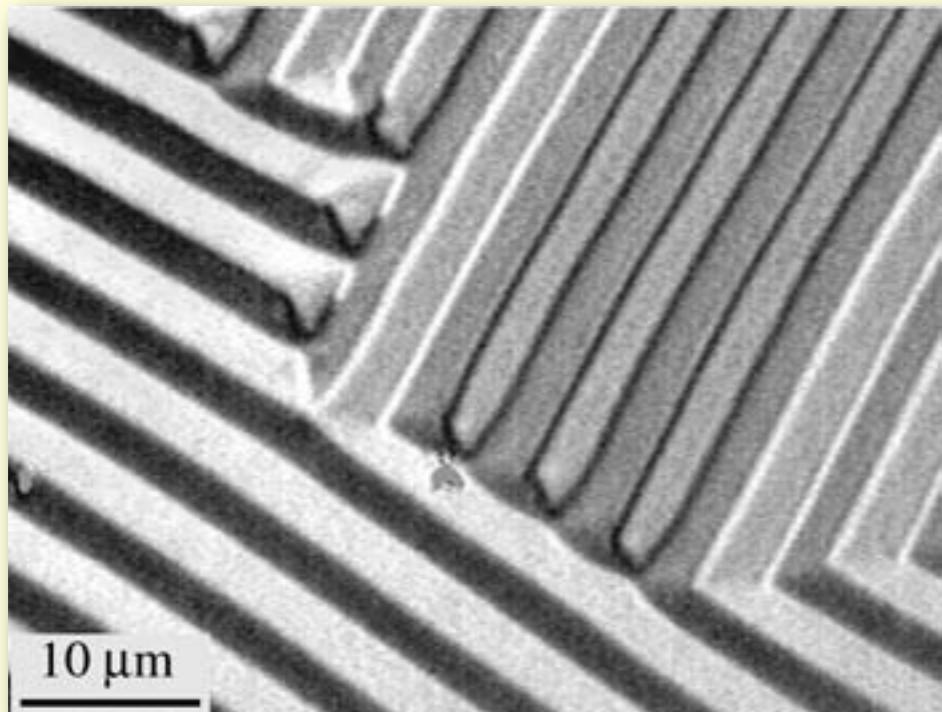
amorphous ribbon (20 μm thick)
increasing perpendicular anisotropy (stress)



(FeSiB)

Branched domains in amorphous ribbons

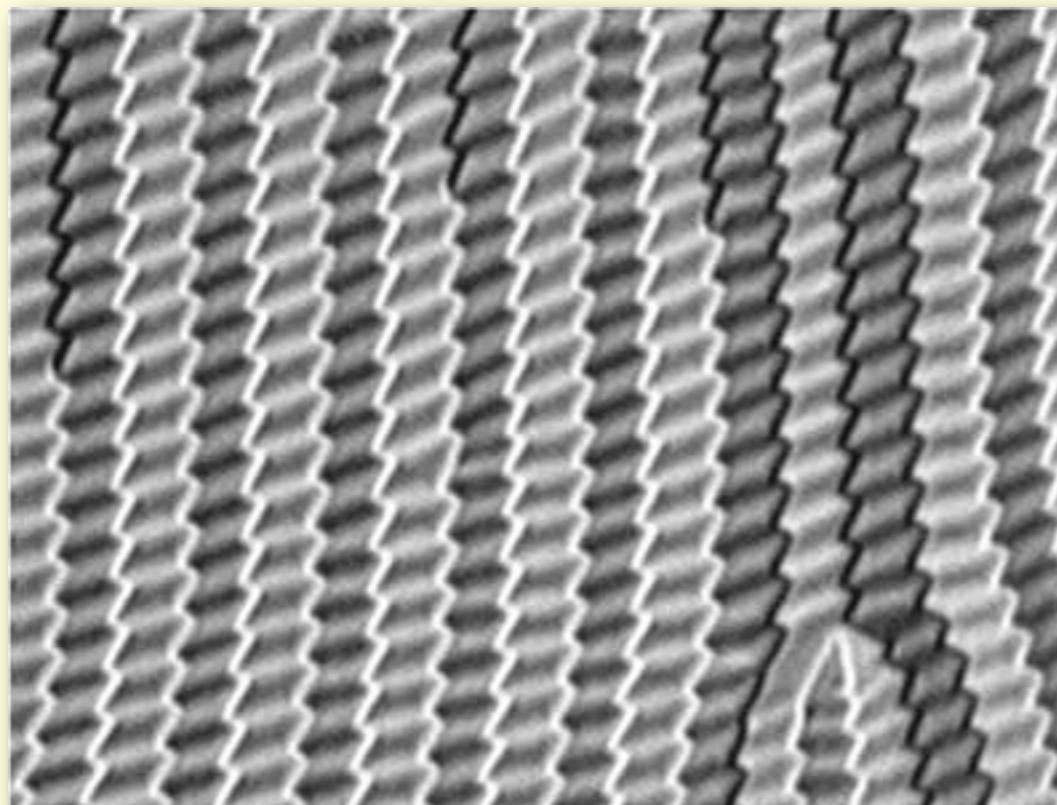
amorphous ribbon (20 μm thick)
increasing perpendicular anisotropy (stress)



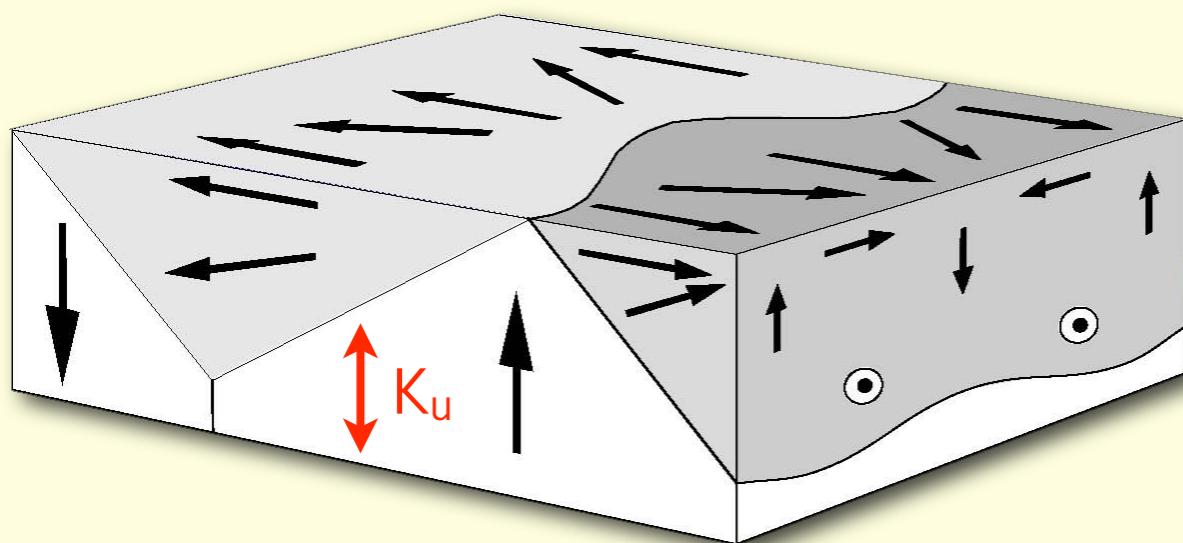
(FeSiB)

Branched domains in amorphous ribbons

amorphous ribbon (20 μm thick)
increasing perpendicular anisotropy (stress)



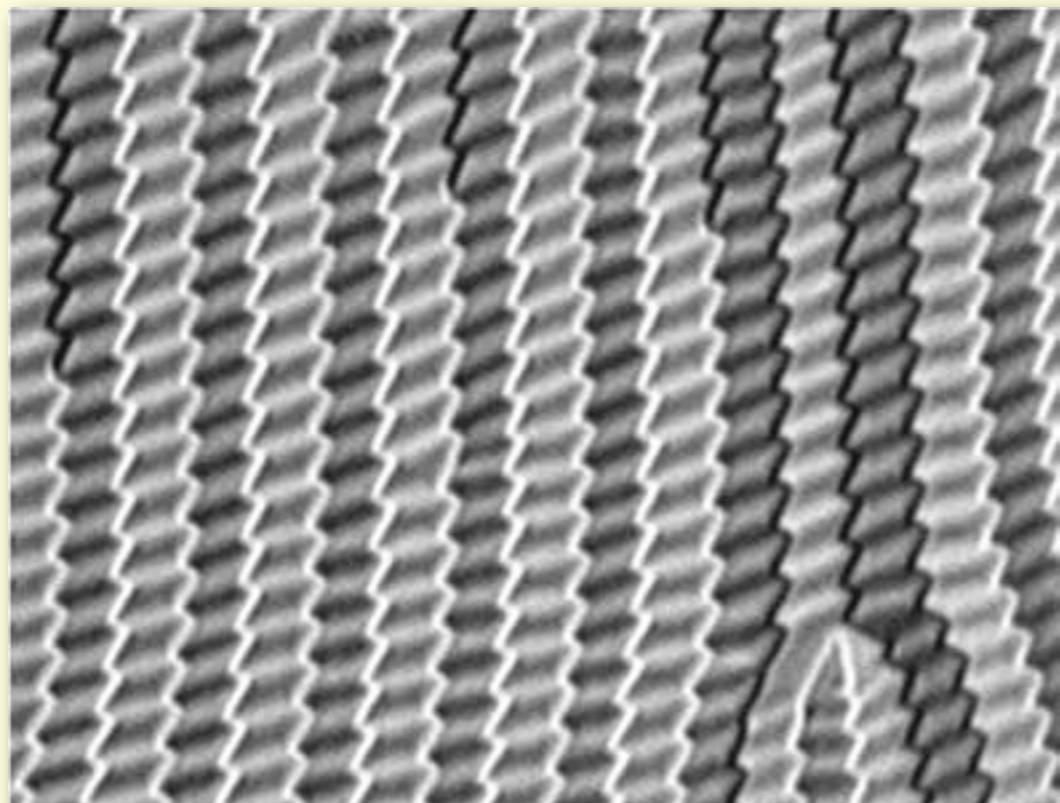
10 μm



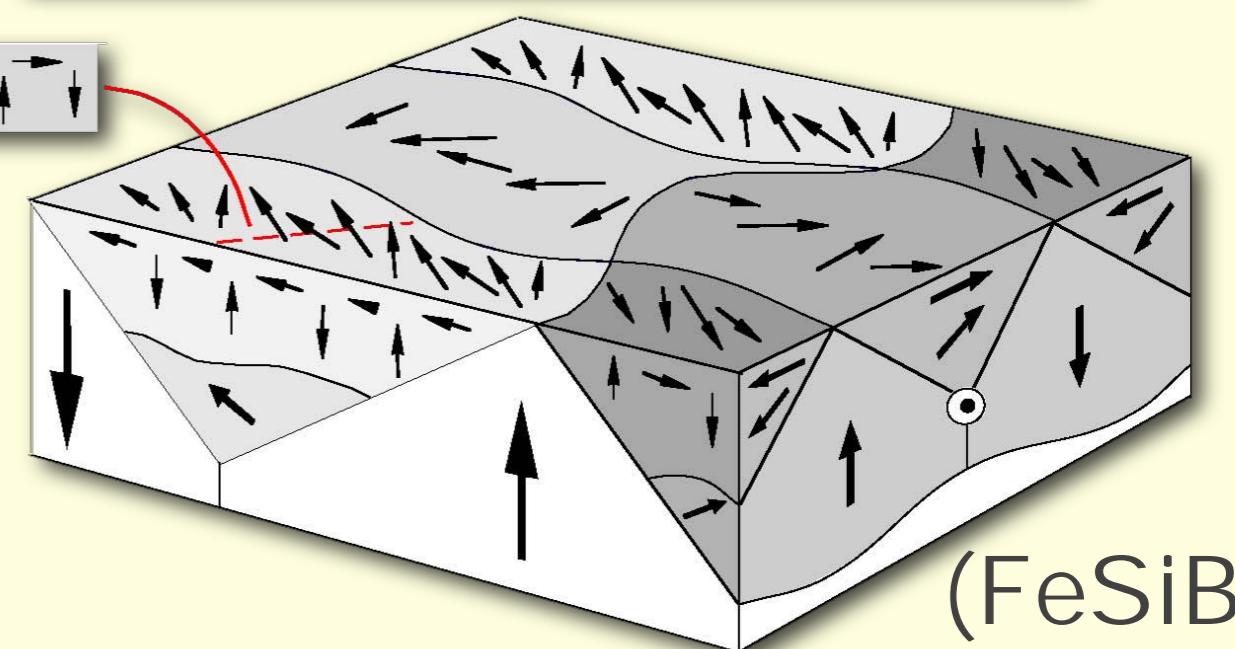
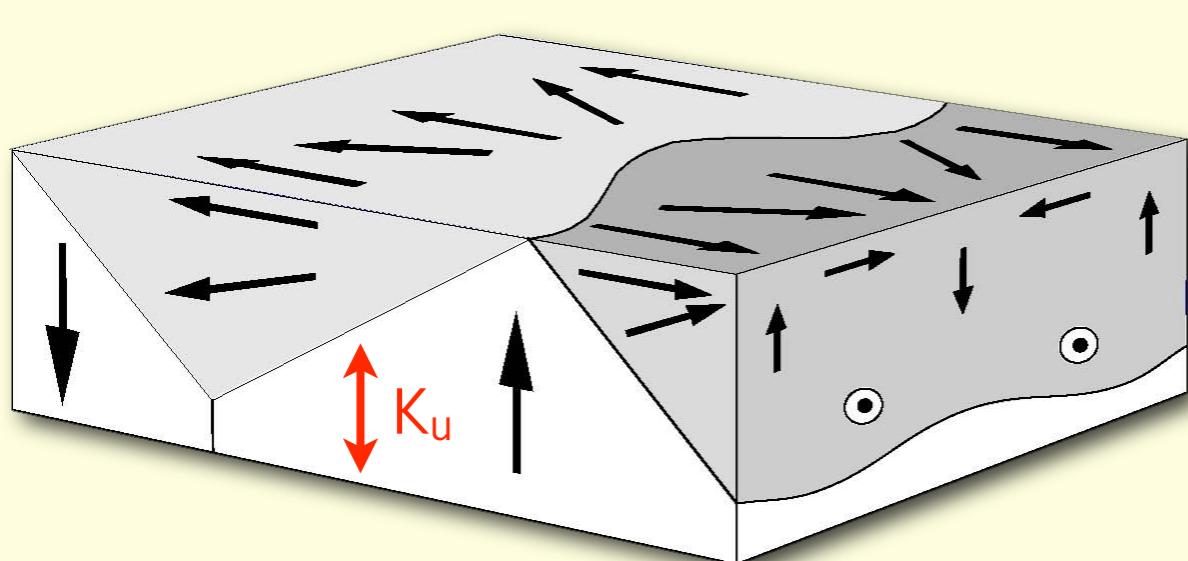
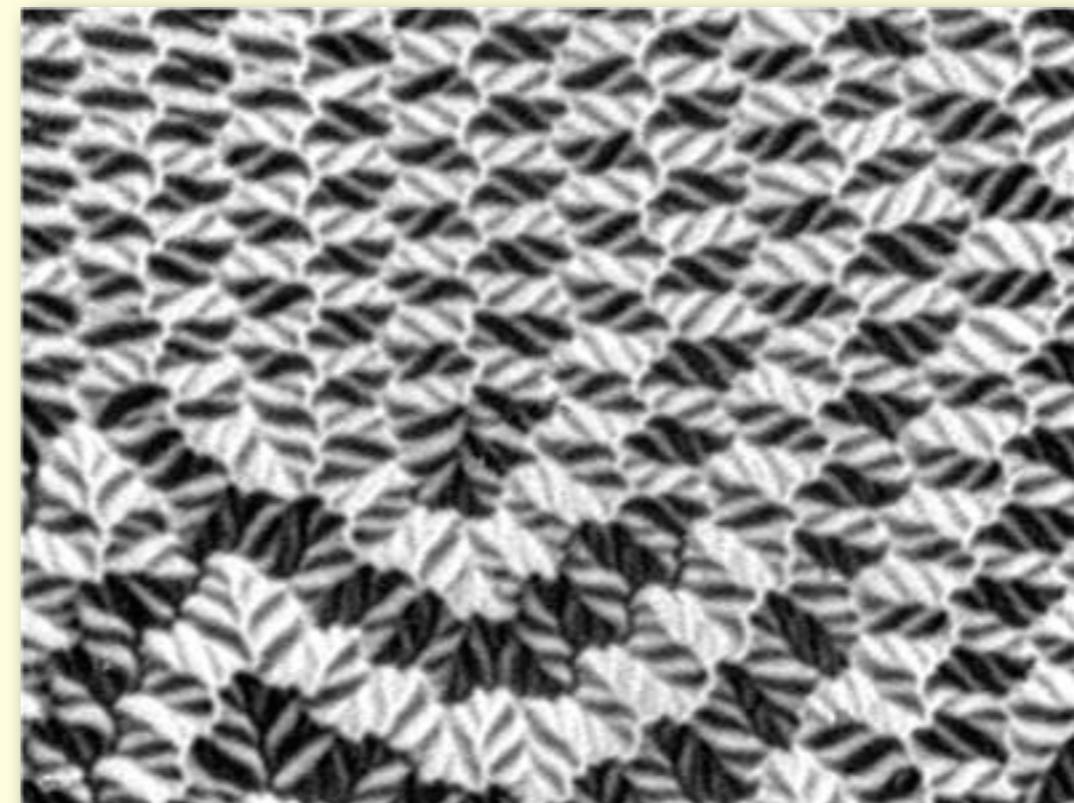
(FeSiB)

Branched domains in amorphous ribbons

amorphous ribbon (20 μm thick)
increasing perpendicular anisotropy (stress)



10 μm

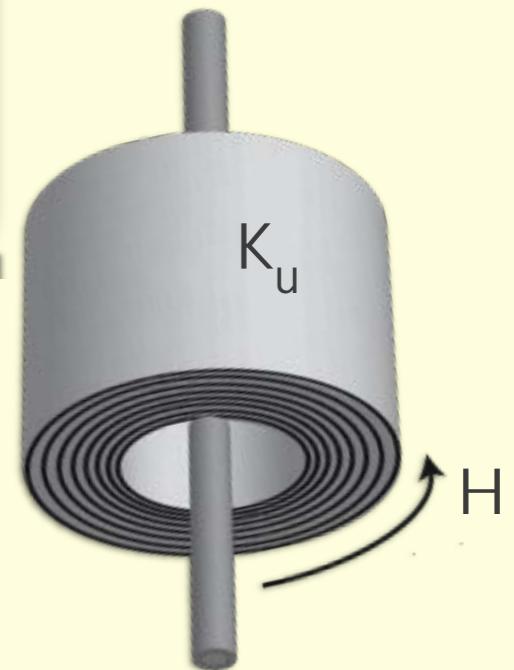
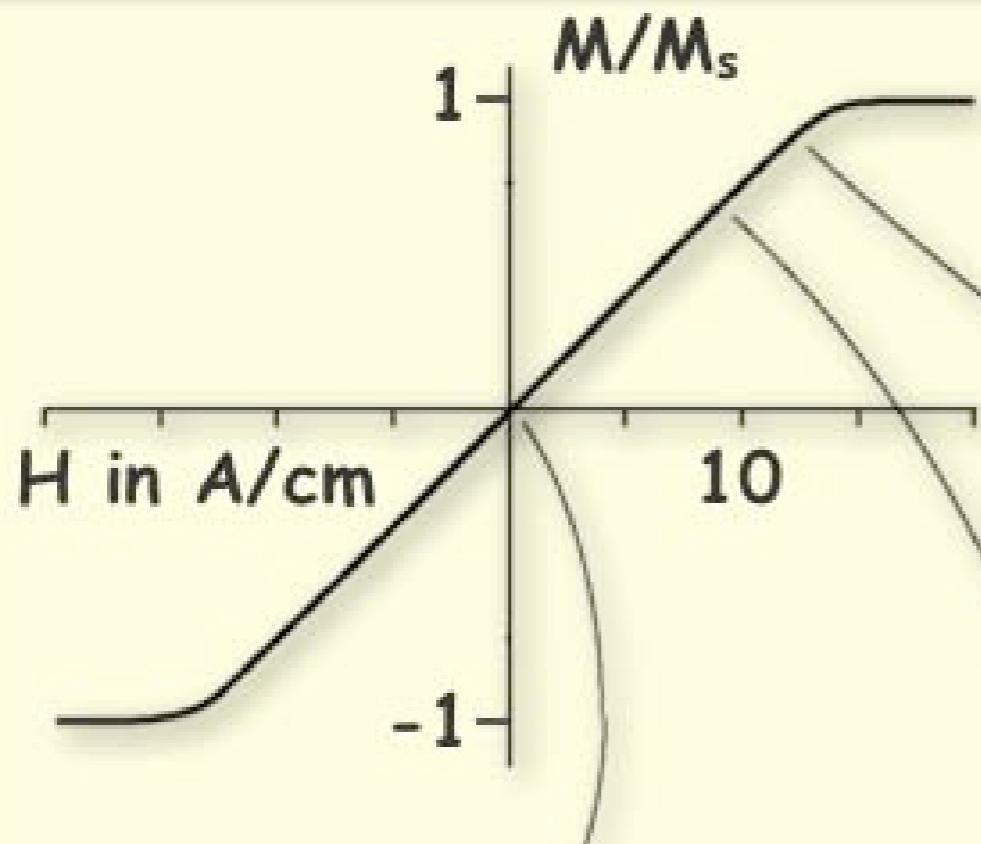


Domain control by field annealing

CoFeSiB-alloy with $\lambda_s \sim 0$

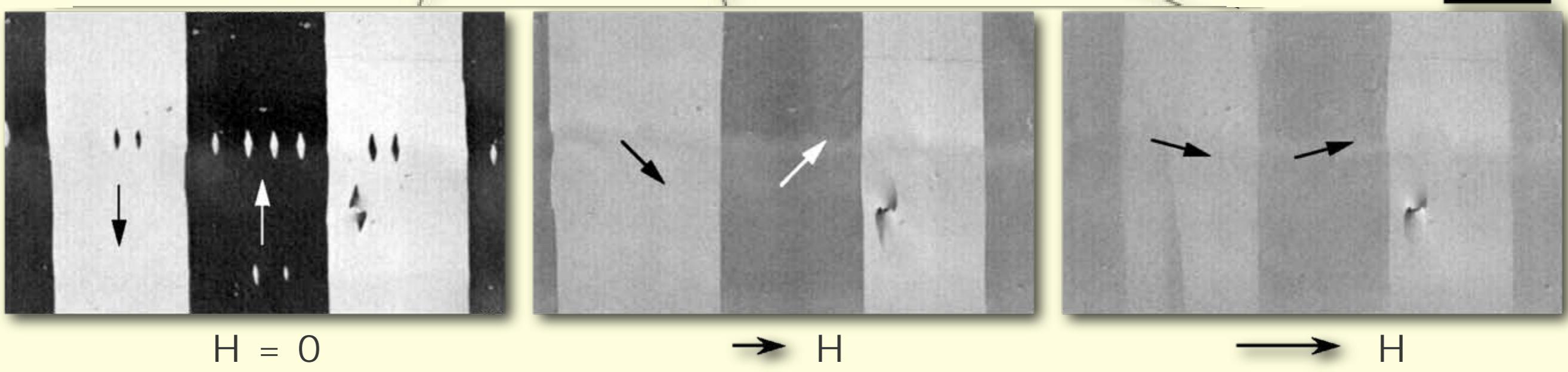
→ no stress effects

→ controlled anisotropy by field-annealing



transverse
anisotropy

100 μm

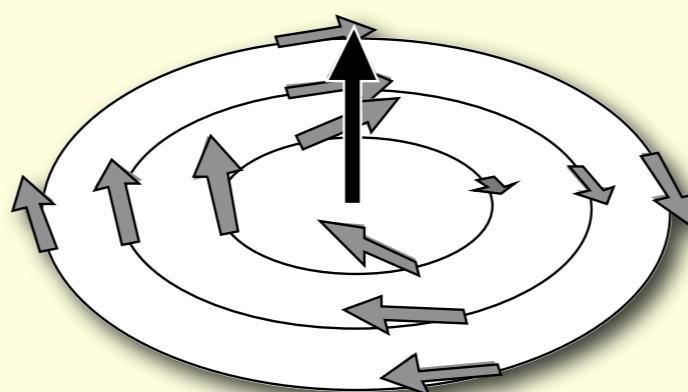
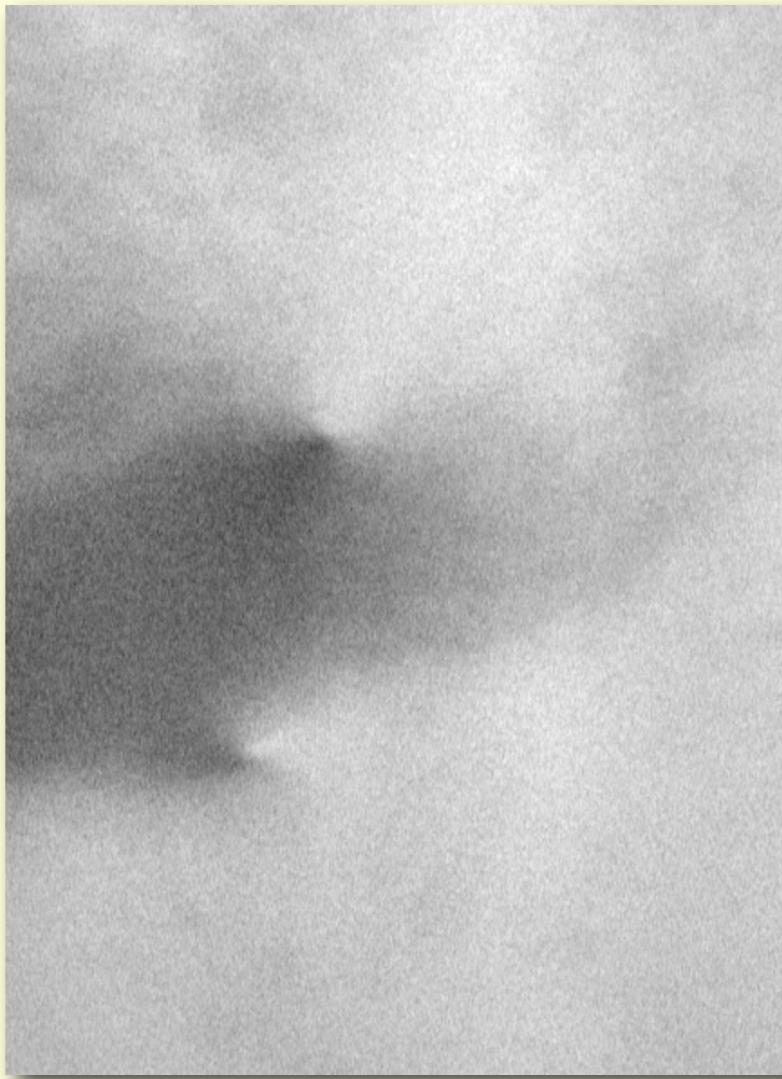
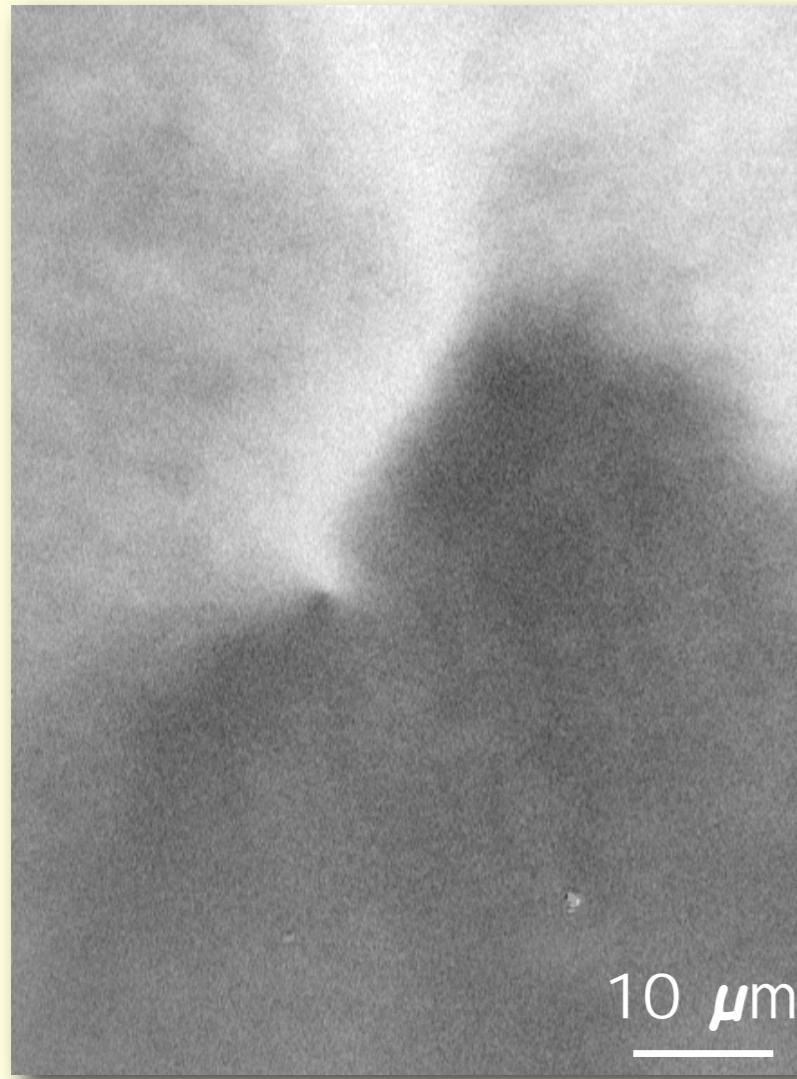


Generation of anisotropy-free amorphous ribbons:

- magnetostriction-free ribbon (Co-based alloy)
($T_{\text{Curie}} = 220^\circ \text{C}$, $T_{\text{cryst}} = 540^\circ \text{C}$)
- polished on both sides
- stress relieve annealed just below T_{cryst} (at 430°C)
- cooled in rotating field

Continuous magnetization-patterns

in magnetostriction-free metallic glass
after annealing in rotating field



Continuous magnetization-patterns

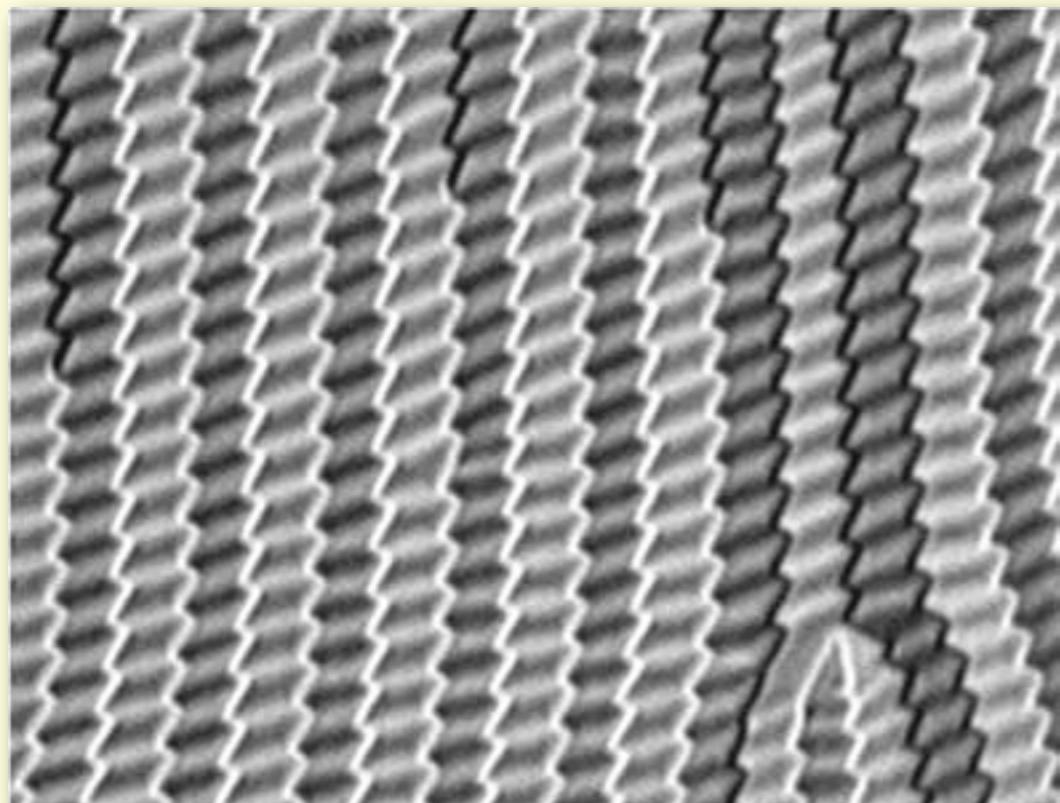
in magnetostriction-free metallic glass
after annealing in rotating field



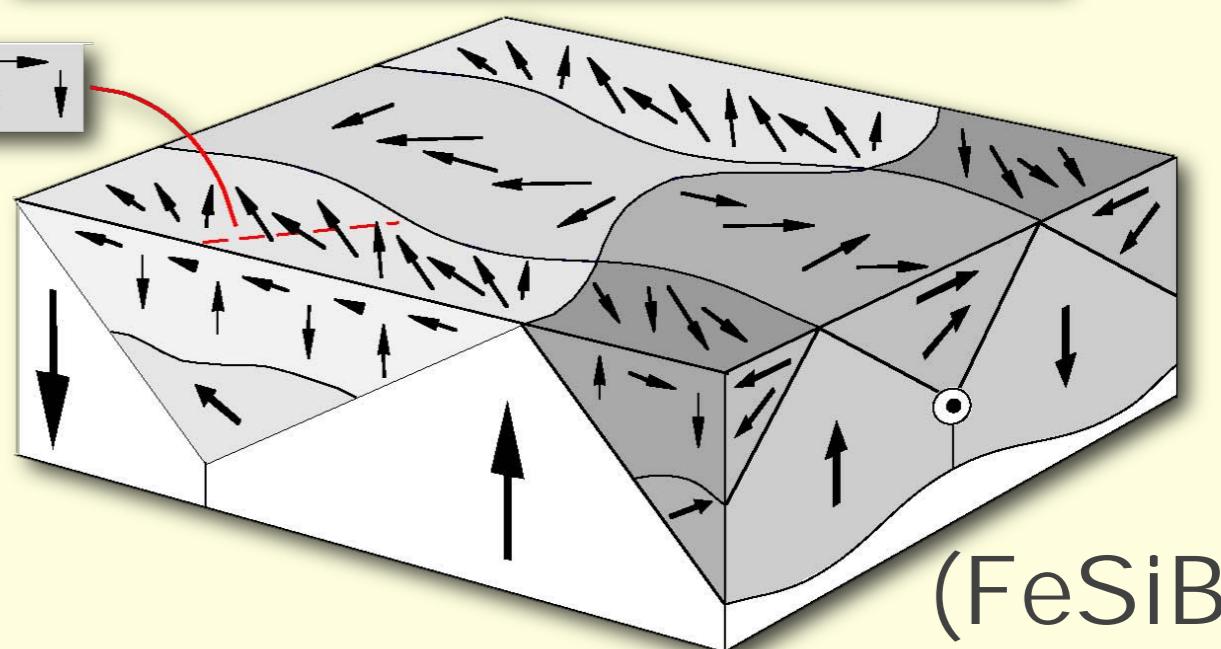
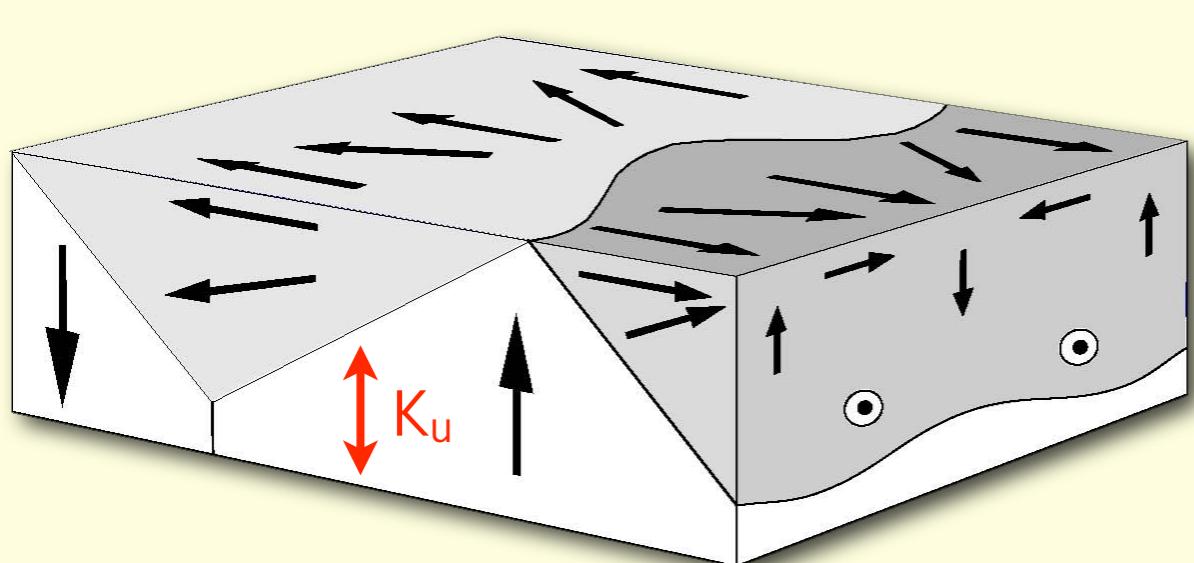
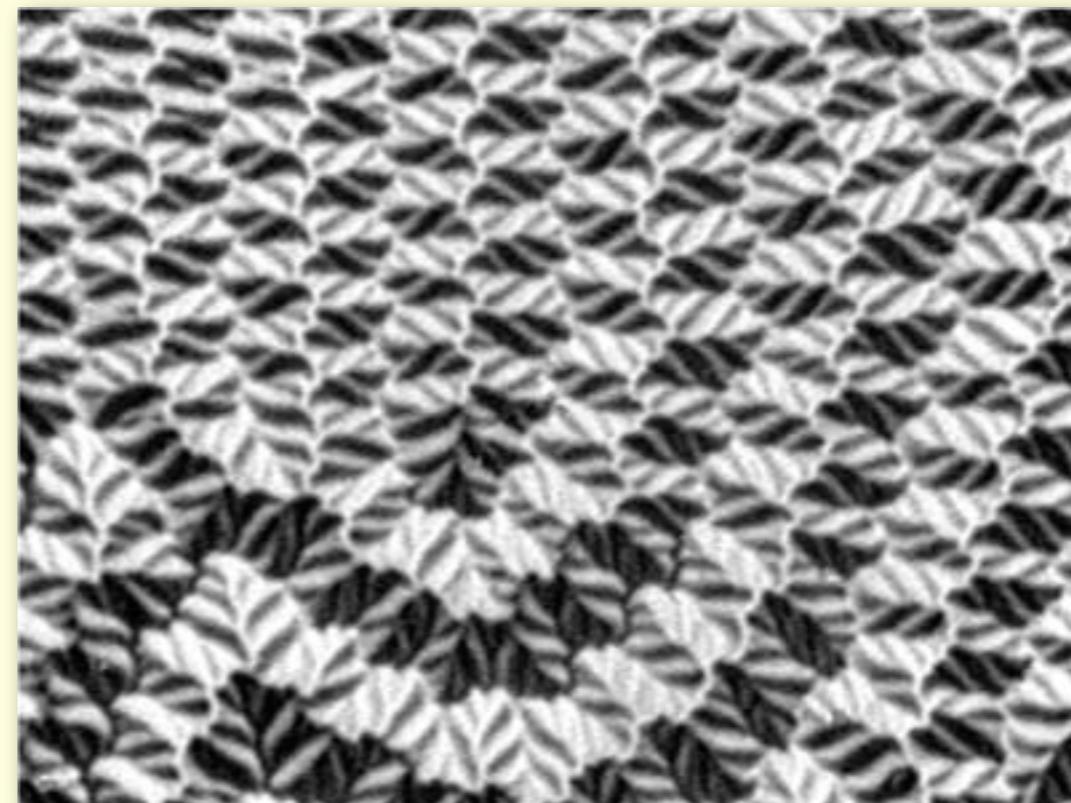
Continuously „flowing“ patterns are
possible in specially treated
amorphous ribbons
(suppression of residual anisotropies)

Branched domains in amorphous ribbons

amorphous ribbon (20 μm thick)
increasing perpendicular anisotropy (stress)

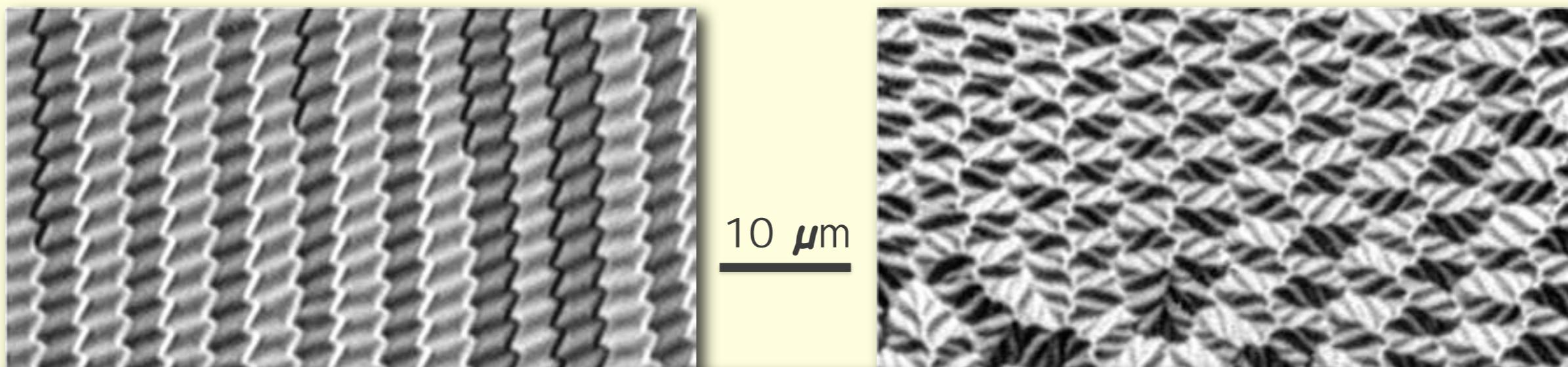


10 μm



Branched domains in amorphous ribbons

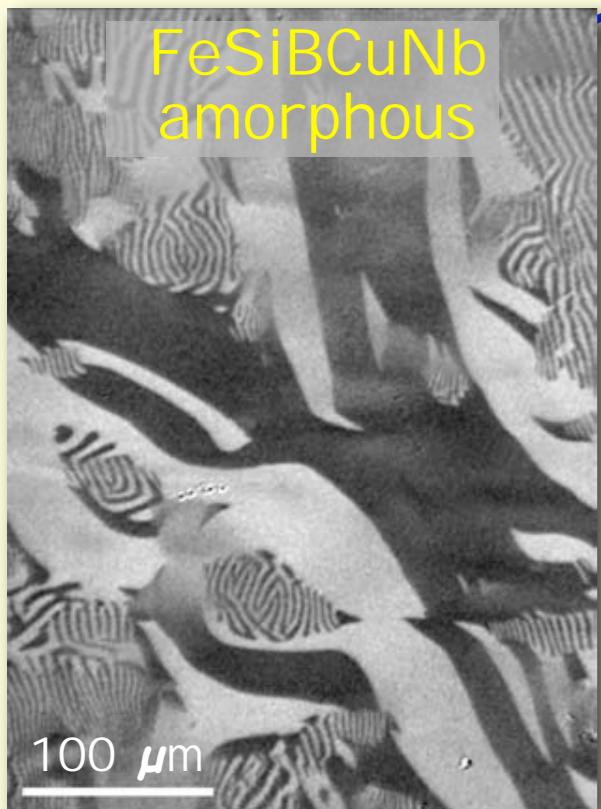
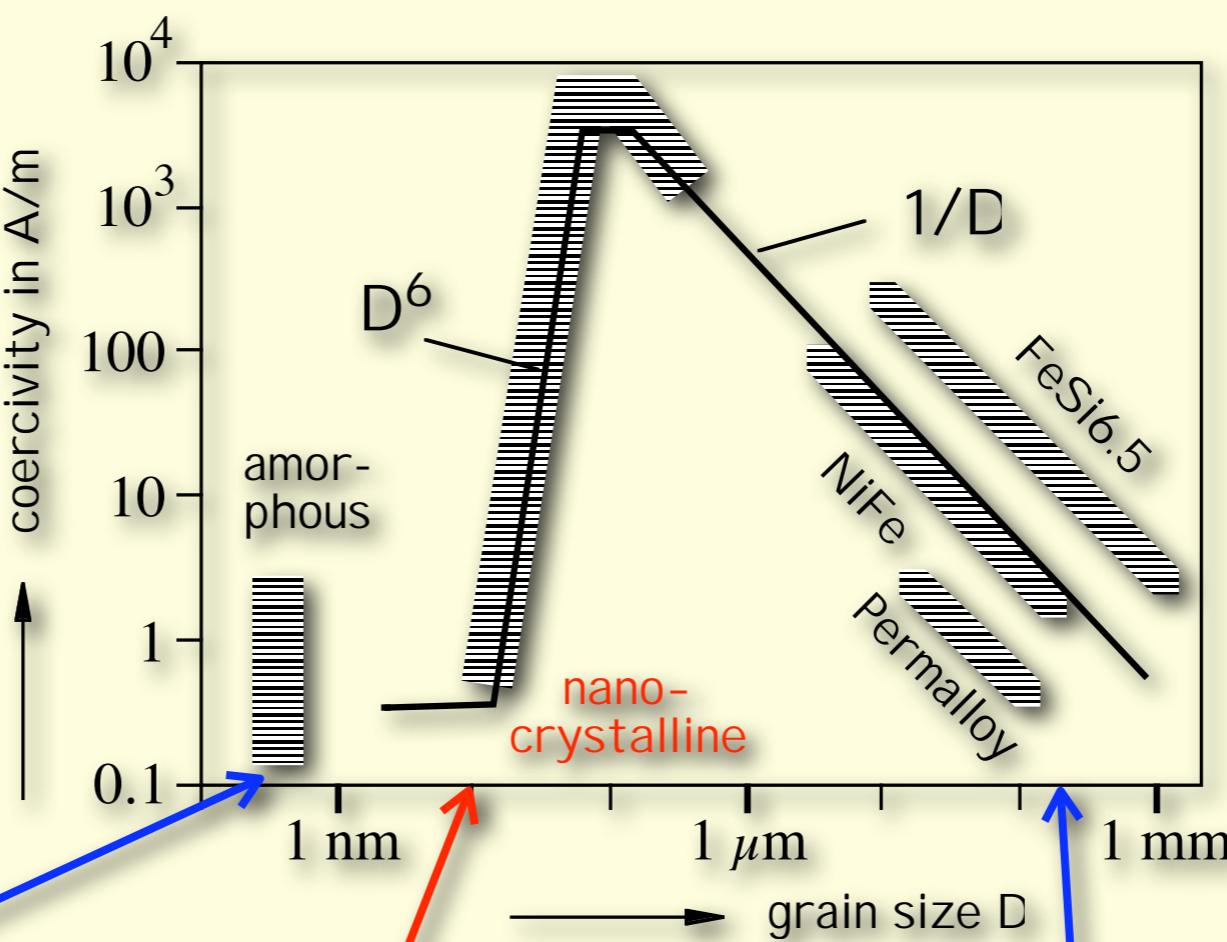
amorphous ribbon (20 μm thick)
increasing perpendicular anisotropy (stress)



Continuously „flowing” patterns also
occur in case of conflicting influences
(anisotropy plays role)

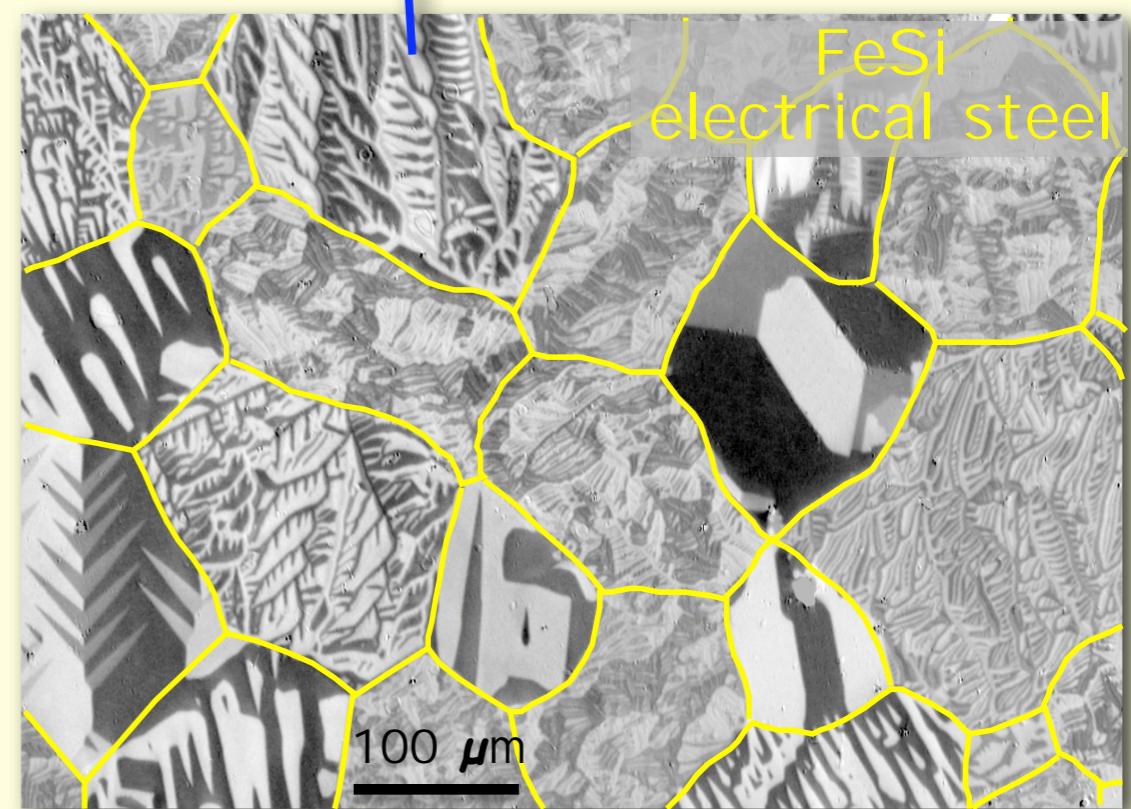
(FeSiB)

Summary: Coercivity and domains



FeSiBCuNb
amorphous

?



FeSi
electrical steel

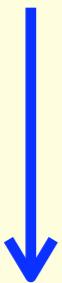
Overview

1. Domains in coarse-grained material
2. Domains in amorphous material
3. Domains in nanocrystalline,
soft magnetic ($Q \ll 1$) materials
4. Domains in fine- and nanostructured,
permanent magnetic ($Q > 1$) materials

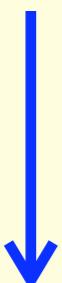
Nanocrystalline soft magnets

Nanocrystalline ribbon $\text{Fe}_{73}\text{Si}_{16}\text{B}_7\text{Cu}_1\text{Nb}_3$
(Finemet, Vitroperm)

rapid
quenching

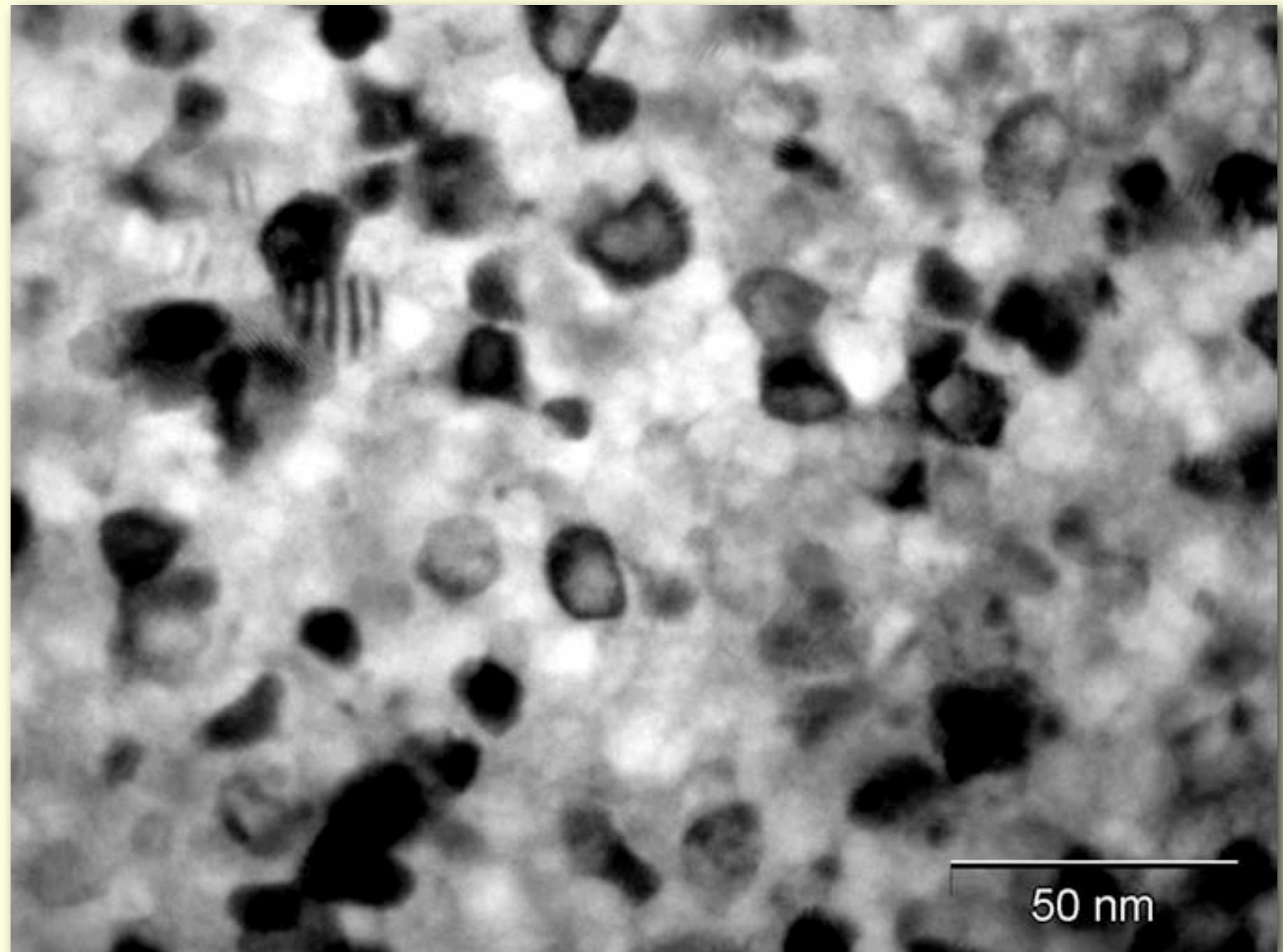


amorphous
ribbon



550°C

nanocrystalline
ribbon



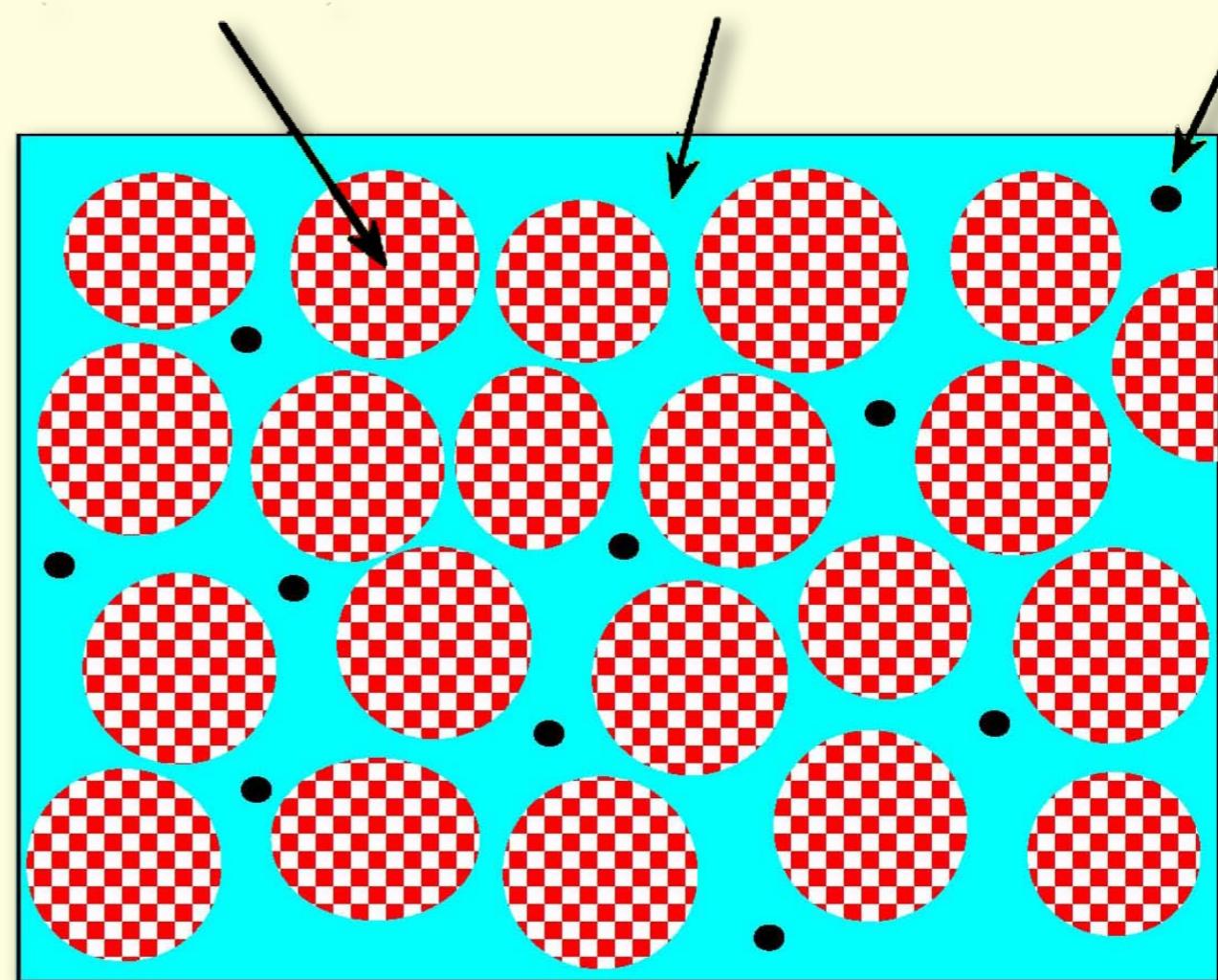
Nanocrystalline soft magnets

Nanocrystalline ribbon $\text{Fe}_{73}\text{Si}_{16}\text{B}_7\text{Cu}_1\text{Nb}_3$ (Finemet, Vitroperm)

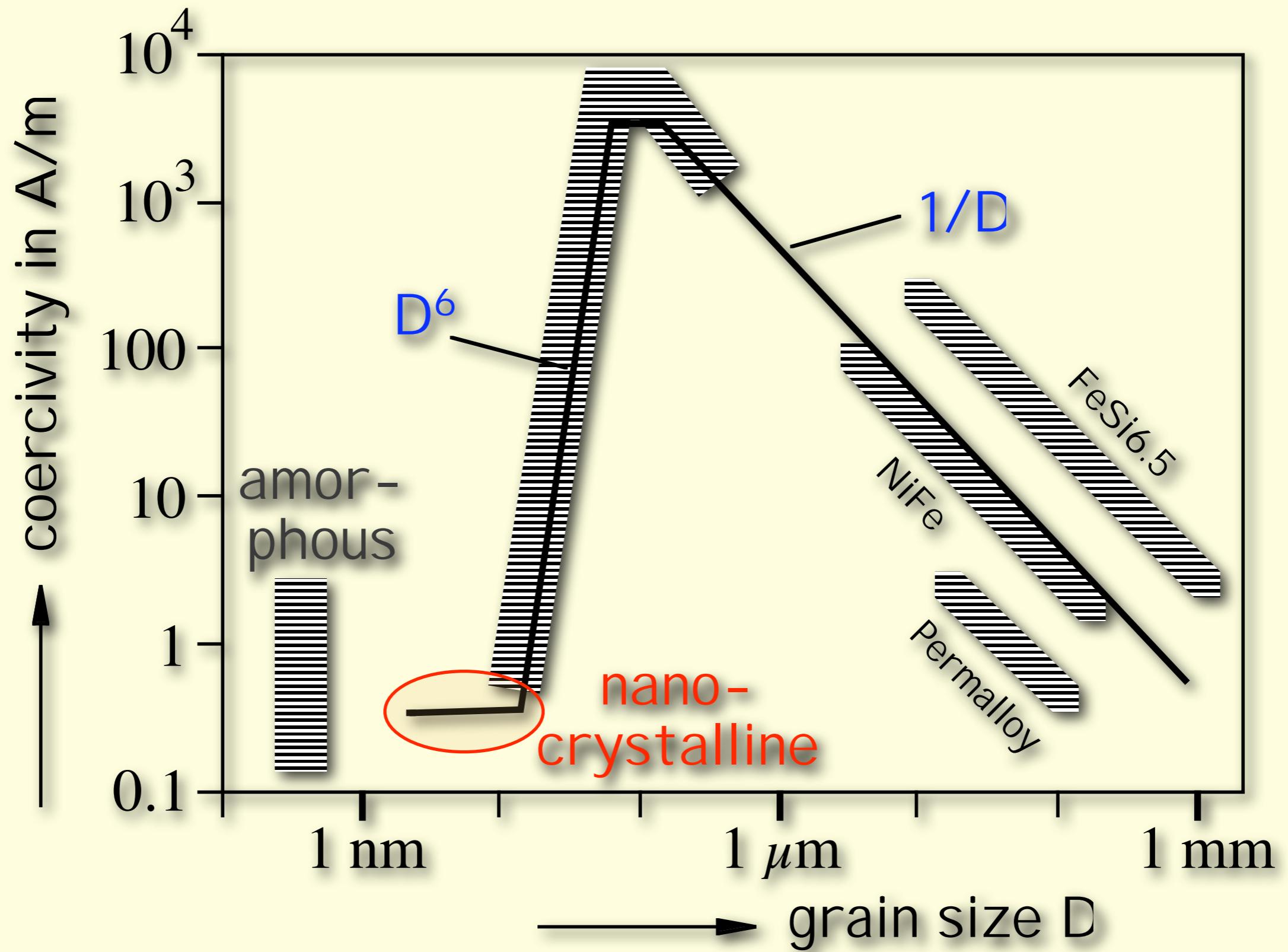
rapid quenching

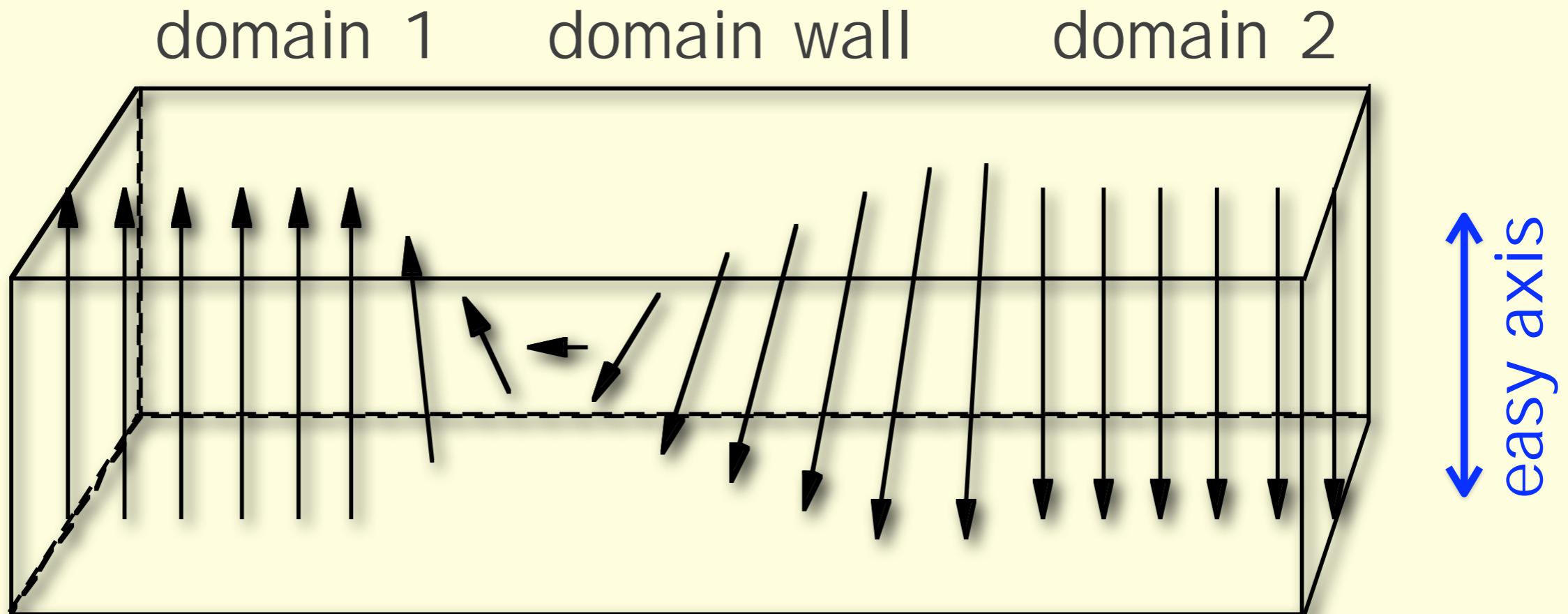
amorphous ribbon

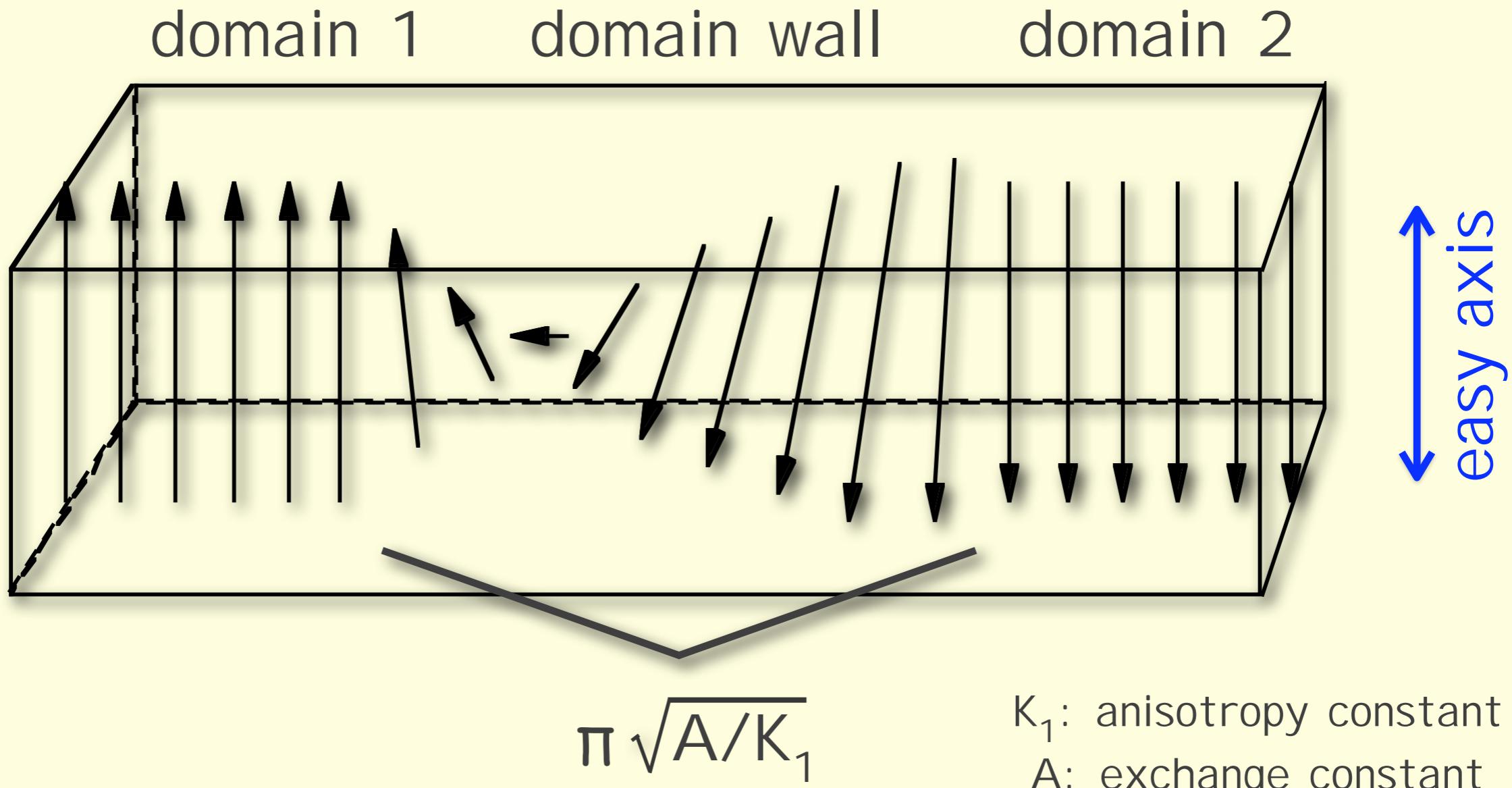
bcc Fe-Si amorphous Cu
(~10 nm) Fe-Nb-B matrix cluster

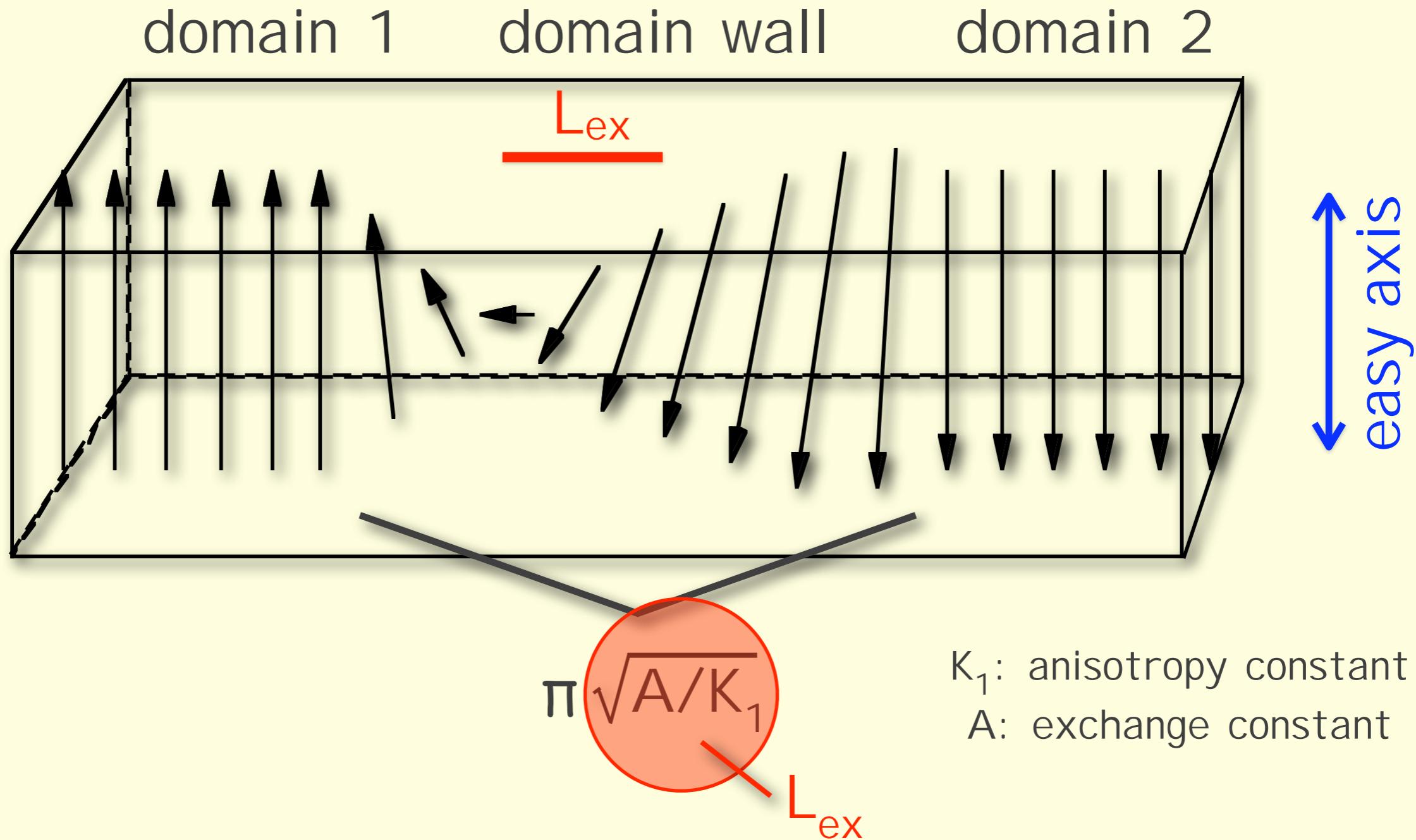


Coercivity and grain size

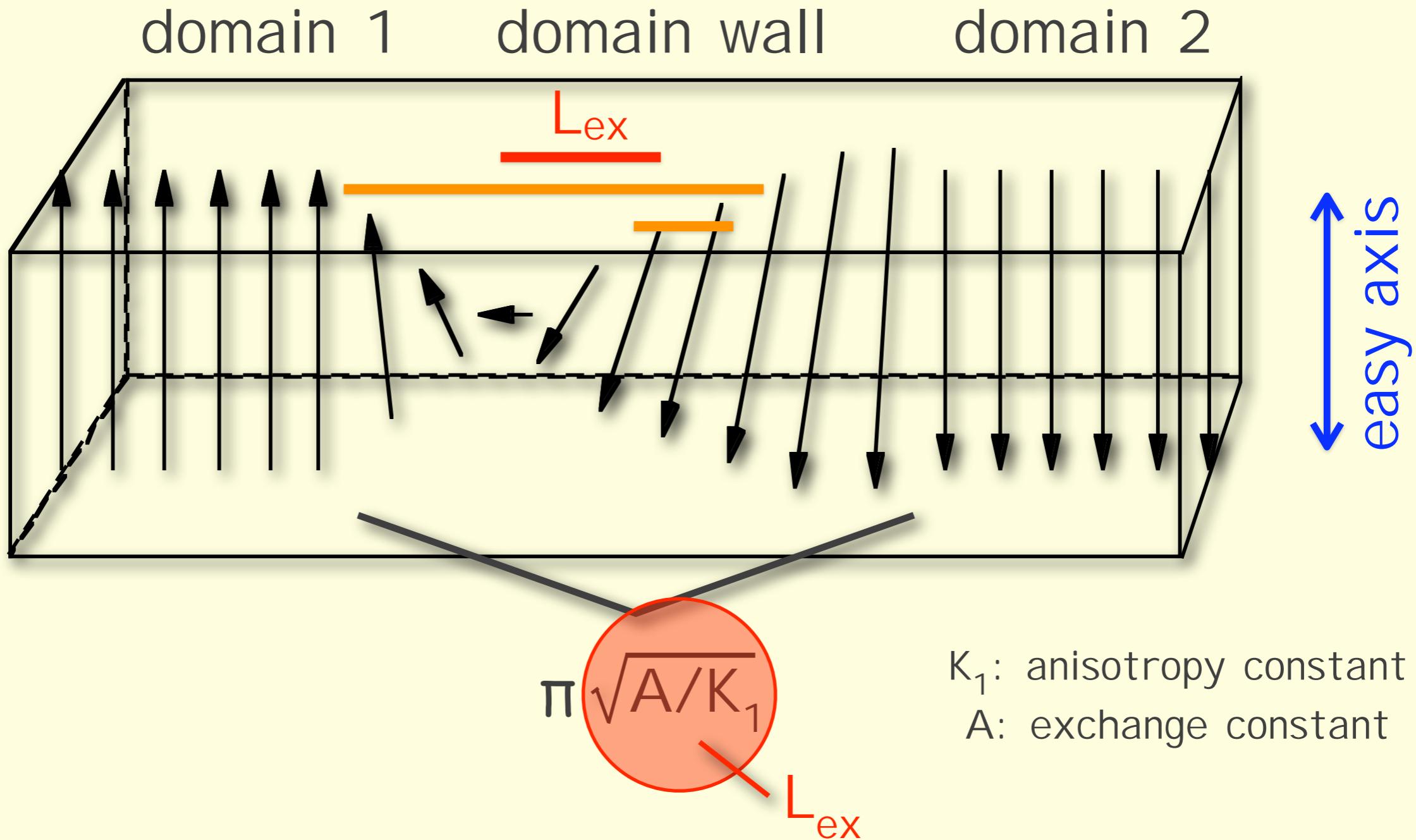




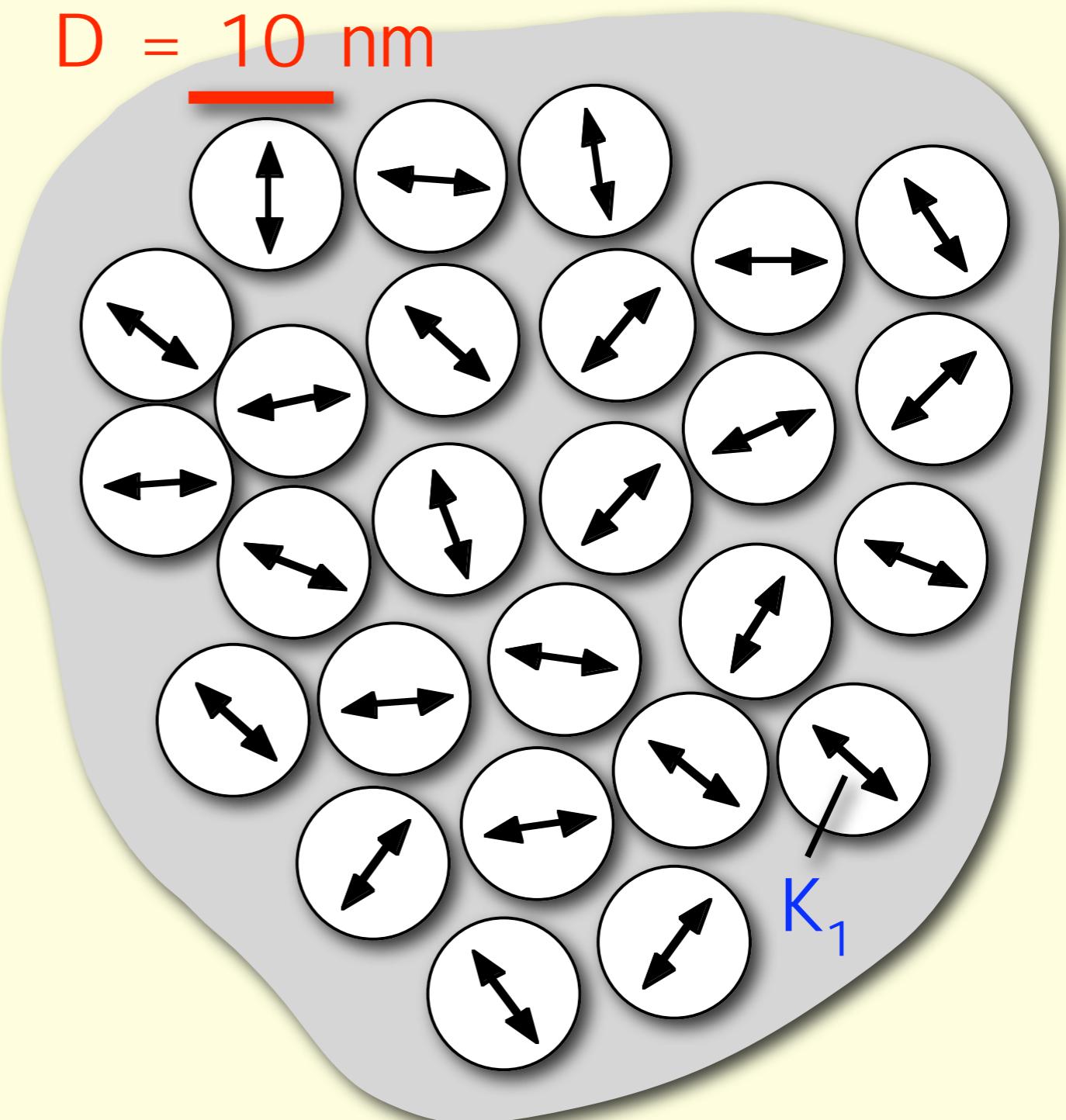




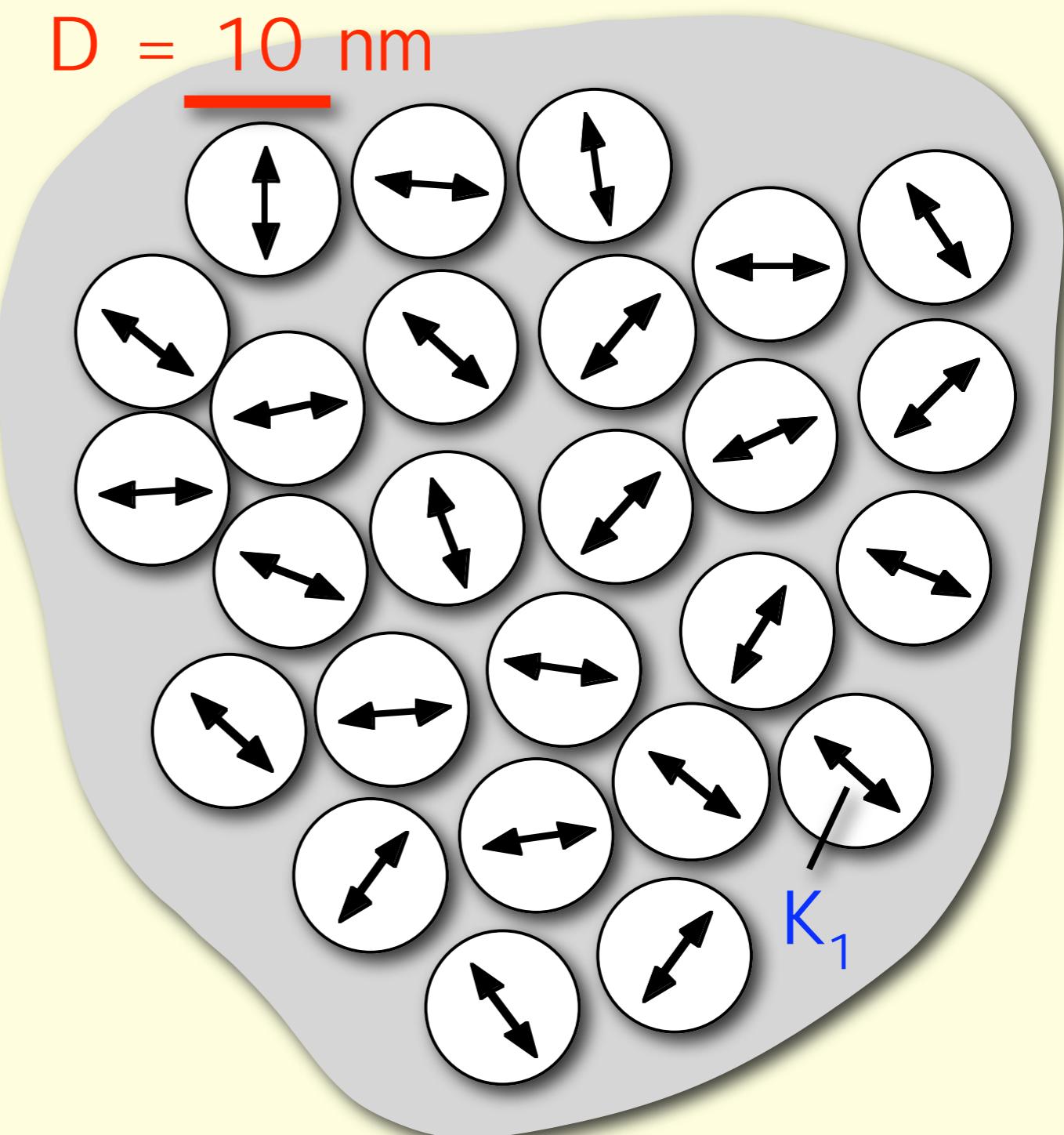
ferromagnetic correlation length (exchange length):
minimum scale for appreciable variation of magnetization
(parallel moments for $L < L_{ex}$)



ferromagnetic correlation length (exchange length):
minimum scale for appreciable variation of magnetization
(parallel moments for $L < L_{ex}$)

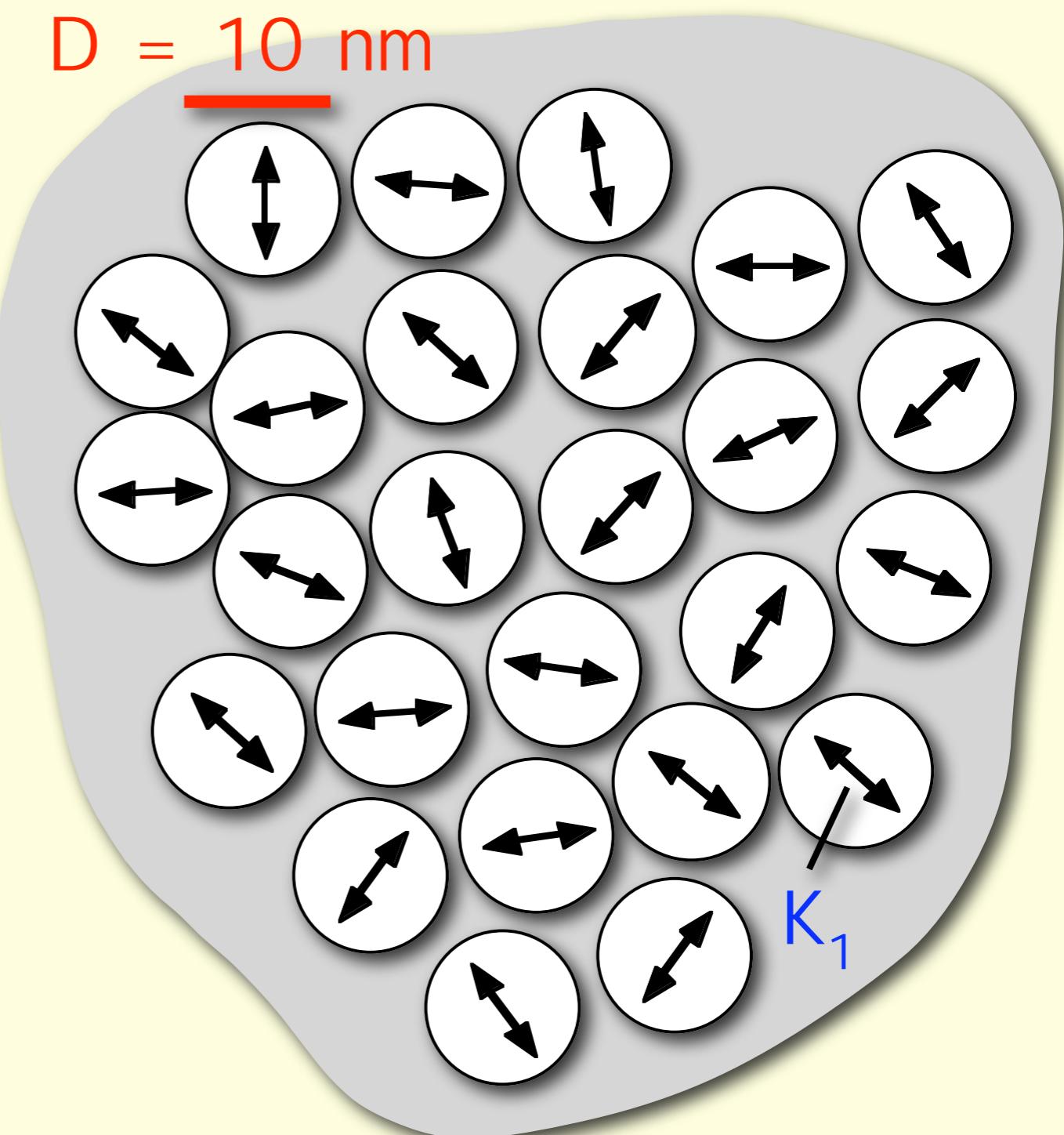


$\text{Fe}_{80}\text{Si}_{20}$:
 $K_1 = 8 \text{ kJ/m}^3$
 $A = 10^{-11} \text{ J/m}$



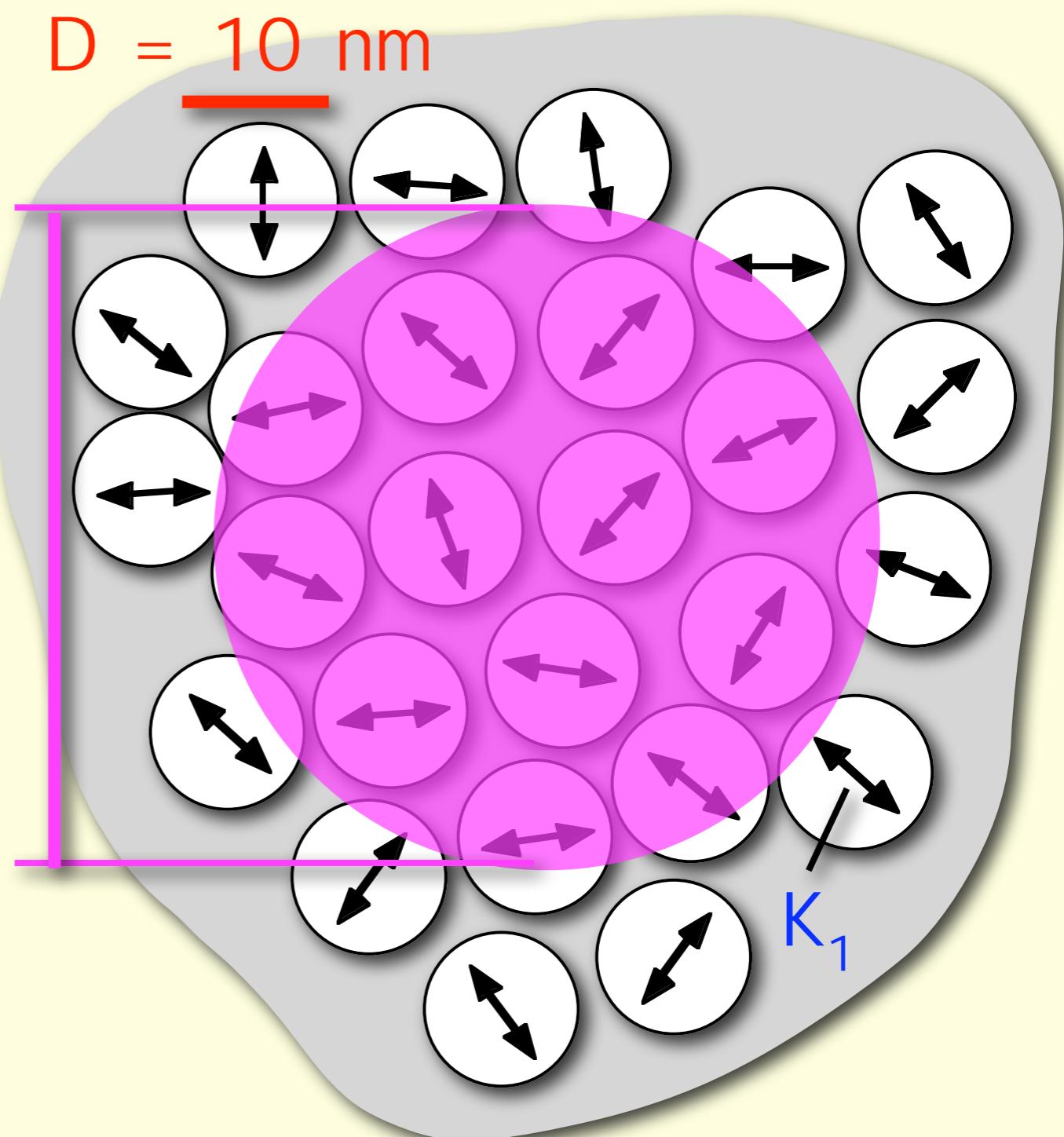
$\text{Fe}_{80}\text{Si}_{20}$:
 $K_1 = 8 \text{ kJ/m}^3$
 $A = 10^{-11} \text{ J/m}$

- $L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$
- $D < L_{\text{ex}}$



$\text{Fe}_{80}\text{Si}_{20}$:
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- $L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$
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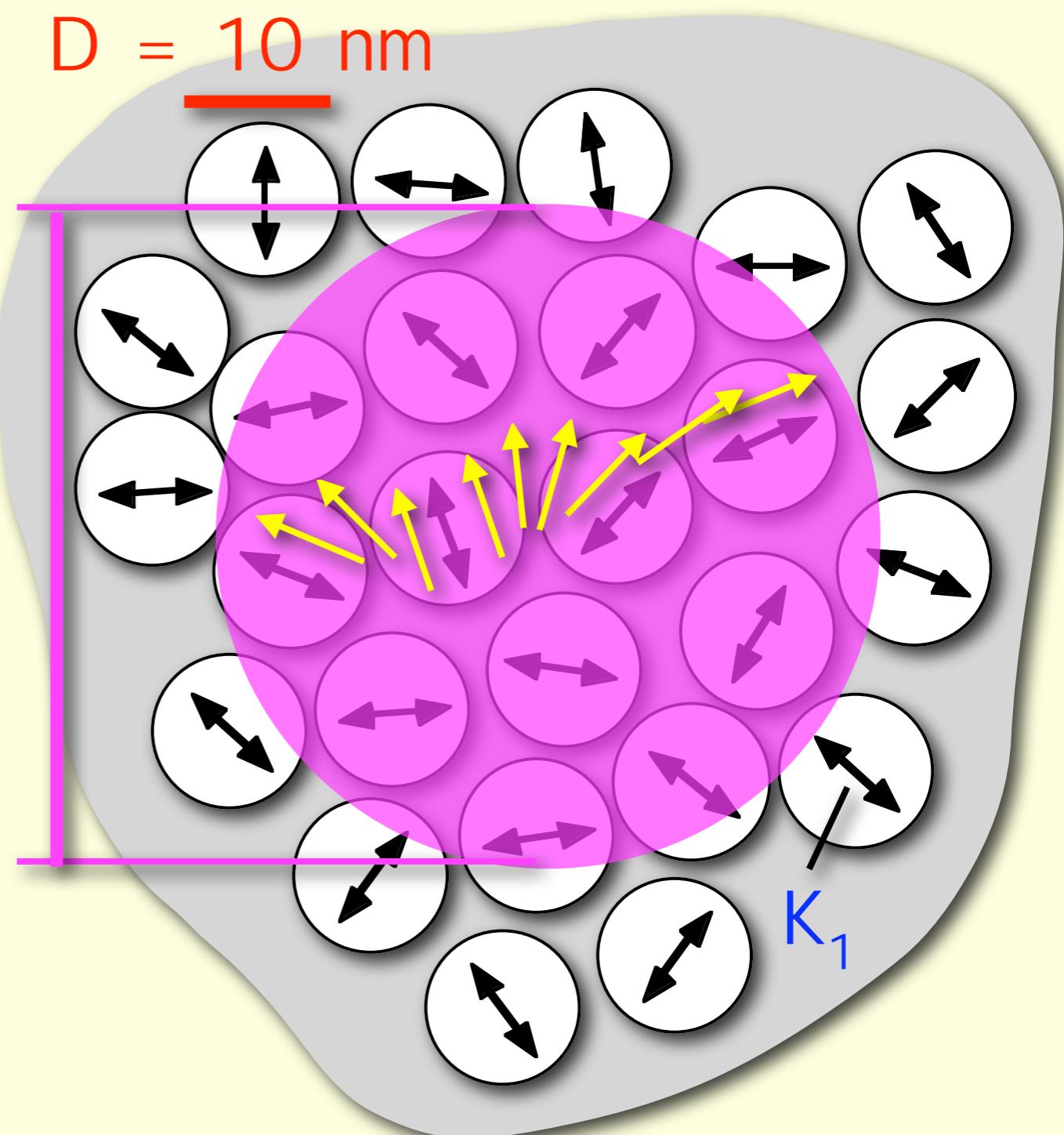


Nanocrystalline soft magnets: Principle

$\text{Fe}_{80}\text{Si}_{20}$:
 $K_1 = 8 \text{ kJ/m}^3$
 $A = 10^{-11} \text{ J/m}$

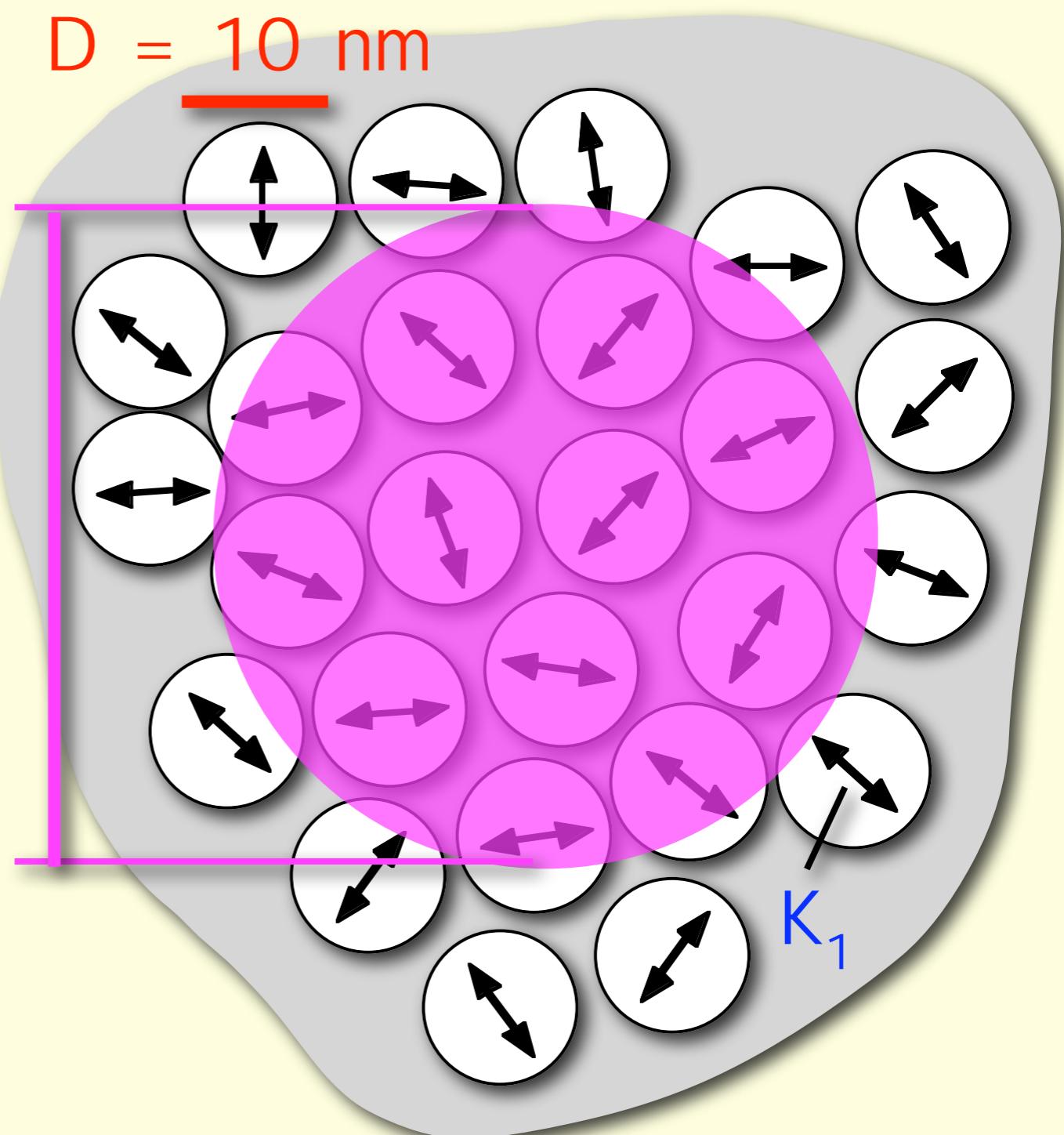
$$\rightarrow L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$$

$$\rightarrow D < L_{\text{ex}}$$



$\text{Fe}_{80}\text{Si}_{20}$:
 $K_1 = 8 \text{ kJ/m}^3$
 $A = 10^{-11} \text{ J/m}$

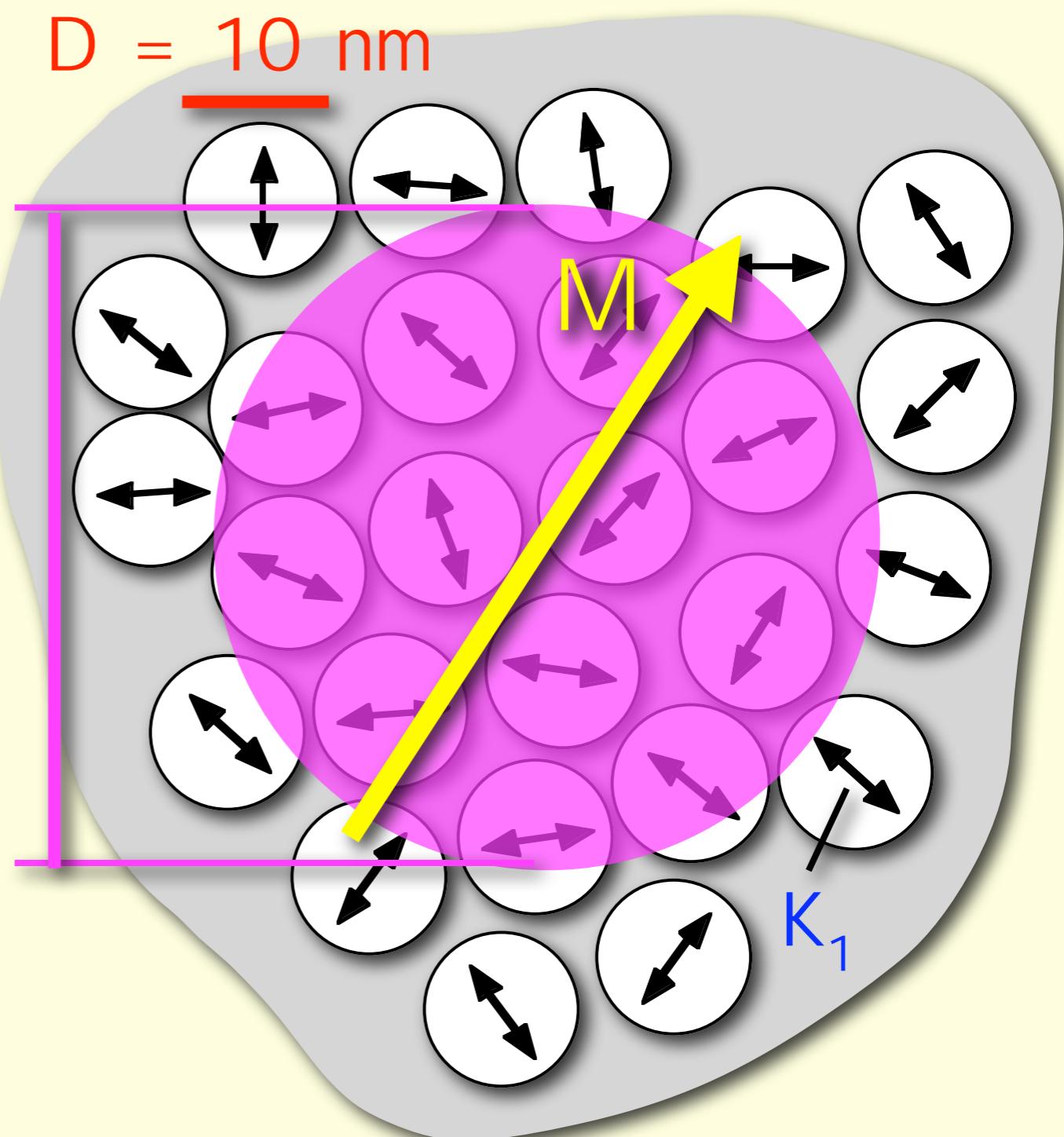
- $L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$
- $D < L_{\text{ex}}$



$\text{Fe}_{80}\text{Si}_{20}$:
 $K_1 = 8 \text{ kJ/m}^3$
 $A = 10^{-11} \text{ J/m}$

$$\rightarrow L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$$

$$\rightarrow D < L_{\text{ex}}$$

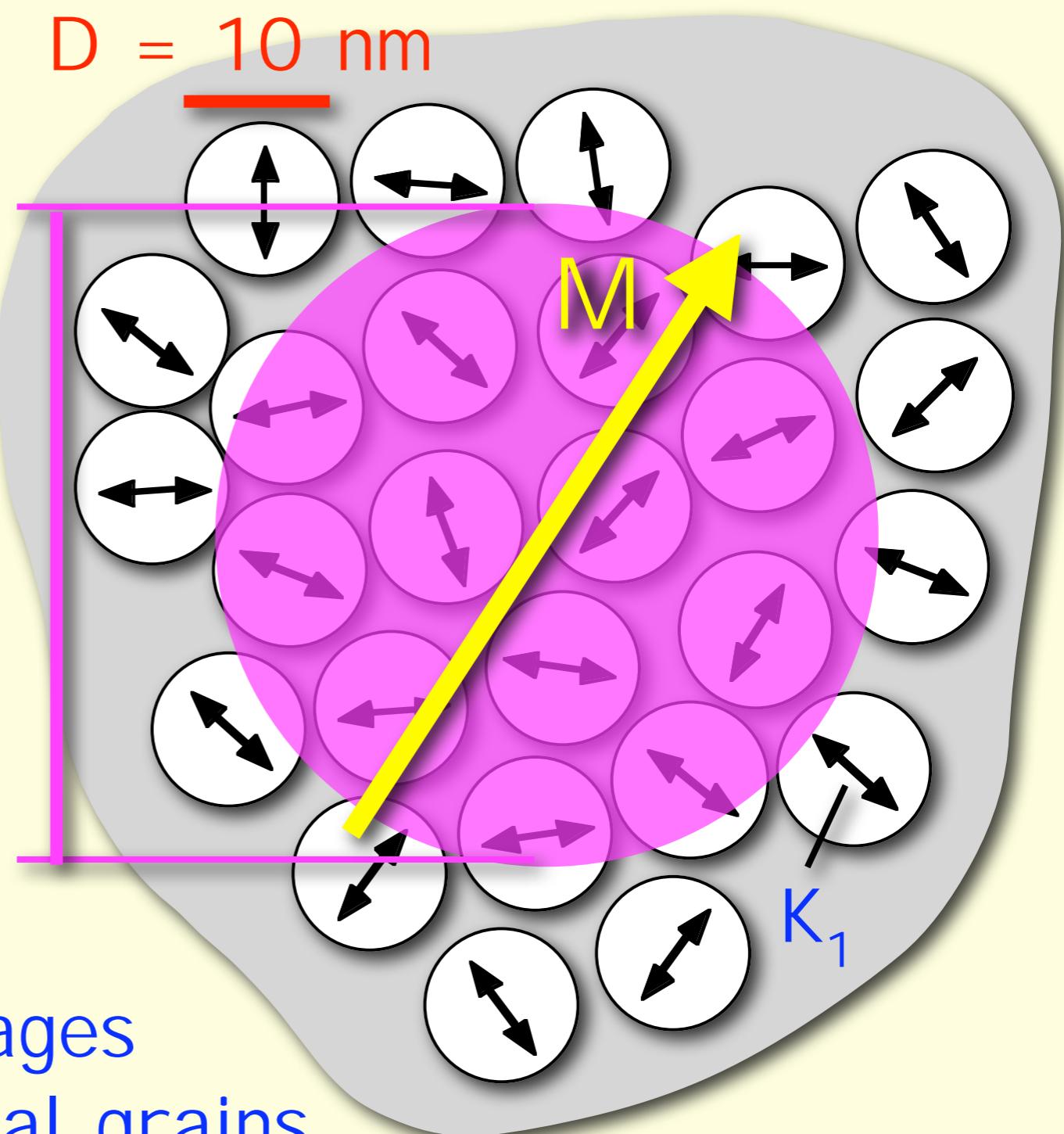


$\text{Fe}_{80}\text{Si}_{20}$:
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 $A = 10^{-11} \text{ J/m}$

$$\rightarrow L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$$

$$\rightarrow D < L_{\text{ex}}$$

random anisotropy model
[Herzer 1989]:
exchange interaction averages
over anisotropy of individual grains



$\text{Fe}_{80}\text{Si}_{20}$:
 $K_1 = 8 \text{ kJ/m}^3$
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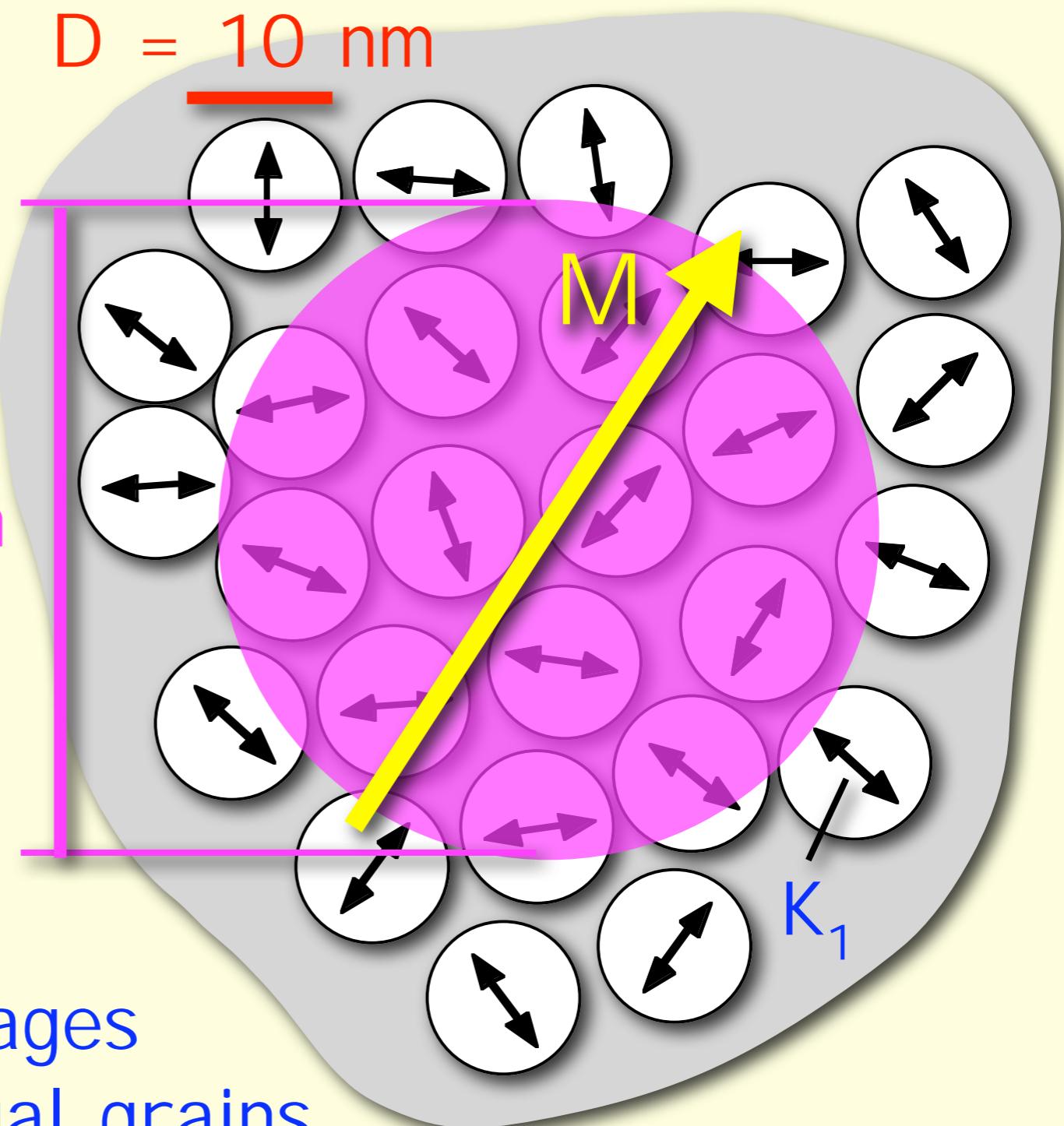
$$\rightarrow L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$$

$$\rightarrow D < L_{\text{ex}}$$

random anisotropy model
[Herzer 1989]:
exchange interaction averages
over anisotropy of individual grains

$$\rightarrow \langle K_1 \rangle \approx |K_1| (D/L_{\text{ex}})^6 = 3 \text{ J/m}^3 \rightarrow$$

very weak
eff. anisotropy

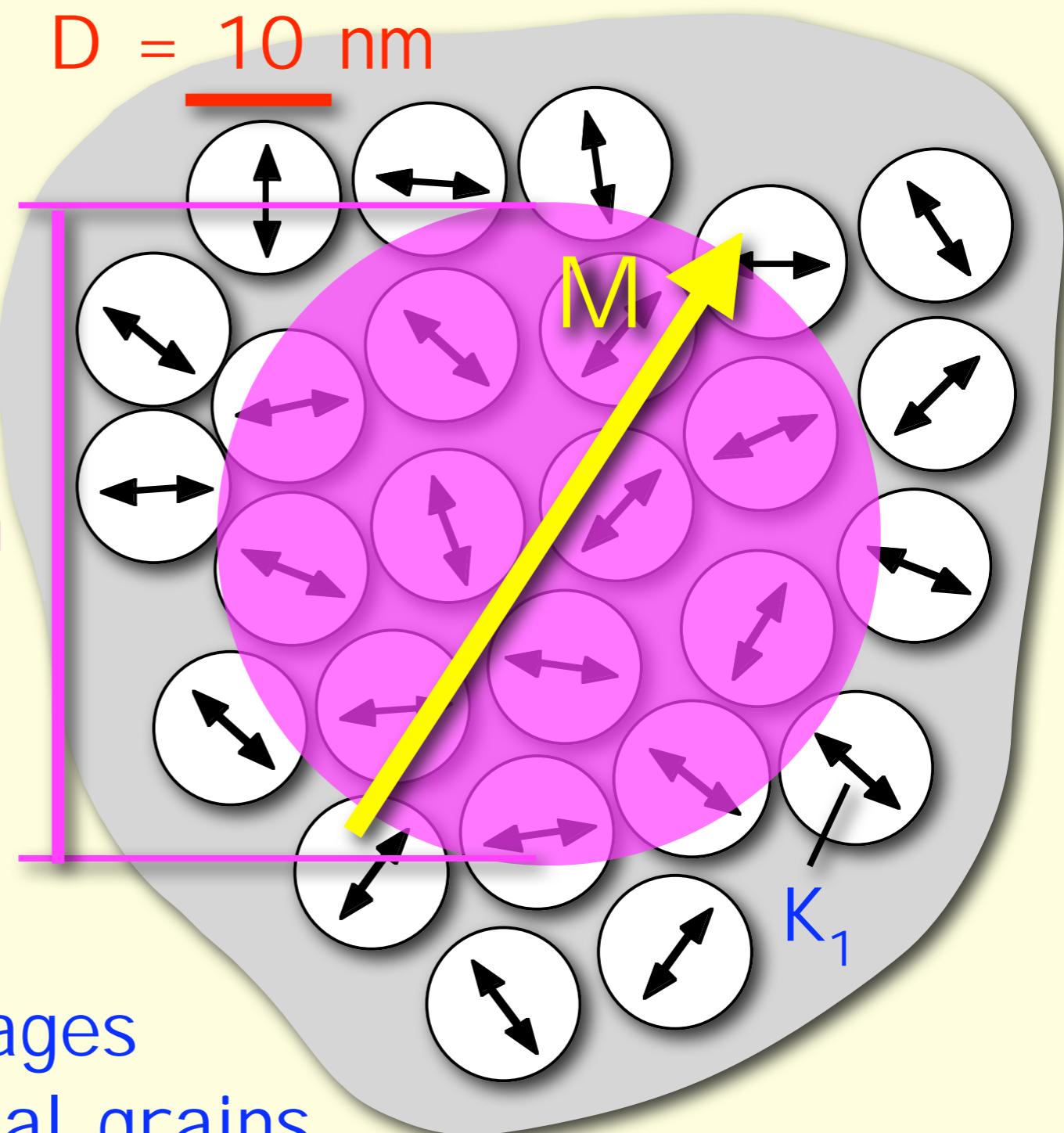


$$\text{Fe}_{80}\text{Si}_{20}: \\ K_1 = 8 \text{ kJ/m}^3 \\ A = 10^{-11} \text{ J/m}$$

$$\rightarrow L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$$

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random anisotropy model
[Herzer 1989]:
exchange interaction averages
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$$\rightarrow \langle K_1 \rangle \approx |K_1| (D/L_{\text{ex}})^6 = 3 \text{ J/m}^3 \rightarrow$$

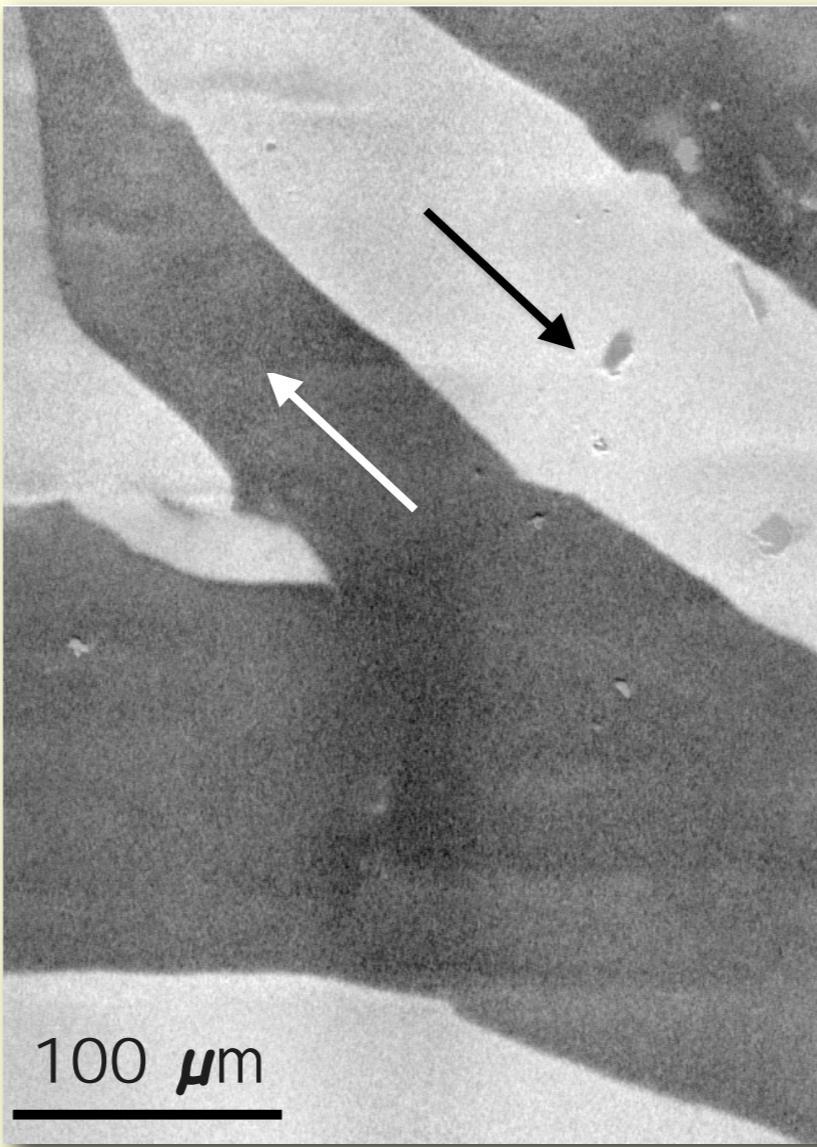
very weak
eff. anisotropy

FeSiBCuNb: domain state

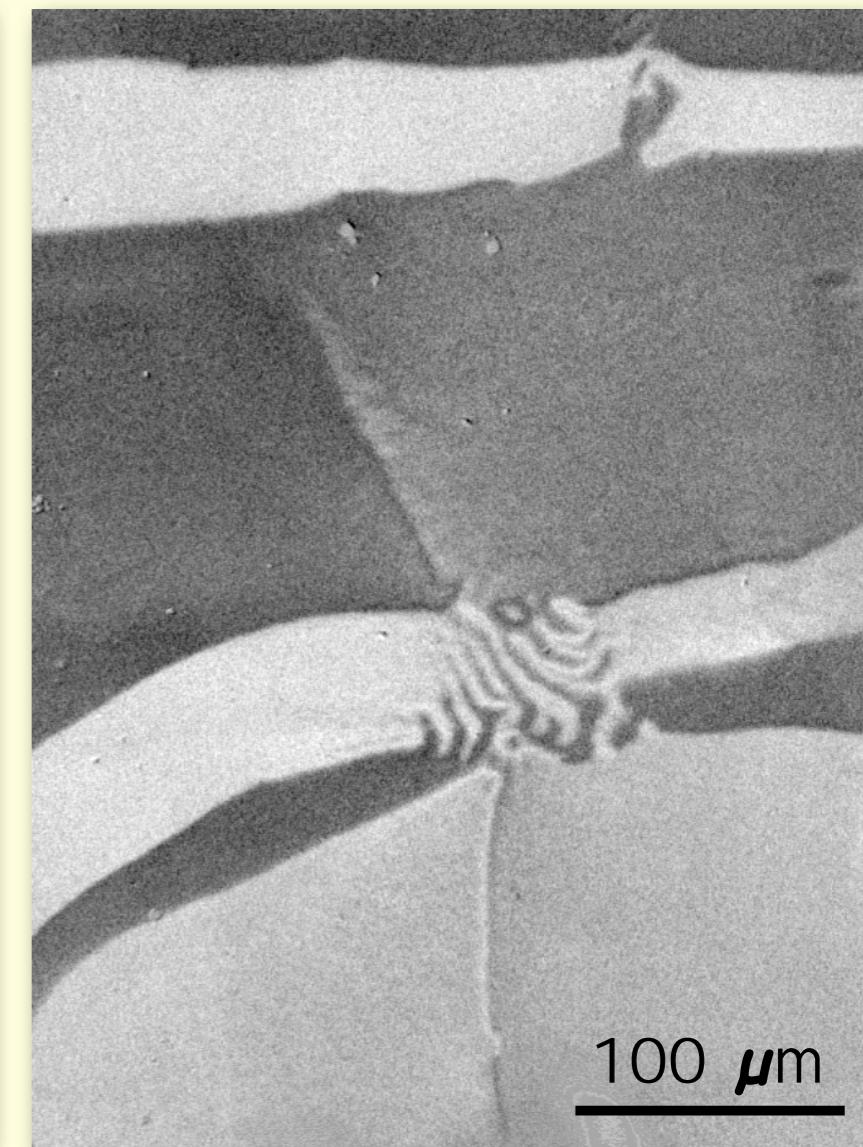
amorphous
(as-quenched)



nanocrystalline



nanocrystalline



homogeneous domains on macroscopic scale, direction determined by induced anisotropy

$\text{Fe}_{80}\text{Si}_{20}$:

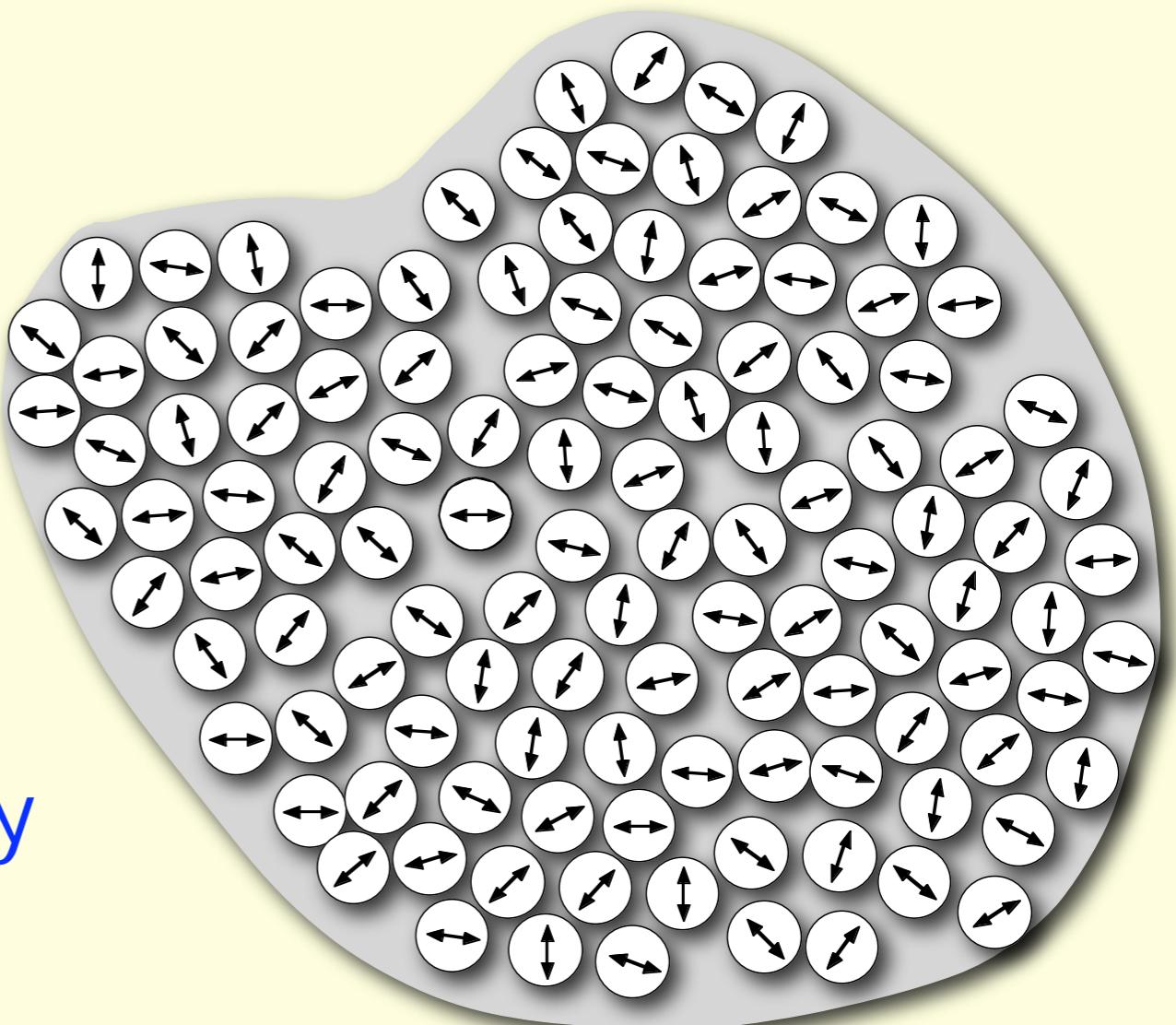
$$K_1 = 8 \text{ kJ/m}^3$$

$$A = 10^{-11} \text{ J/m}$$

→ $L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$
exchange length

random anisotropy model

→ $\langle K_1 \rangle = 3 \text{ J/m}^3$
average anisotropy



$\text{Fe}_{80}\text{Si}_{20}$:

$$K_1 = 8 \text{ kJ/m}^3$$

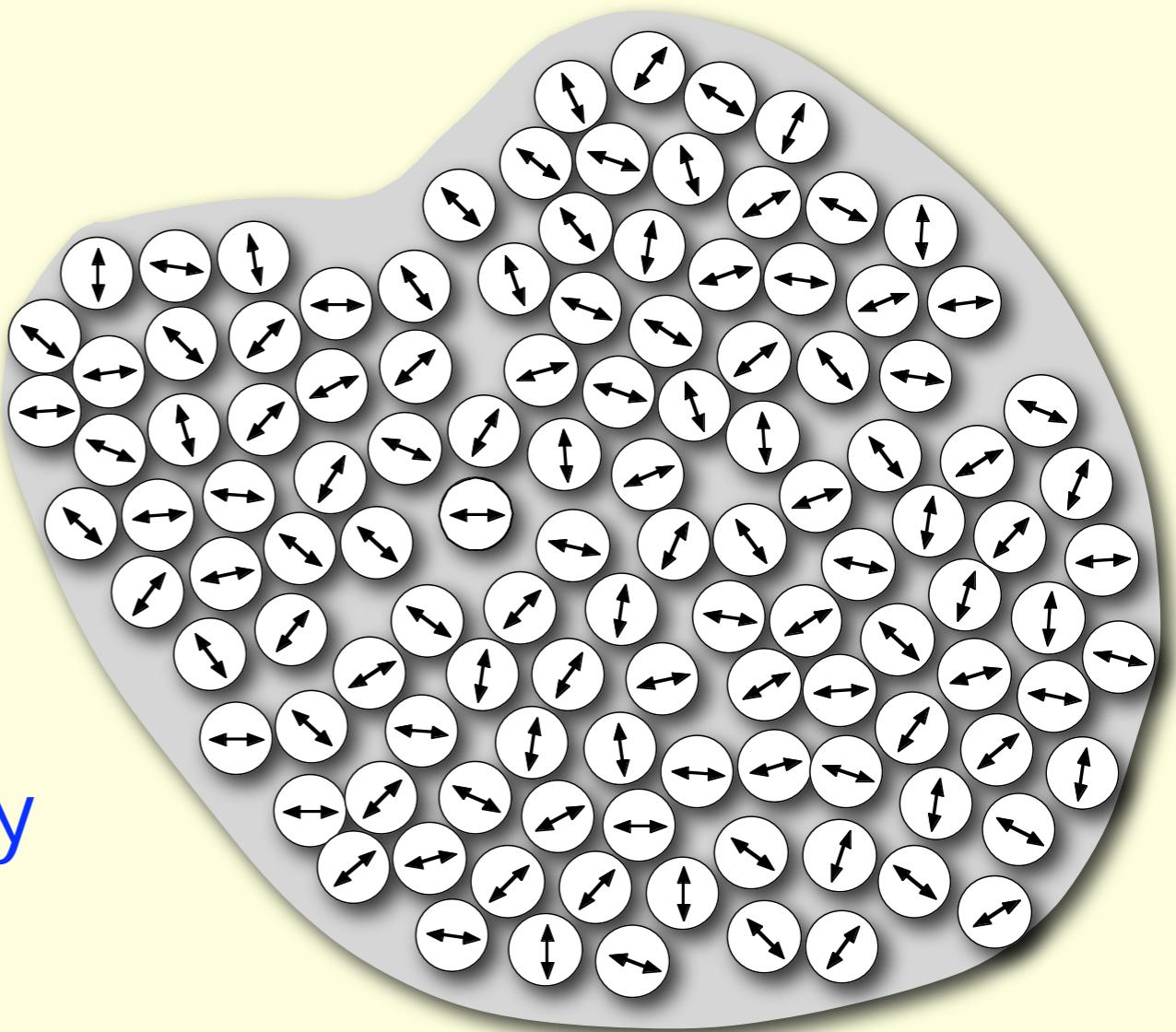
$$A = 10^{-11} \text{ J/m}$$

→ $L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$
exchange length

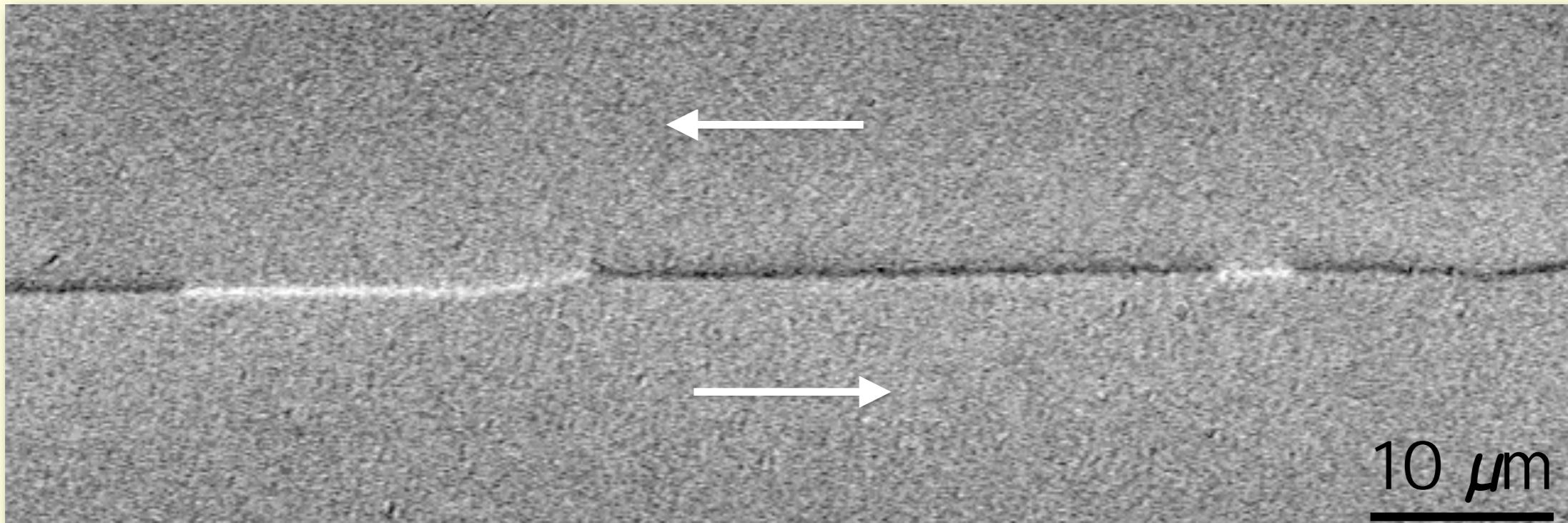
random anisotropy model

→ $\langle K_1 \rangle = 3 \text{ J/m}^3$
average anisotropy

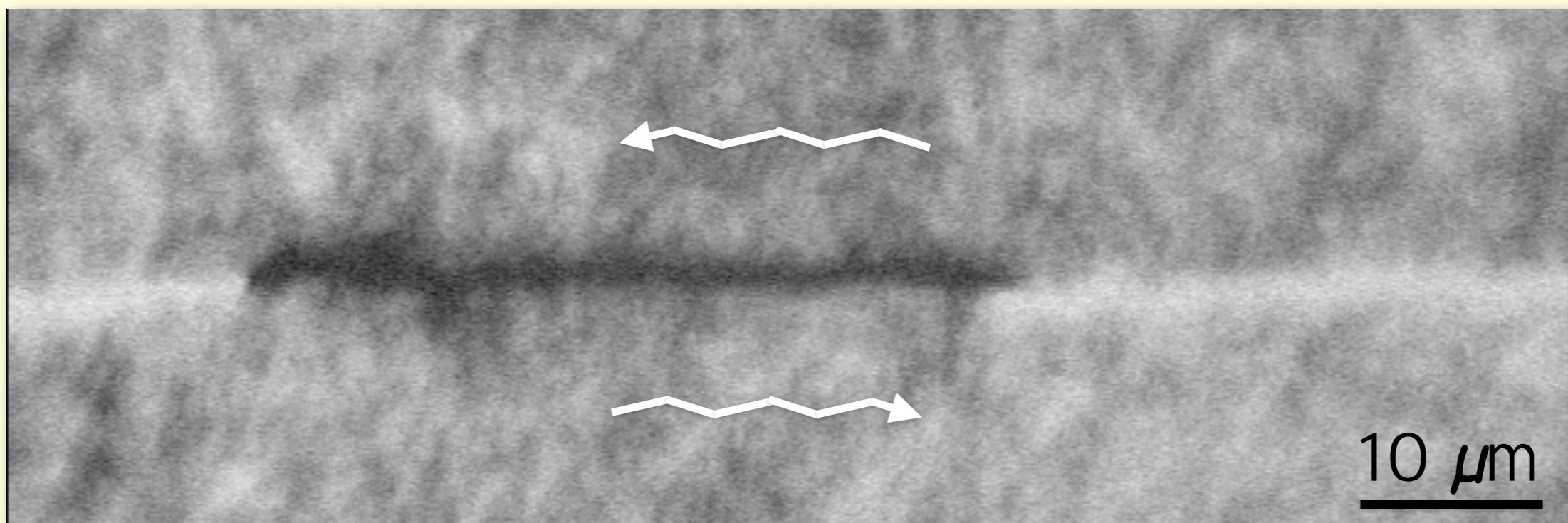
→ $L_{\text{ex}} = \sqrt{A/\langle K_1 \rangle} = 2 \mu\text{m}$
renormalized exchange length



Comparison of domain walls



Fe-Si Goss sheet, surface wall width: 150 nm



nanocrystalline ribbon, surface wall width: several μm

$\text{Fe}_{80}\text{Si}_{20}$:

$$K_1 = 8 \text{ kJ/m}^3$$

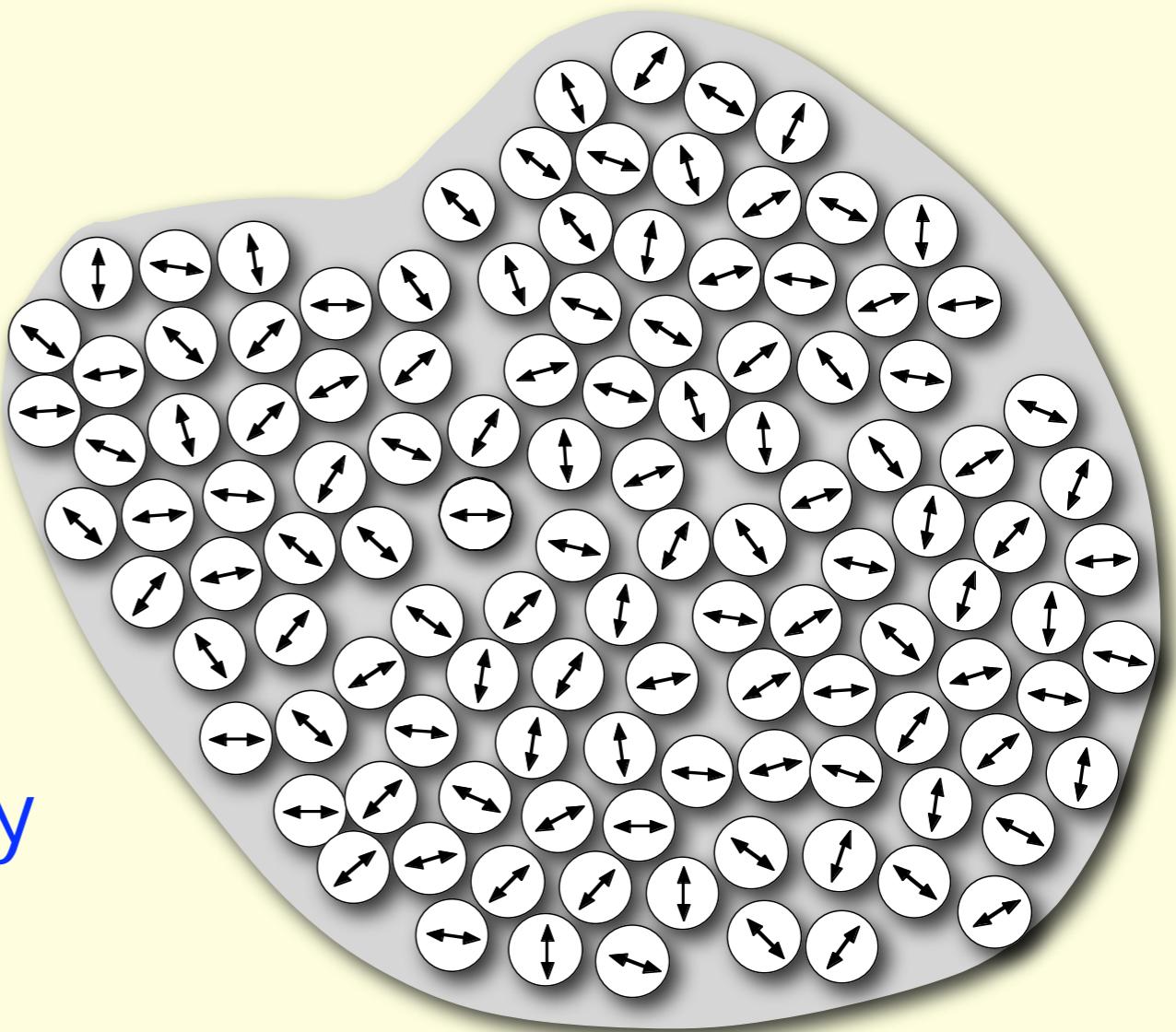
$$A = 10^{-11} \text{ J/m}$$

→ $L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$
exchange length

random anisotropy model

→ $\langle K_1 \rangle = 2.3 \text{ J/m}^3$
average anisotropy

→ $L_{\text{ex}} = \sqrt{A/\langle K_1 \rangle} = 2 \mu\text{m}$
renormalized exchange length



$\text{Fe}_{80}\text{Si}_{20}$:

$$K_1 = 8 \text{ kJ/m}^3$$

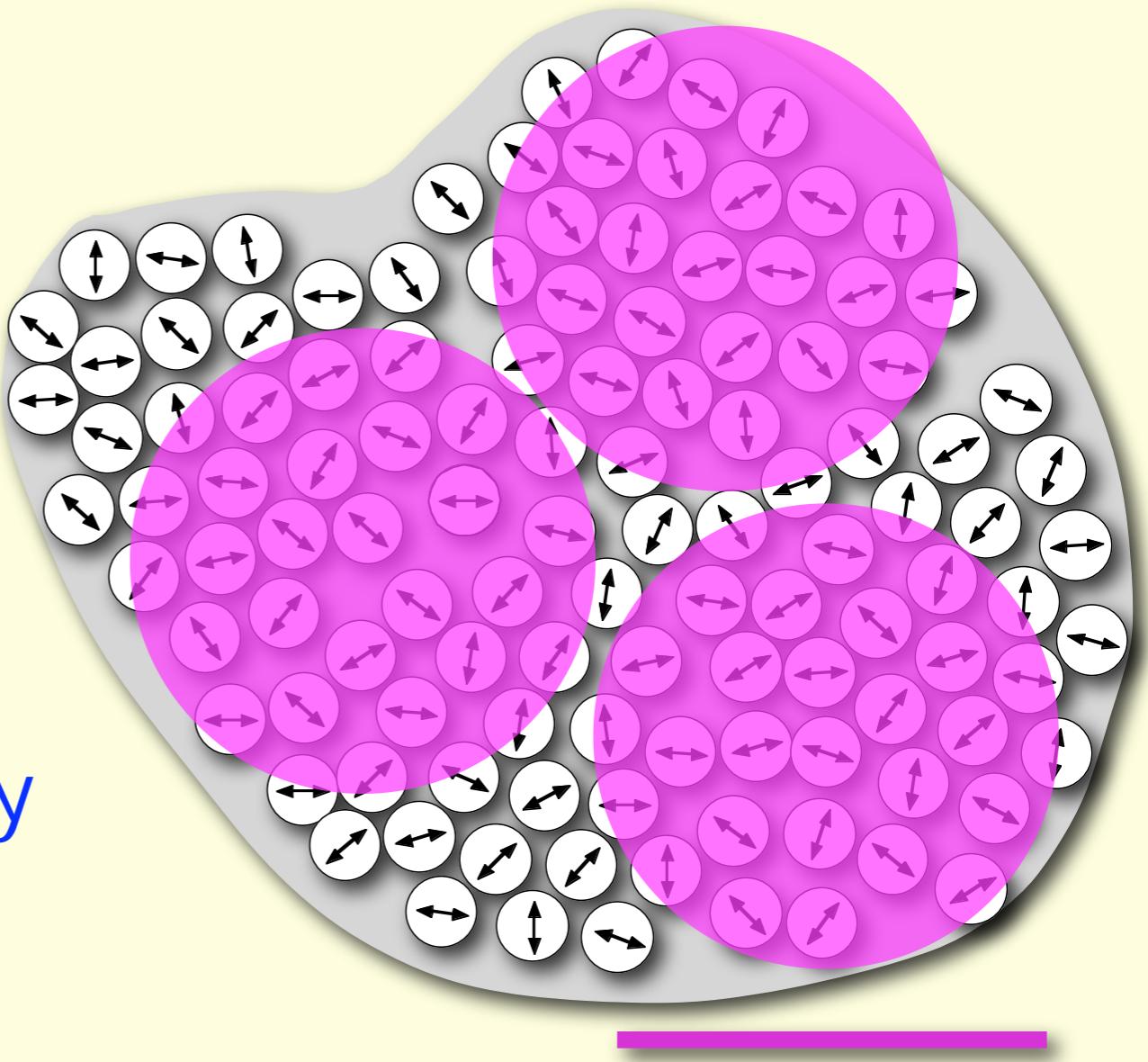
$$A = 10^{-11} \text{ J/m}$$

→ $L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$
exchange length

random anisotropy model

→ $\langle K_1 \rangle = 2.3 \text{ J/m}^3$
average anisotropy

→ $L_{\text{ex}} = \sqrt{A/\langle K_1 \rangle} = 2 \mu\text{m}$
renormalized exchange length



$$L_{\text{ex}} = 2 \mu\text{m}$$

$\text{Fe}_{80}\text{Si}_{20}$:

$$K_1 = 8 \text{ kJ/m}^3$$

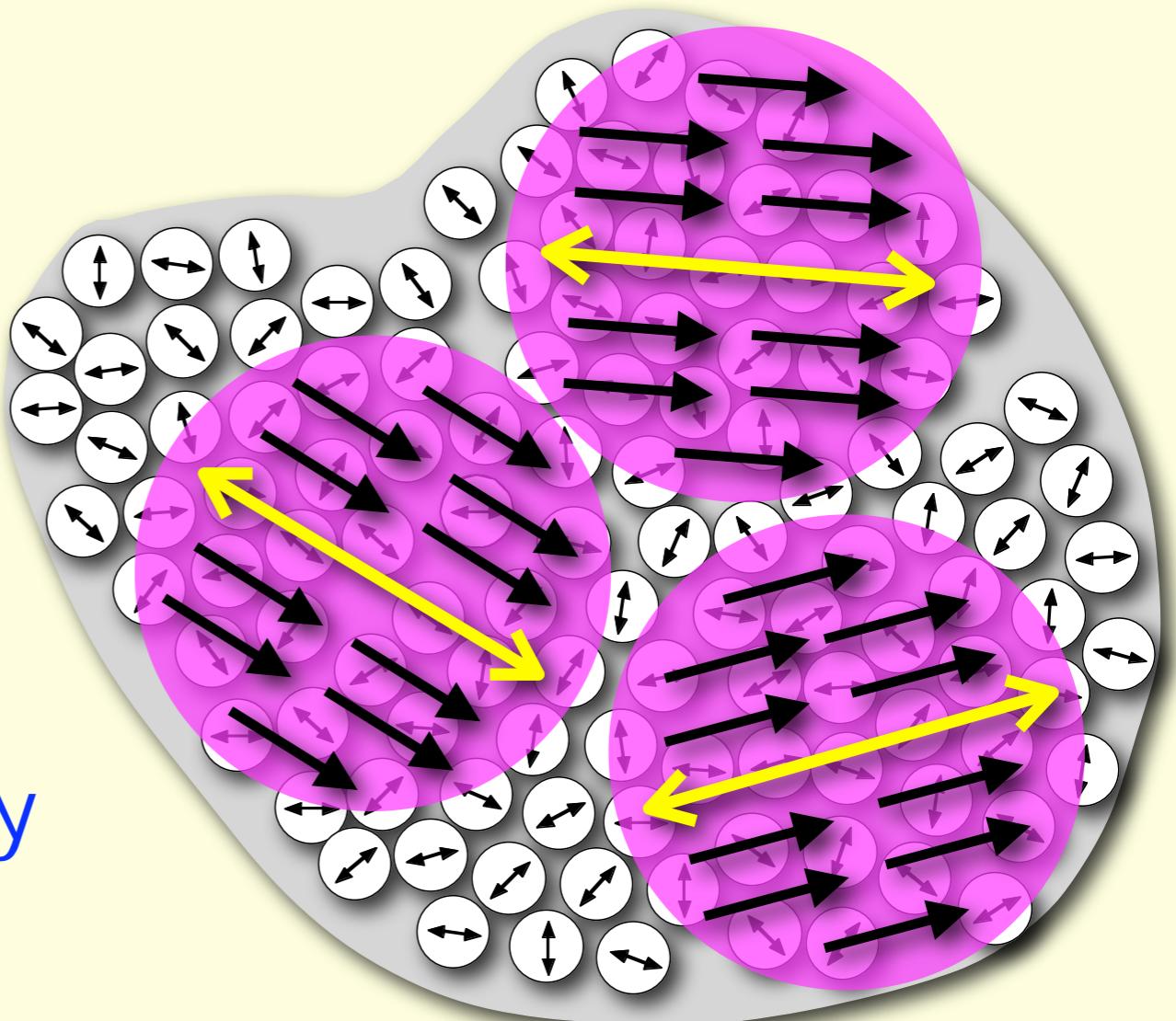
$$A = 10^{-11} \text{ J/m}$$

→ $L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$
exchange length

random anisotropy model

→ $\langle K_1 \rangle = 2.3 \text{ J/m}^3$
average anisotropy

→ $L_{\text{ex}} = \sqrt{A/\langle K_1 \rangle} = 2 \mu\text{m}$
renormalized exchange length



$$L_{\text{ex}} = 2 \mu\text{m}$$

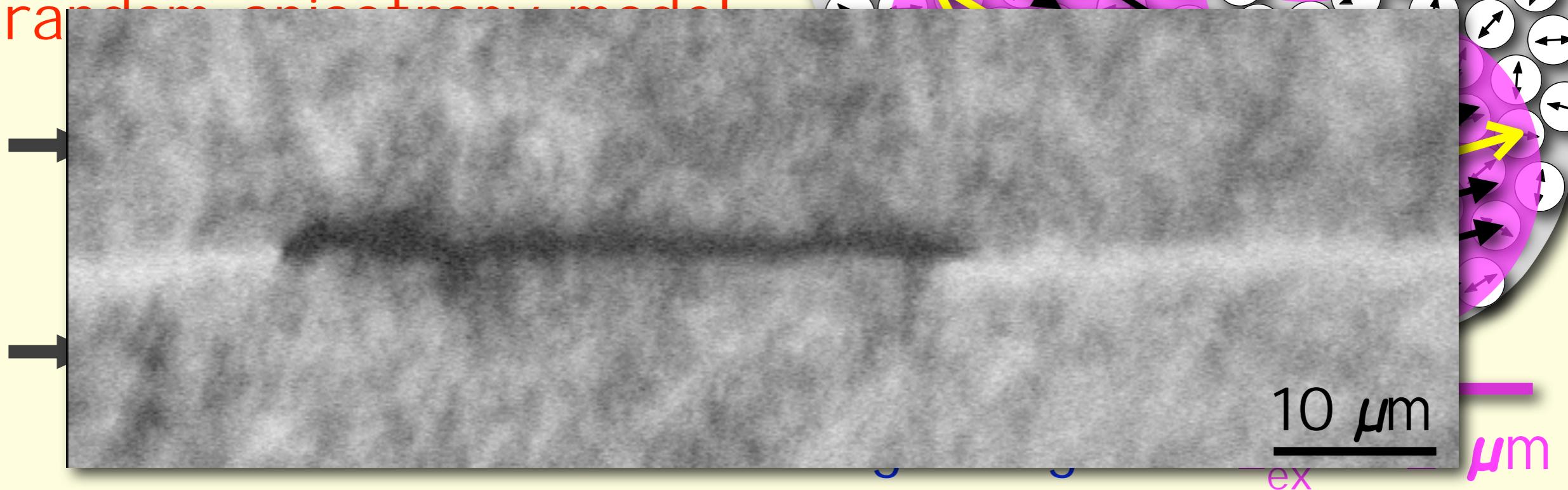
$\text{Fe}_{80}\text{Si}_{20}$:

$$K_1 = 8 \text{ kJ/m}^3$$

$$A = 10^{-11} \text{ J/m}$$

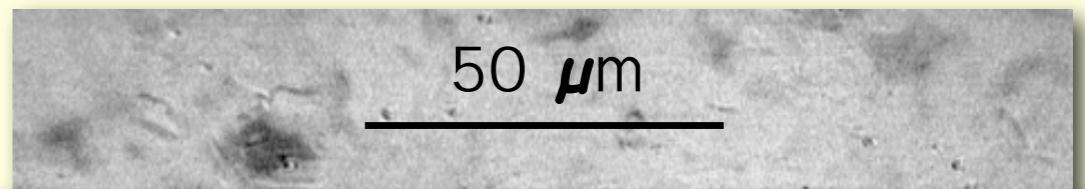
→ $L_{\text{ex}} = \sqrt{A/K_1} = 35 \text{ nm}$
exchange length

random anisotropy model



coarse-grained material
(grain size: 30 μm)

fine-grained material
(grain size: 13 μm)

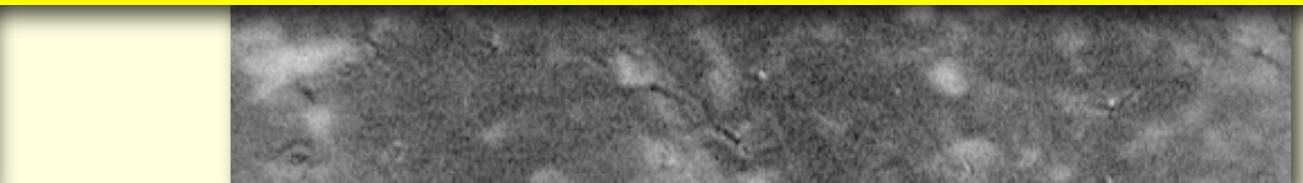
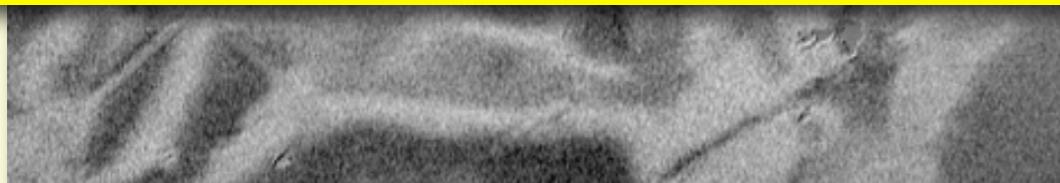


Permalloy:

K_{cryst} much smaller than in FeSi

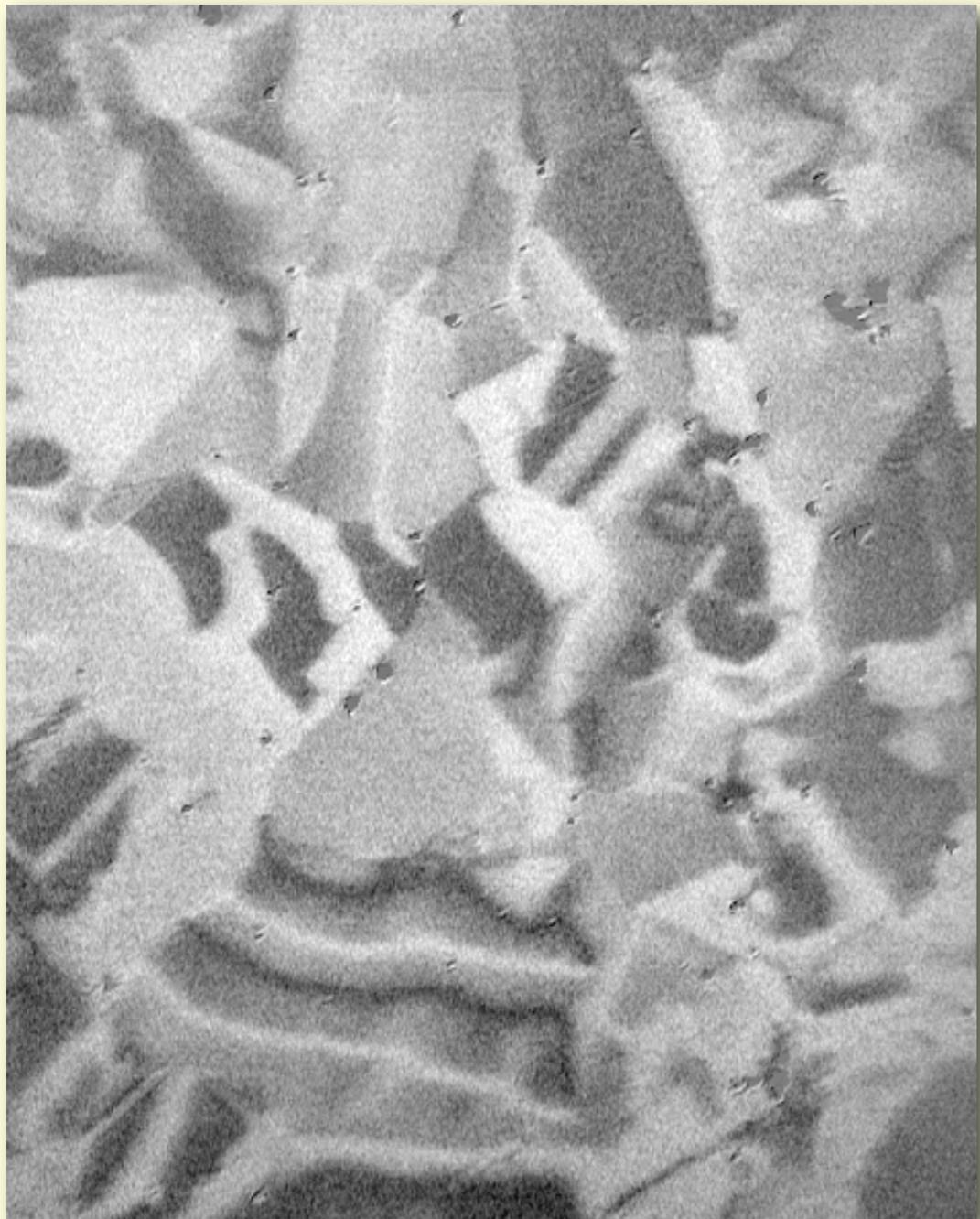


much larger correlation volume

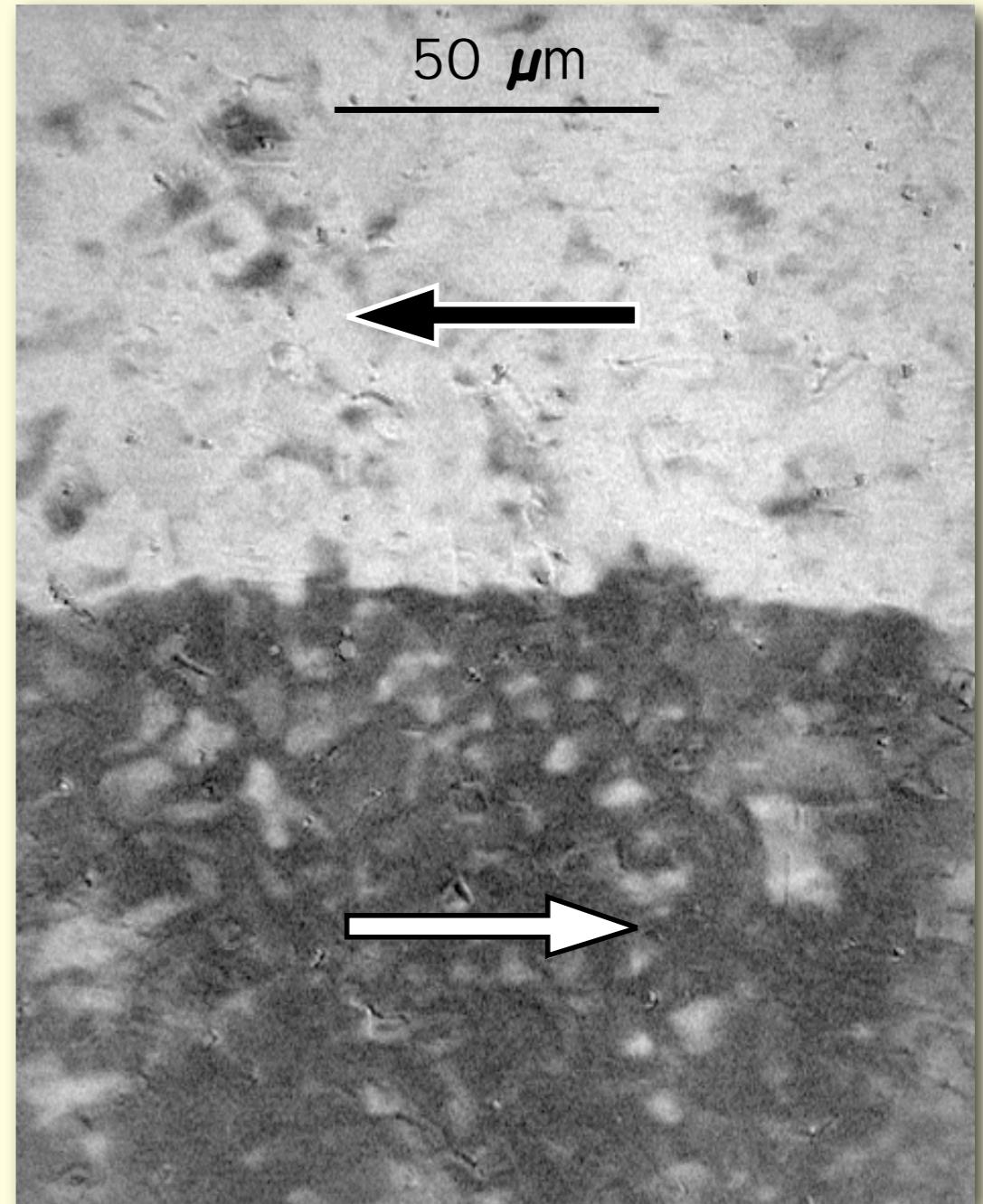


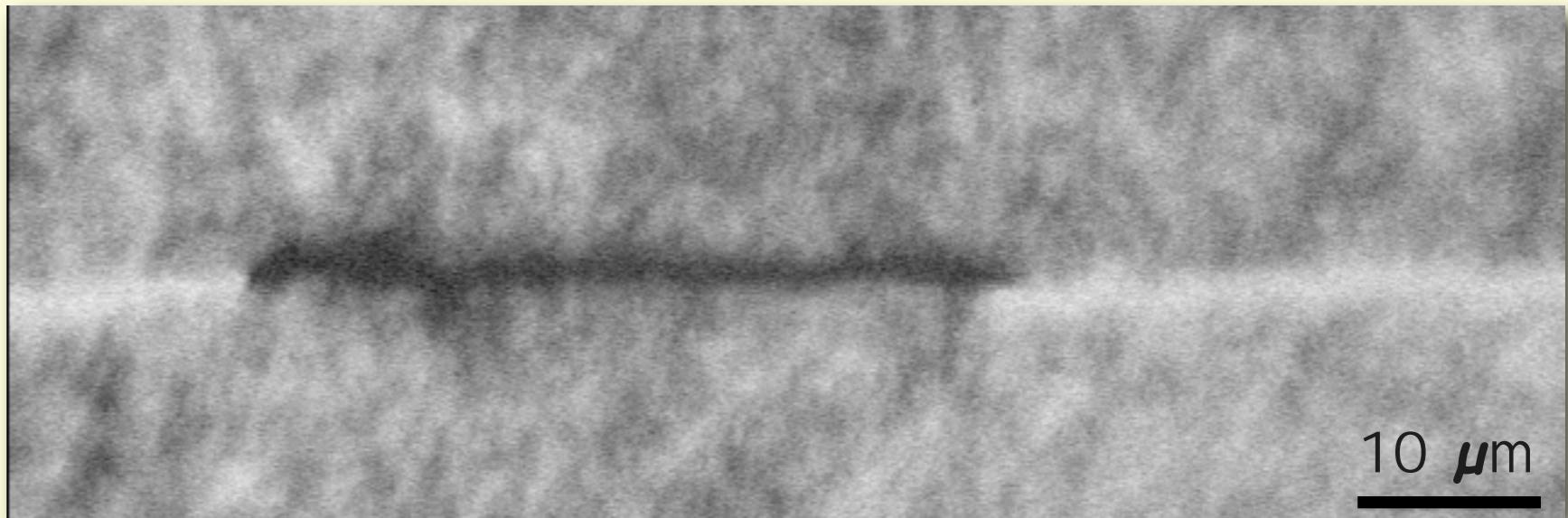
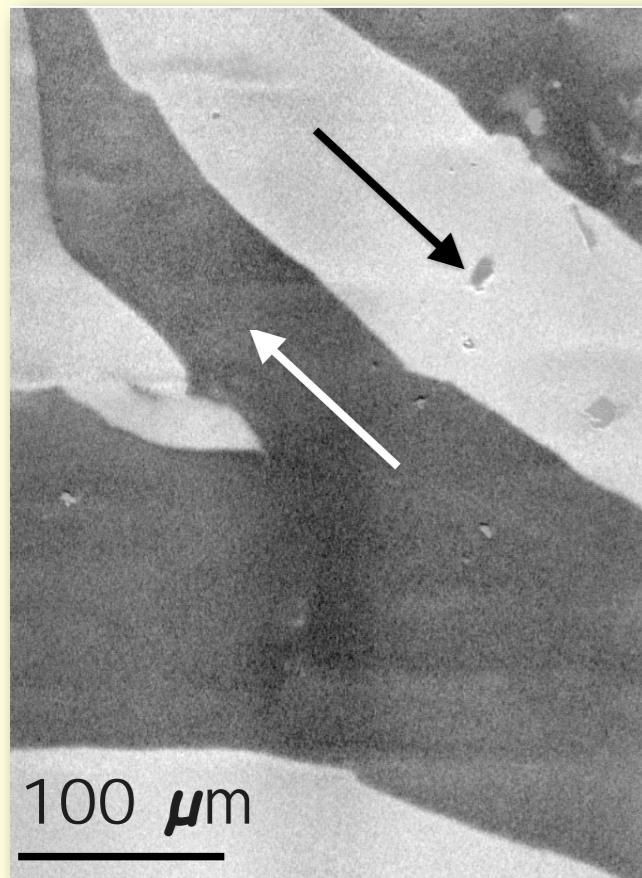
Random anisotropy effect in Permalloy

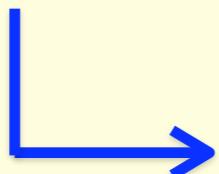
coarse-grained material
(grain size: 30 μm)



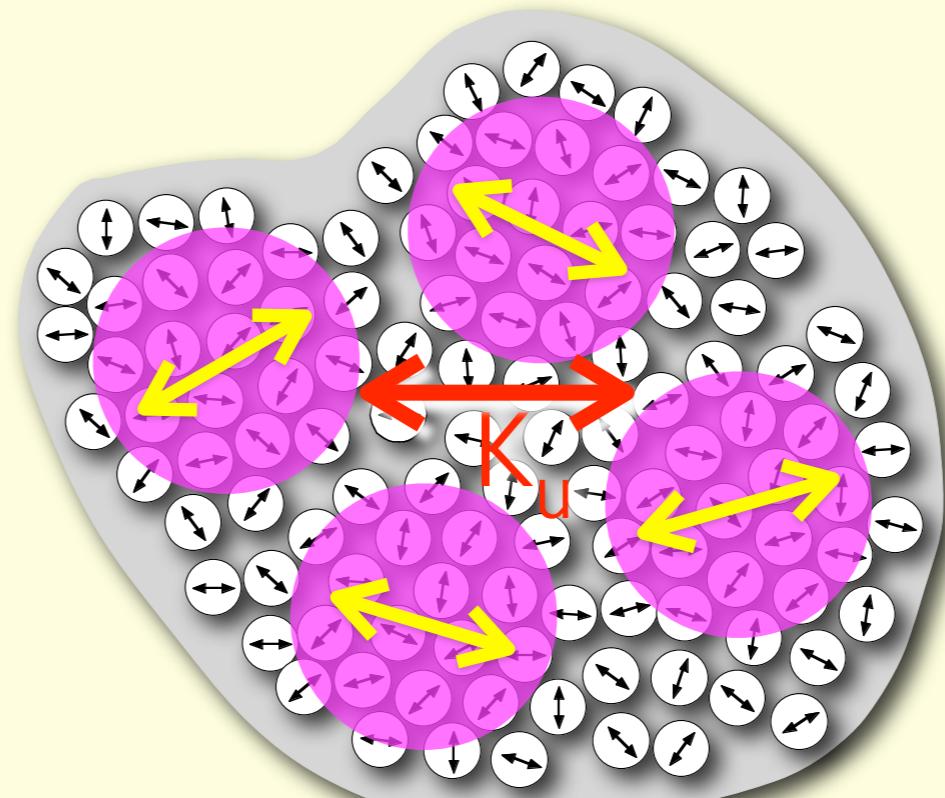
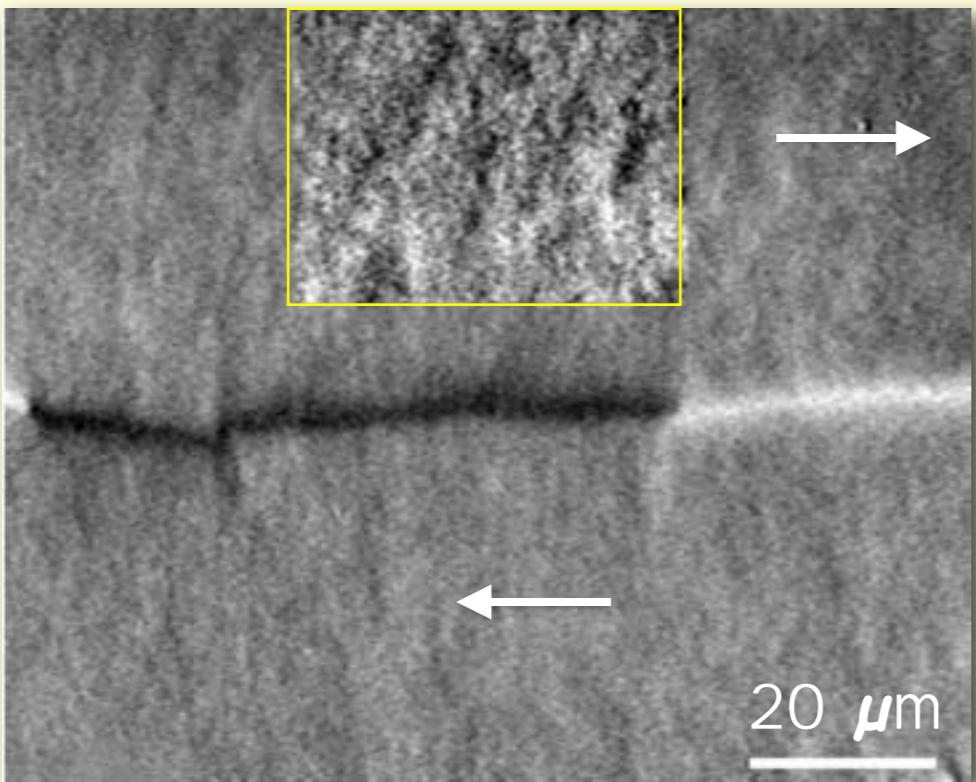
fine-grained material
(grain size: 13 μm)



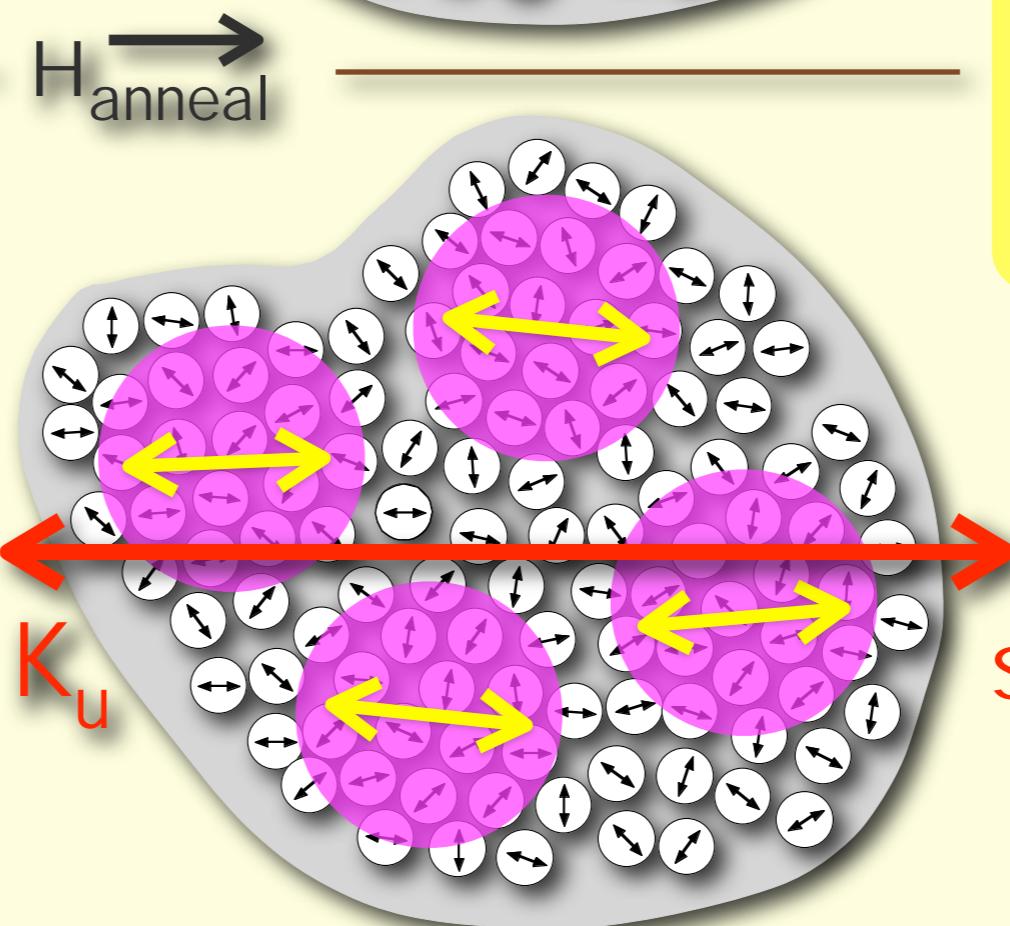
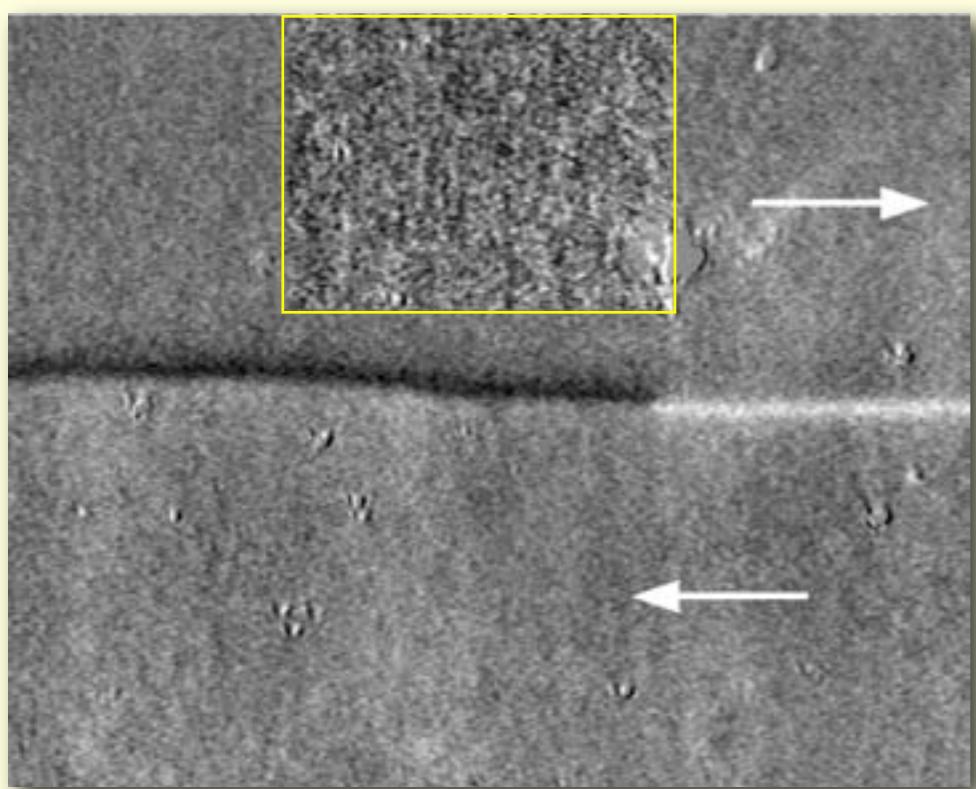


- random anisotropy $\langle K_1 \rangle$: modulated on scale of renormalized exchange length, $\langle K_1 \rangle \approx 3 \text{ J/m}^3$
 - induced anisotropy K_u : uniform on large scale, $K_u \approx 3 - 30 \text{ J/m}^3$
-  interplay

Interplay random/induced anisotropy



low induced
anisotropy
($K_u = 3 \text{ J/m}^3$)

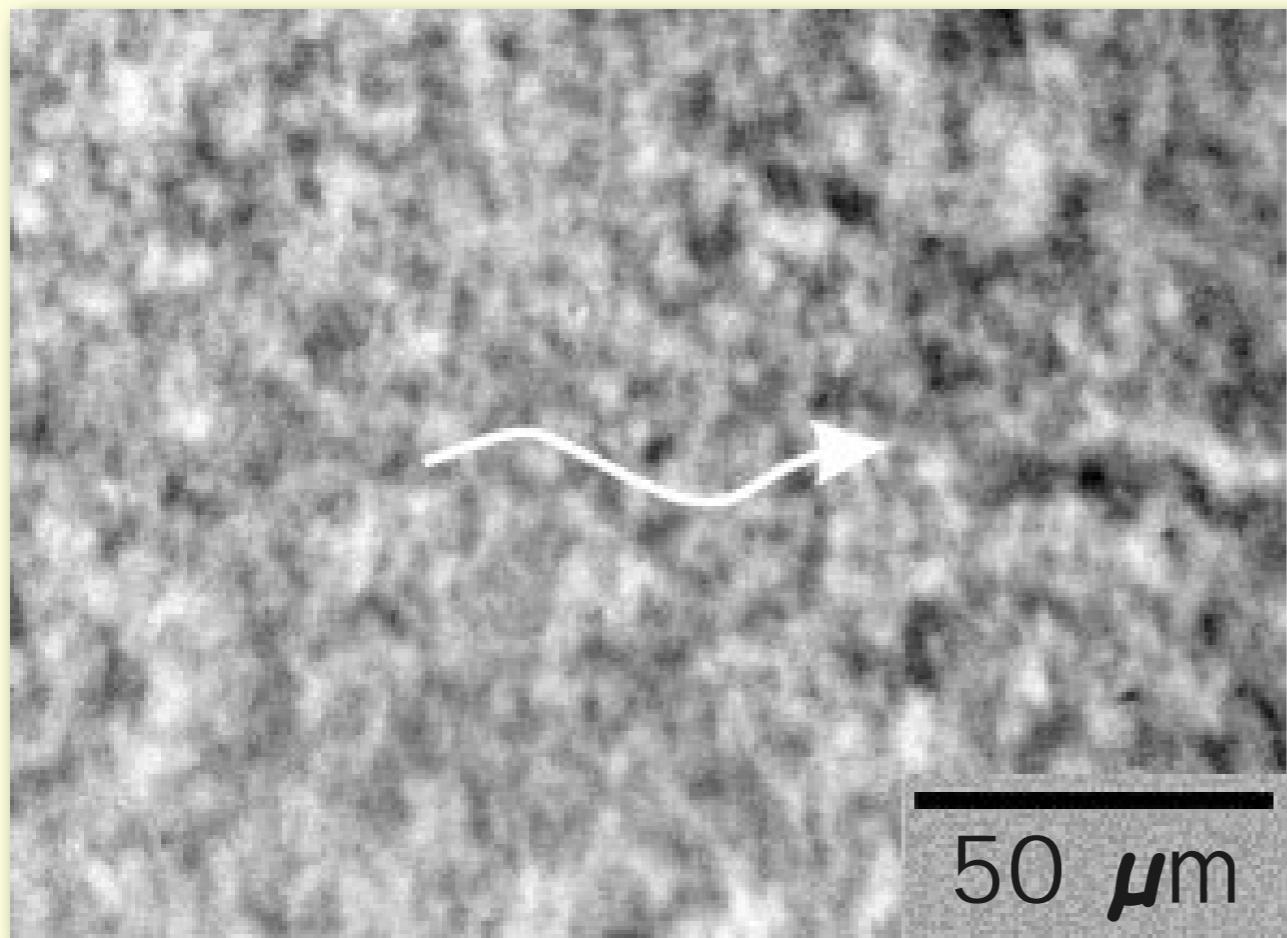


$$L_{\text{ex}} = \sqrt{A/\langle K \rangle}$$

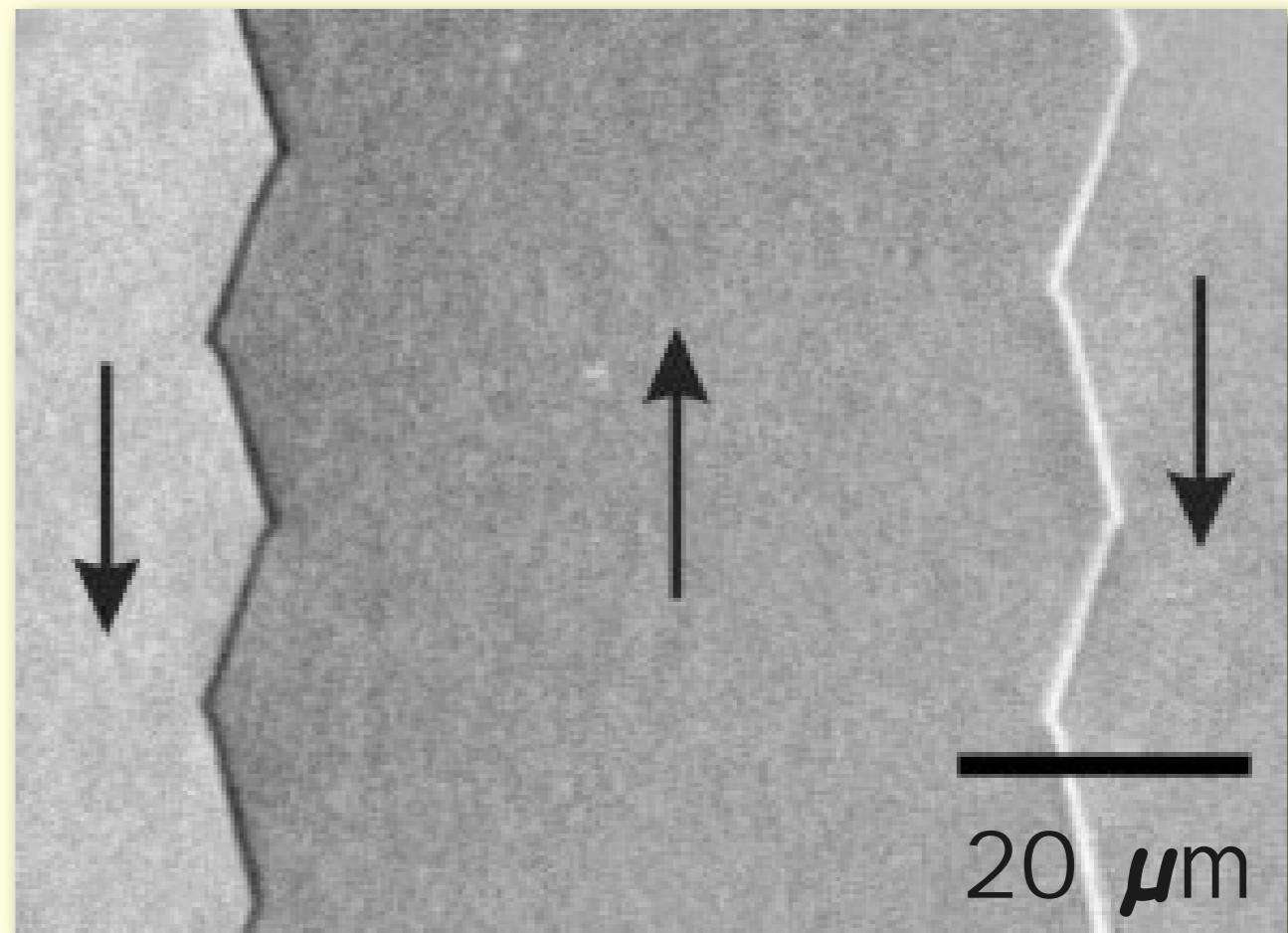
$$\langle K \rangle = \sqrt{\langle K_1^2 \rangle + K_u^2}$$

\uparrow
 3 J/m^3

strong induced
anisotropy
($K_u = 30 \text{ J/m}^3$)



low induced
anisotropy



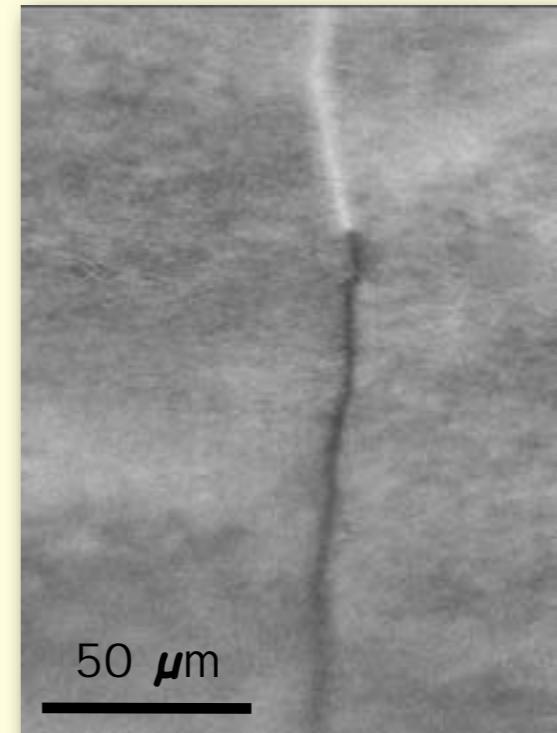
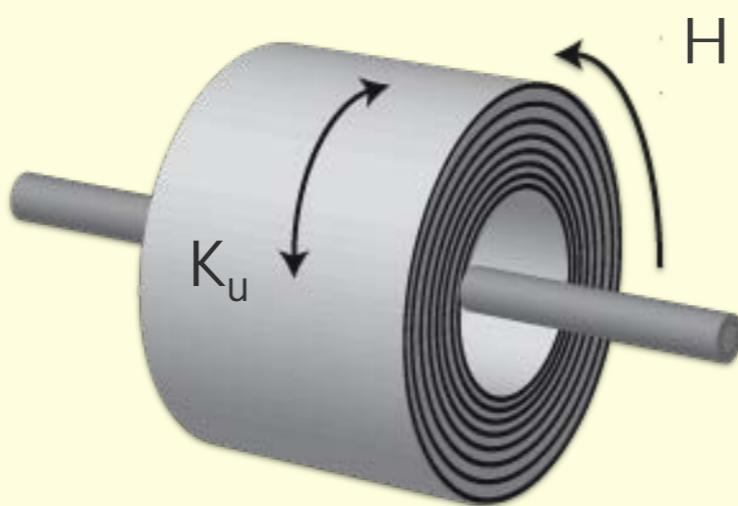
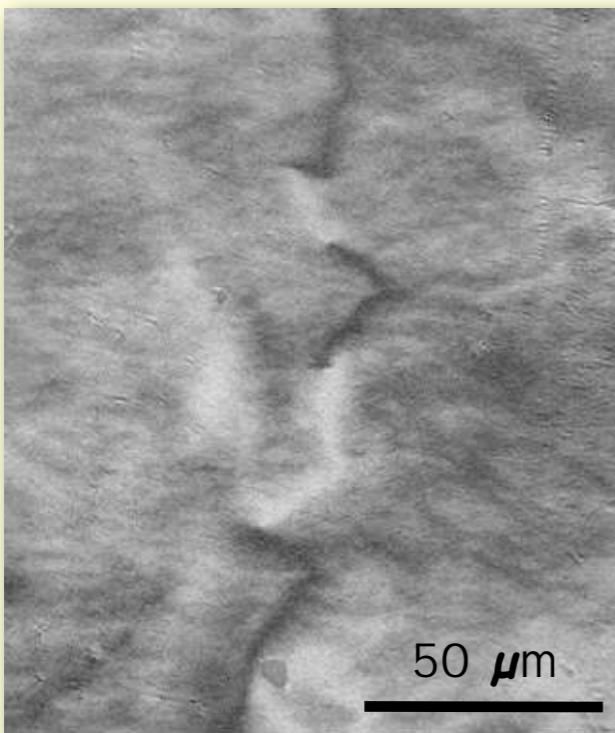
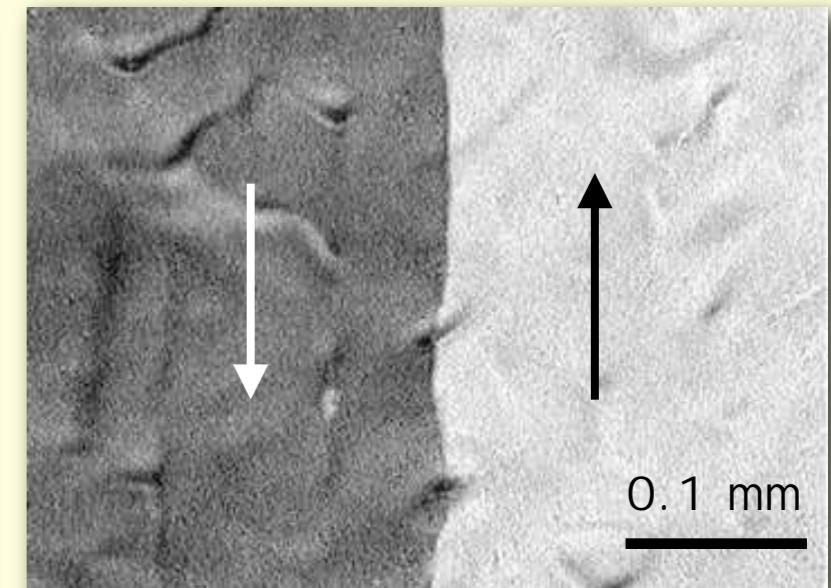
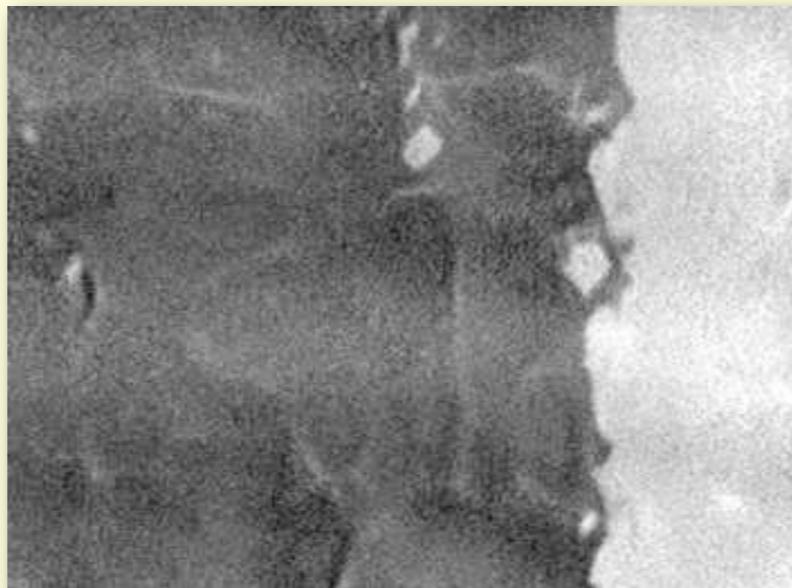
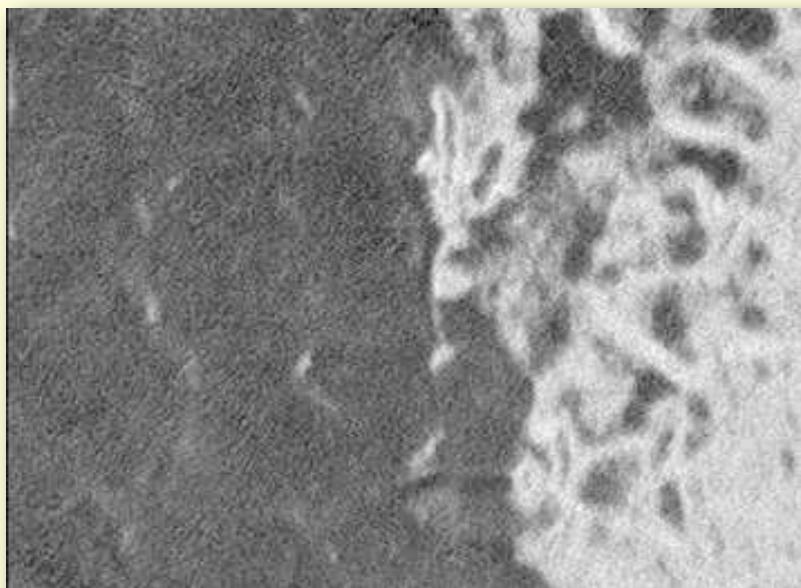
strong creep-induced
anisotropy

Nanocryst. core with longitudinal anisotropy

$K_u = 5 \text{ J/m}^3$
(weak)

$K_u = 10 \text{ J/m}^3$
(moderate)

$K_u = 29 \text{ J/m}^3$
(strong)



Nanocryst. core with transverse anis.

— decreasing induced transverse anisotropy →

$$K_u = 33 \text{ J/m}^3$$

$$\mu_{15} = 22.000$$

$$7.7 \text{ J/m}^3$$

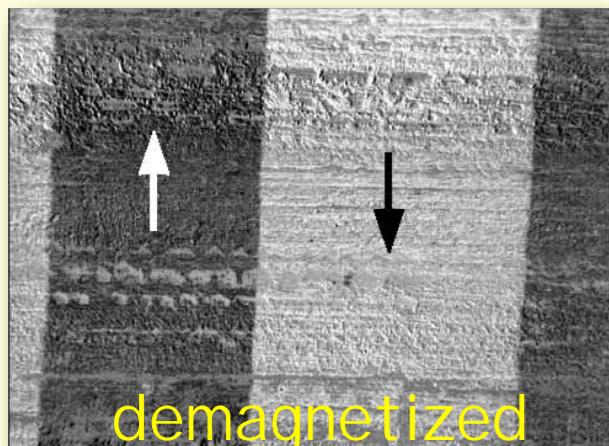
$$86.200$$

$$2.3 \text{ J/m}^3$$

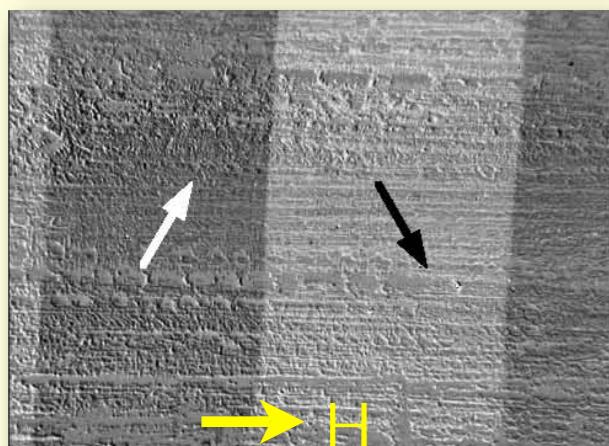
$$274.500$$

$$0.6 \text{ J/m}^3$$

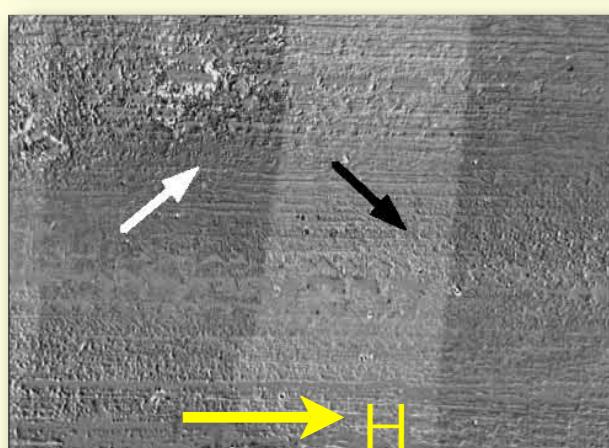
$$559.900$$



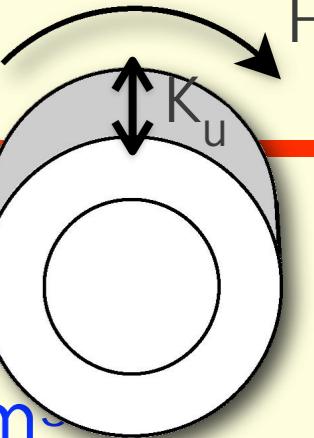
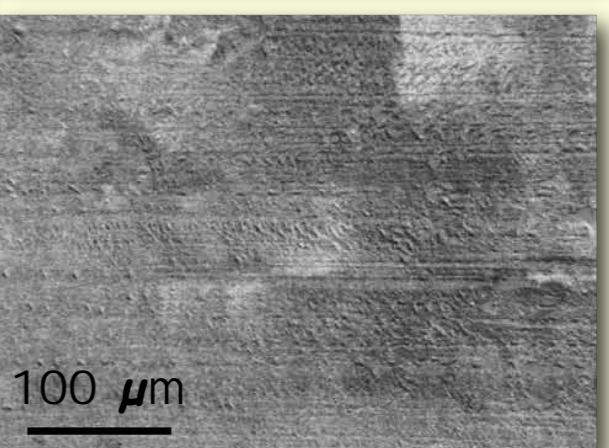
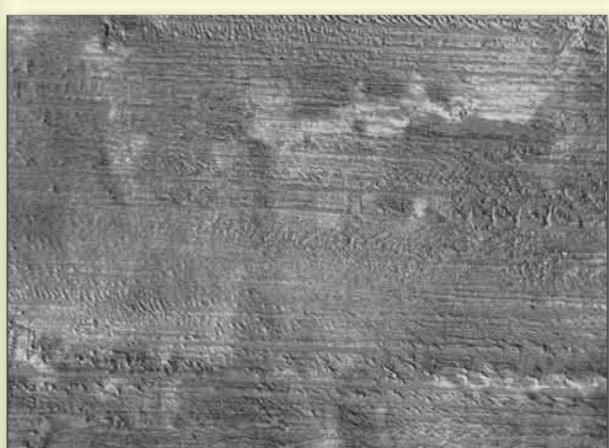
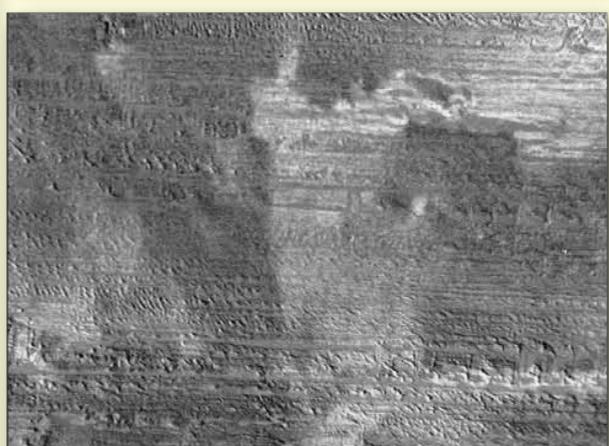
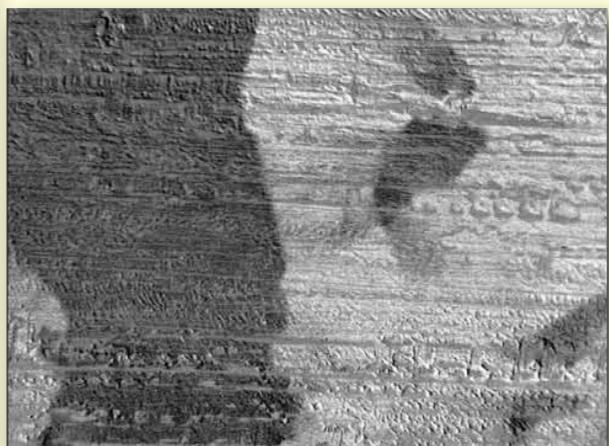
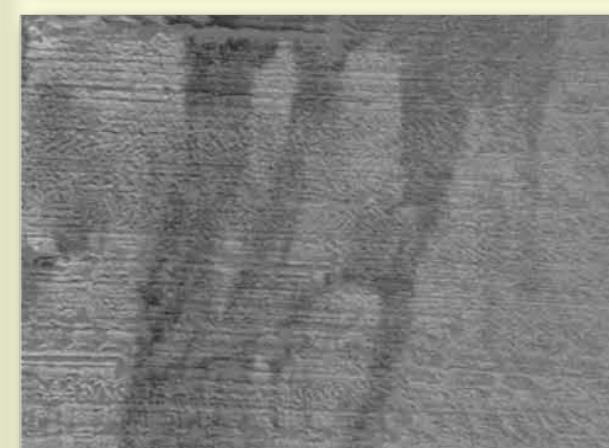
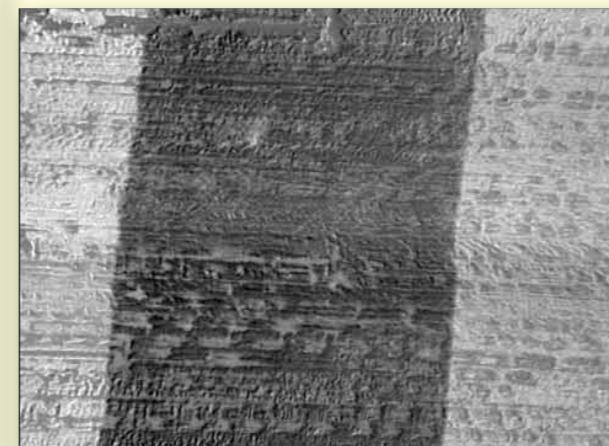
demagnetized



→ H



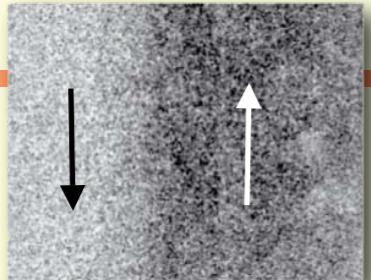
→ H



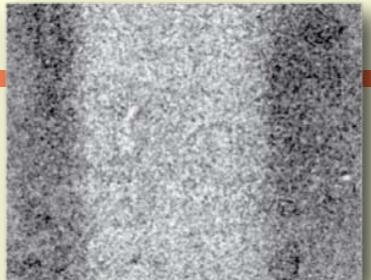
anisotropy

$K_u = 29 \text{ J/m}^3$
strong

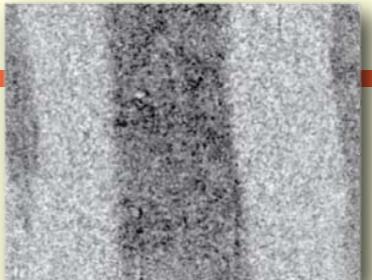
50 Hz



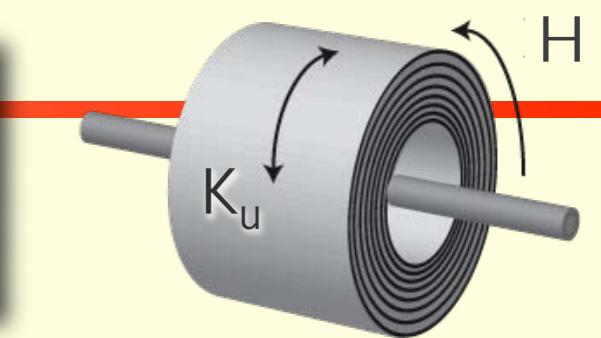
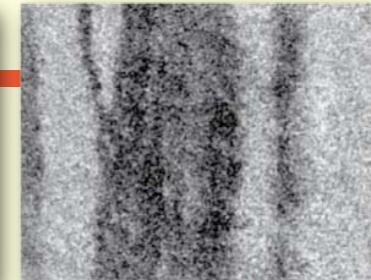
1 kHz



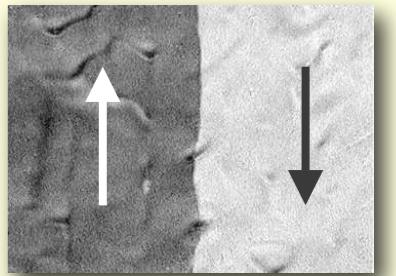
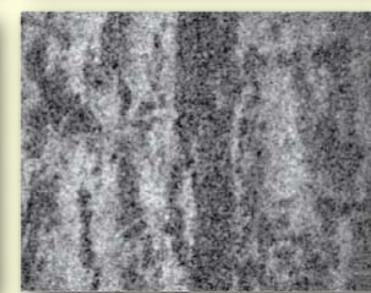
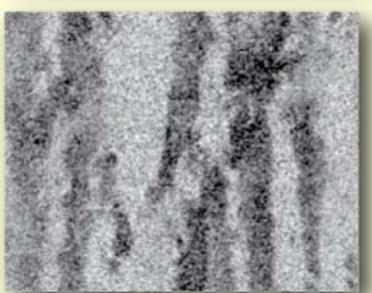
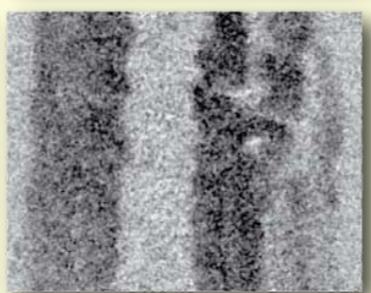
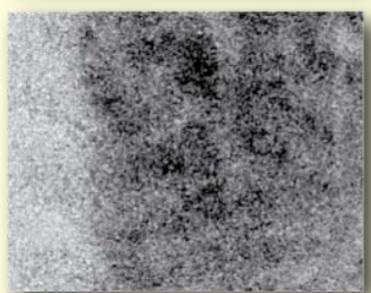
5 kHz



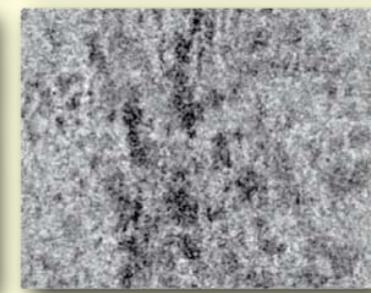
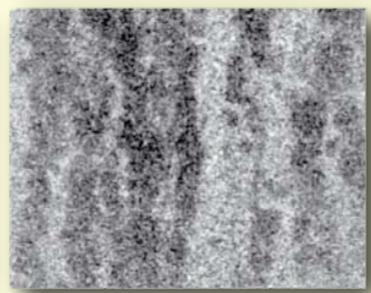
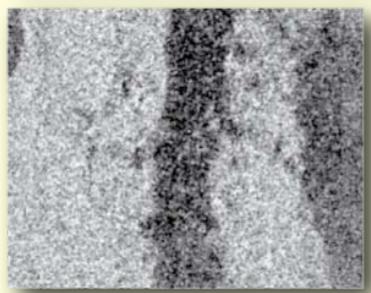
10 kHz



$K_u = 10 \text{ J/m}^3$
moderate

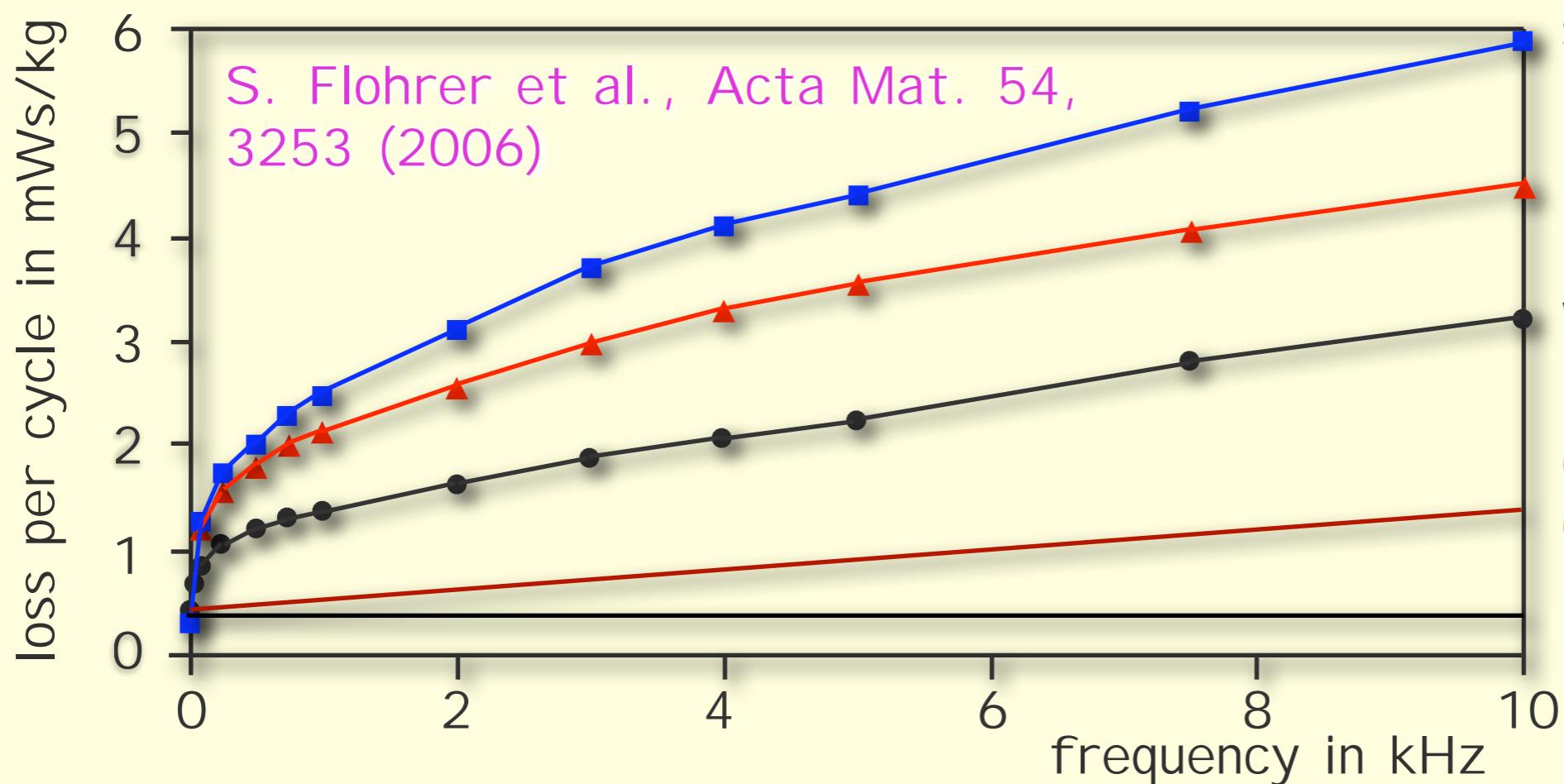


$K_u = 5 \text{ J/m}^3$
weak



0.2 mm
A horizontal black line representing a scale bar of 0.2 mm.

strong K_u
moderate K_u
weak K_u
classical eddy current loss
hysteresis loss

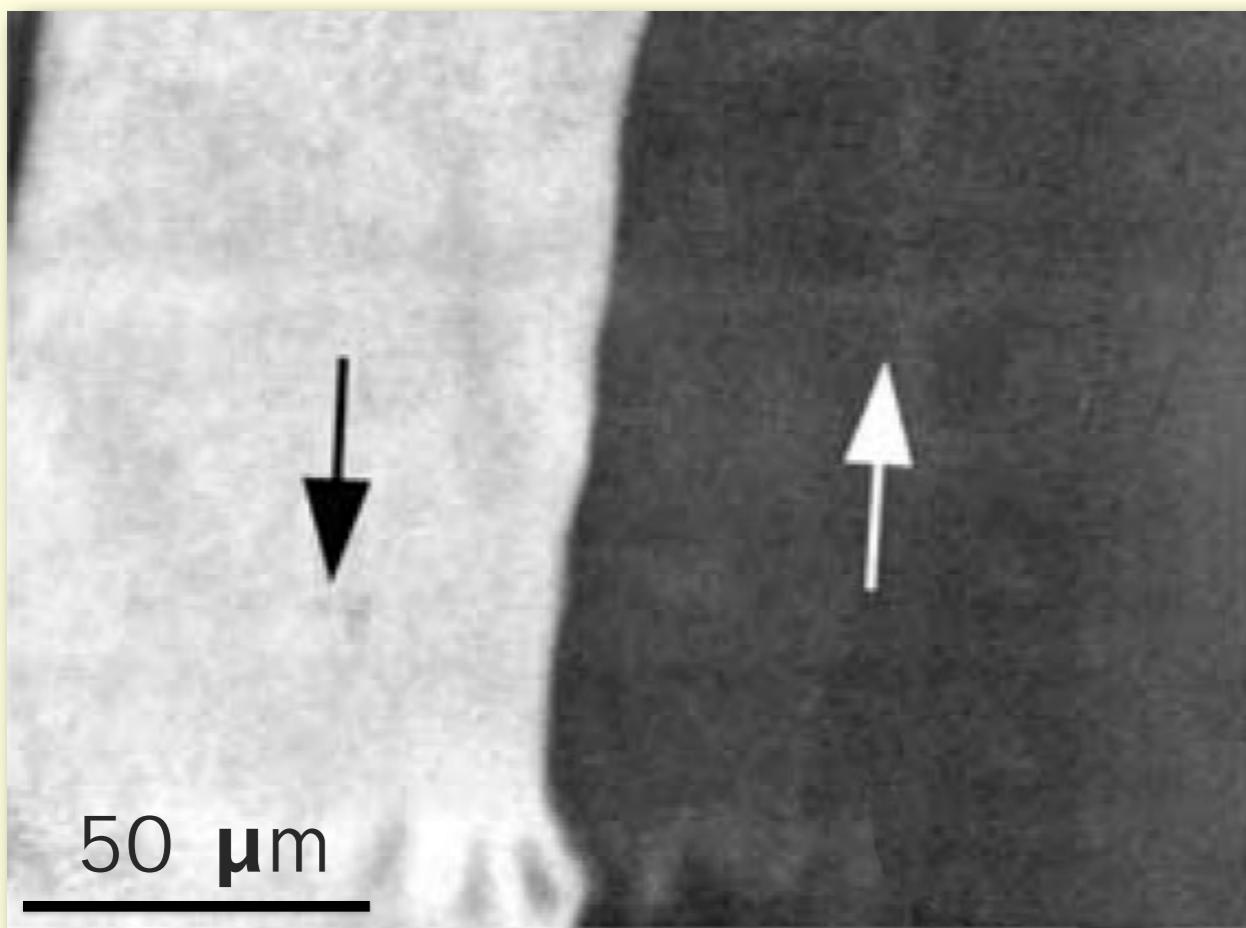


Heating above T_{Curie} of amorphous phase

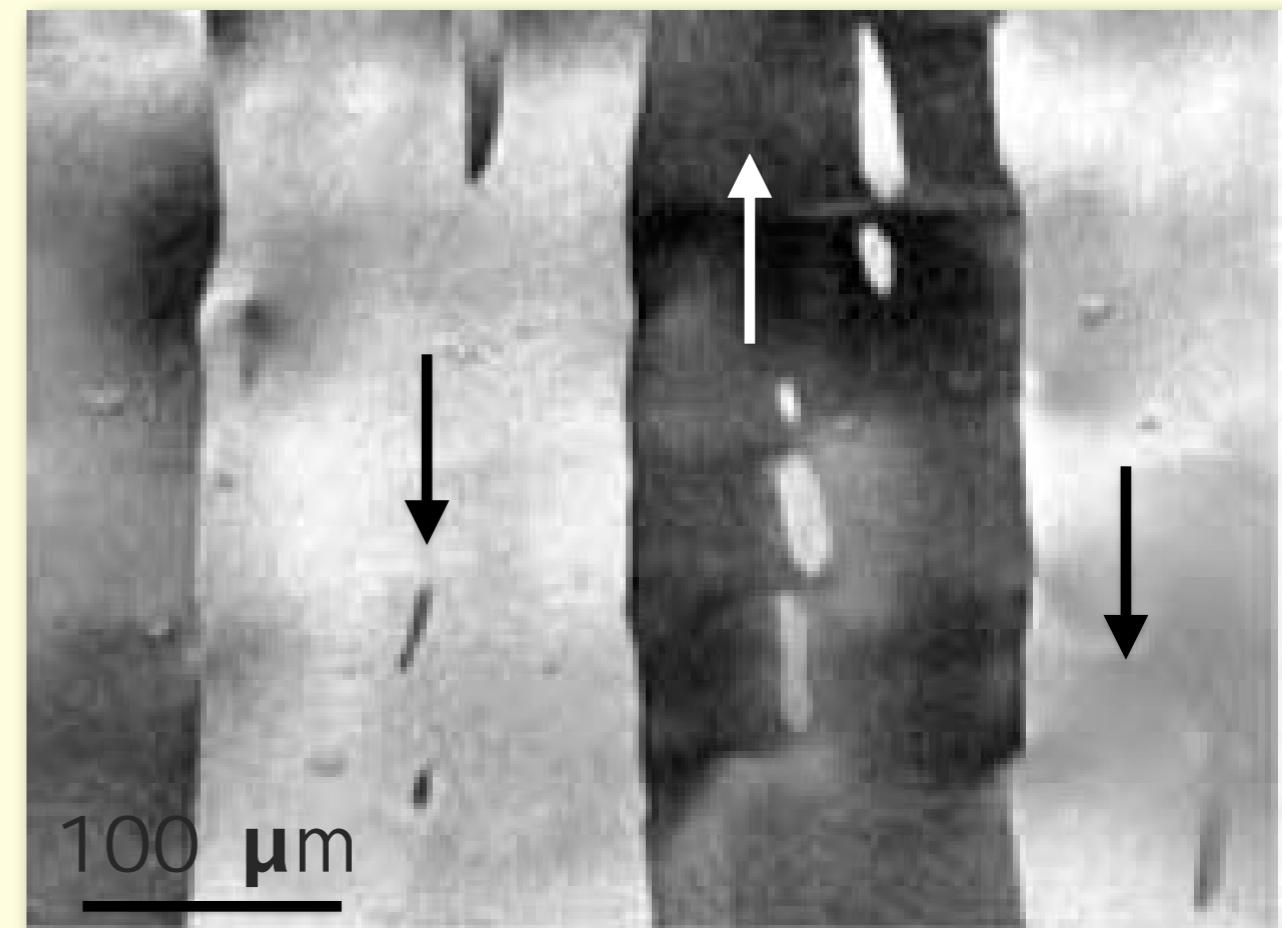
$$\langle K_1 \rangle \sim \frac{K_1}{\sqrt{N}}$$

N: number of grains within correlation volume

low induced anisotropy
($K_u = 3 \text{ J/m}^3$)



strong induced anisotropy
($K_u = 30 \text{ J/m}^3$)



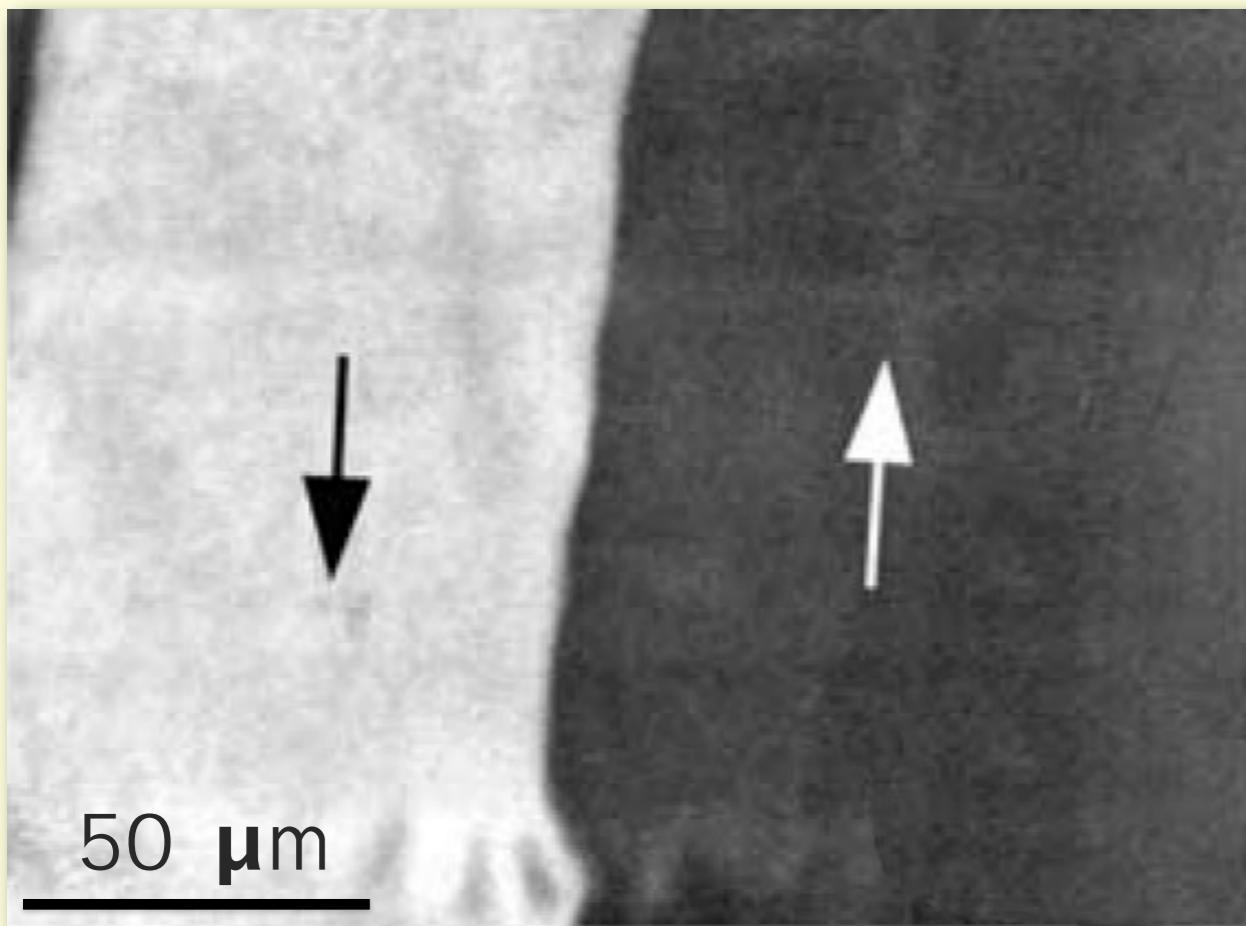
room temperature

Heating above T_{Curie} of amorphous phase

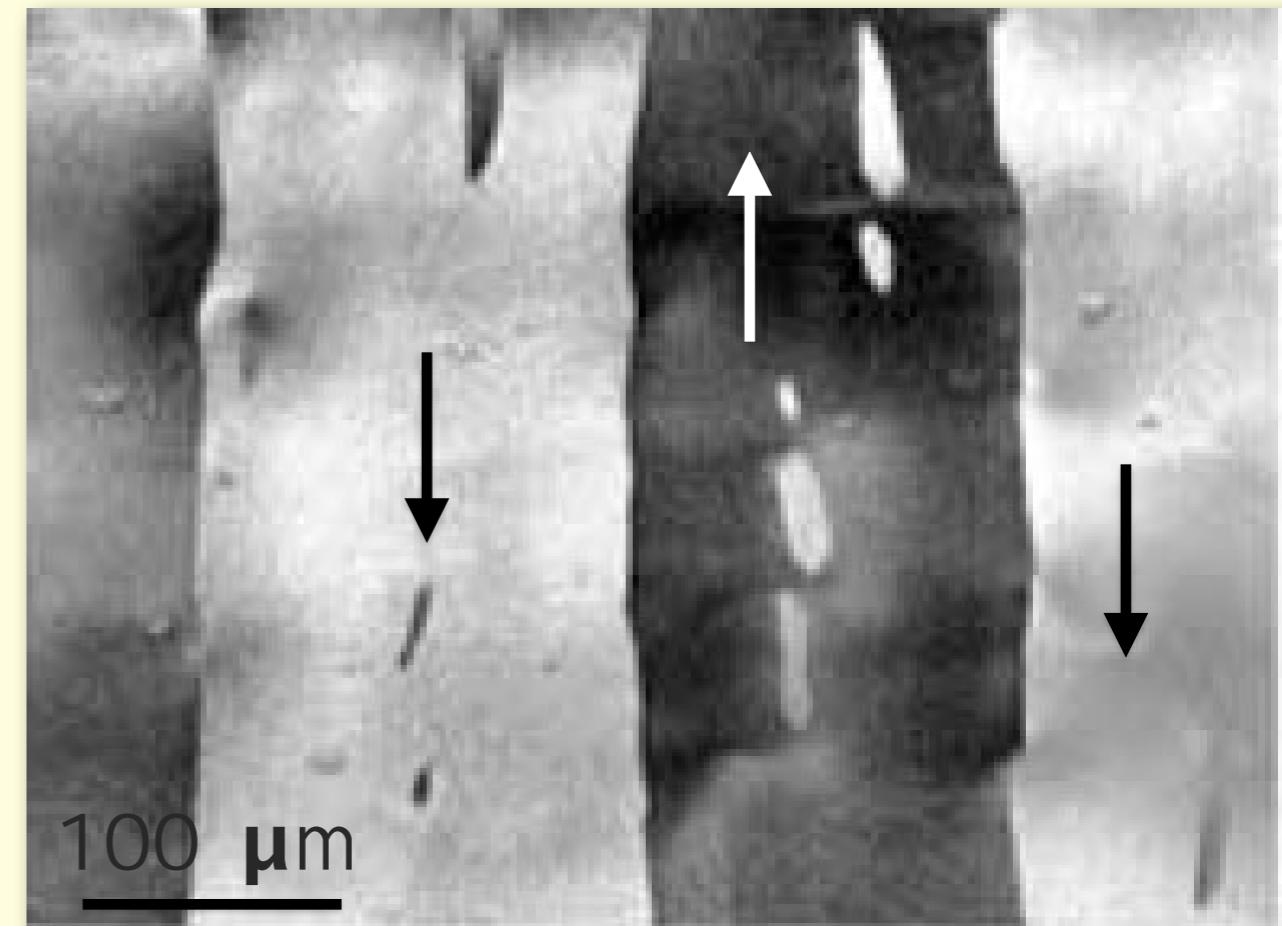
$$\langle K_1 \rangle \sim \frac{K_1}{\sqrt{N}}$$

N: number of grains within correlation volume

low induced anisotropy
($K_u = 3 \text{ J/m}^3$)



strong induced anisotropy
($K_u = 30 \text{ J/m}^3$)

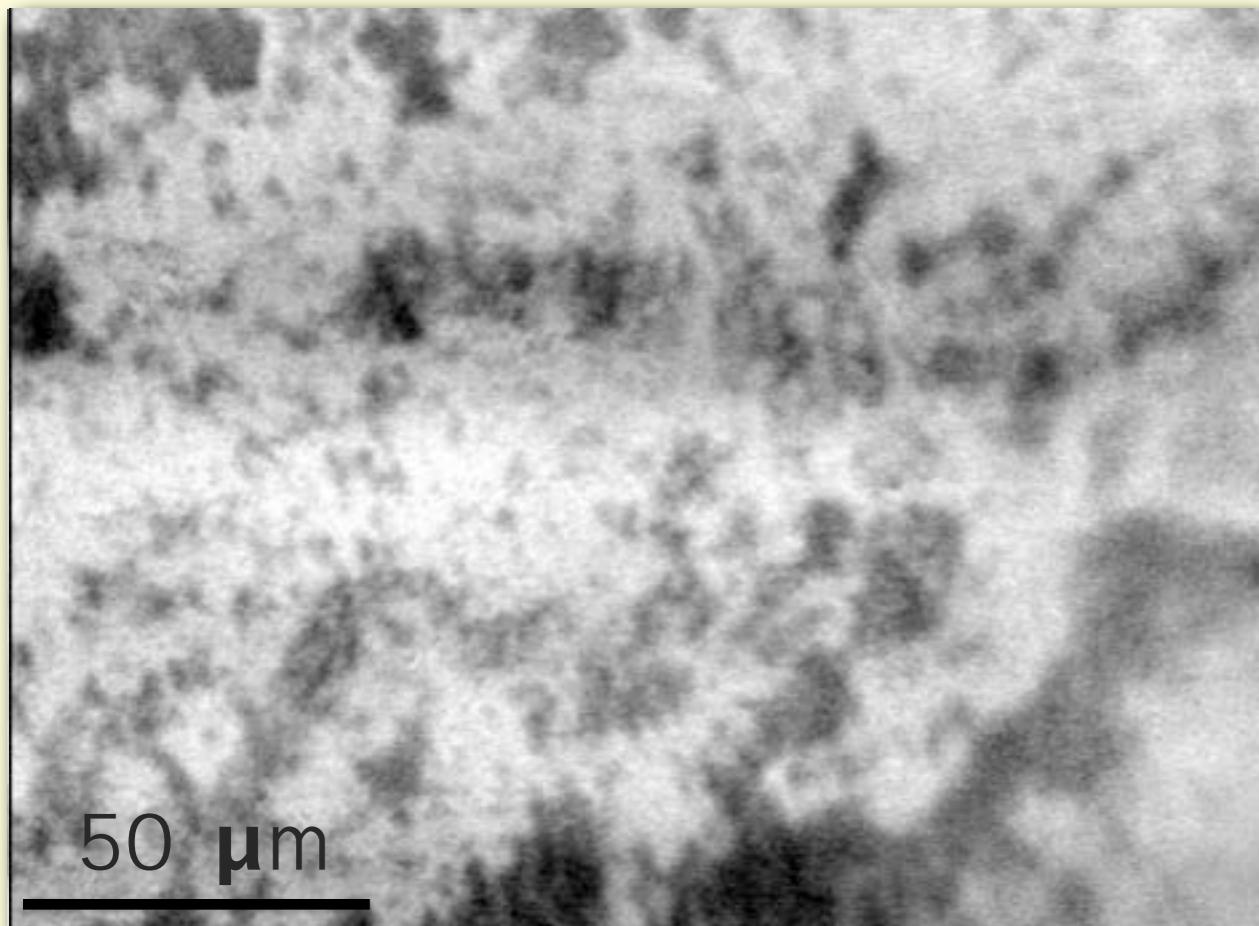


Heating above T_{Curie} of amorphous phase

$$\langle K_1 \rangle \sim \frac{K_1}{\sqrt{N}}$$

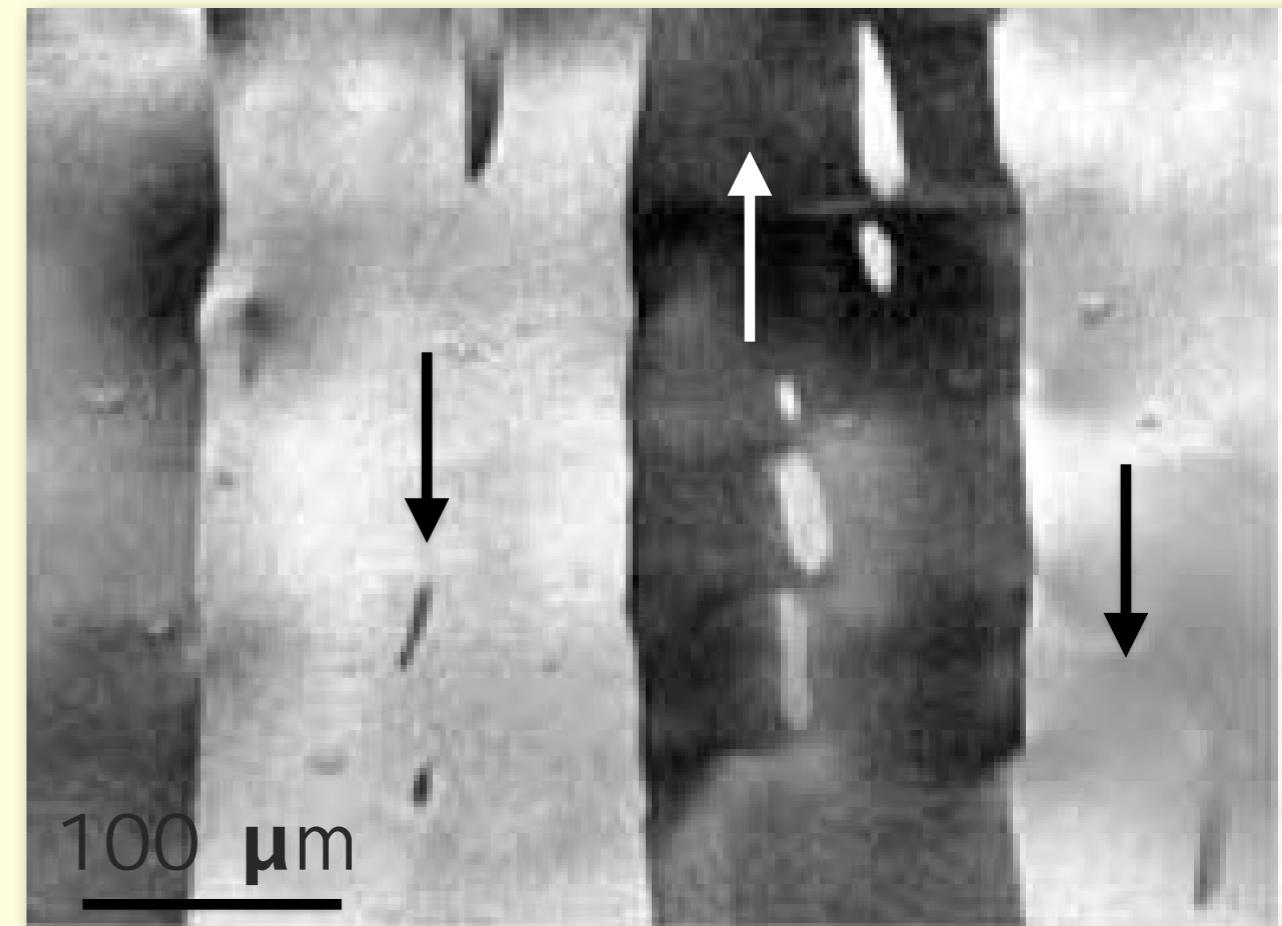
N: number of grains within correlation volume

low induced anisotropy
($K_u = 3 \text{ J/m}^3$)



350°C

strong induced anisotropy
($K_u = 30 \text{ J/m}^3$)

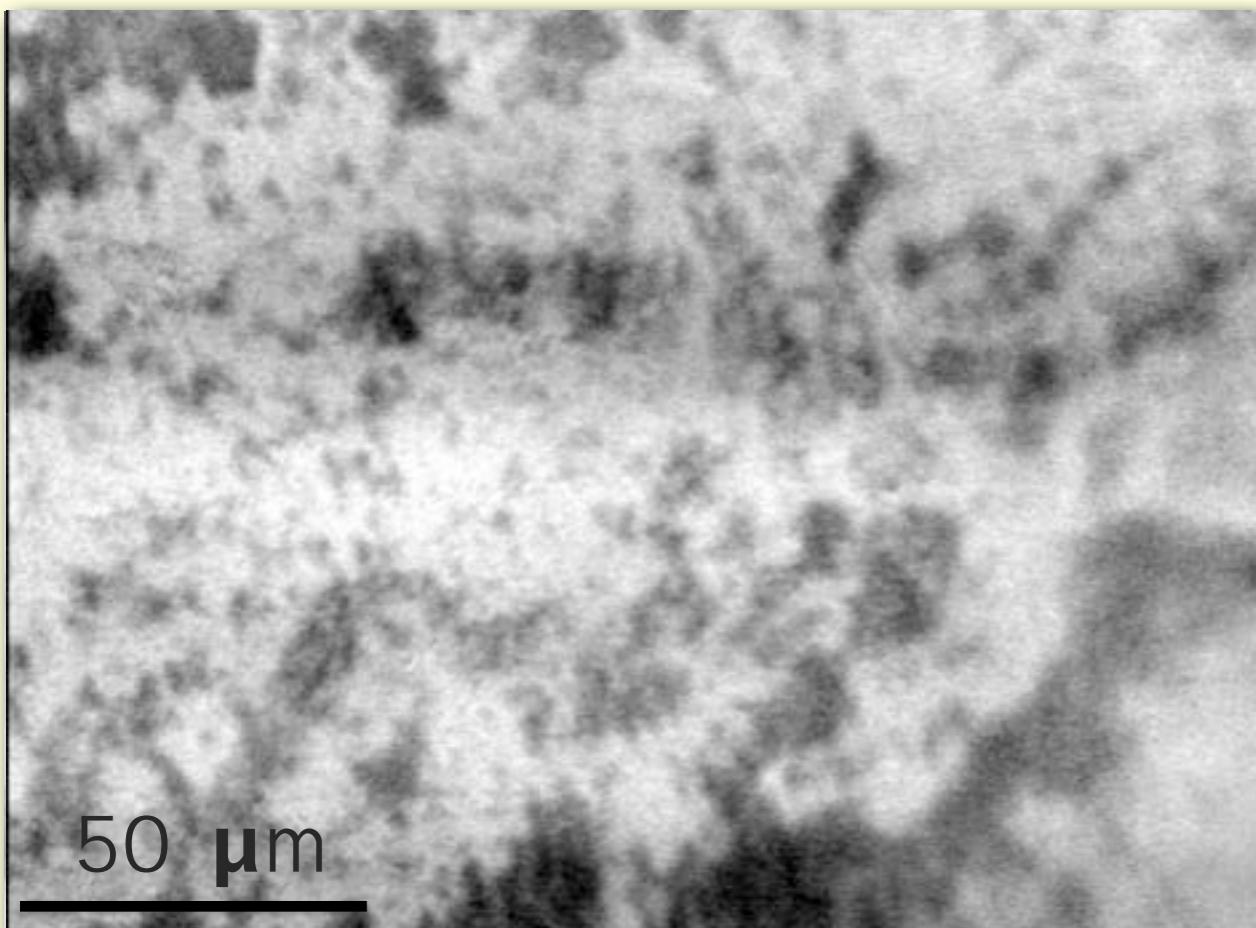


Heating above T_{Curie} of amorphous phase

$$\langle K_1 \rangle \sim \frac{K_1}{\sqrt{N}}$$

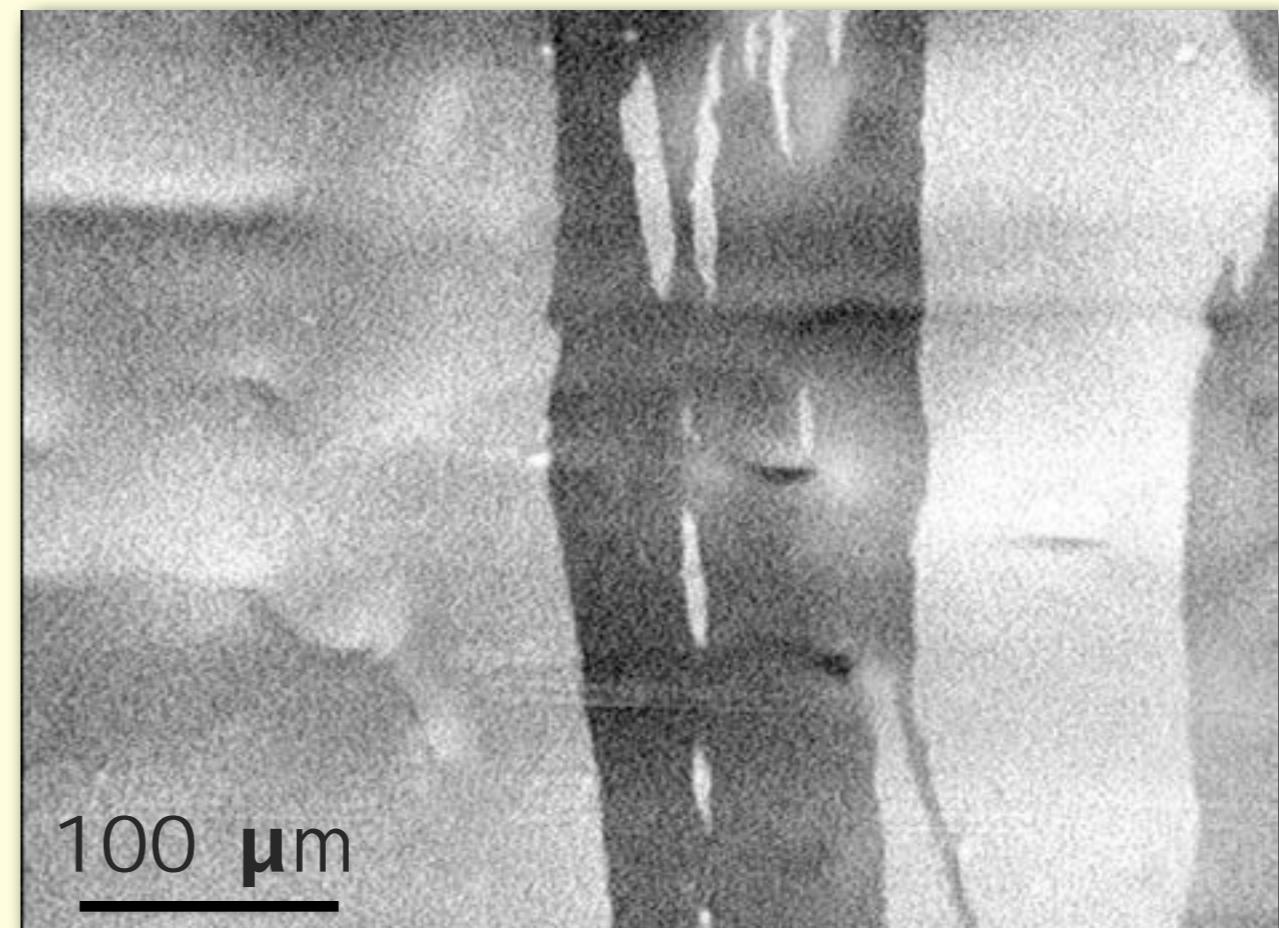
N: number of grains within correlation volume

low induced anisotropy
($K_u = 3 \text{ J/m}^3$)



350°C

strong induced anisotropy
($K_u = 30 \text{ J/m}^3$)



550°C

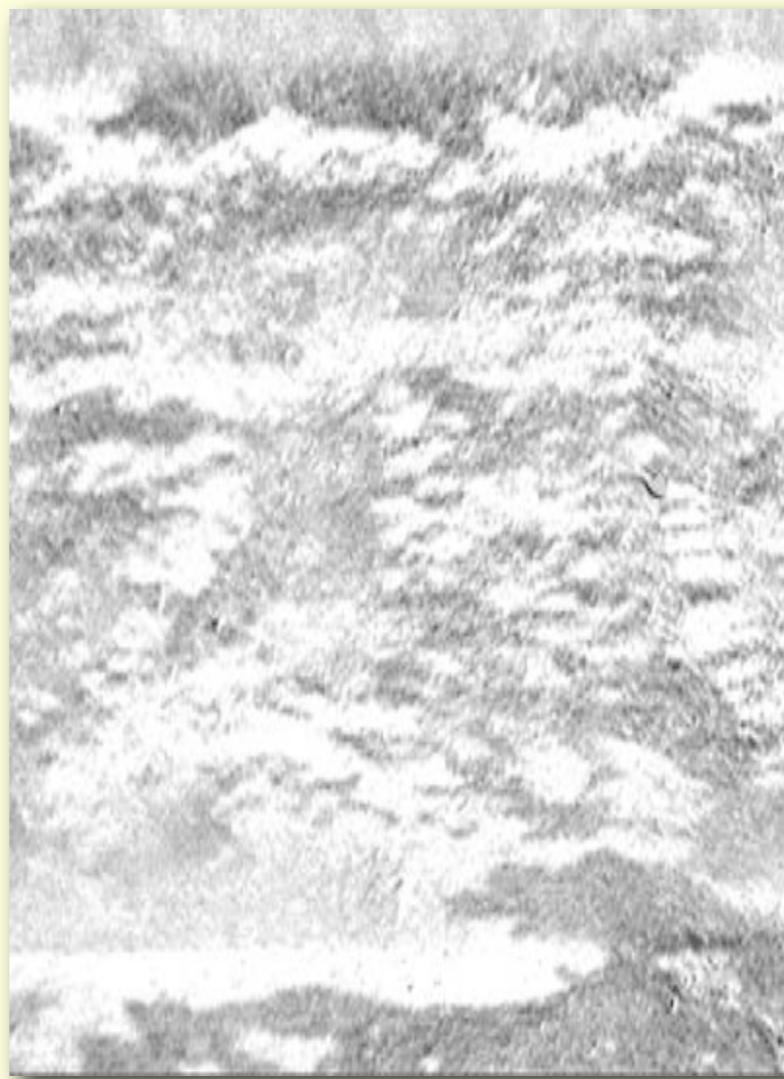
$\text{Co}_{45}\text{Fe}_{28.5}\text{Si}_{13.5}\text{B}_9\text{Cu}_1\text{Nb}_3$

$$\langle K_1 \rangle \sim -\frac{K_1}{\sqrt{N}}$$

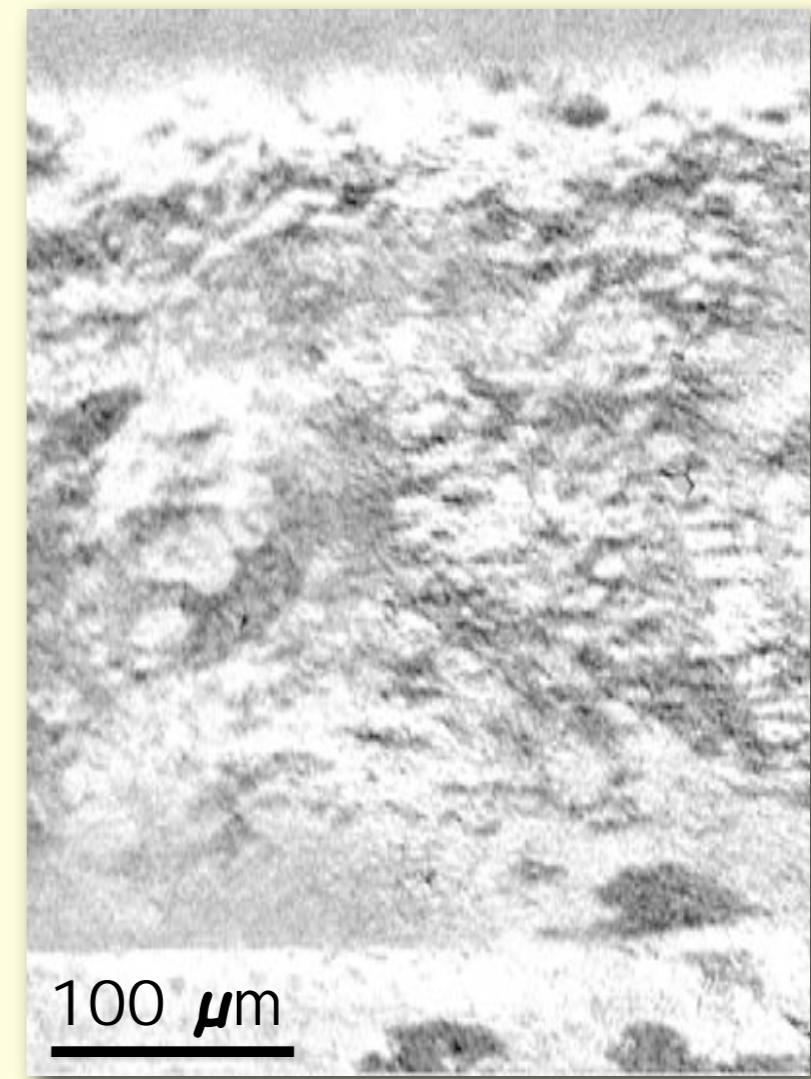
increases anisotropy of grains



$H = -0.15 \text{ kA/m}$



$+0.11 \text{ kA/m}$



$+0.14 \text{ kA/m}$

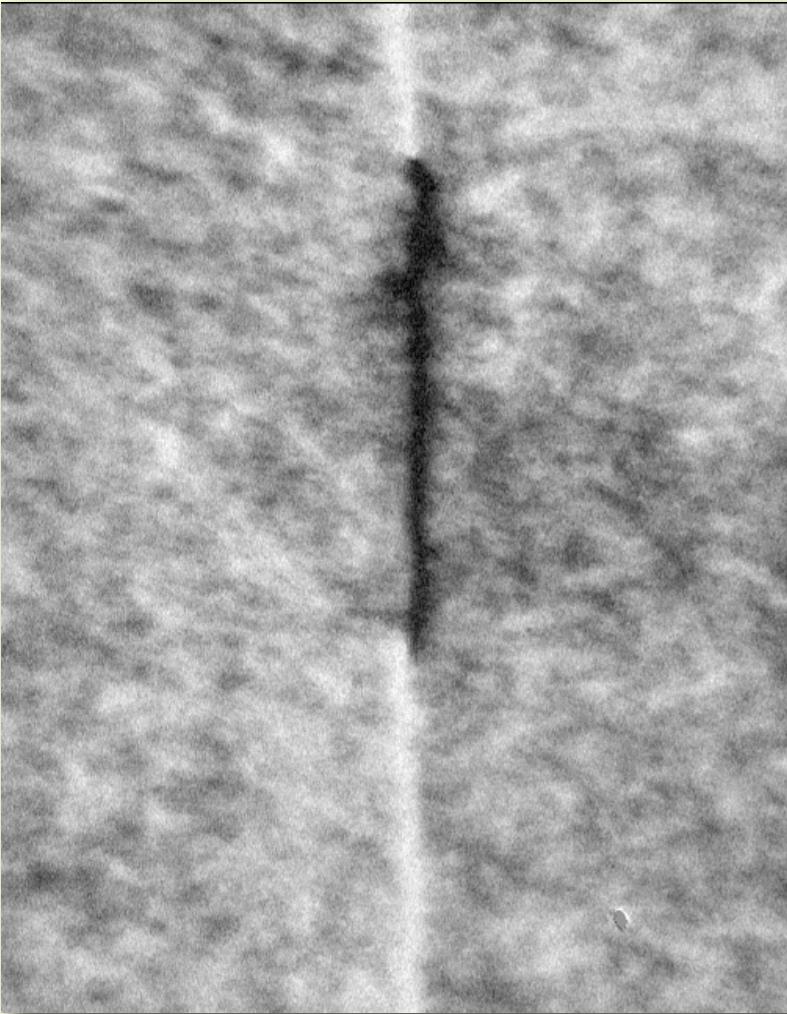
↔
ribbon axis and field direction

sample: Pilar Marin, Madrid

Patches and ripple

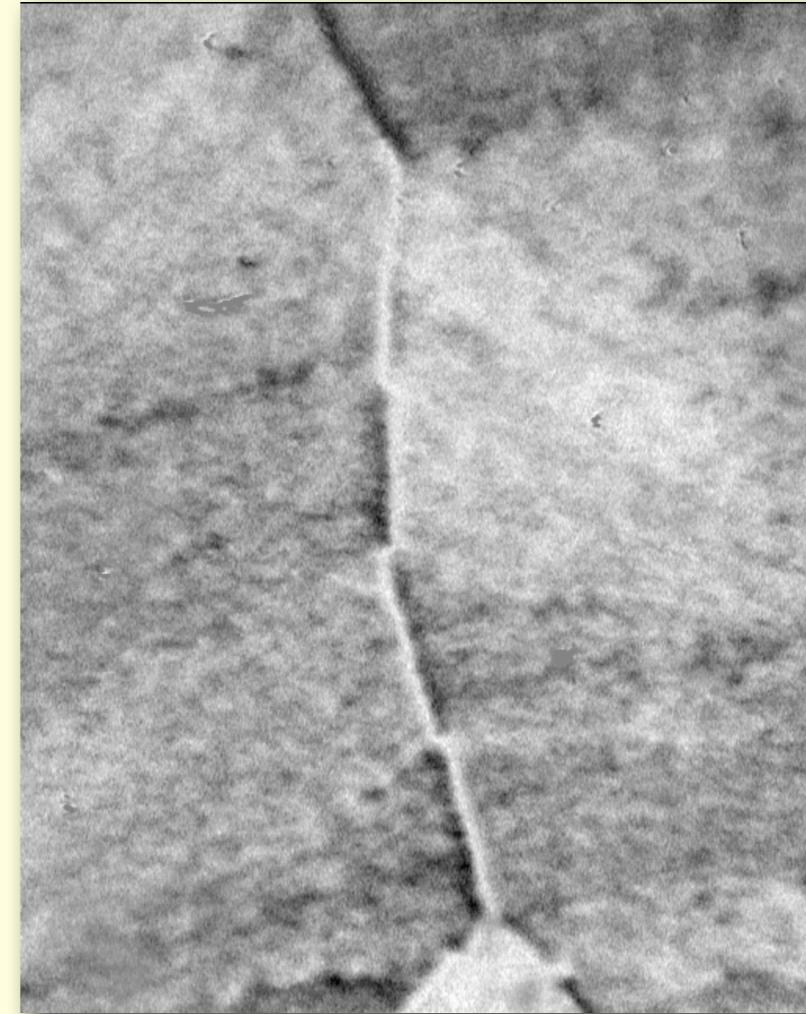
Nanocrystalline $\text{Fe}_{84}\text{Zr}_{3.5}\text{Nb}_{3.5}\text{B}_8\text{Cu}_1$

20 μm thick

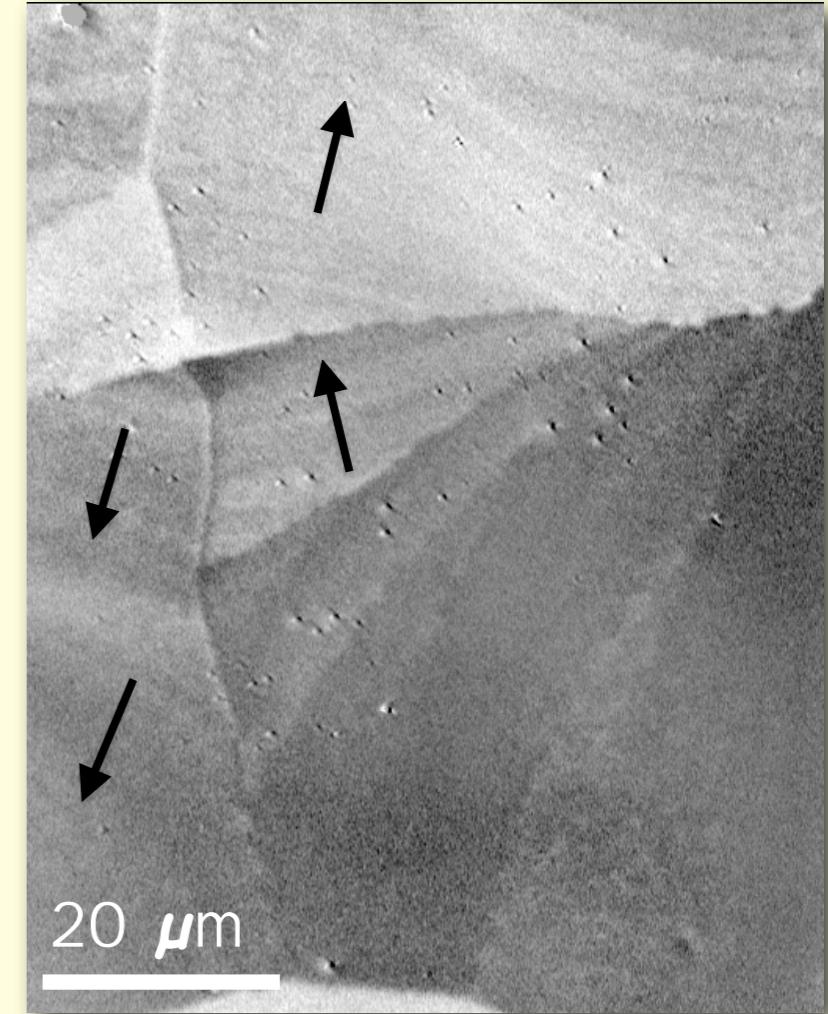


patches

thinned to μm



still thinner

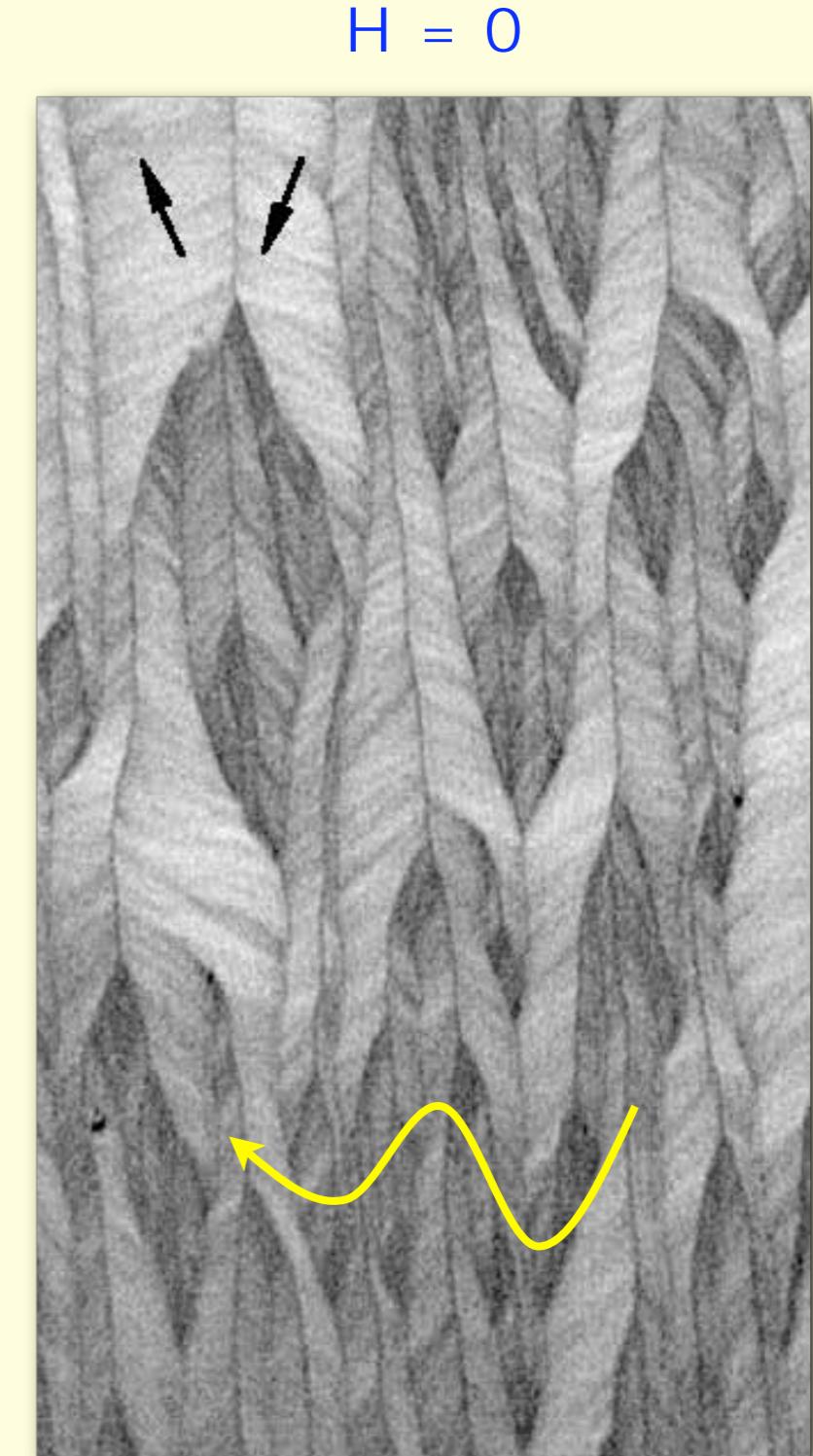
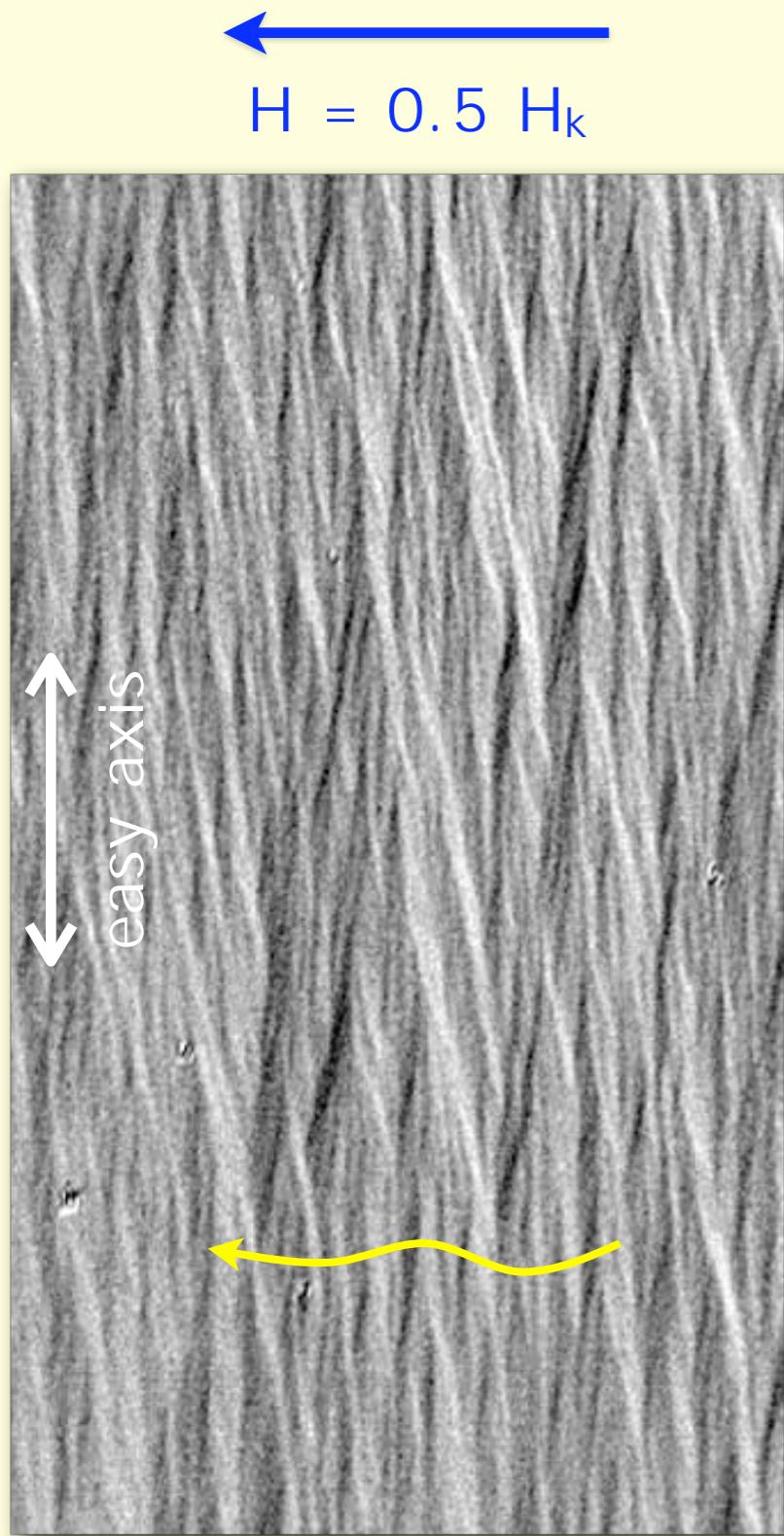


ripple

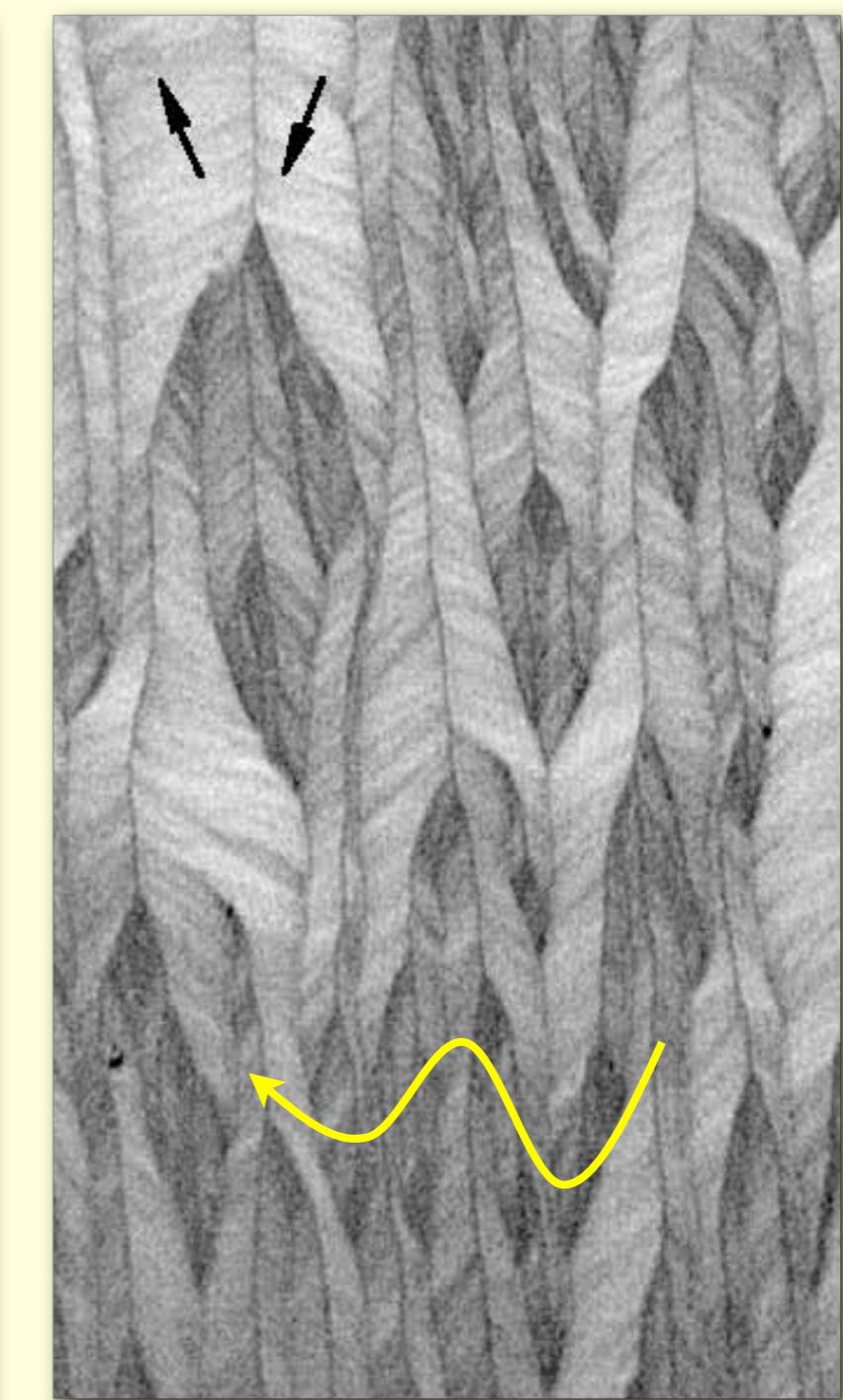
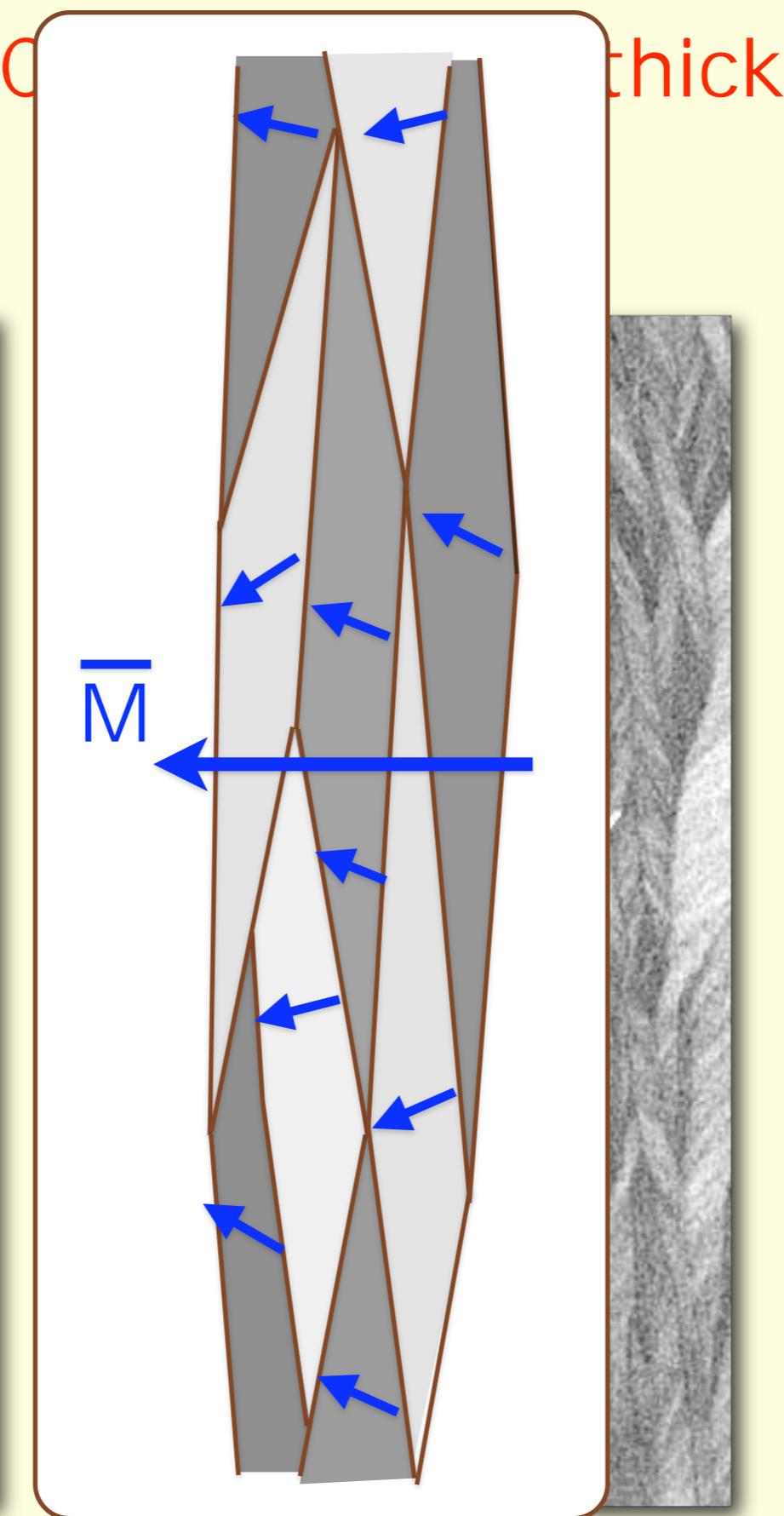
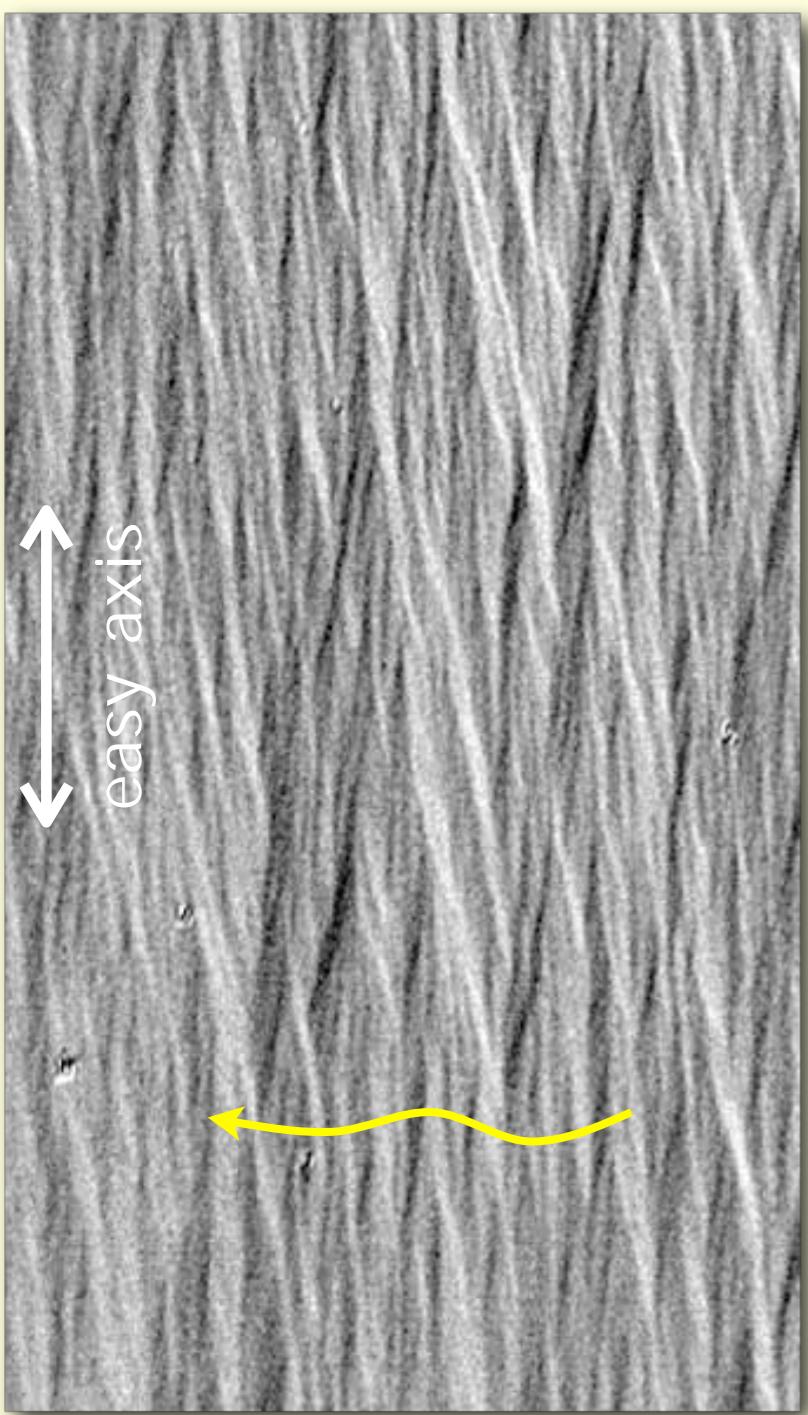
Excursion: Ripple phenomenon

Ripple phenomenon: development

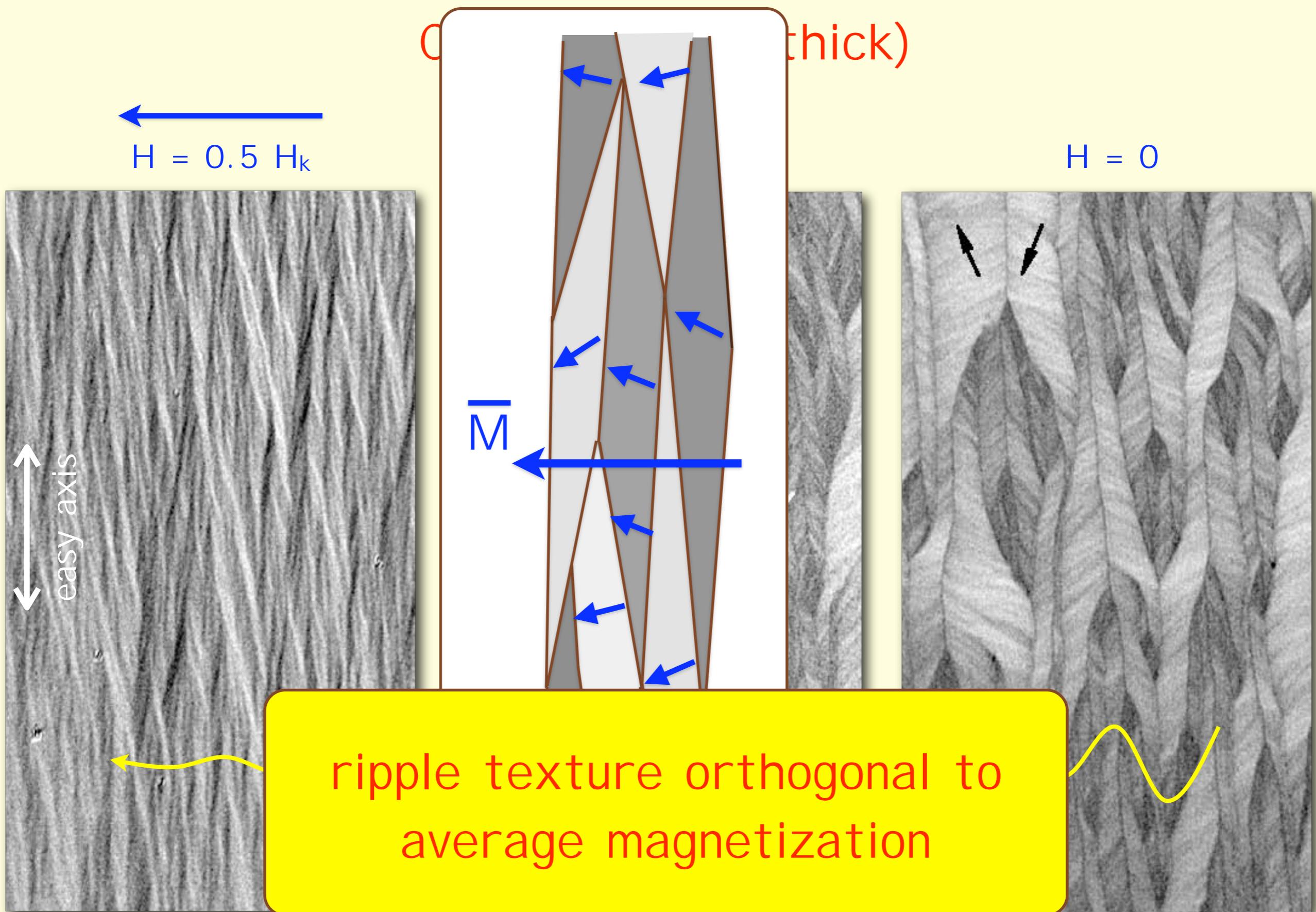
Cobalt (42 nm thick)



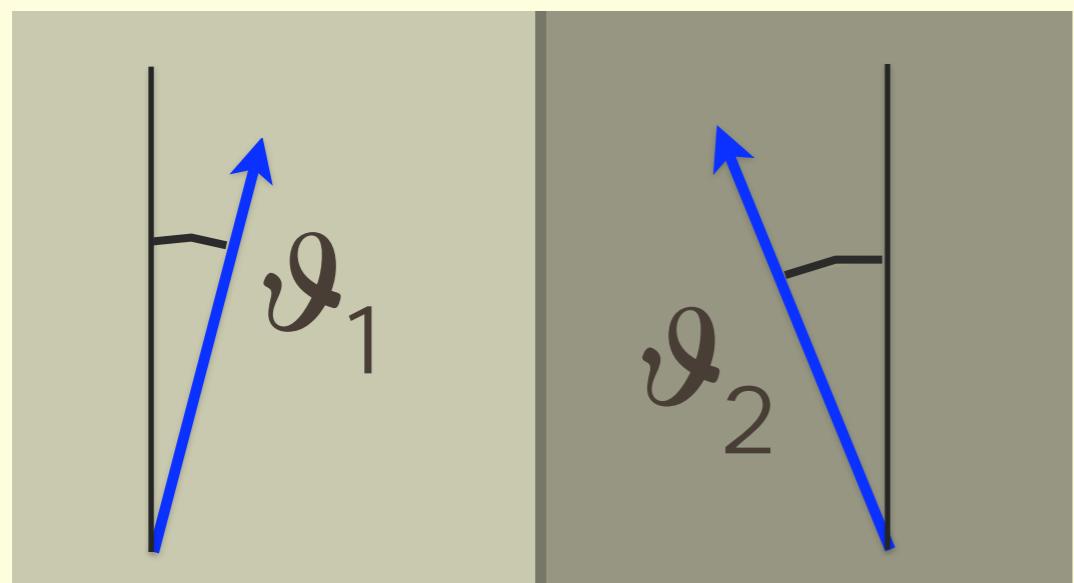
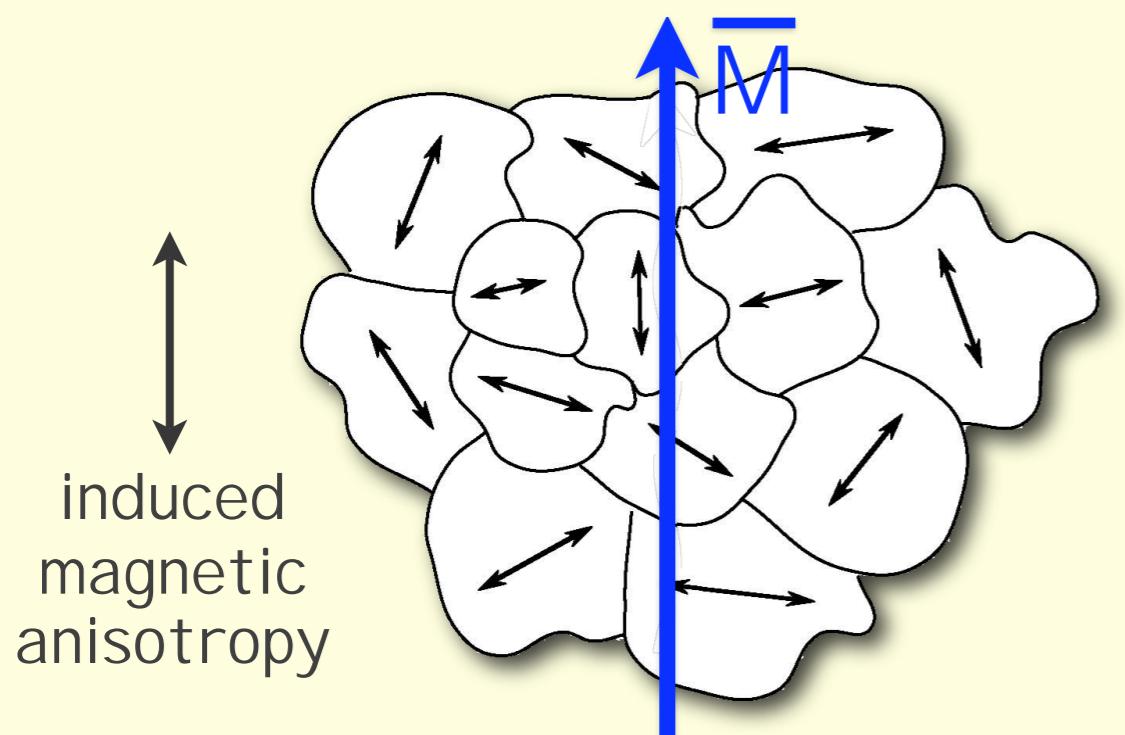
Ripple phenomenon: development



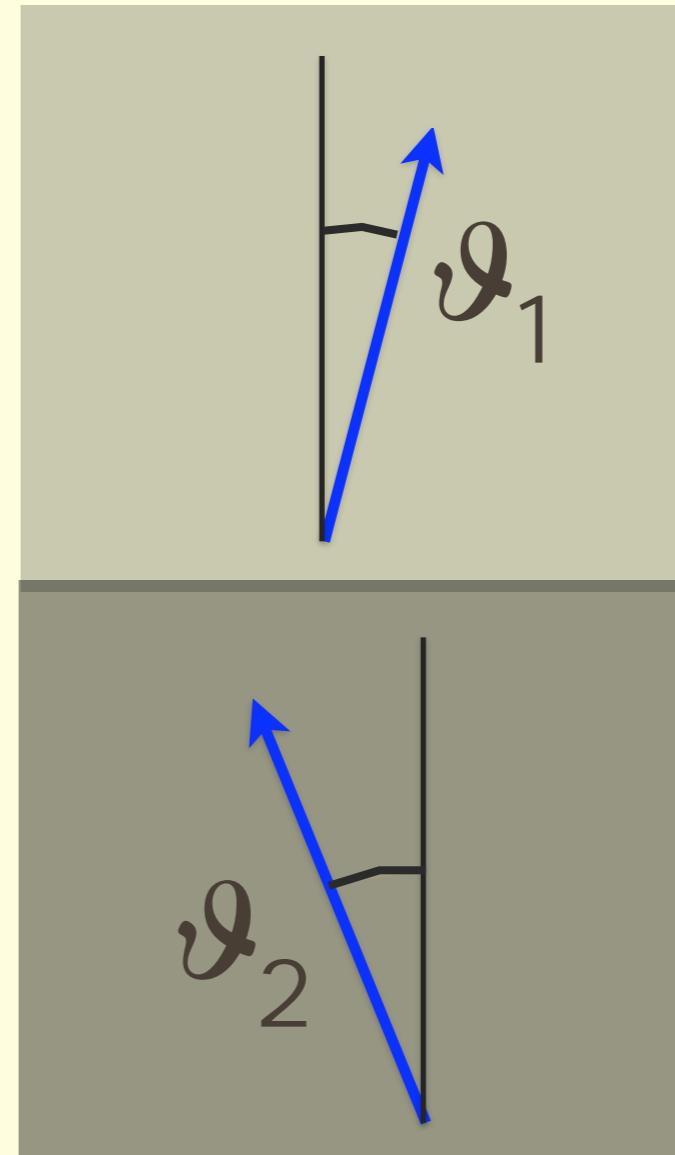
Ripple phenomenon: development



Ripple phenomenon: development

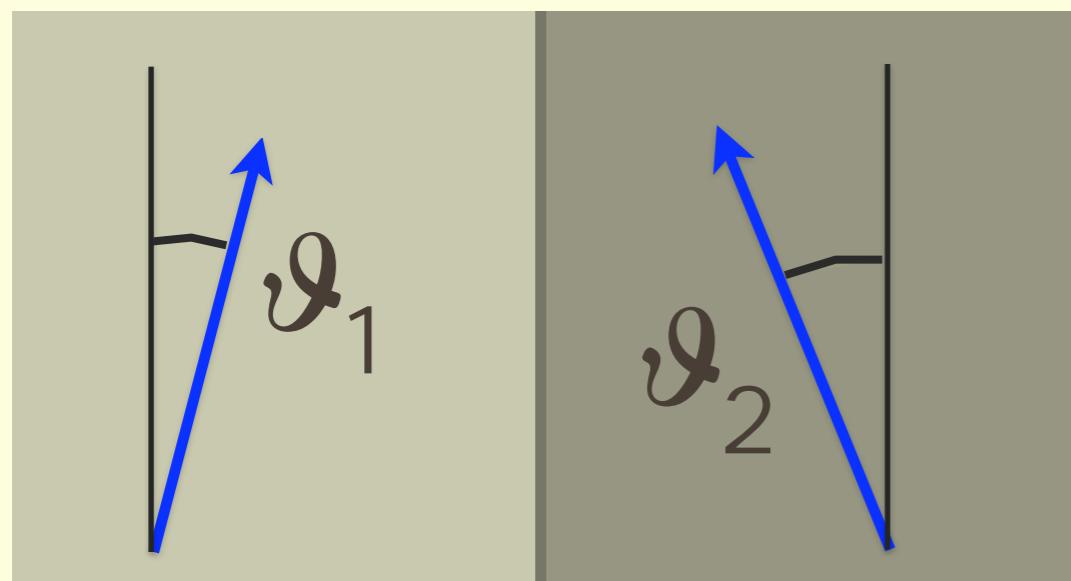
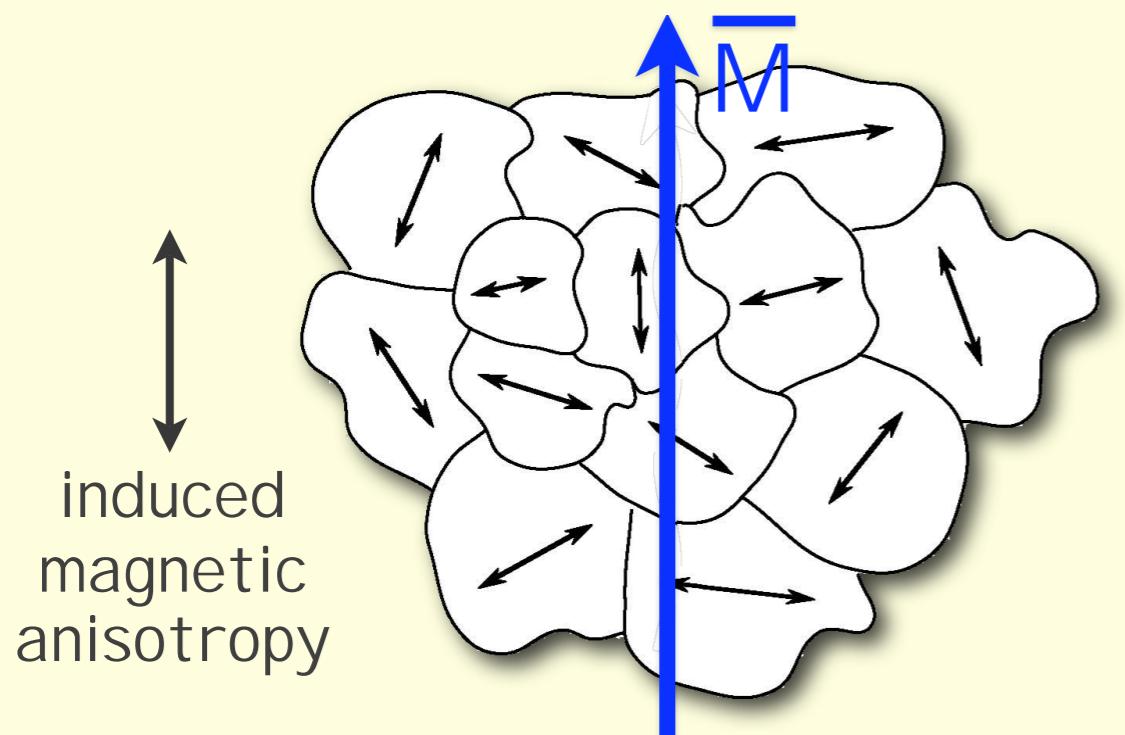


$$\lambda_{\text{trans}} = \sin \vartheta_1 - \sin \vartheta_2$$

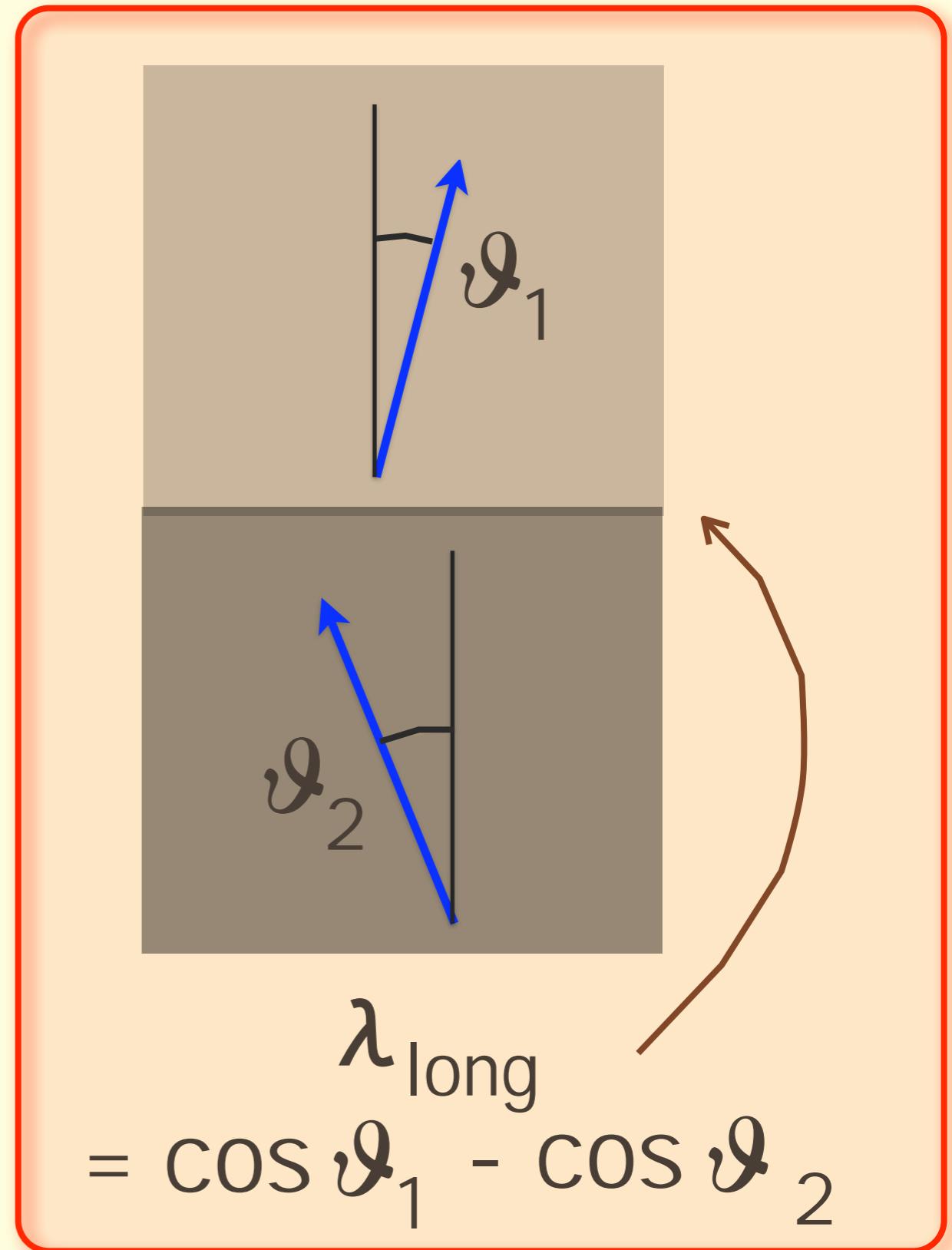


$$\lambda_{\text{long}} = \cos \vartheta_1 - \cos \vartheta_2$$

Ripple phenomenon: development

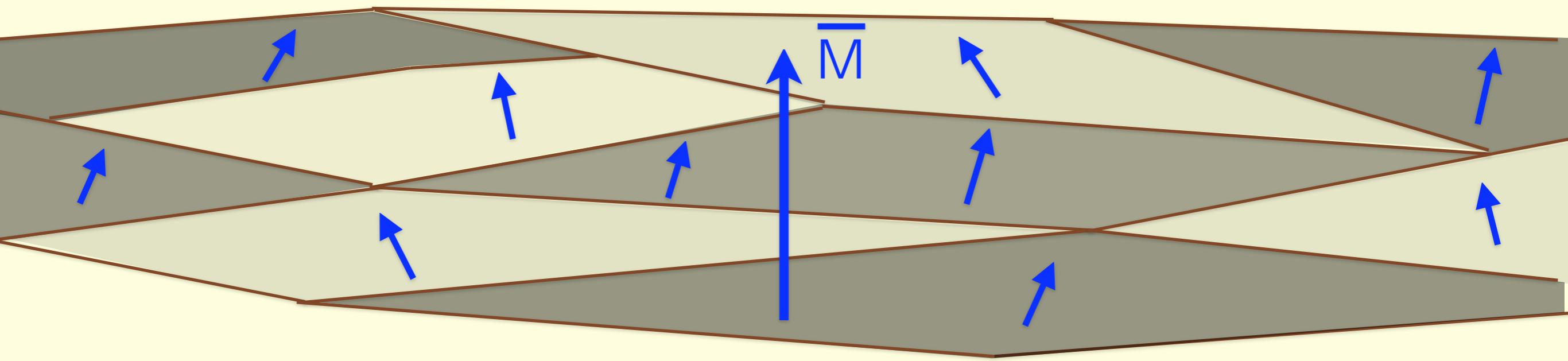


$$\lambda_{\text{trans}} = \sin \varphi_1 - \sin \varphi_2$$

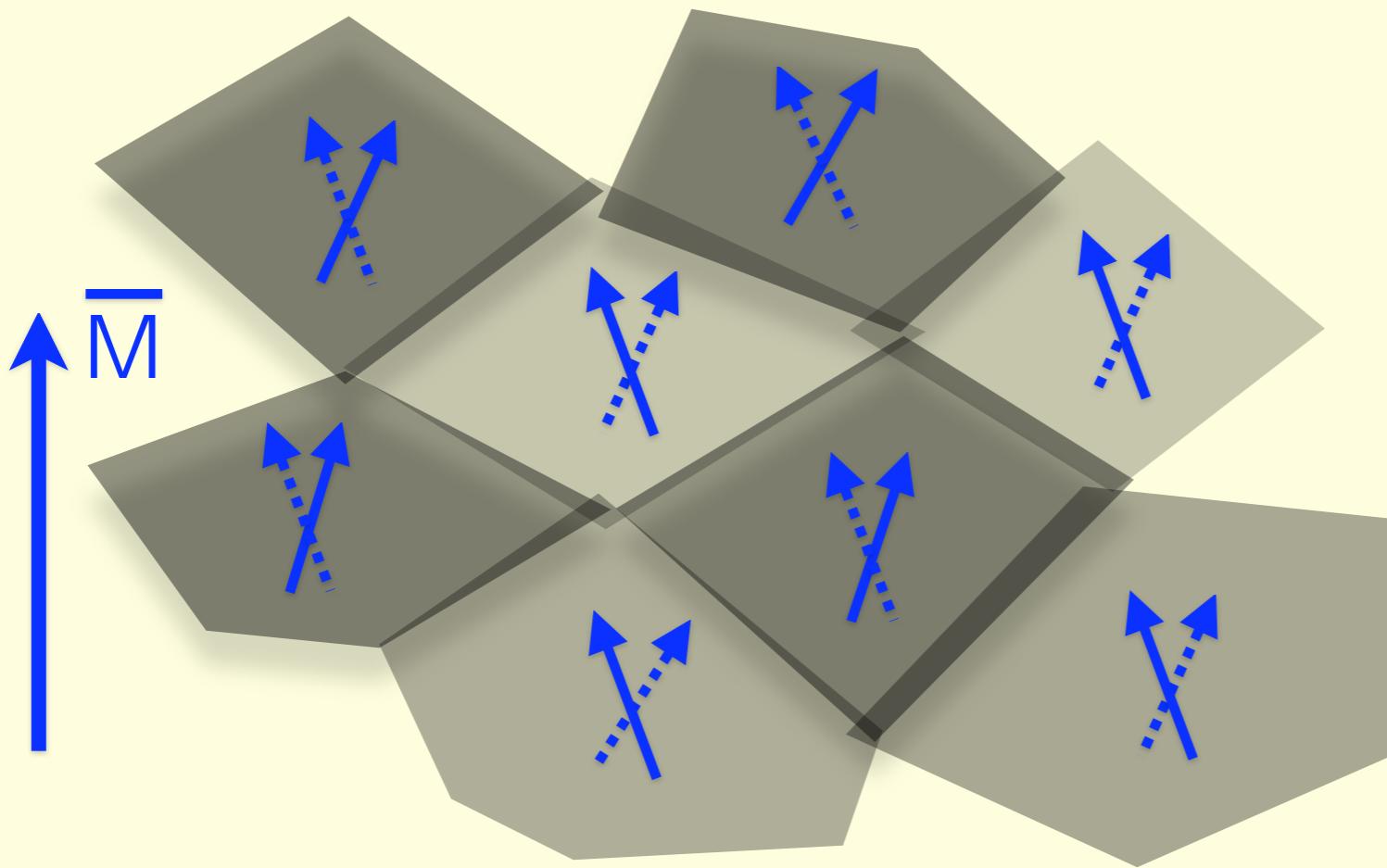


Ripple and patches

ripple in films

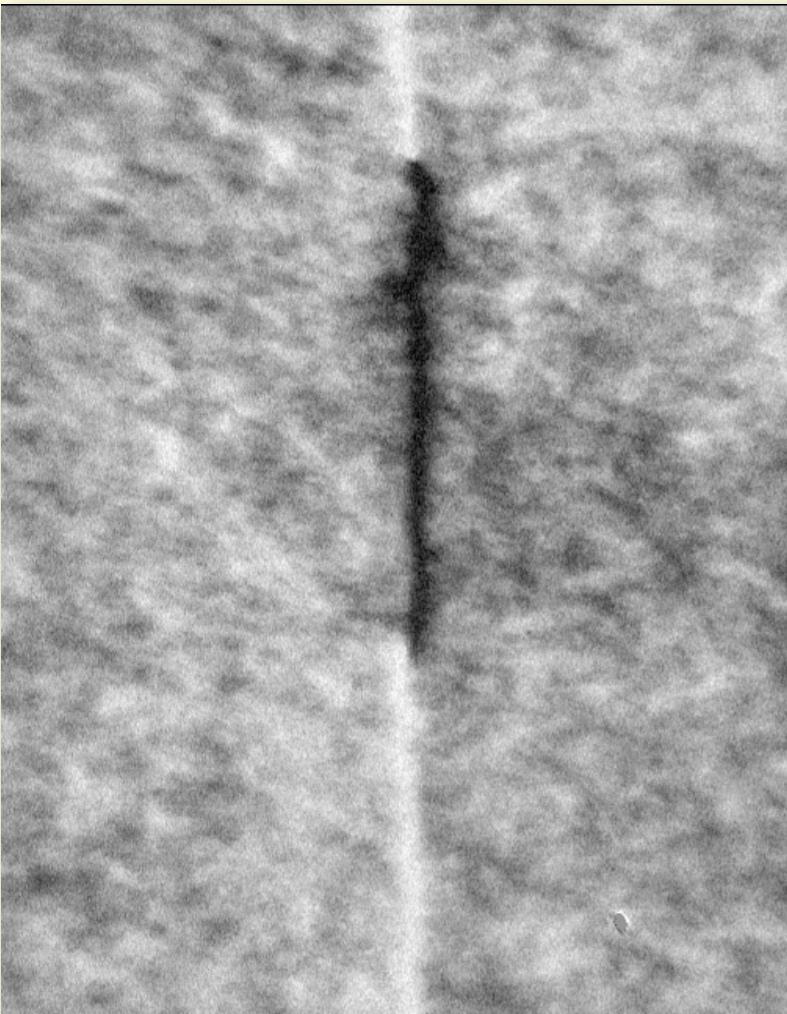


patches in
thick materials

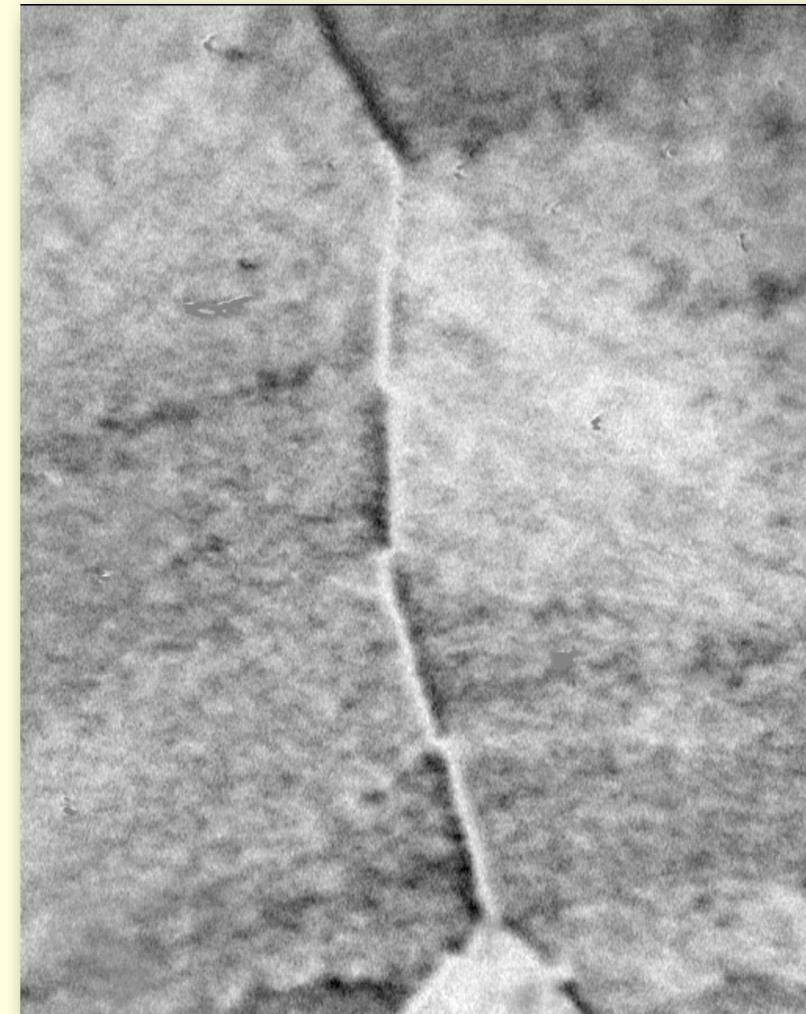


Patches and ripple

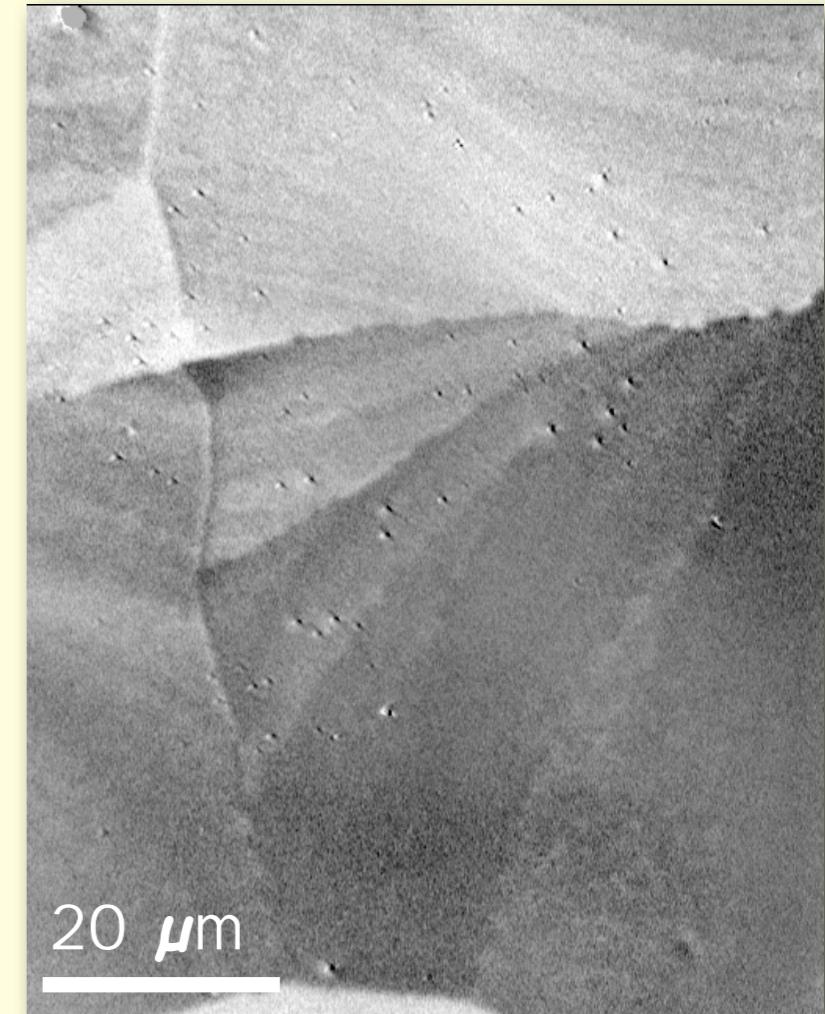
20 μm thick



thinned to μm



still thinner



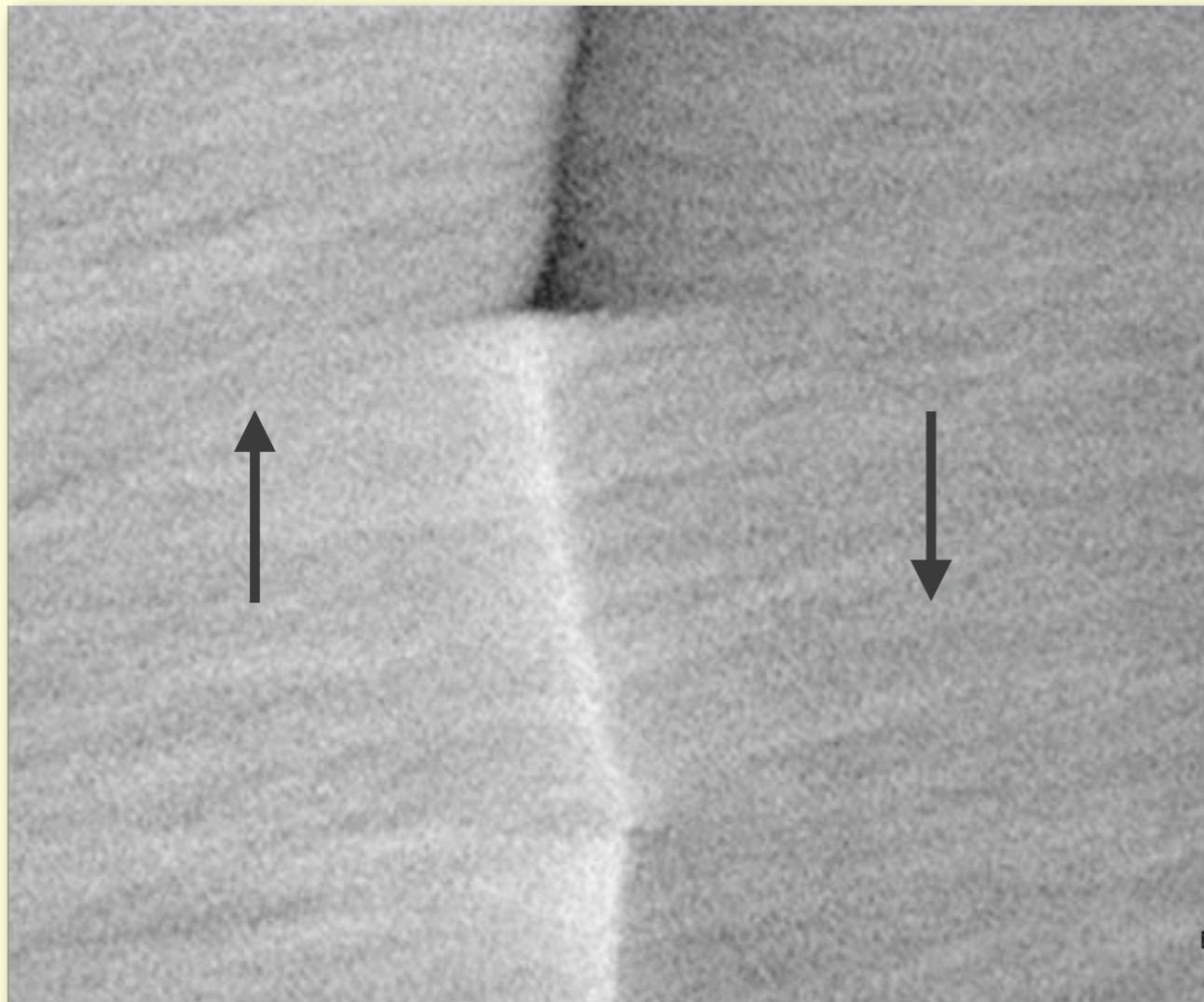
20 μm

statistical perturbation by crystal anisotropy causes:

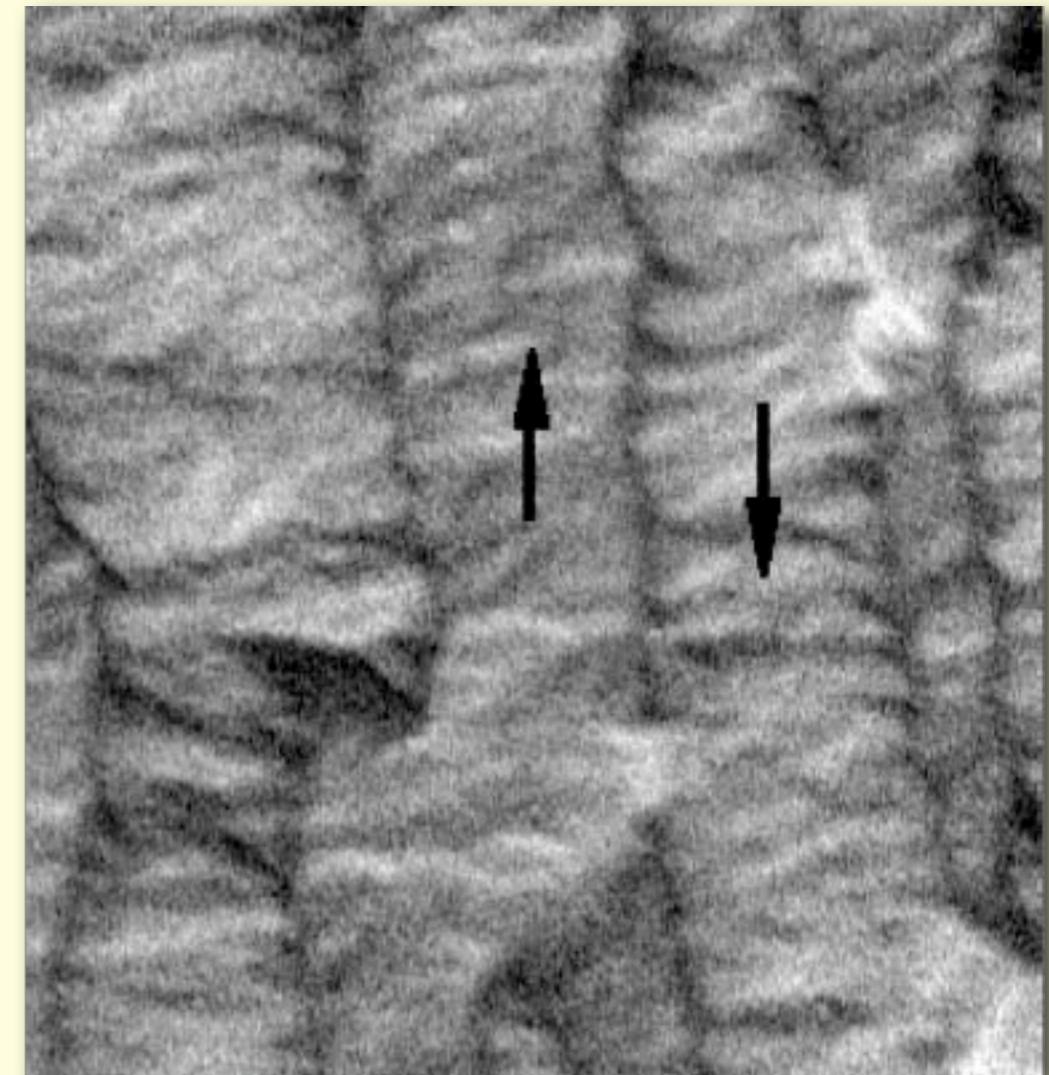
- patches in thick samples (ribbons)
- ripple in thin films

Ripple phenomenon: Comparison Ni/Co

Permalloy (10 nm thick)



Co (6 nm thick)

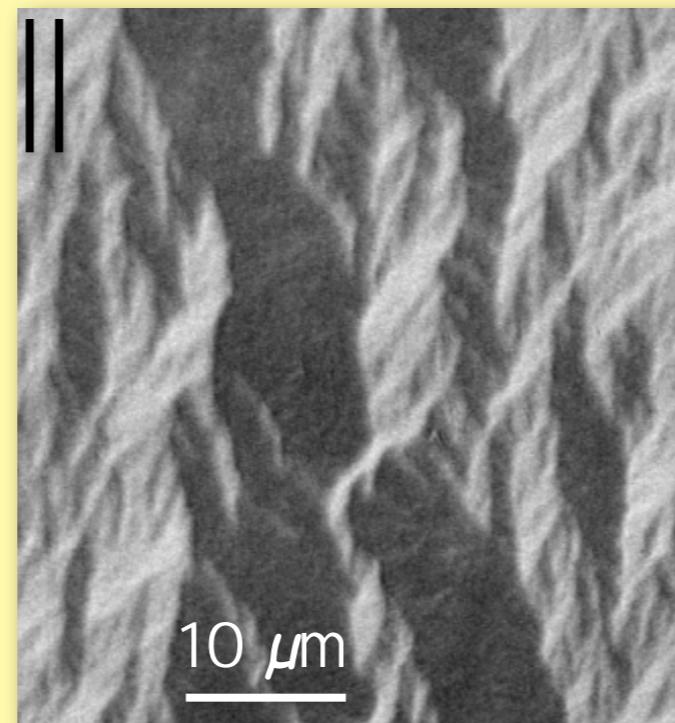
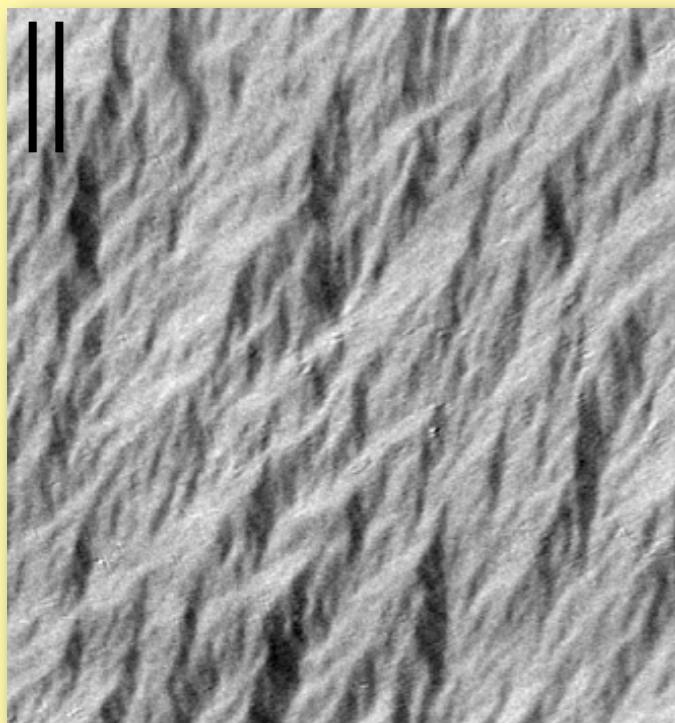


10 μm

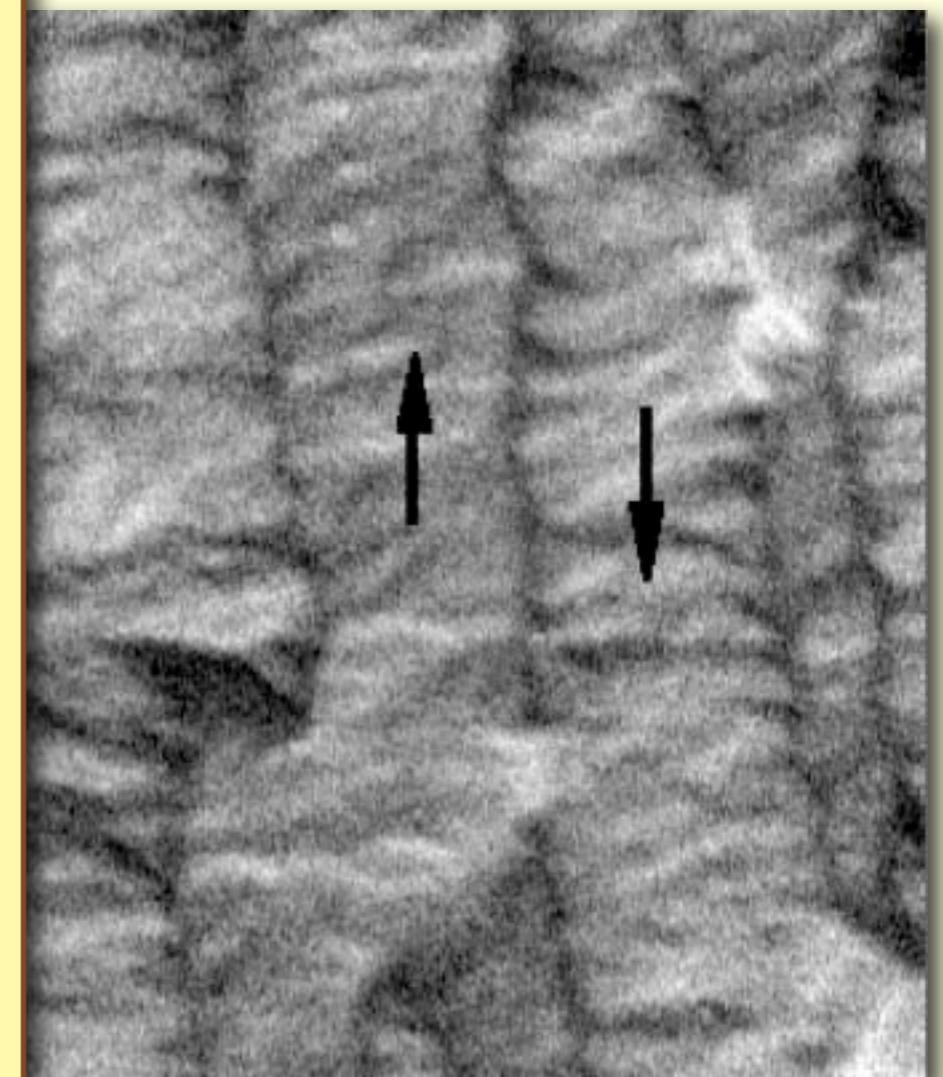
Ripple phenomenon: Comparison Ni/Co

Cobalt film (6 nm thick)

nucleation and growth



Co (6 nm thick)



10 μm

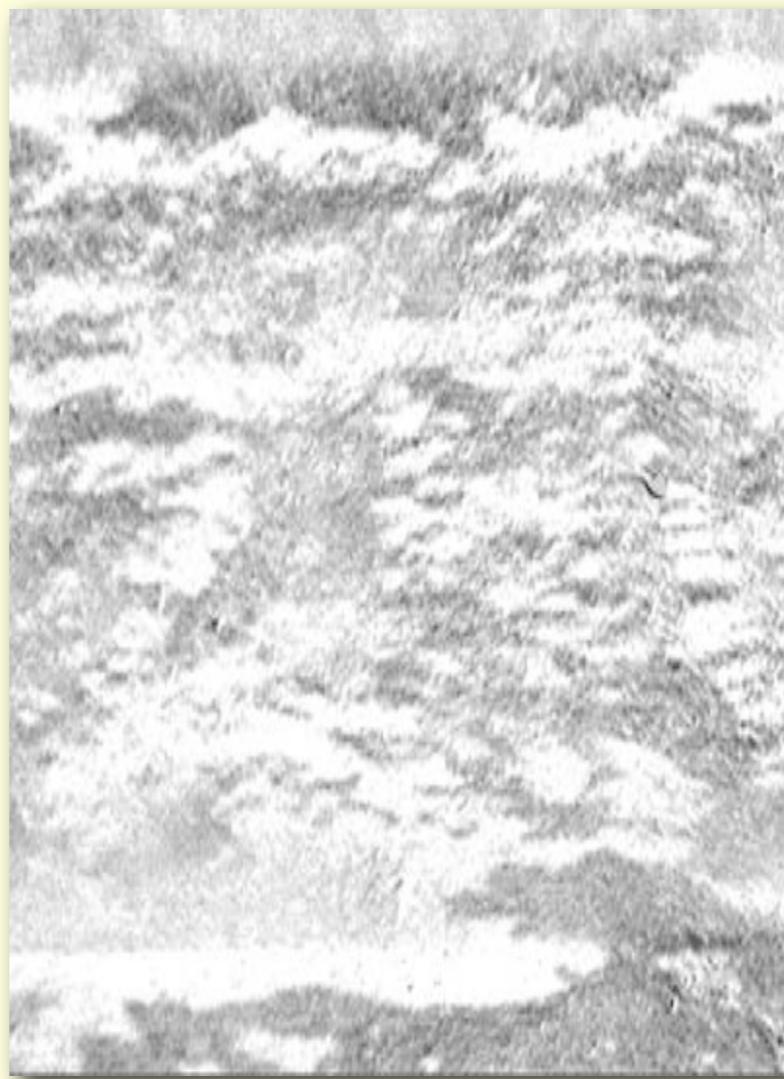
$\text{Co}_{45}\text{Fe}_{28.5}\text{Si}_{13.5}\text{B}_9\text{Cu}_1\text{Nb}_3$

$$\langle K_1 \rangle \sim -\frac{K_1}{\sqrt{N}}$$

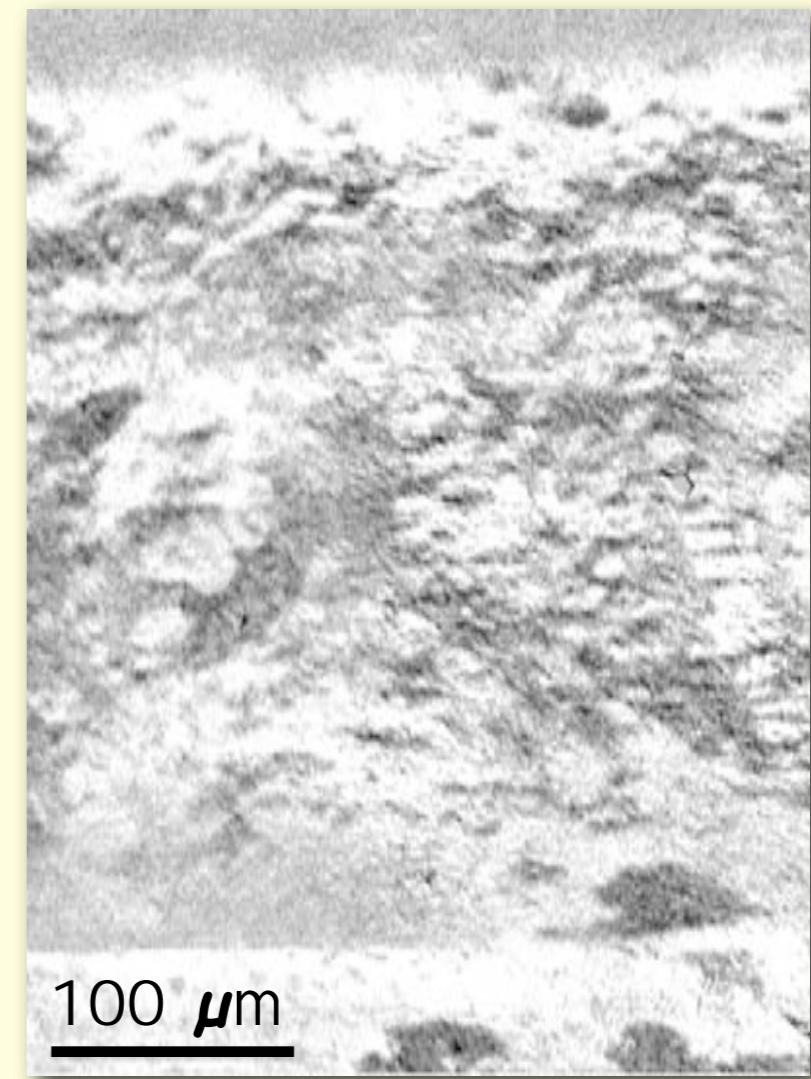
increases anisotropy of grains



$H = -0.15 \text{ kA/m}$



$+0.11 \text{ kA/m}$

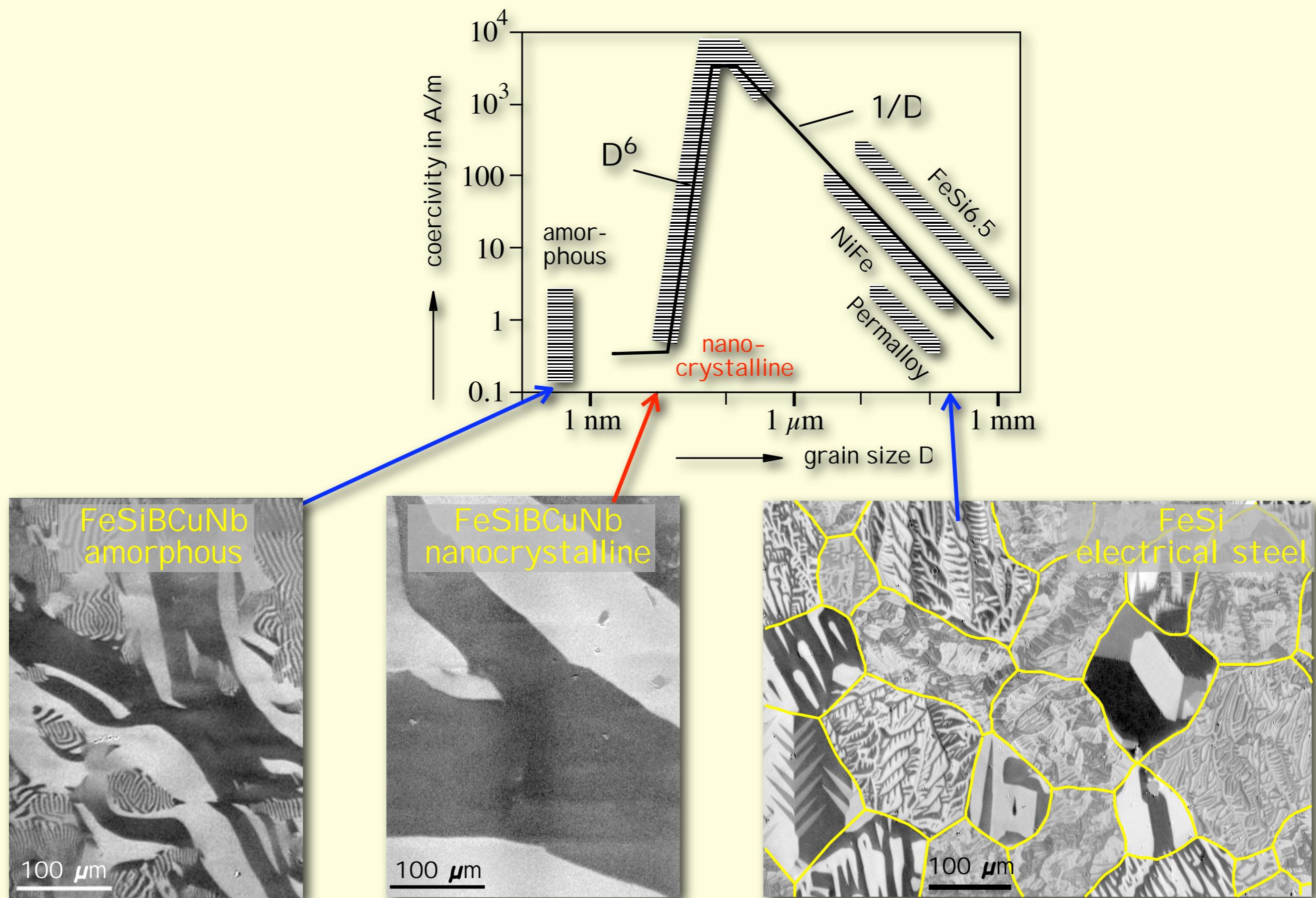


$+0.14 \text{ kA/m}$

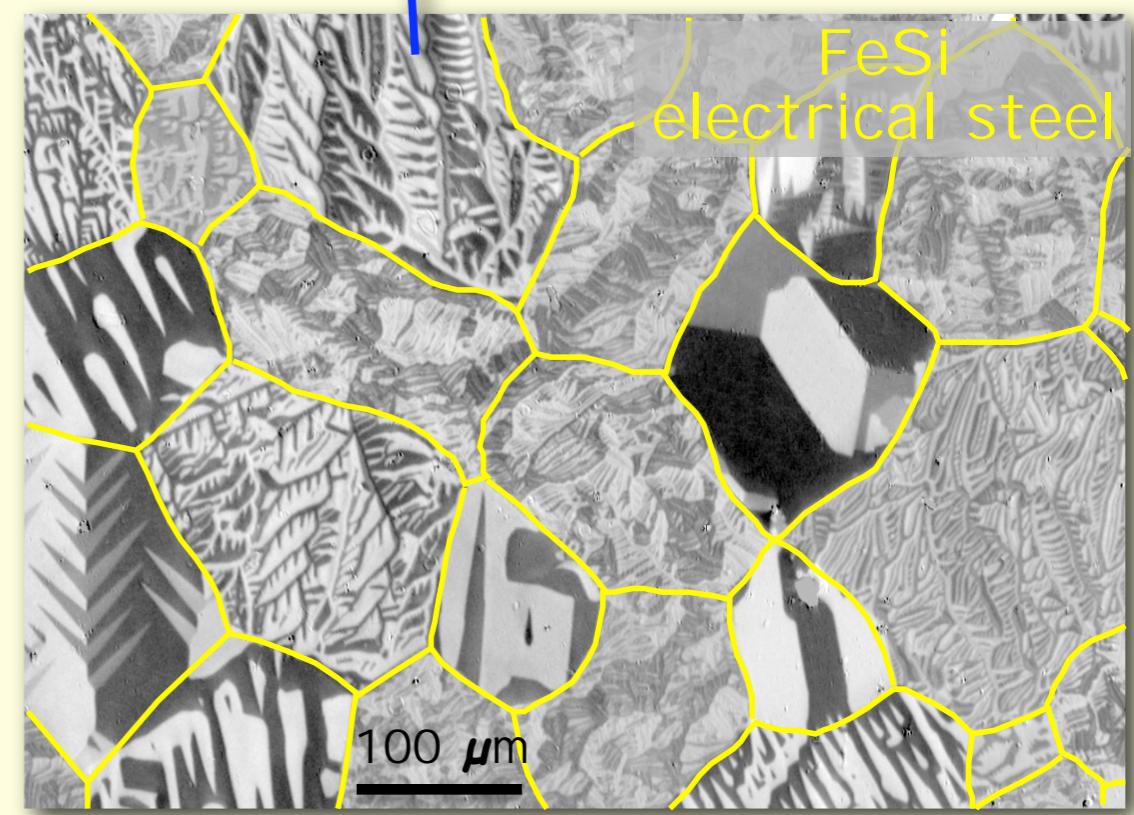
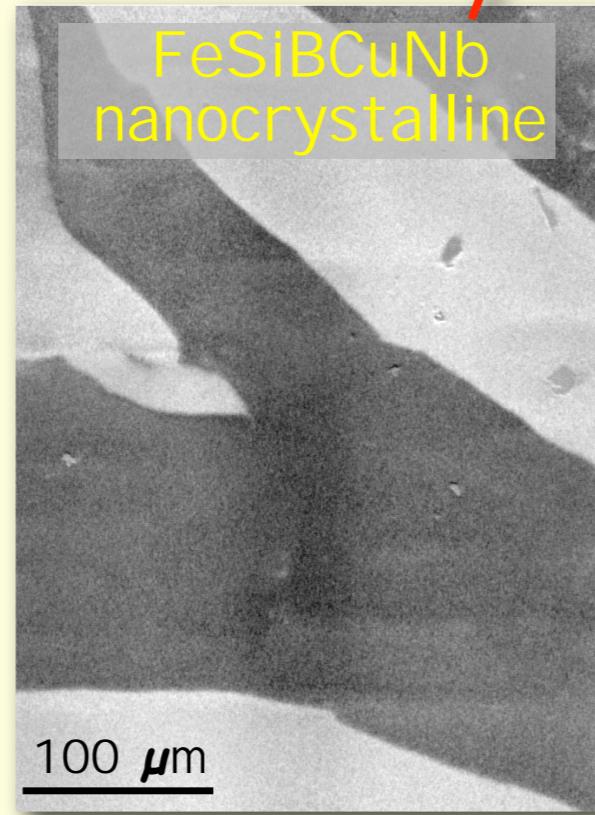
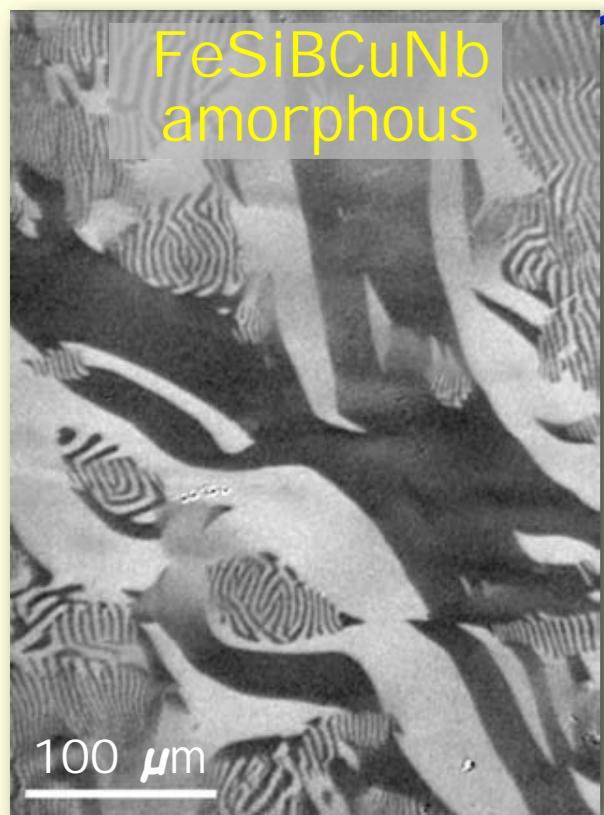
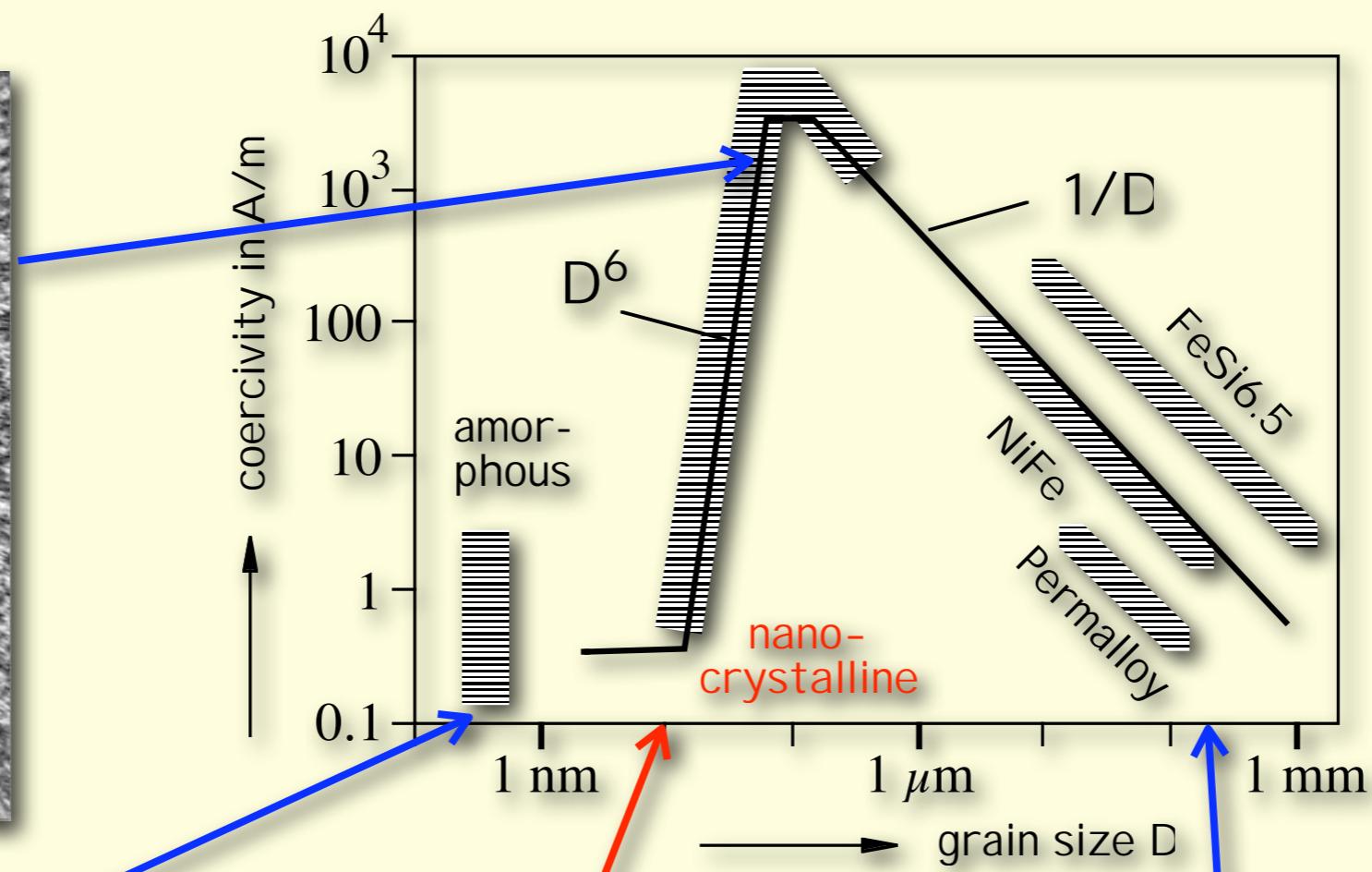
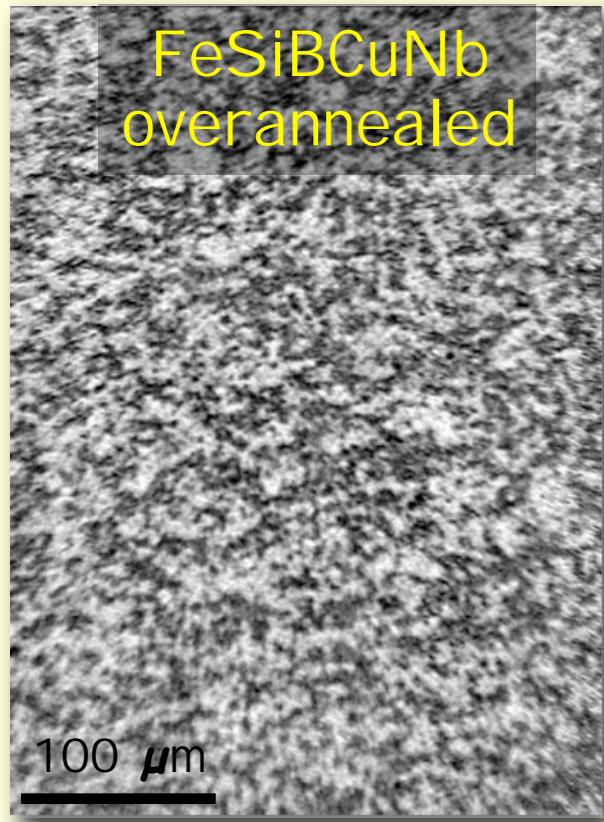
↔
ribbon axis and field direction

sample: Pilar Marin, Madrid

Summary: Coercivity and domains



Summary: Coercivity and domains

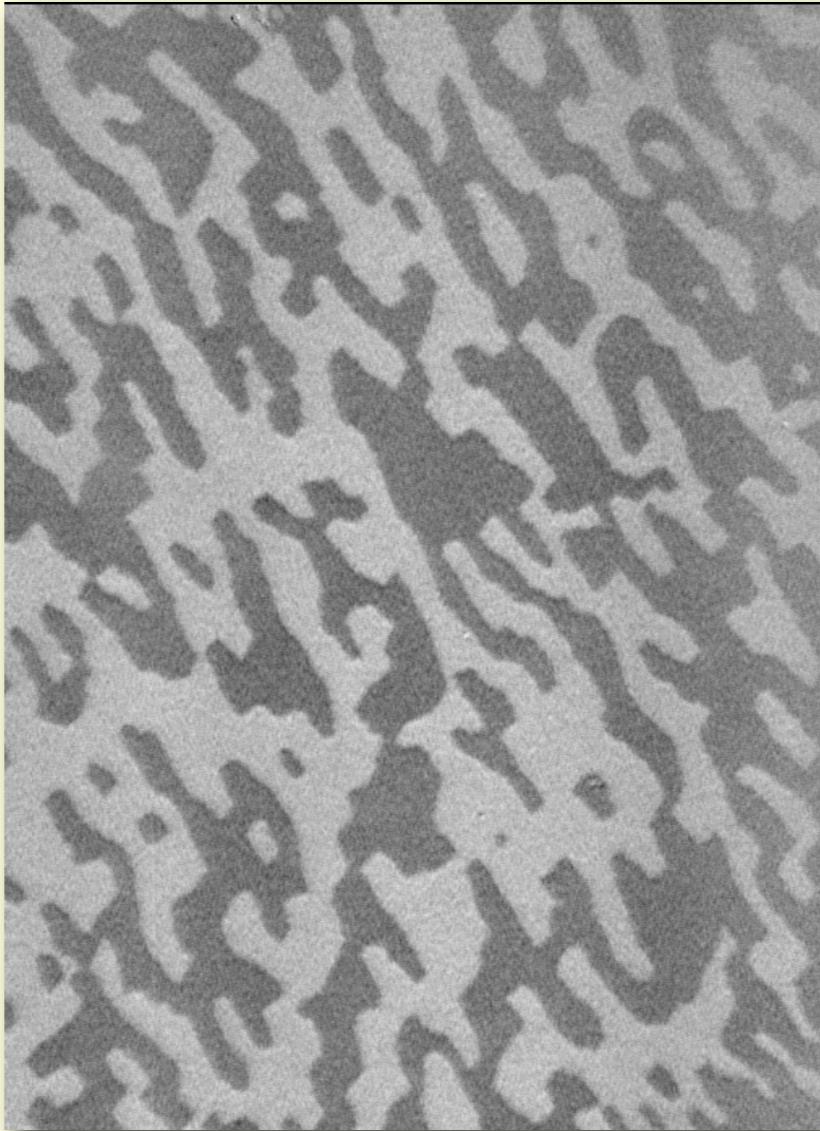


FeSiBCuNb: over-annealed

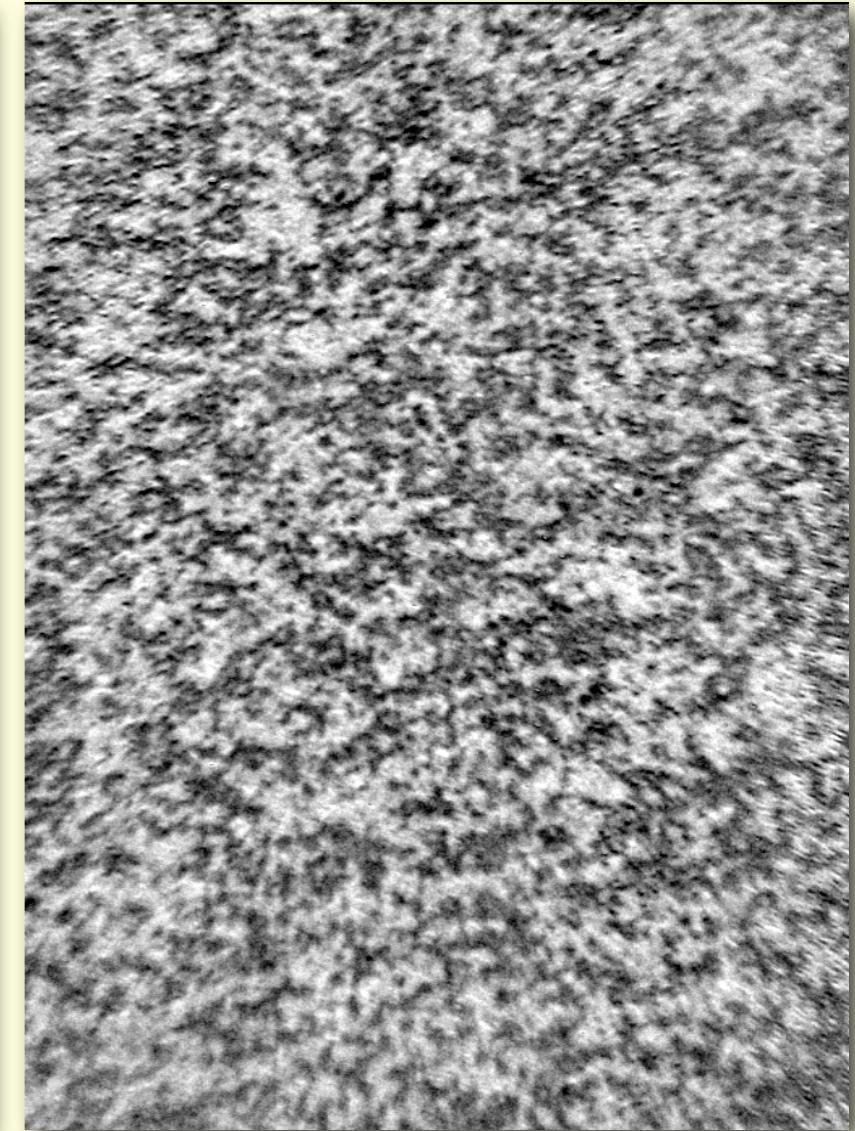
20°C



625°C



800°C

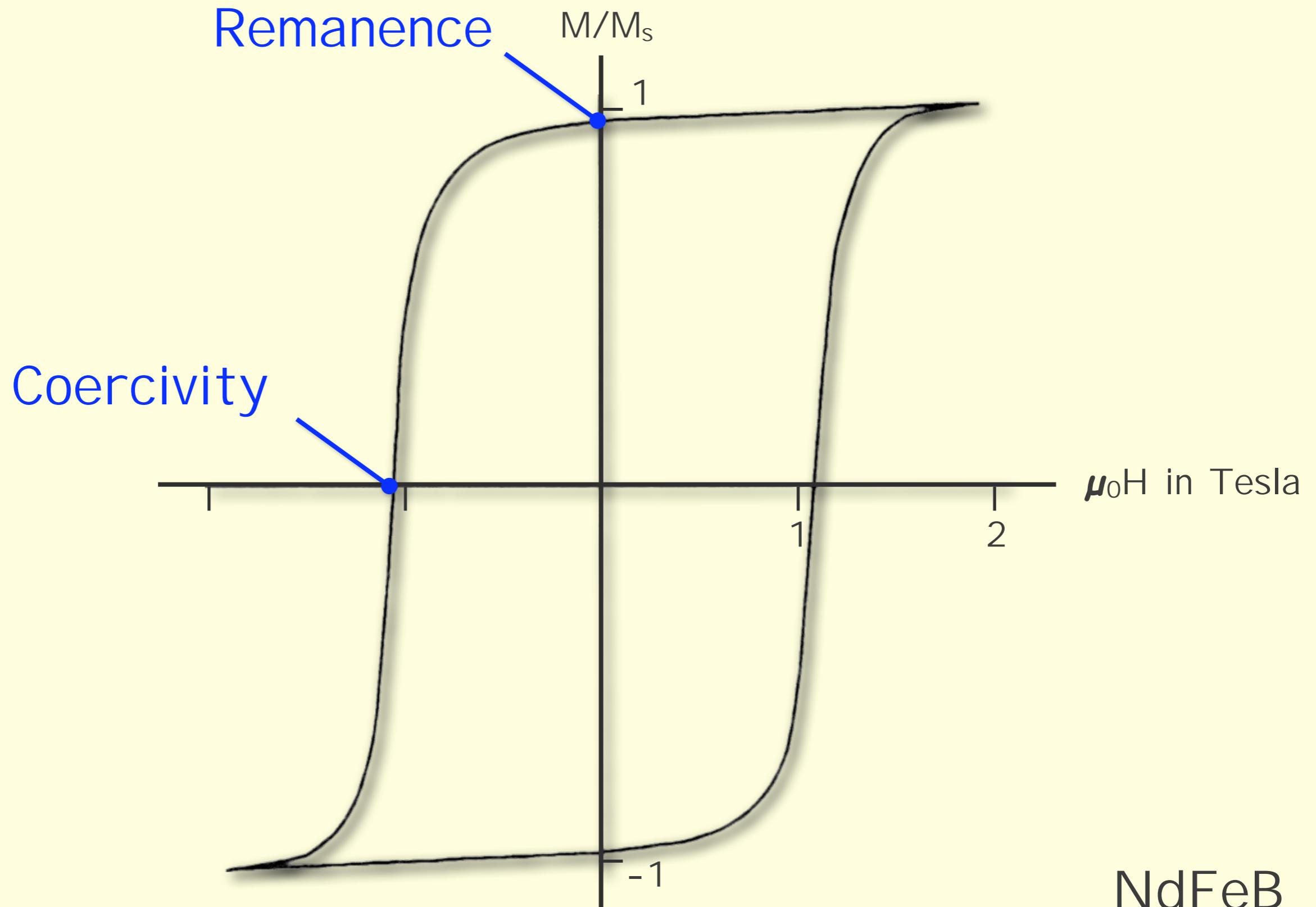


grain coarsening
precipitation of borides

Overview

1. Domains in coarse-grained material
2. Domains in amorphous material
3. Domains in nanocrystalline,
soft magnetic ($Q \ll 1$) materials
4. Domains in fine- and nanostructured,
permanent magnetic ($Q > 1$) materials

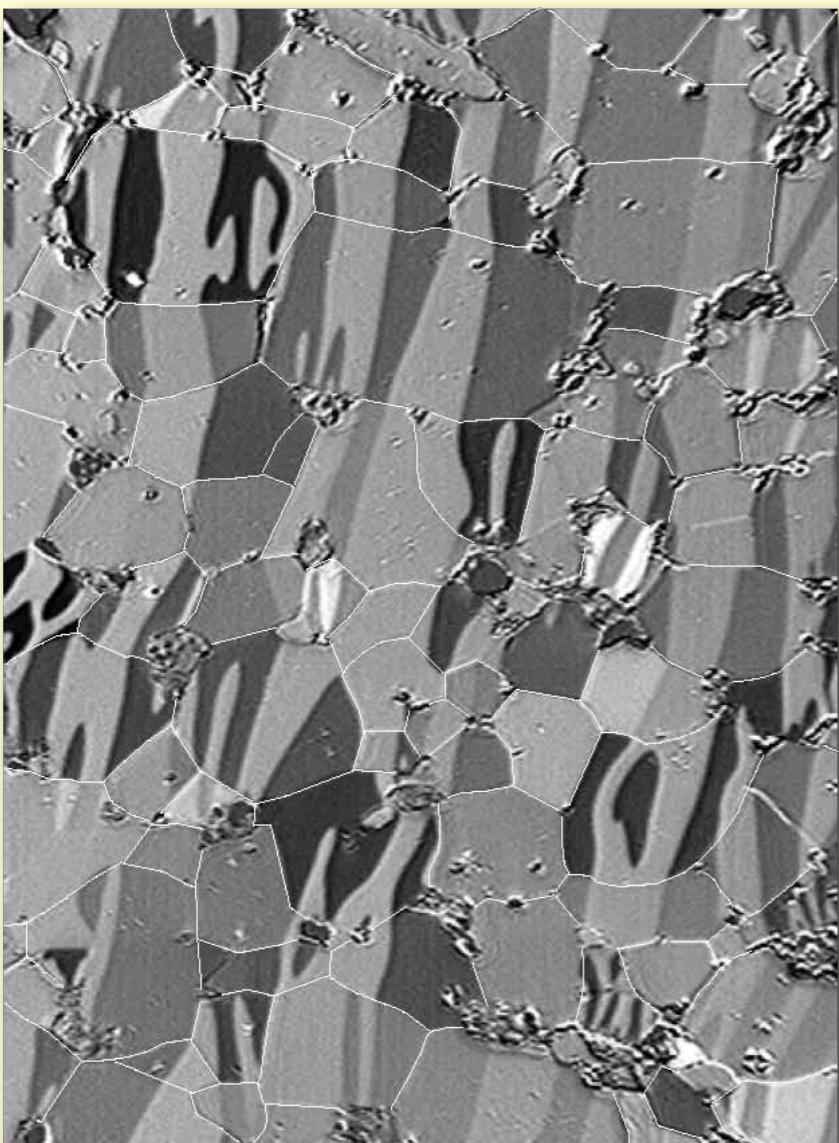
Permanent magnets, basics



NdFeB

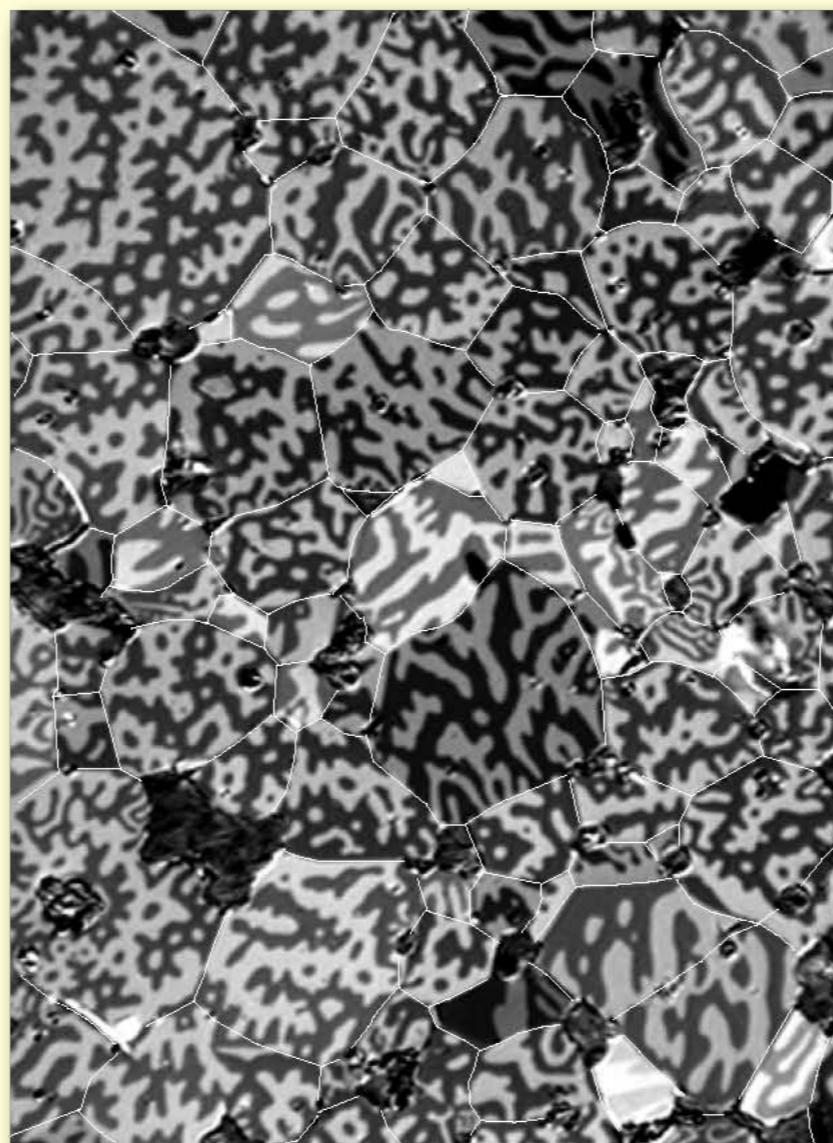
NdFeB permanent magnet

Thermally
demagnetized



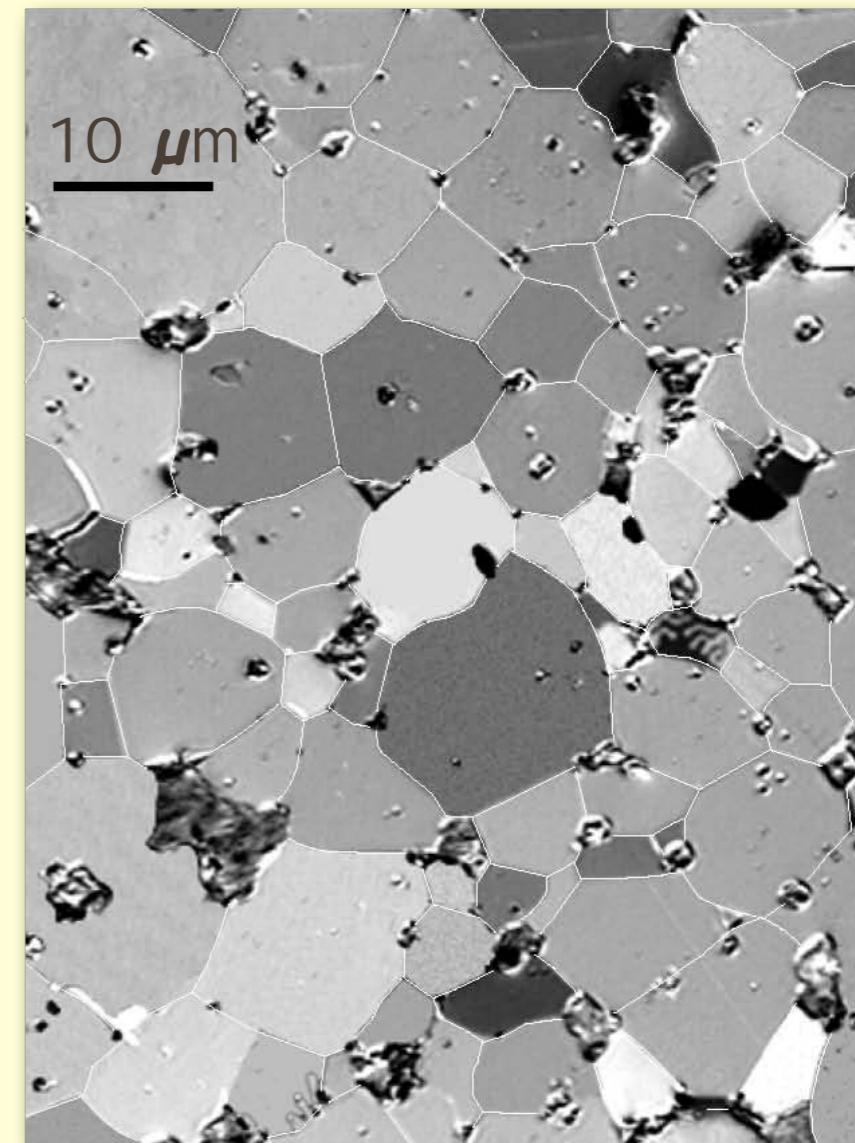
along
texture axis

Thermally
demagnetized



perpendicular
texture axis

Magnetized



perpendicular
texture axis

NdFeB permanent magnet

Thermally
demagnetized

Thermally
demagnetized

Magnetized

What happens to domains,
when grains get smaller,
when structural length approaches
nanometer regime
(= single-domain regime)

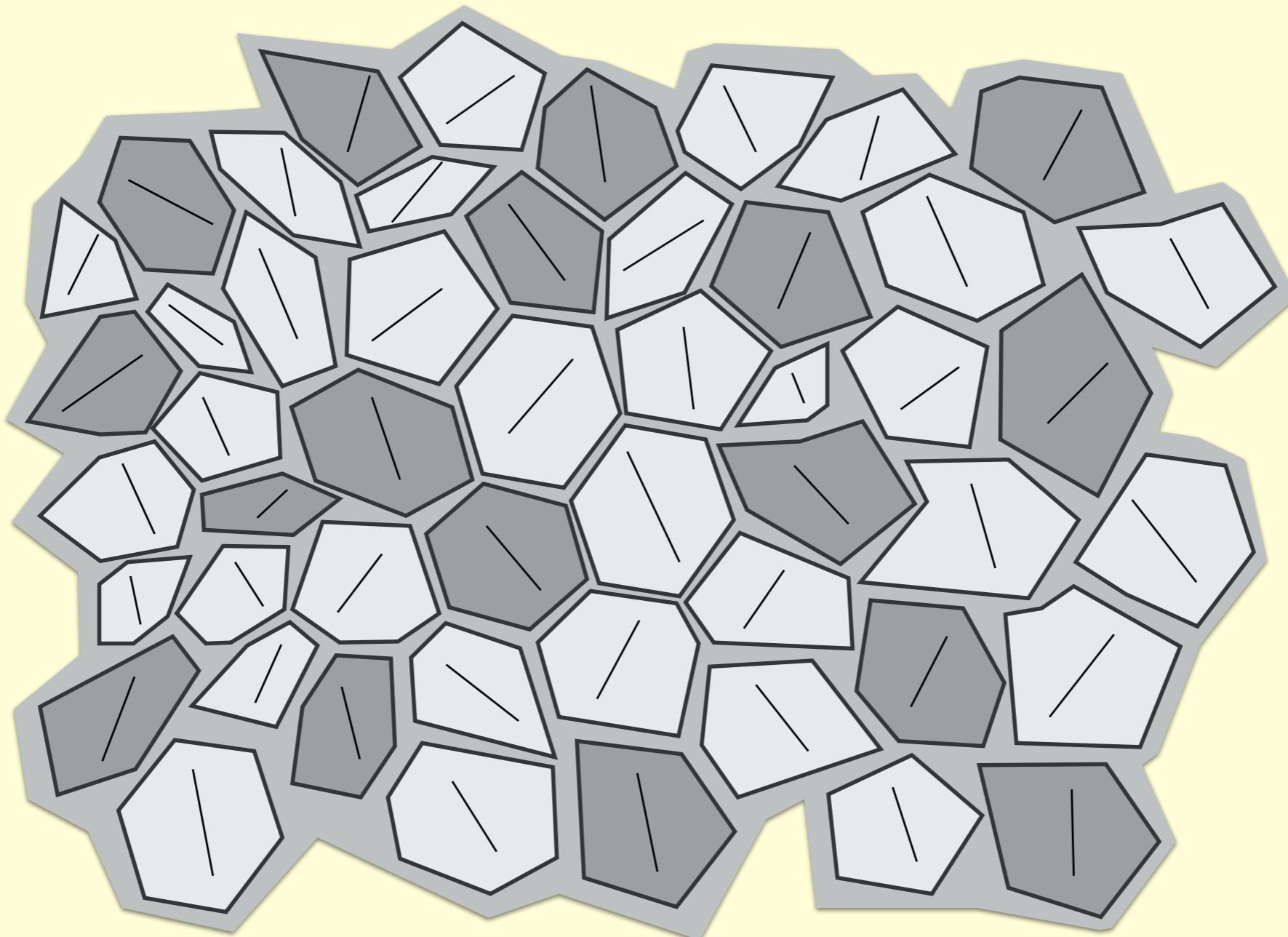
along
texture axis

perpendicular
texture axis

perpendicular
texture axis

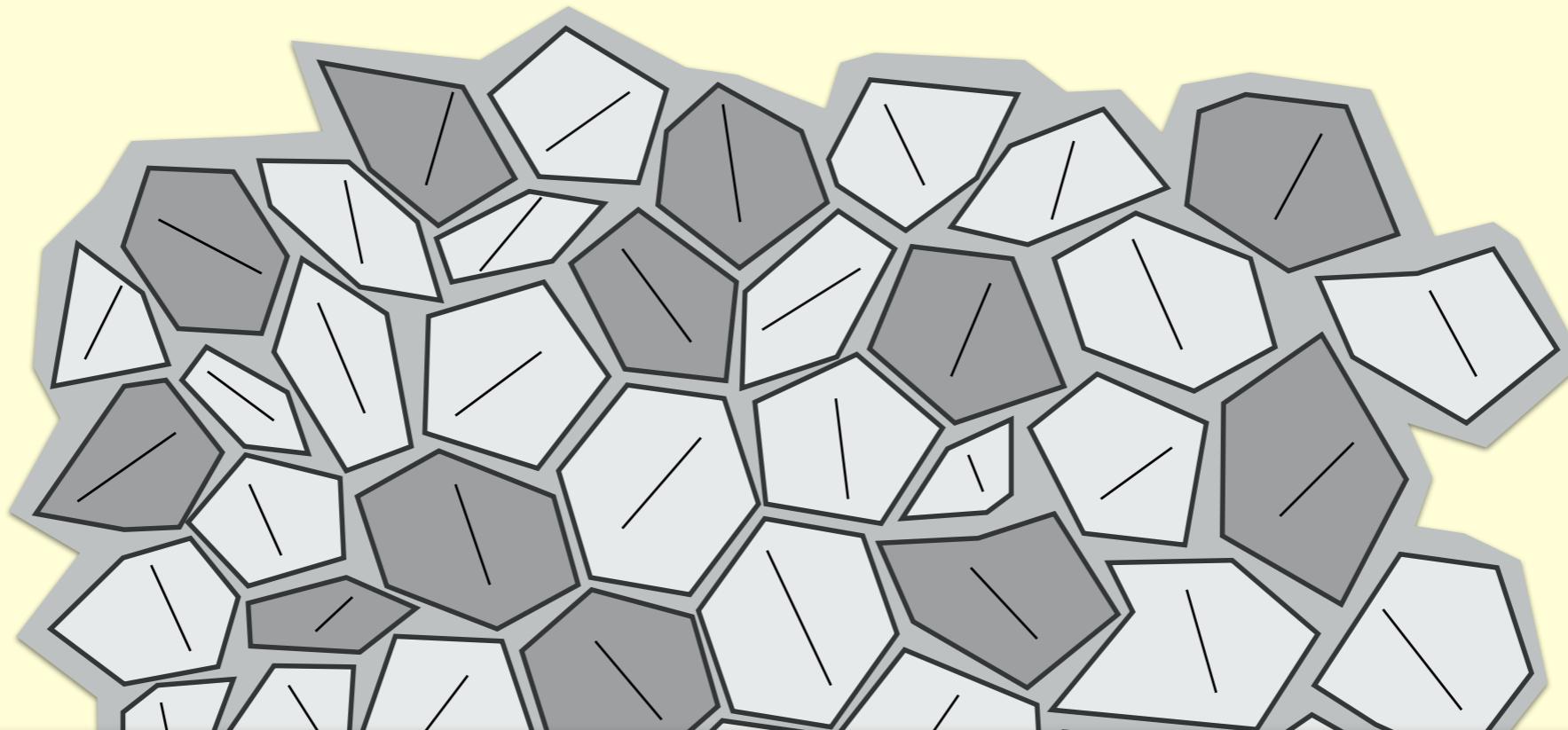
Nanostructured permanent magnet

Ensemble of single-domain grains (or particles)



Nanostructured permanent magnet

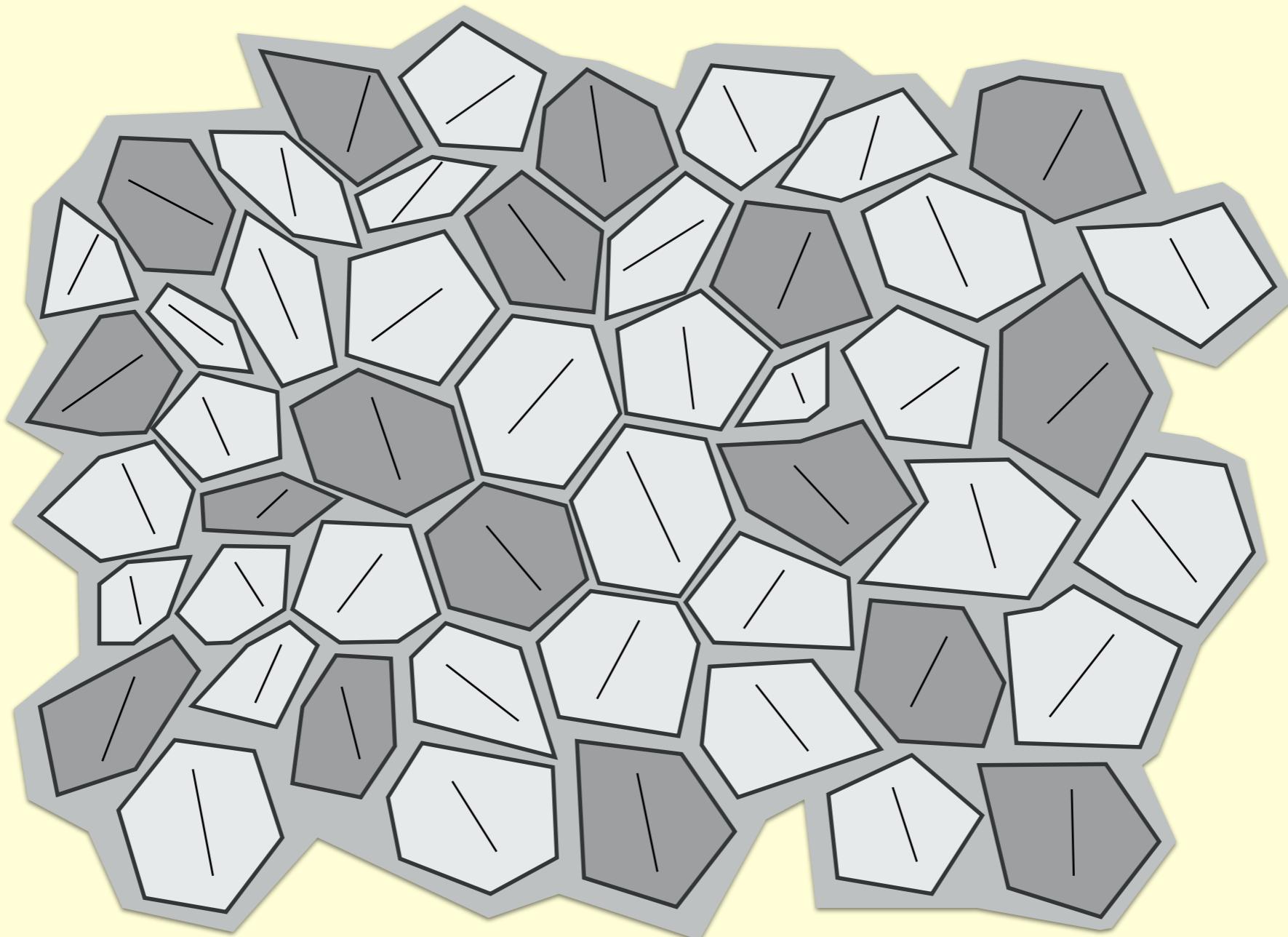
Ensemble of single-domain grains (or particles)



Expectation:
each grain (particle) magnetized
along its easy axis.

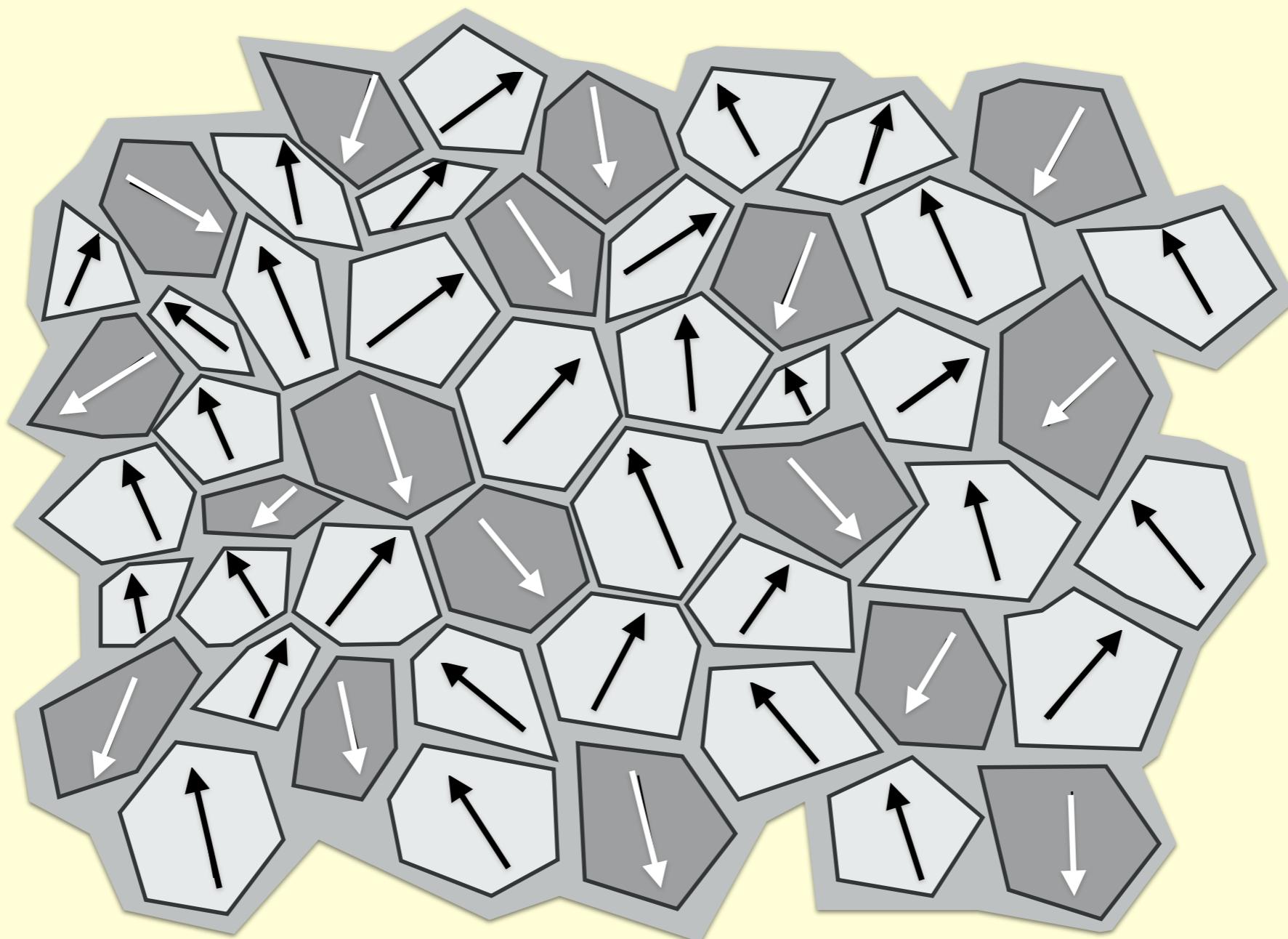
Nanostructured permanent magnet

Ensemble of single-domain grains (or particles)



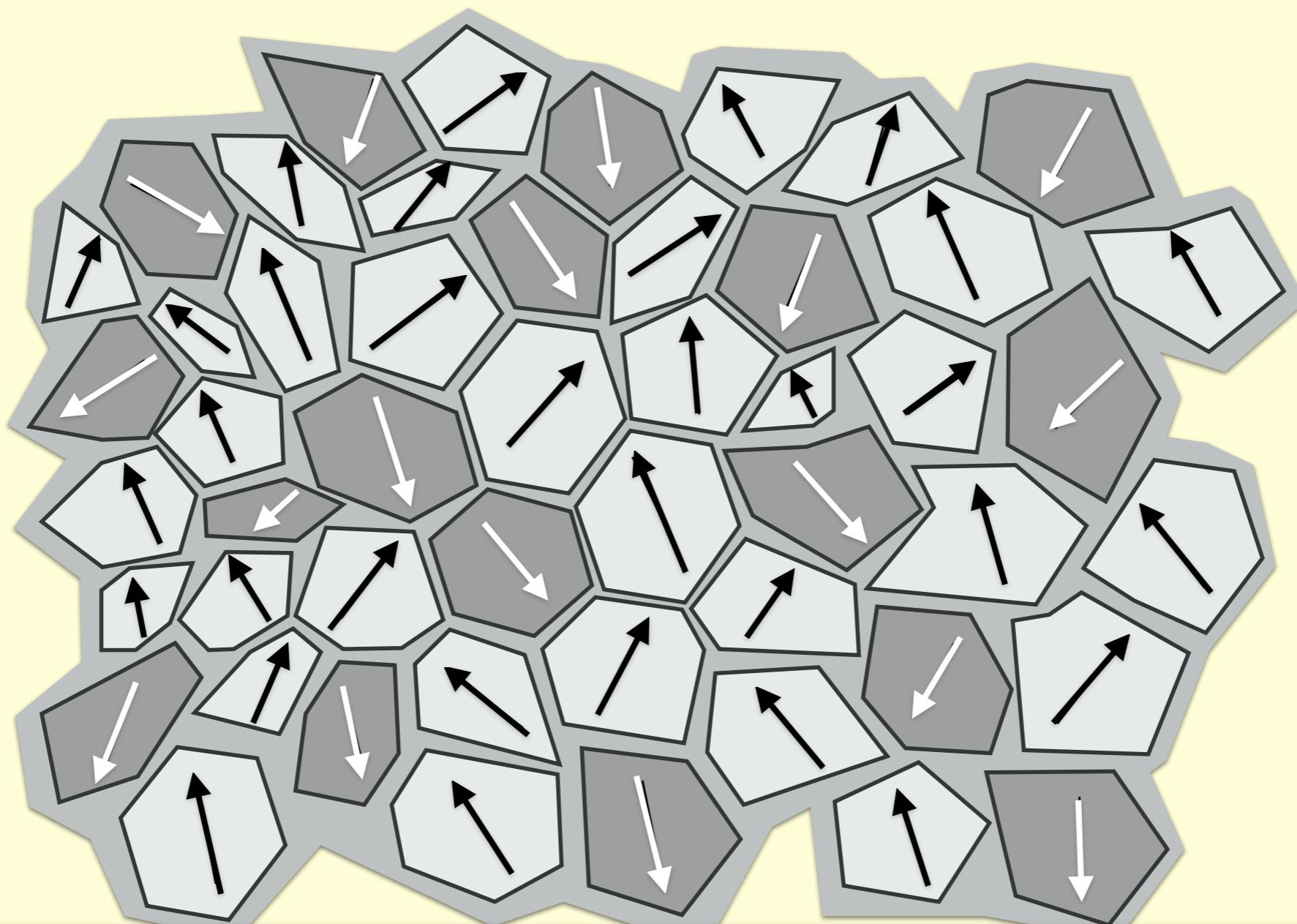
Nanostructured permanent magnet

Ensemble of single-domain grains (or particles)



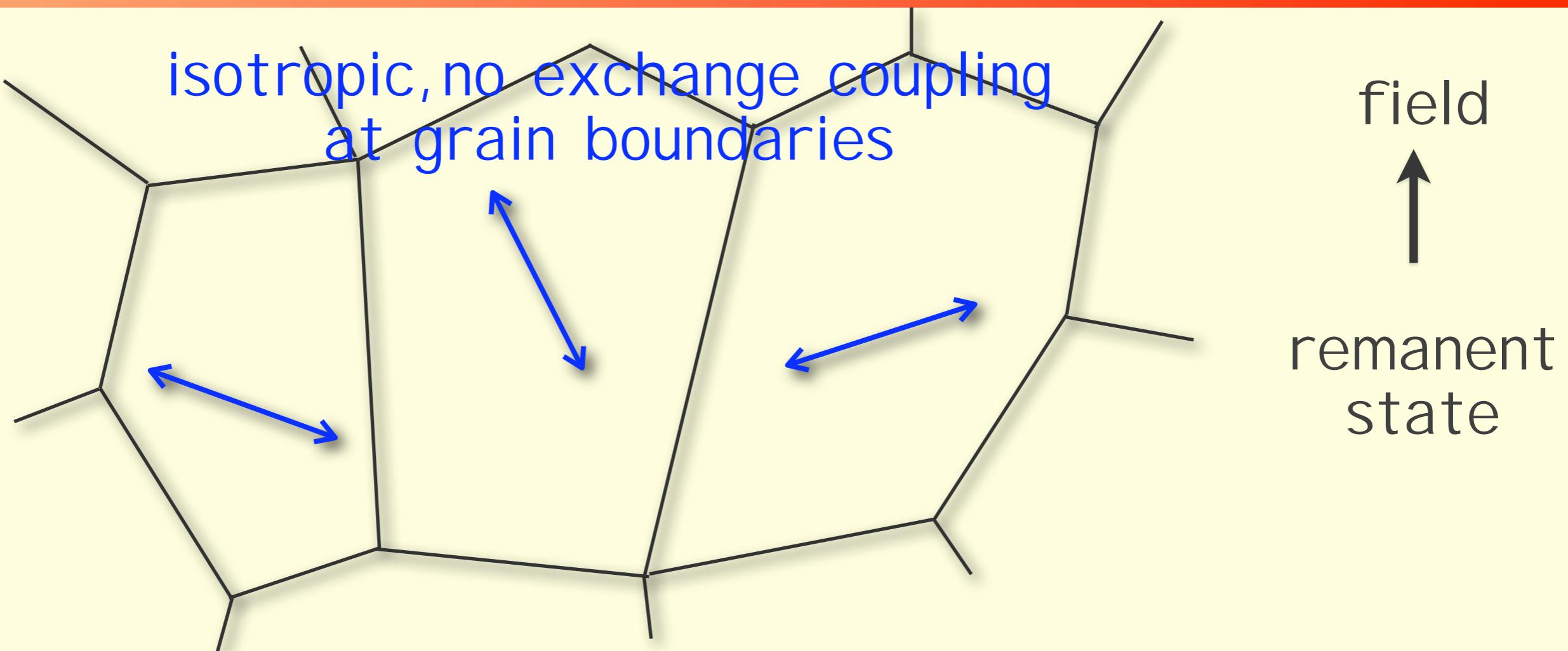
Nanostructured permanent magnet

Ensemble of single-domain grains (or particles)

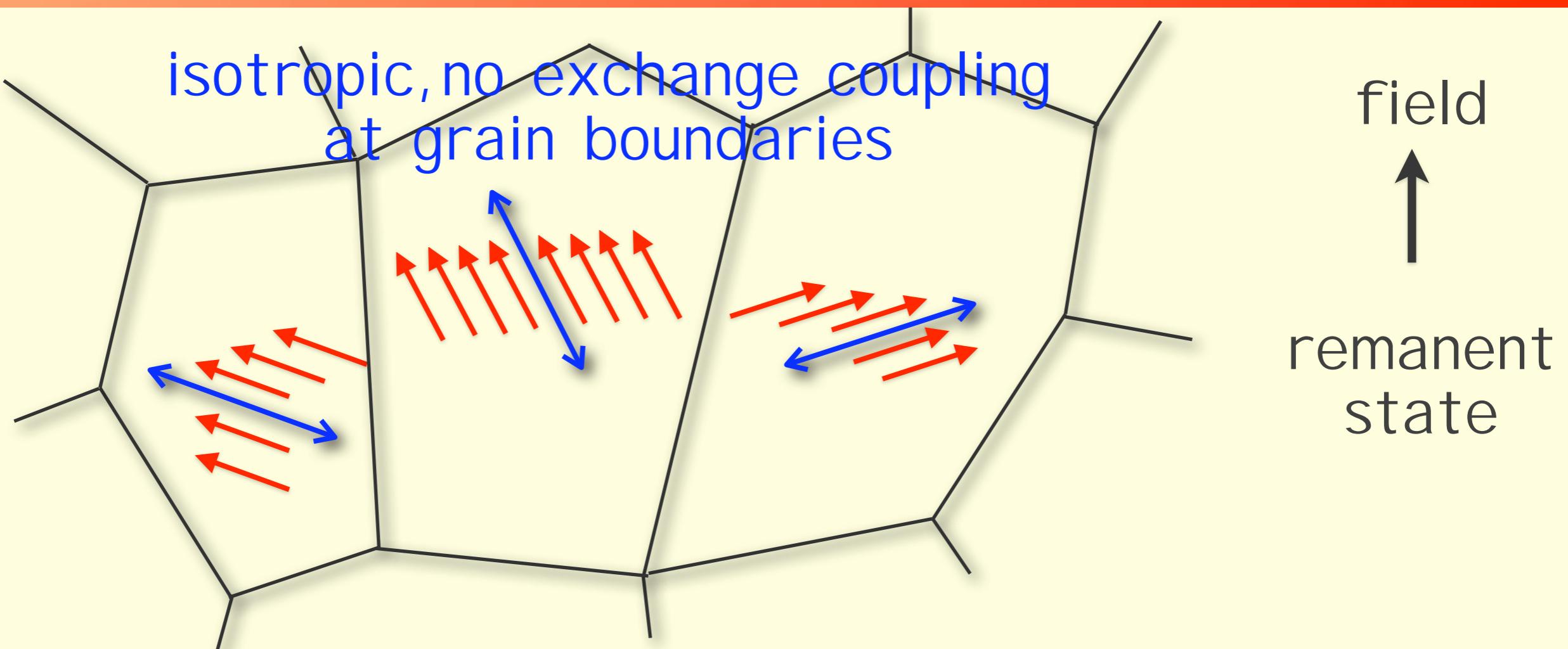


Details depend on grain interaction

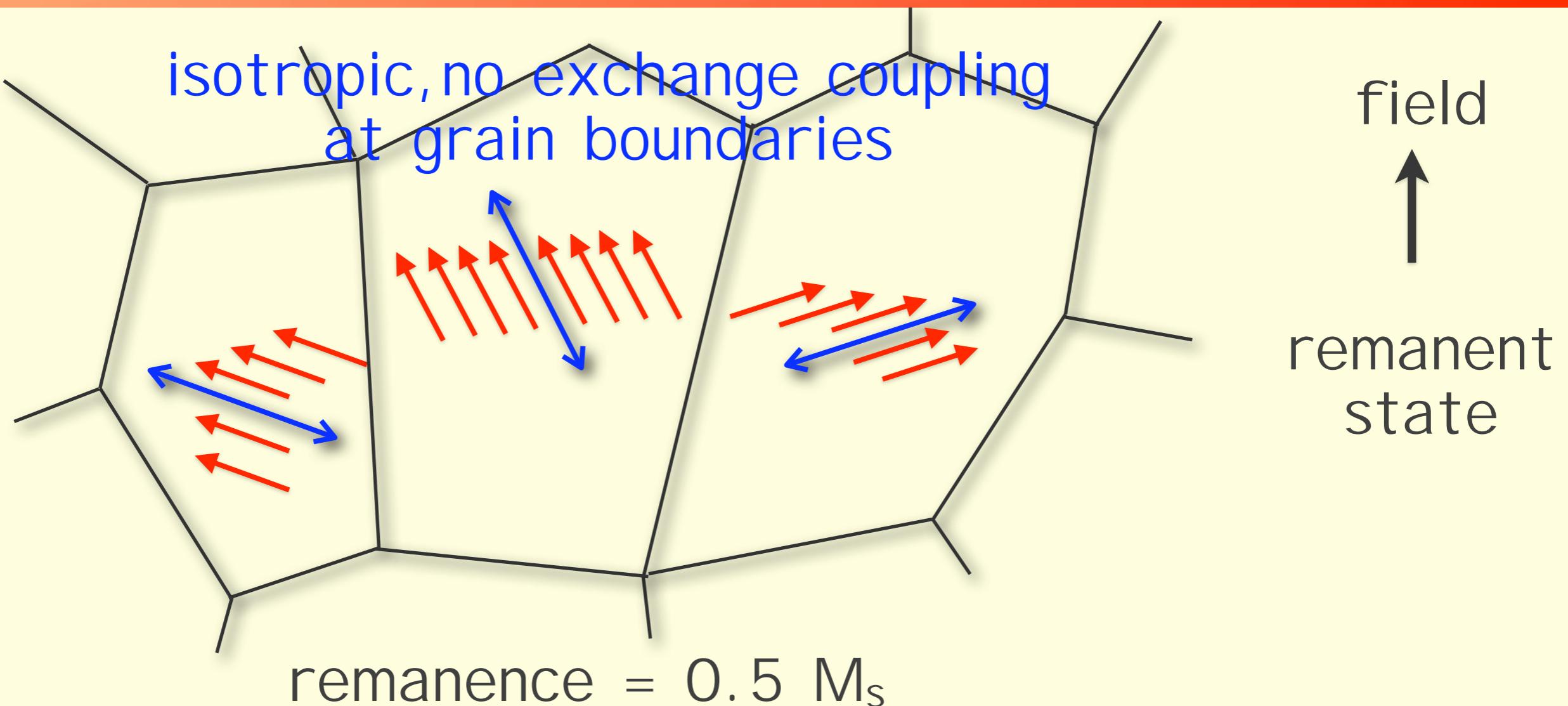
Nanostructured NdFeB: remanence enhancement



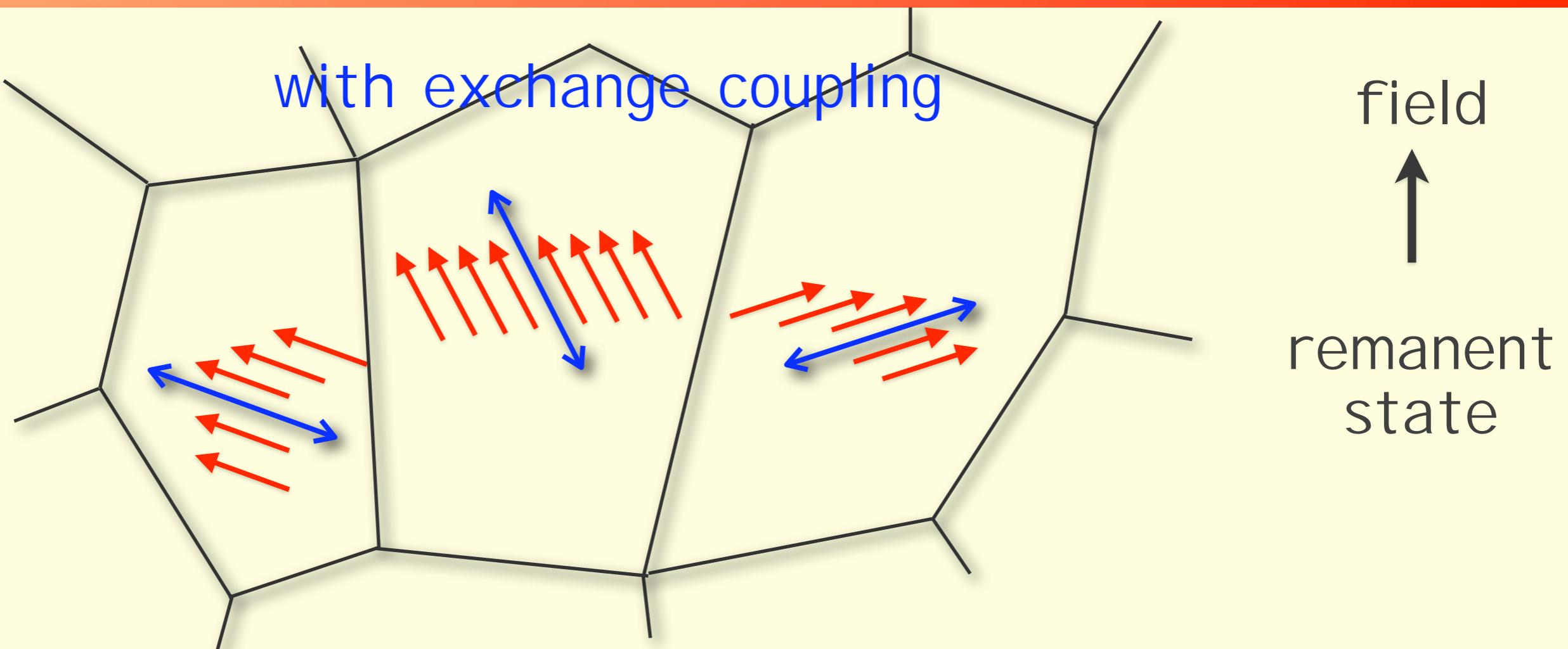
Nanostructured NdFeB: remanence enhancement



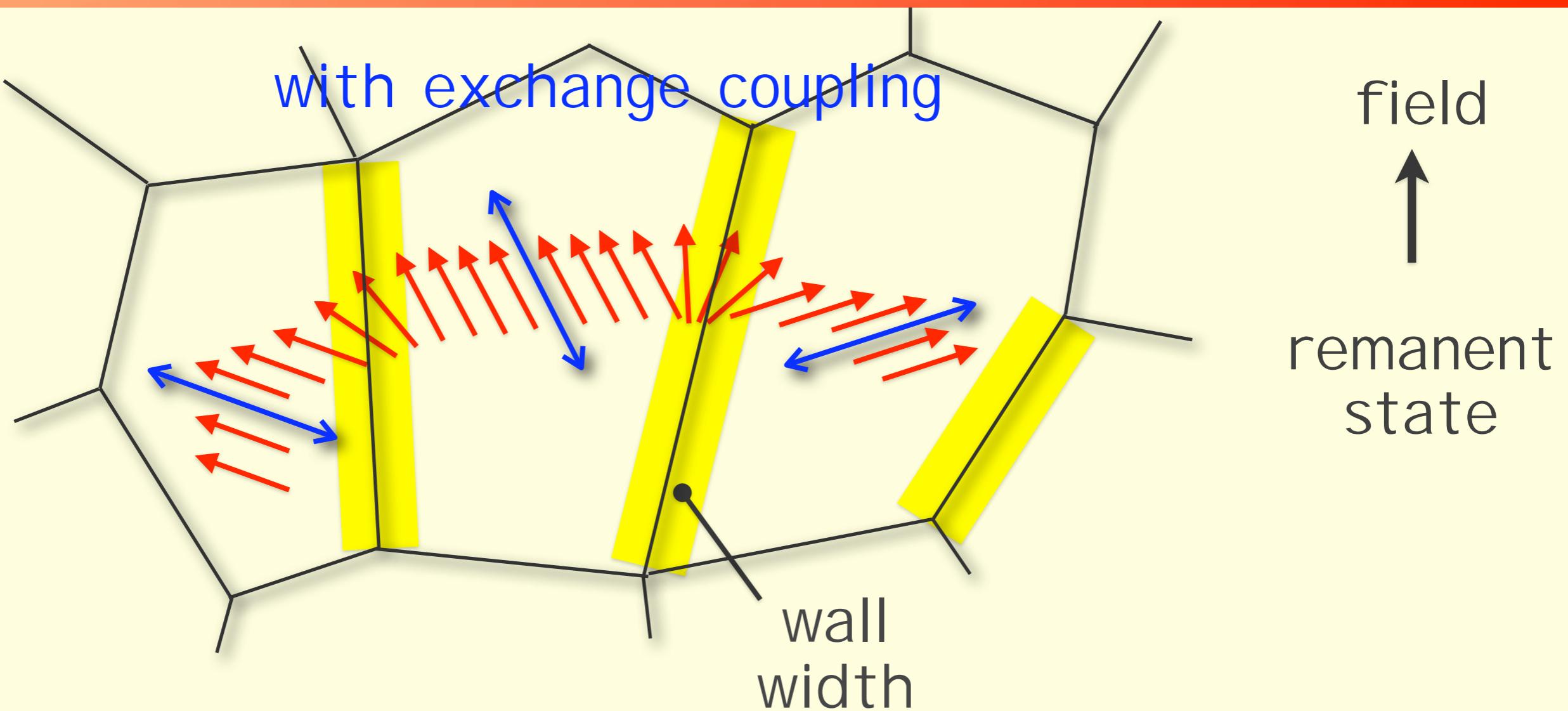
Nanostructured NdFeB: remanence enhancement



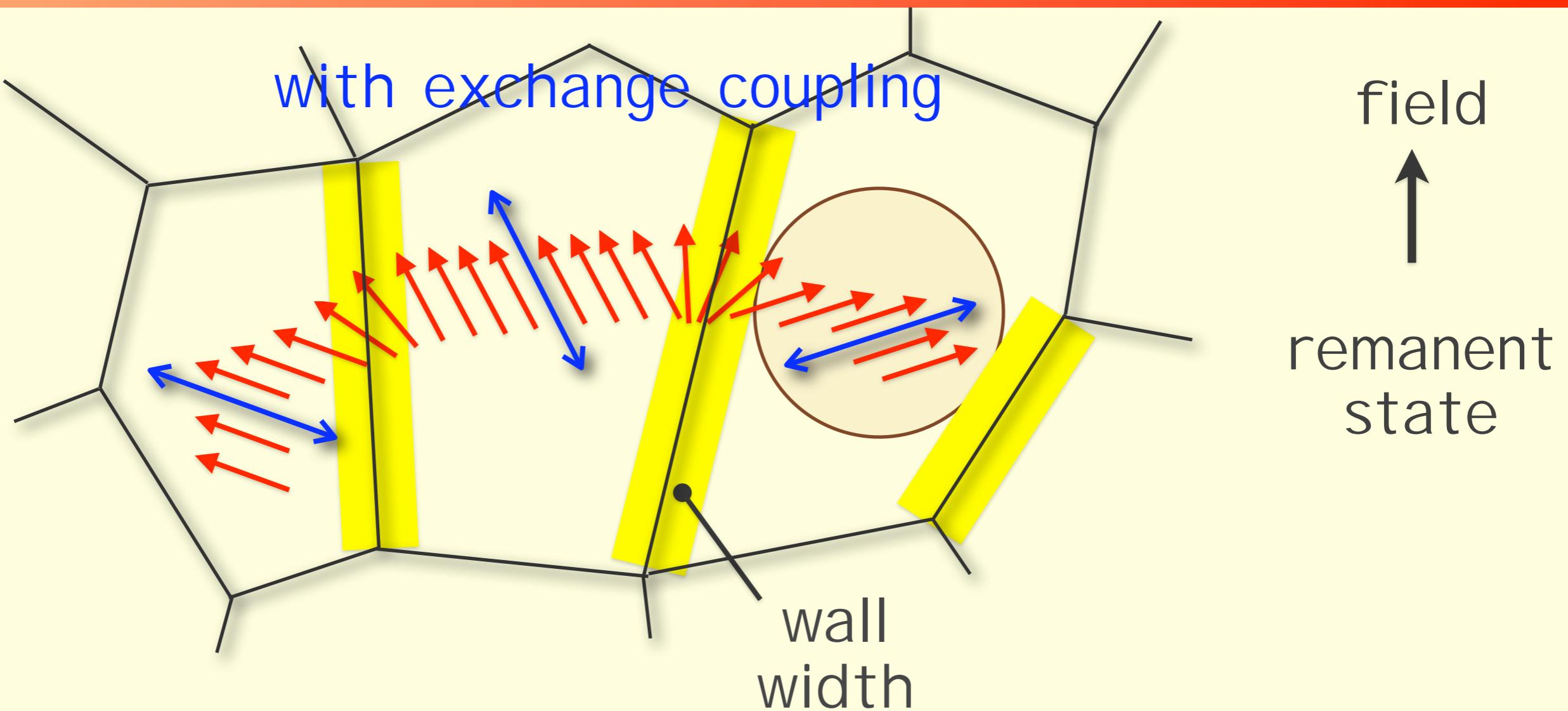
Nanostructured NdFeB: remanence enhancement



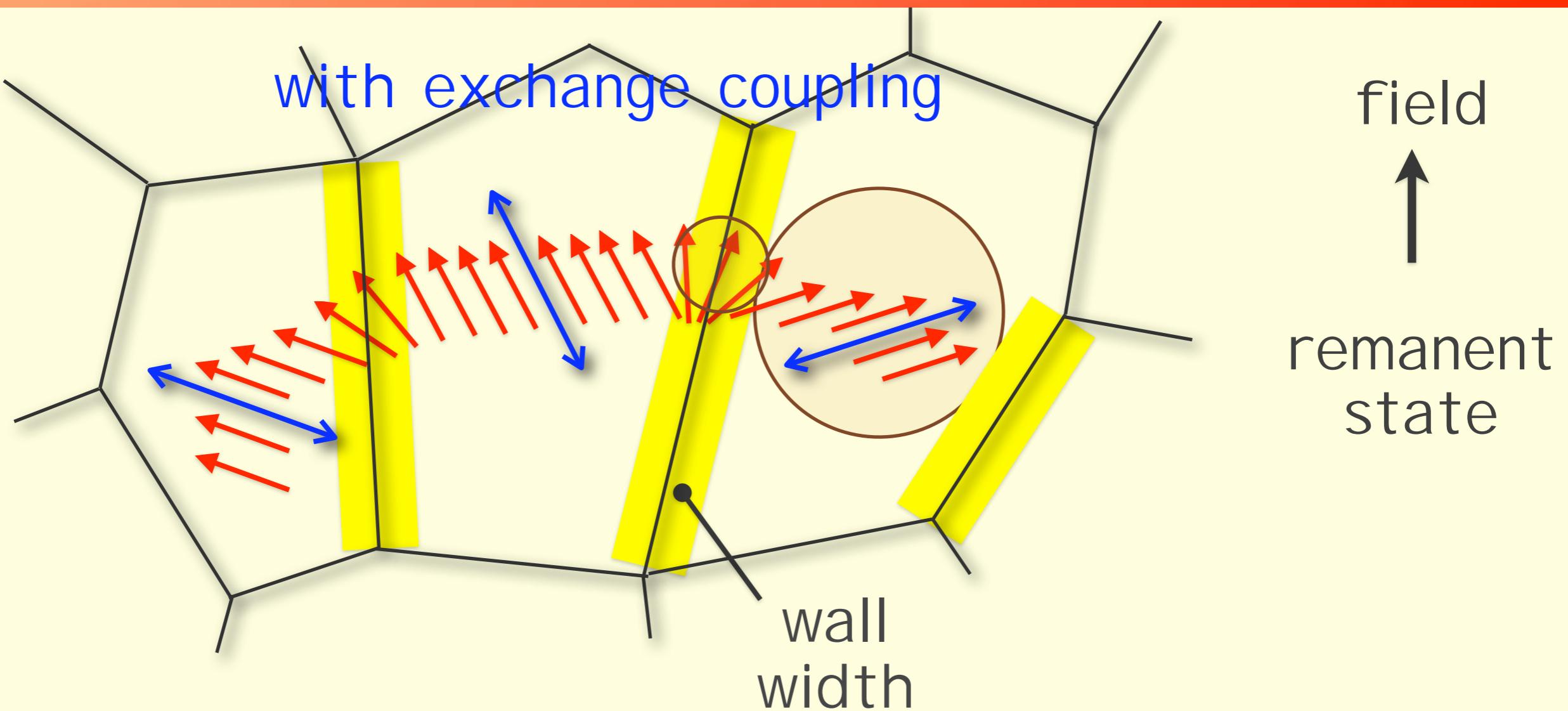
Nanostructured NdFeB: remanence enhancement



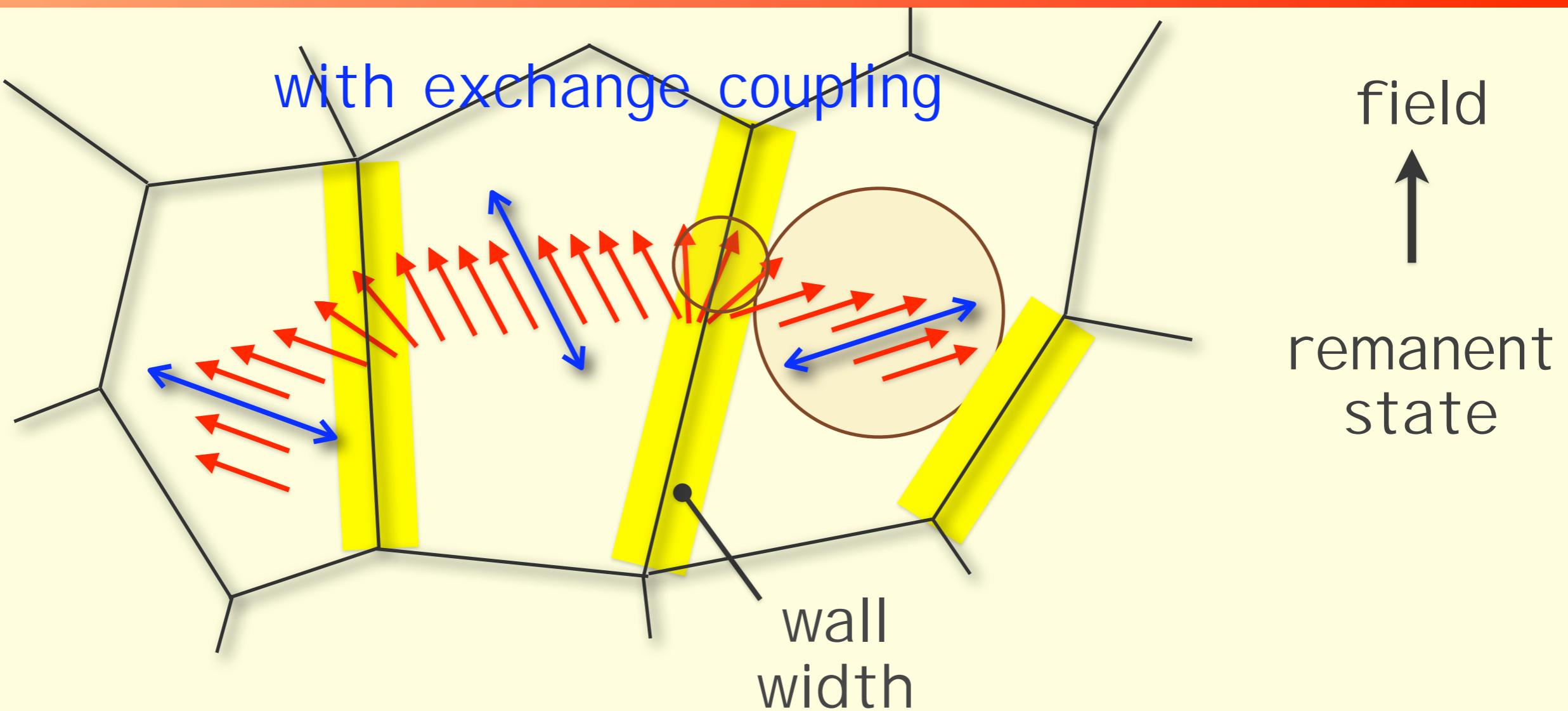
Nanostructured NdFeB: remanence enhancement



Nanostructured NdFeB: remanence enhancement

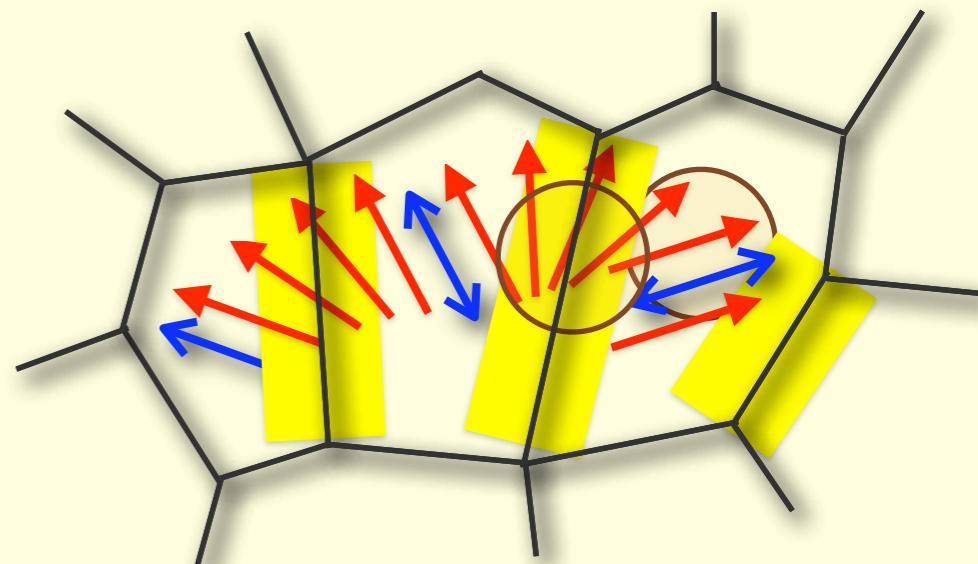
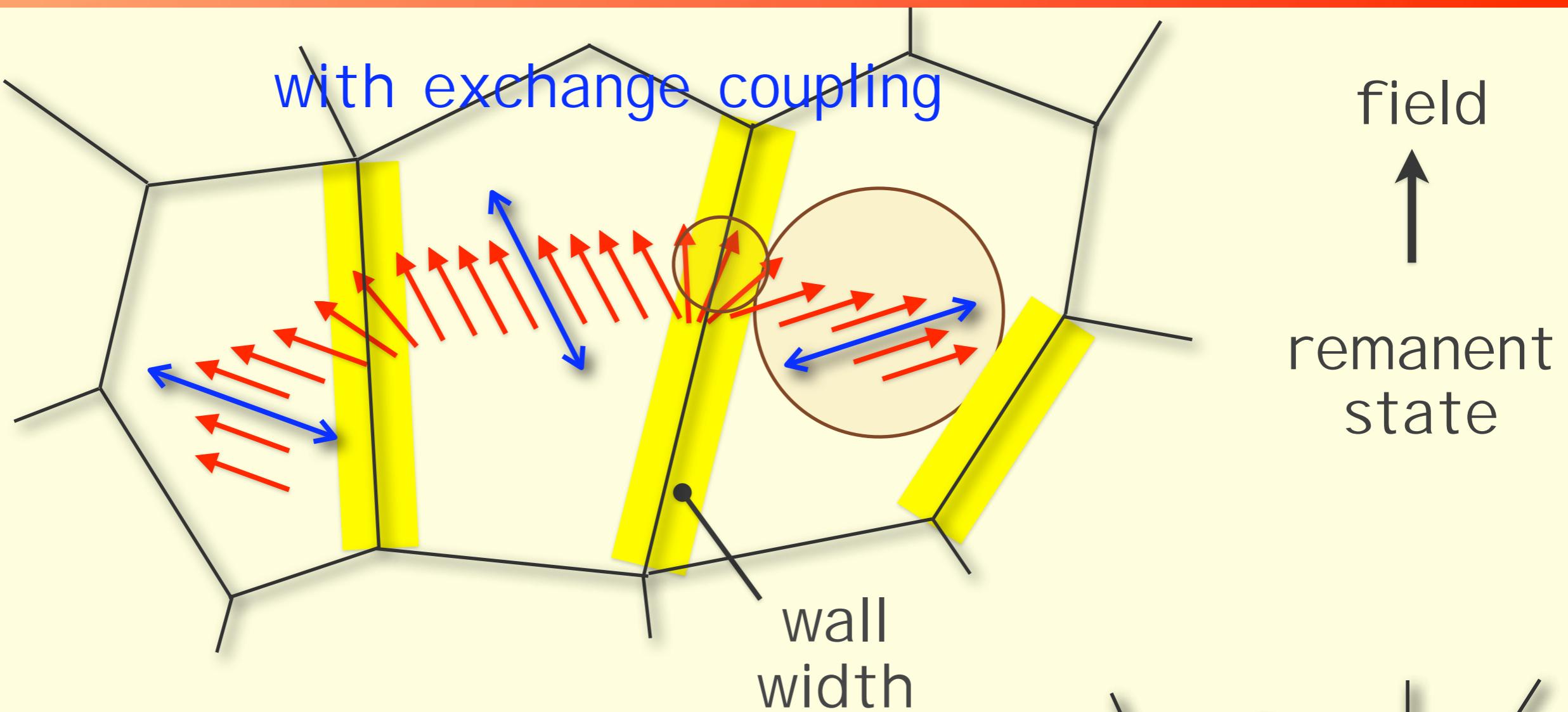


Nanostructured NdFeB: remanence enhancement

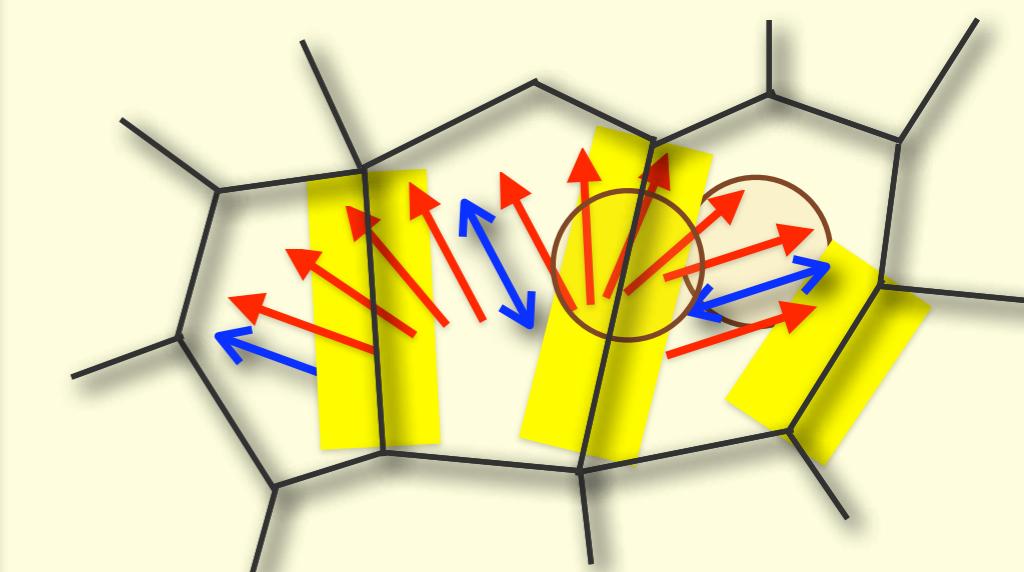
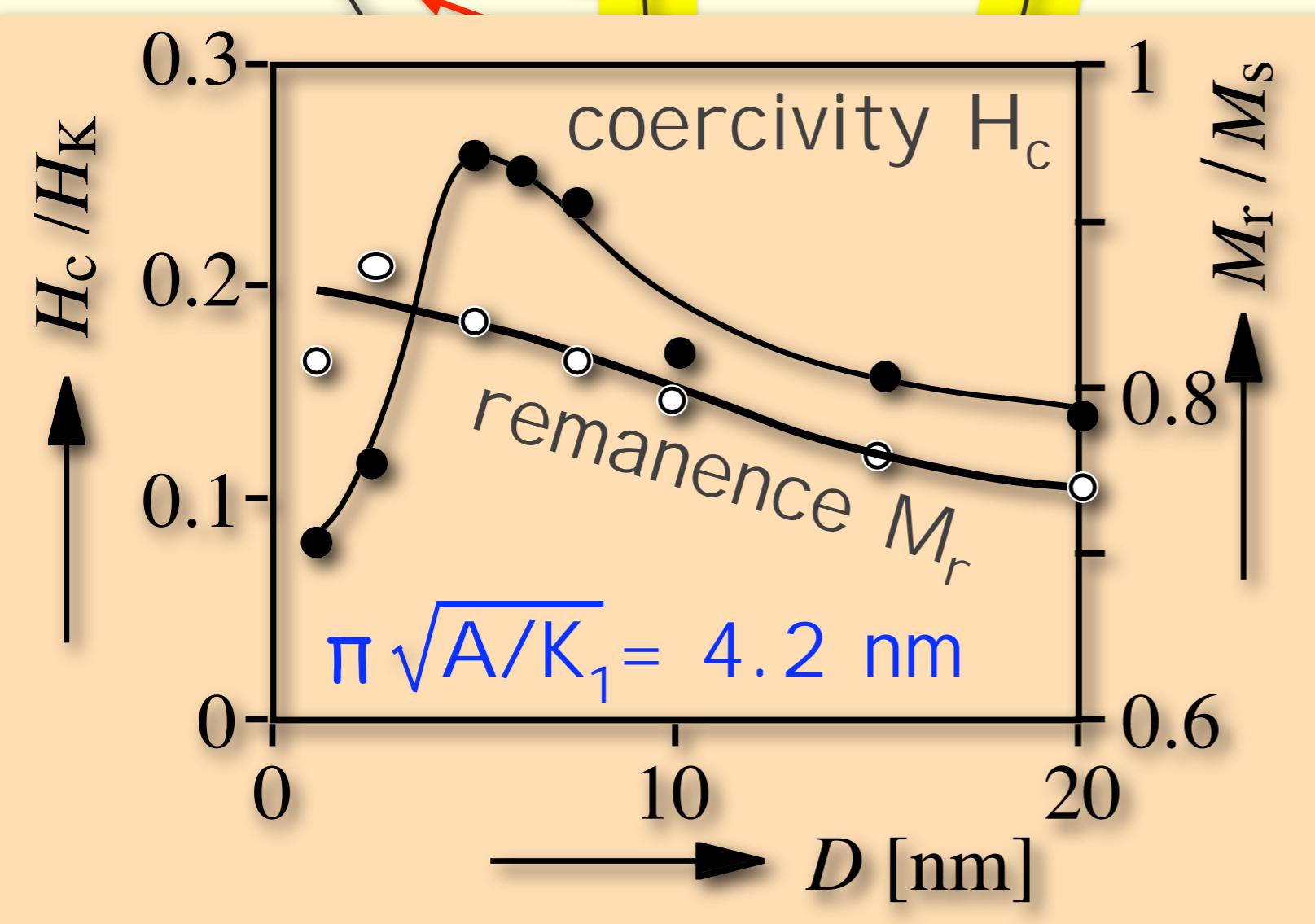
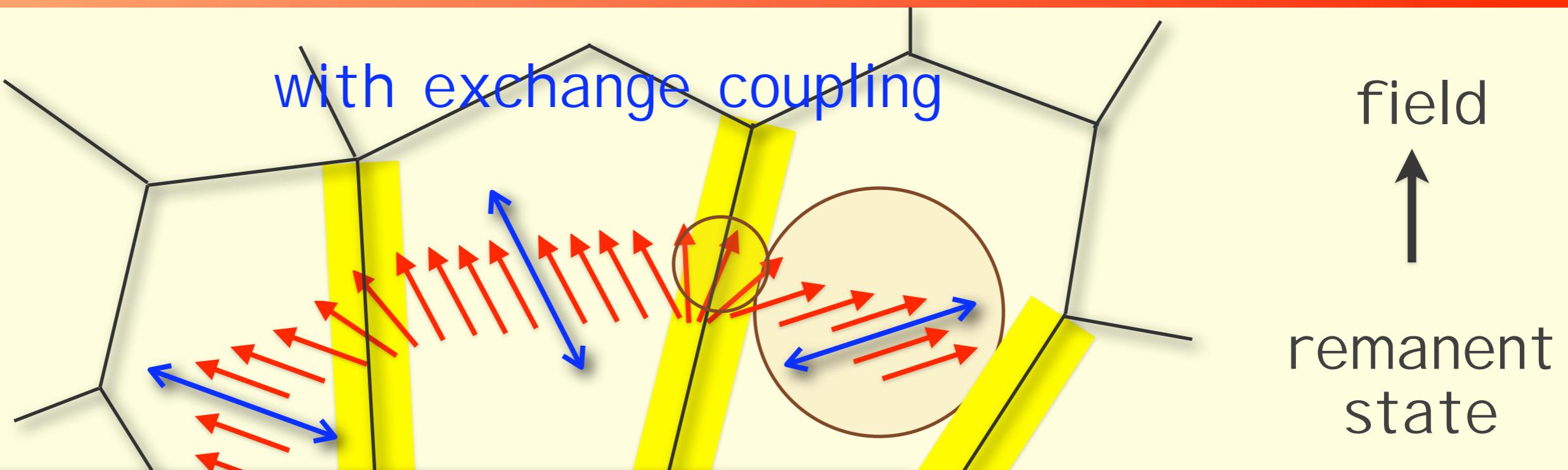


remanence > 0.5 M_s

Nanostructured NdFeB: remanence enhancement

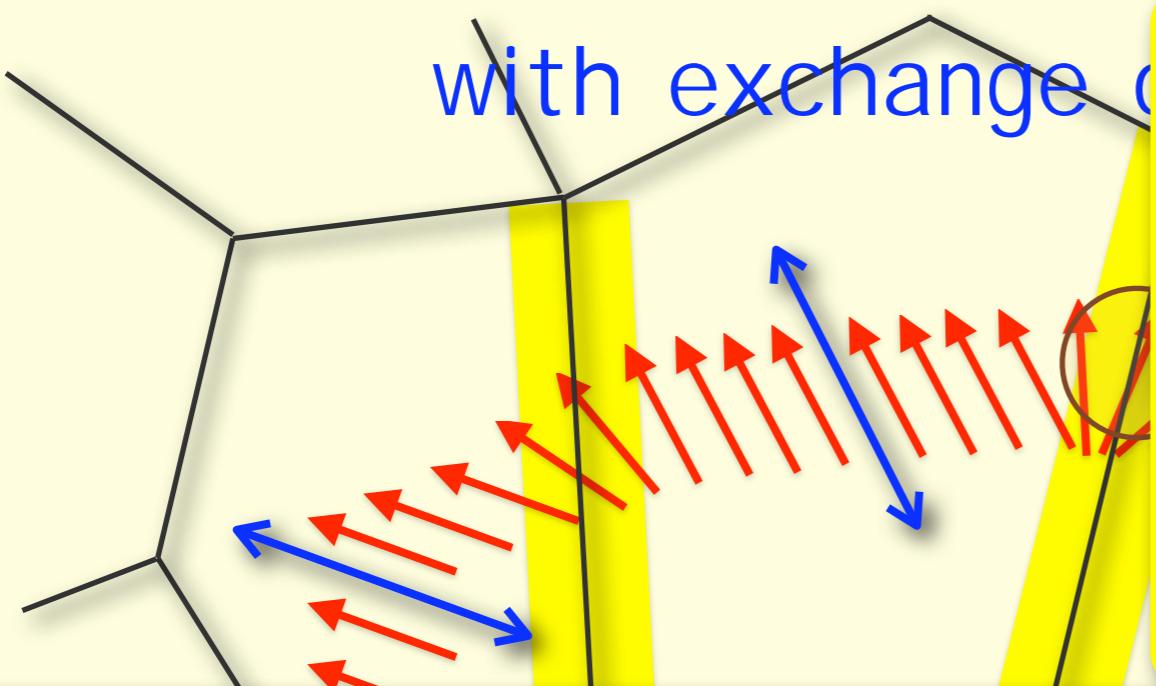


Nanostructured NdFeB: remanence enhancement

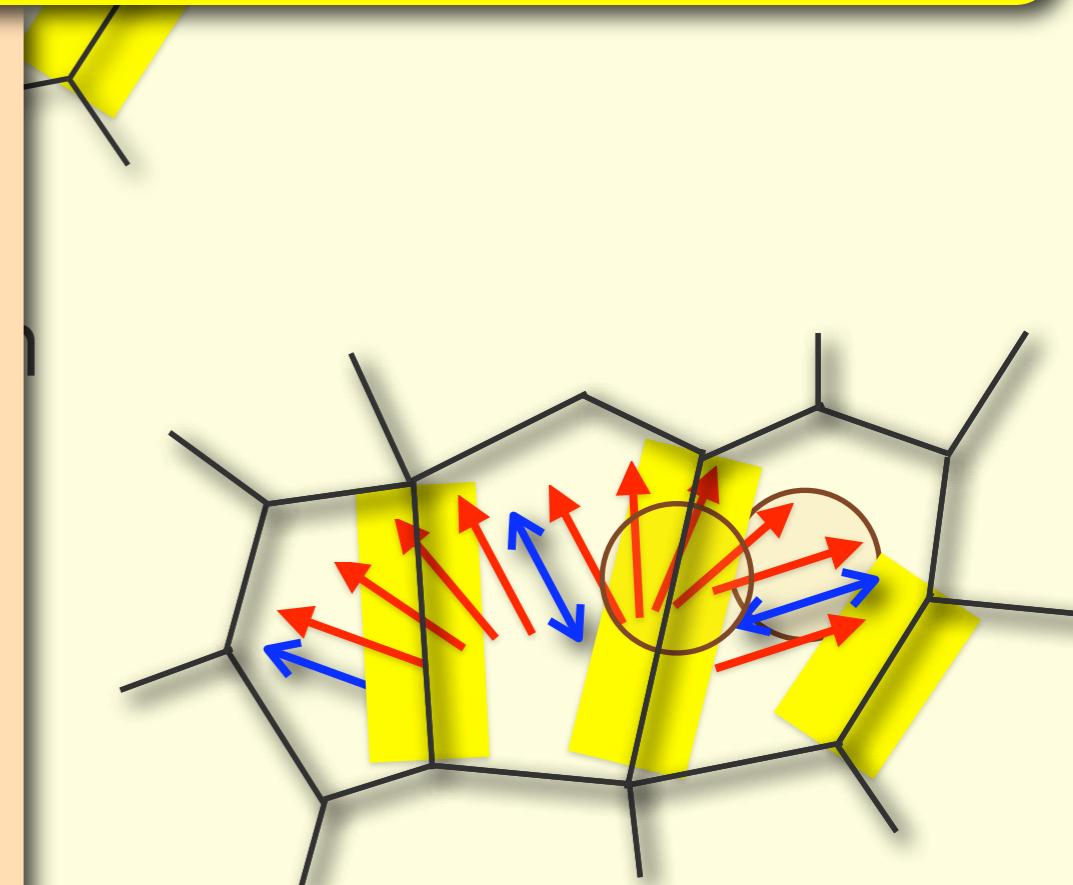
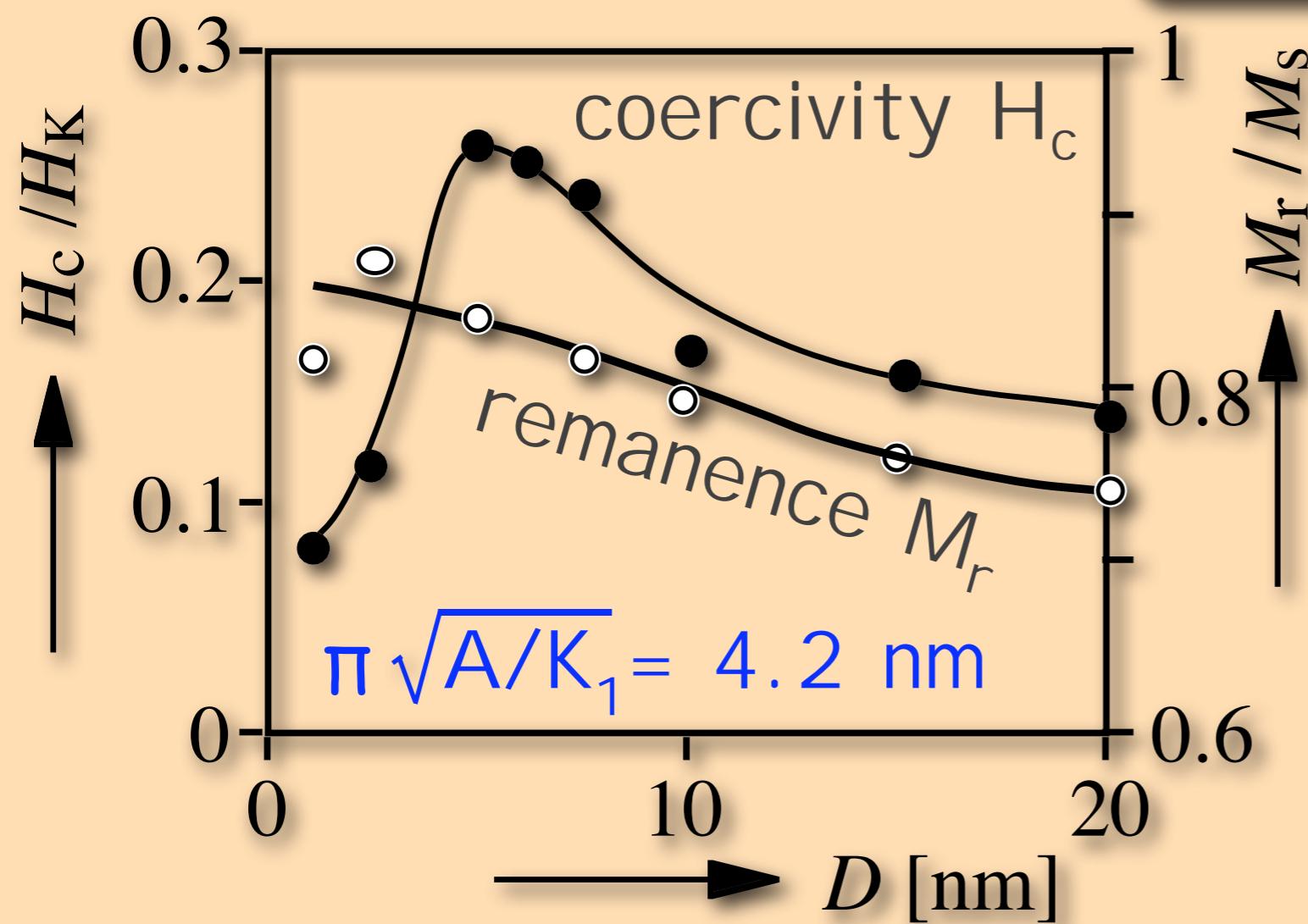


W. Rave & K. Ramstöck,
JMMM 171 (1997)

Nanostructured NdFeB: remanence enhancement

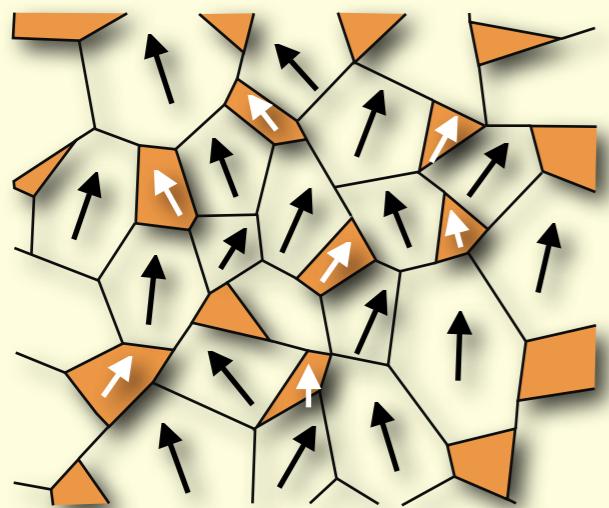


$\text{Nd}_2\text{Fe}_{14}\text{B}:$
 $K_u = 4.3 \cdot 10^6 \text{ kJ/m}^3$
 $A = 8 \cdot 10^{-12} \text{ J/m}$
 $L_{ex} = \sqrt{A/K_1} = 1.3 \text{ nm}$



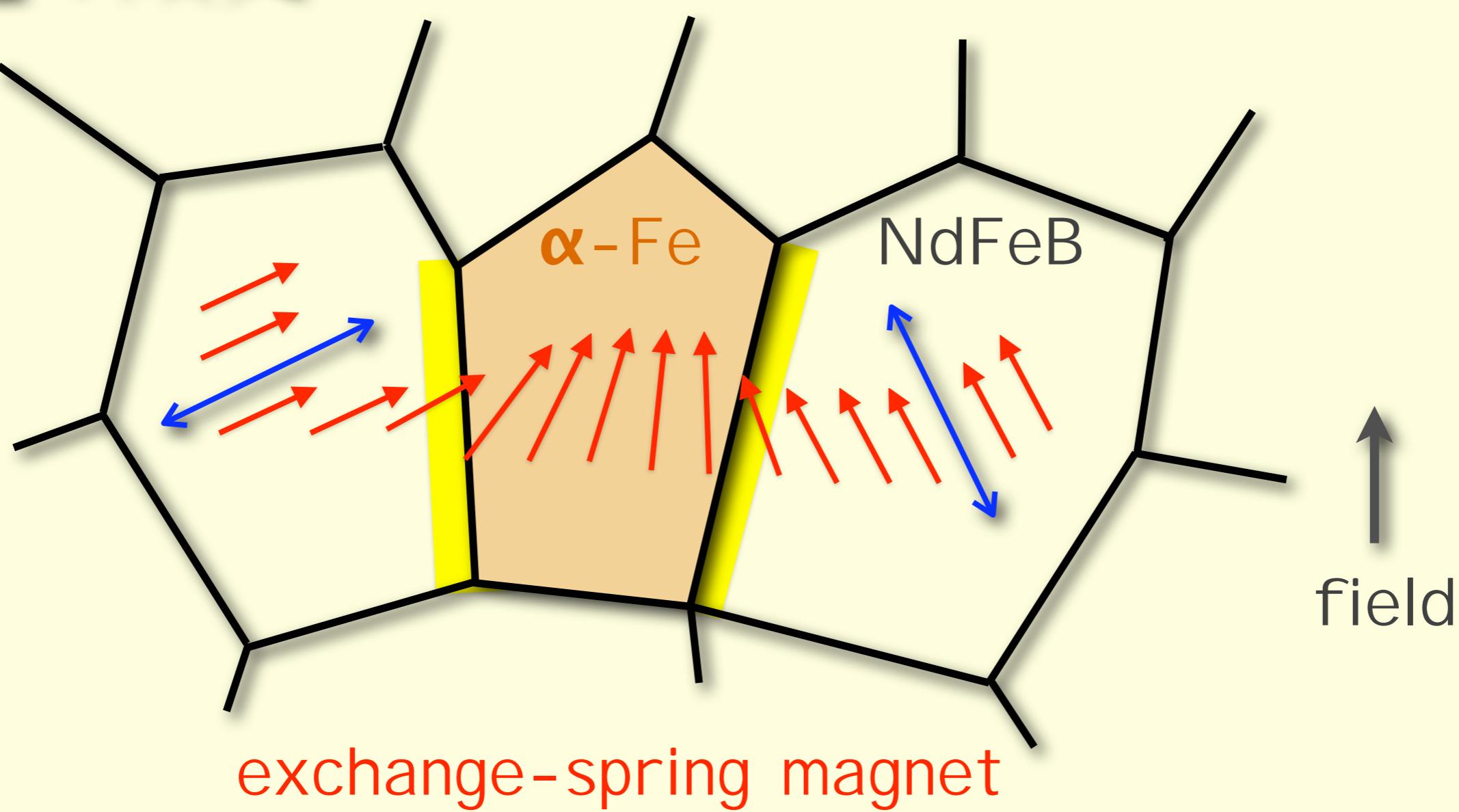
W. Rave & K. Ramstöck,
JMMM 171 (1997)

Nanostructured NdFeB: remanence enhancement

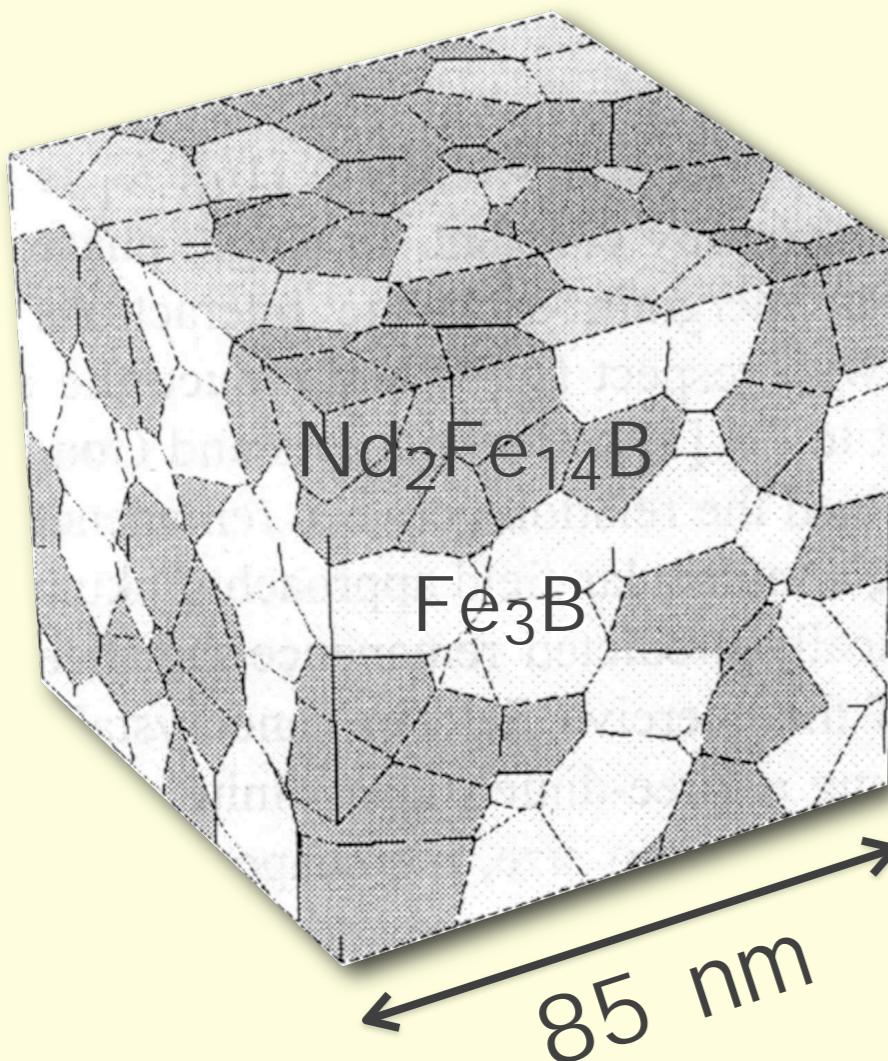


$\text{Nd}_2\text{Fe}_{14}\text{B}$ ($J_s = 1.6 \text{ T}$)

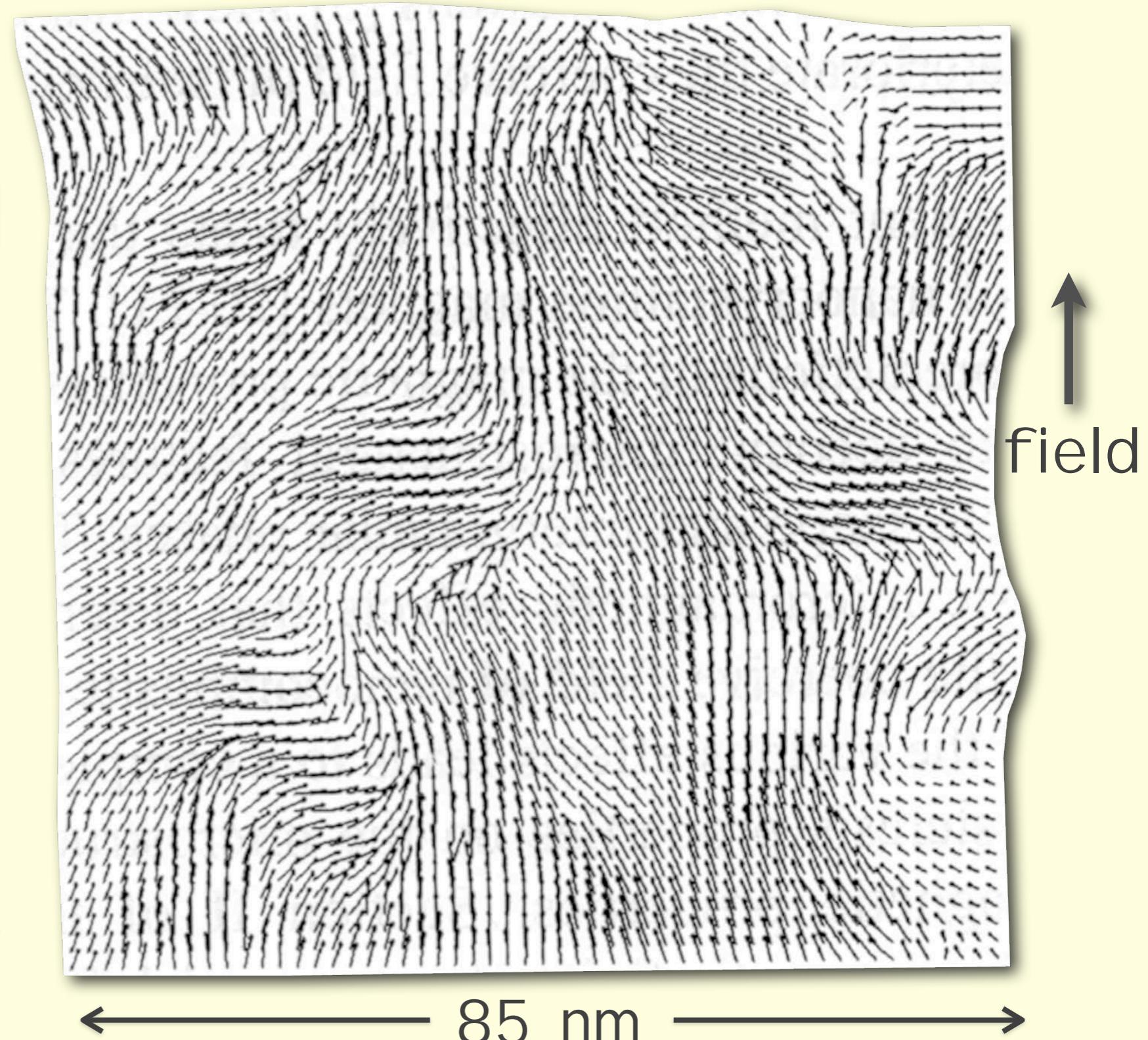
$\alpha\text{-Fe}$ ($J_s = 2.1 \text{ T}$)



Nanostructured NdFeB: exchange-spring magnet



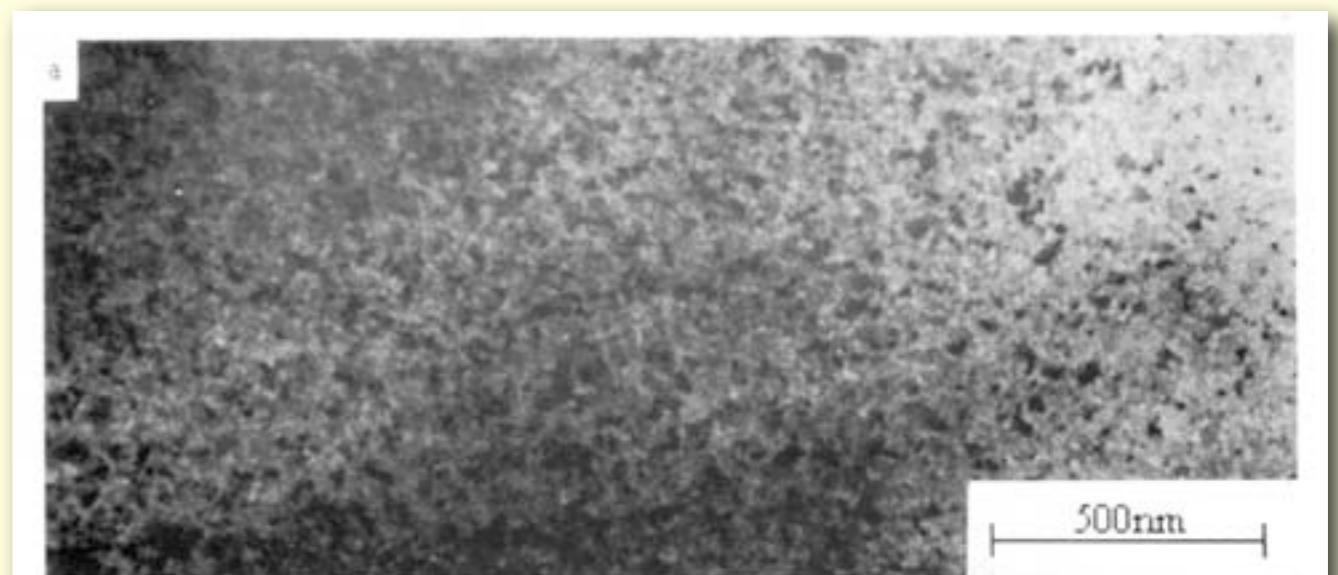
remanent state



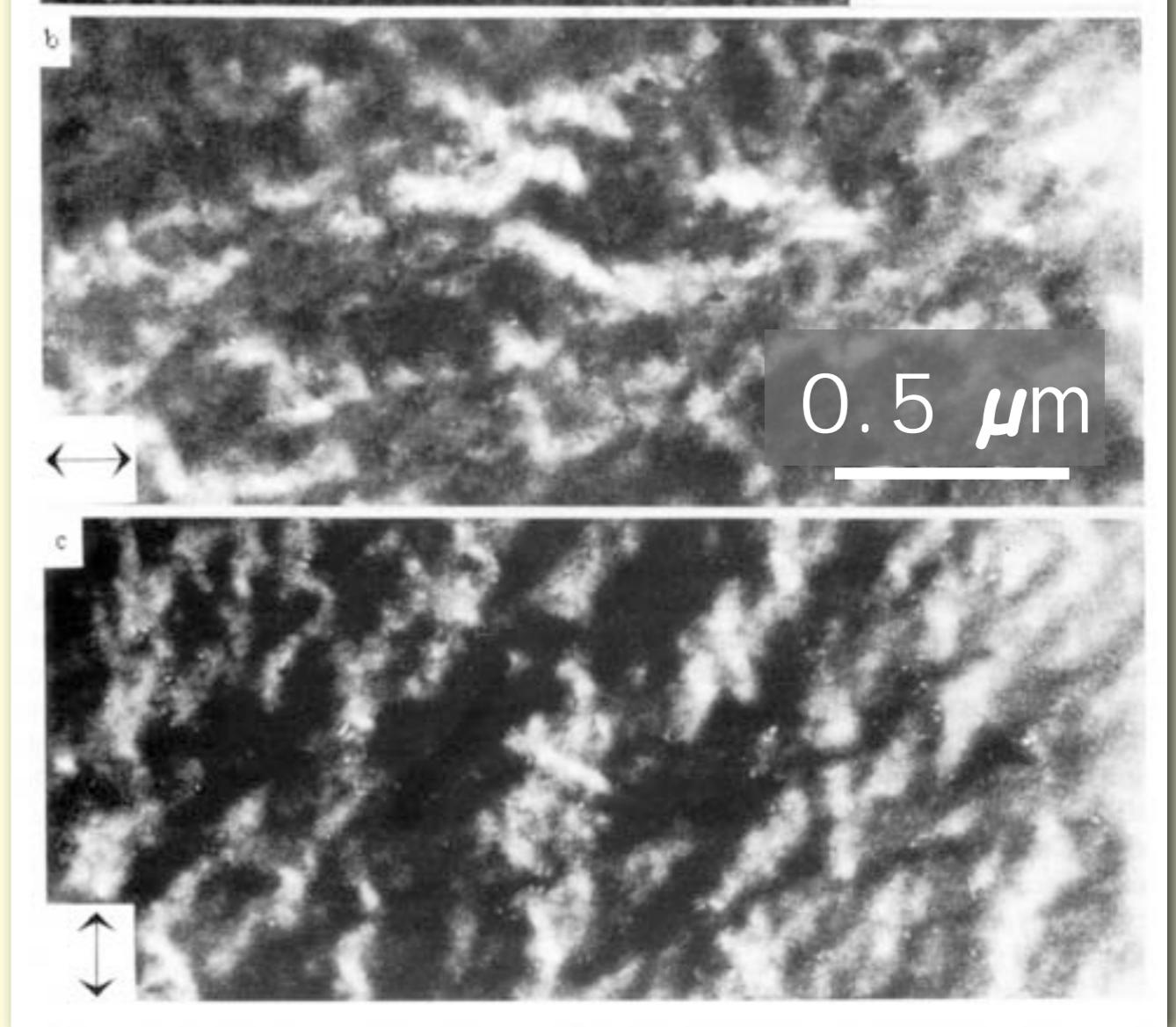
T. Schrefl and J. Fidler,
IEEE Trans. Magn. 35,
3223 (1999)

Nanostructured NdFeB: exchange-spring magnet

Bright field
TEM image



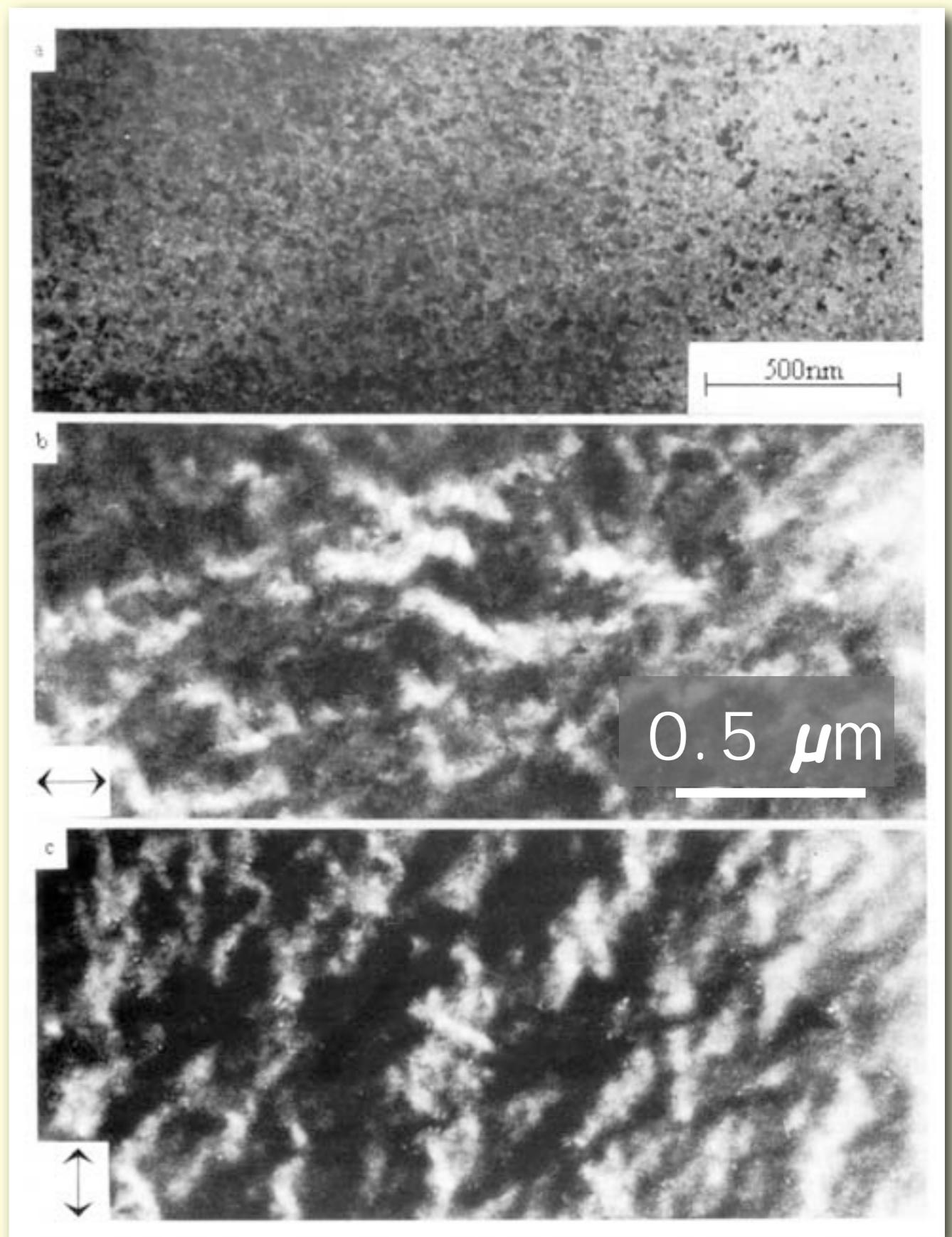
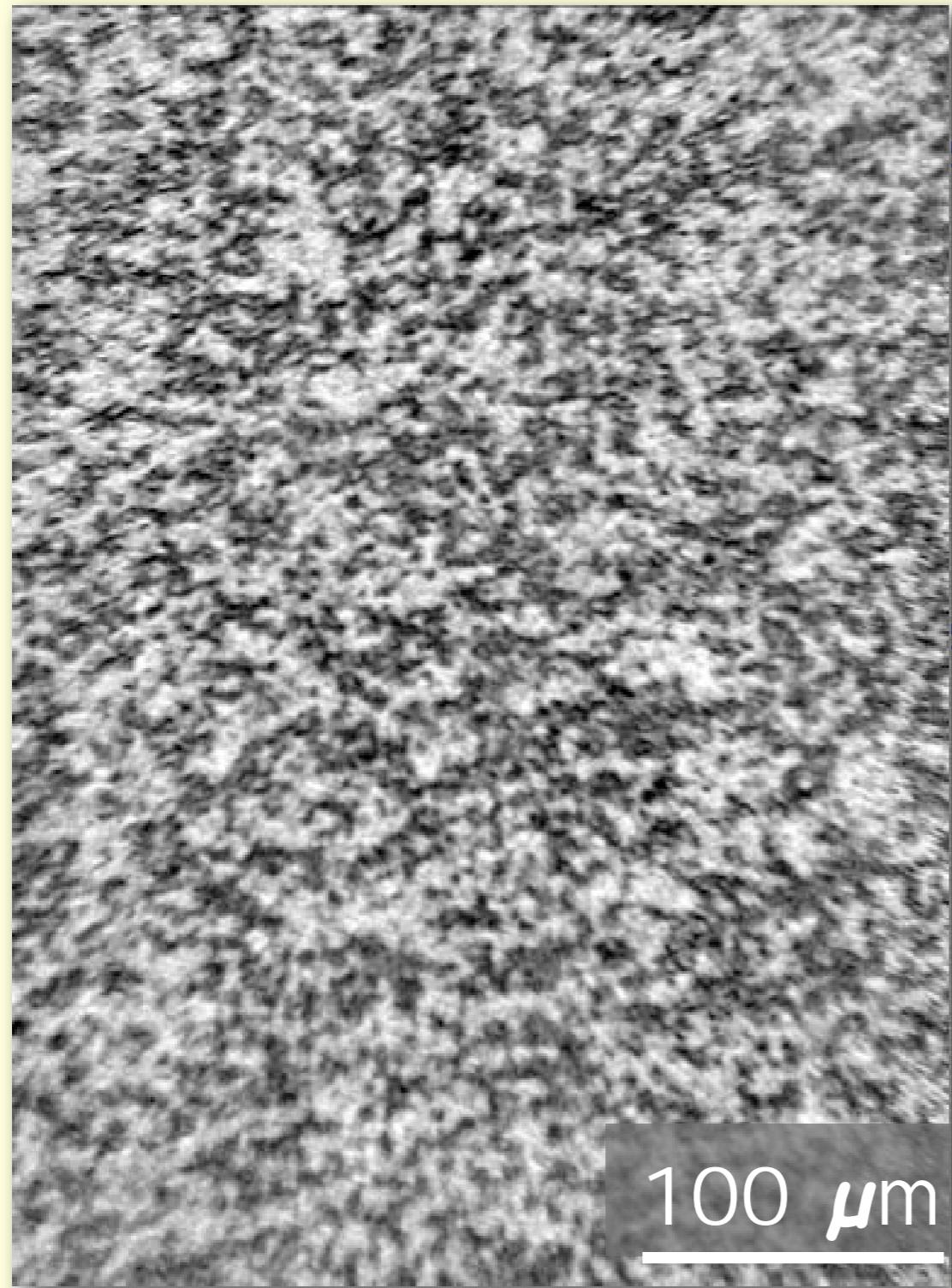
Foucault
image



J. Chapman et al.,
13th Int. Workshop on
RE Magnets and their
Applications (1994)

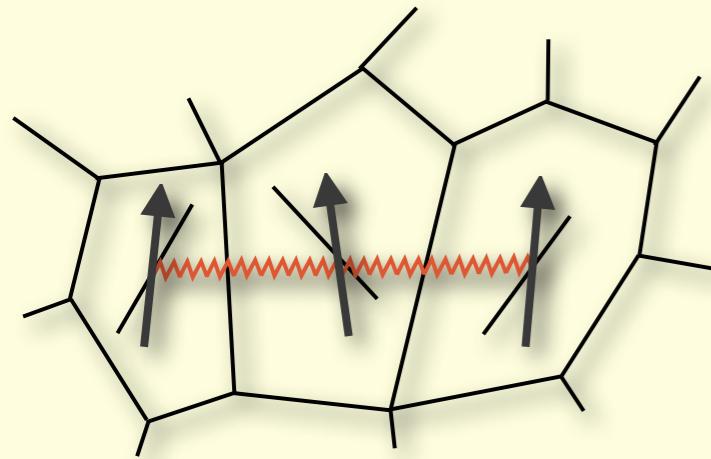
Nanostructured NdFeB: exchange-spring magnet

FeSiBCuNb overannealed



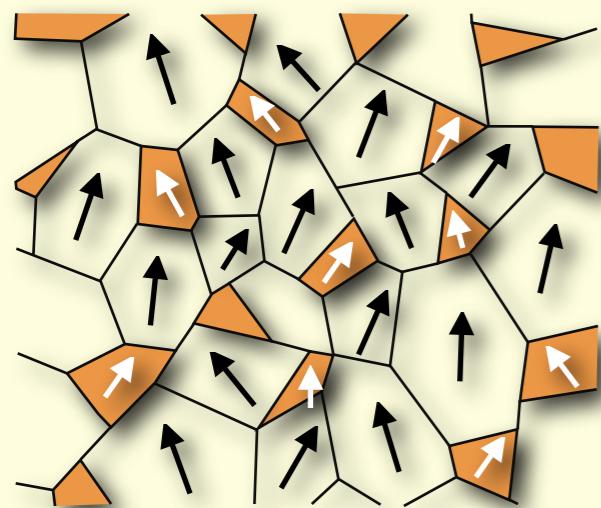
3 types of nanostructured NdFeB magnets

Isotropic magnets: Remanence ($M_r = M_s/2$)



exchanged coupled grains
based on stoichiometric
 $Nd_2Fe_{14}B$

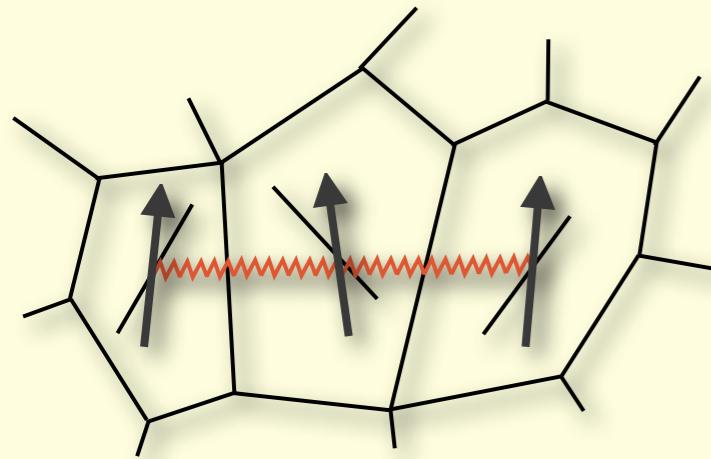
Remanence
enhancement
for isotropic
magnets



exchanged coupled grains
based on nanocomposite
 $Nd_2Fe_{14}B / \alpha\text{-Fe}$

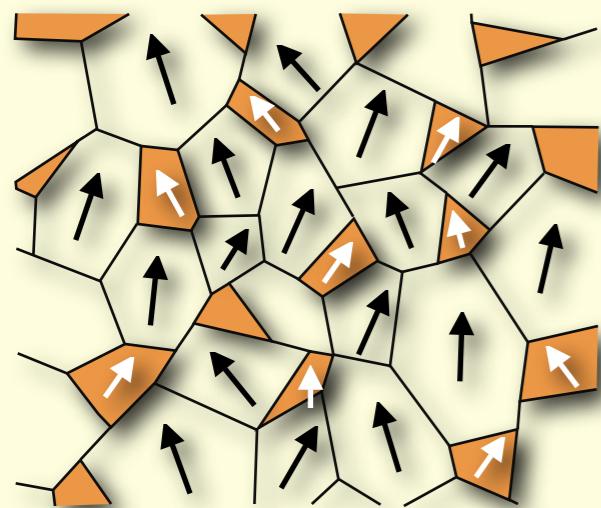
3 types of nanostructured NdFeB magnets

Isotropic magnets: Remanence ($M_r = M_s/2$)

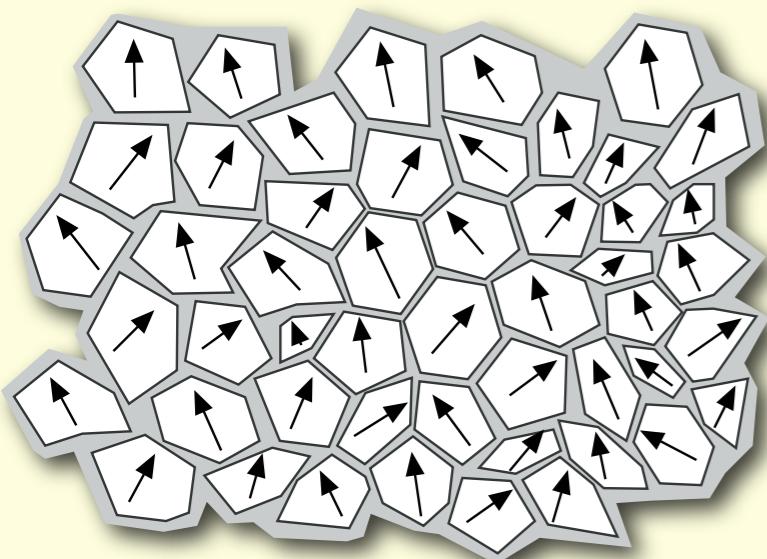


exchanged coupled grains
based on stoichiometric
 $Nd_2Fe_{14}B$

Remanence
enhancement
for isotropic
magnets



exchanged coupled grains
based on nanocomposite
 $Nd_2Fe_{14}B / \alpha\text{-Fe}$

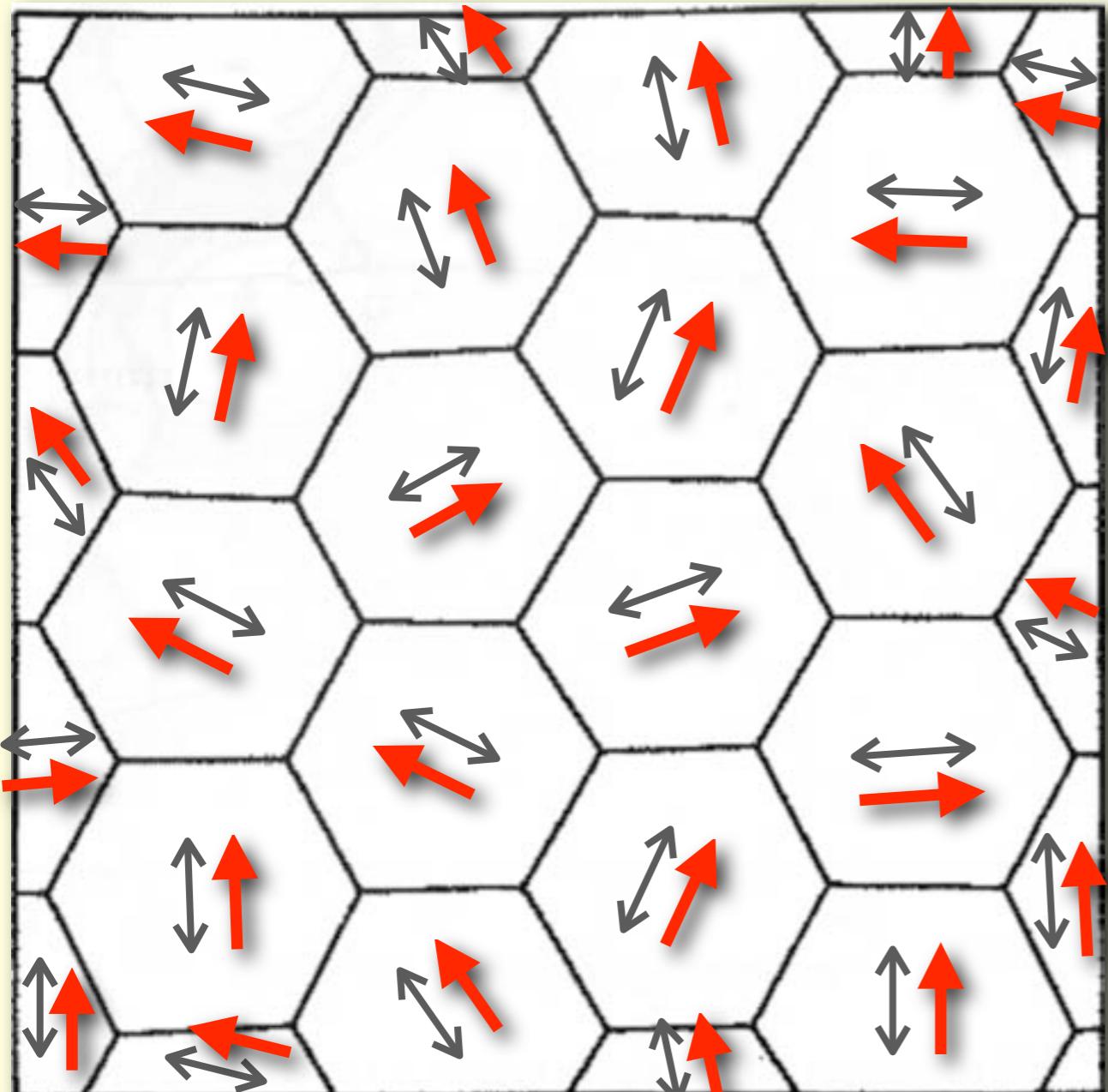


decoupled $Nd_2Fe_{14}B$
grains separated by thin
paramagnetic layer

Remanence
enhancement
by texturing

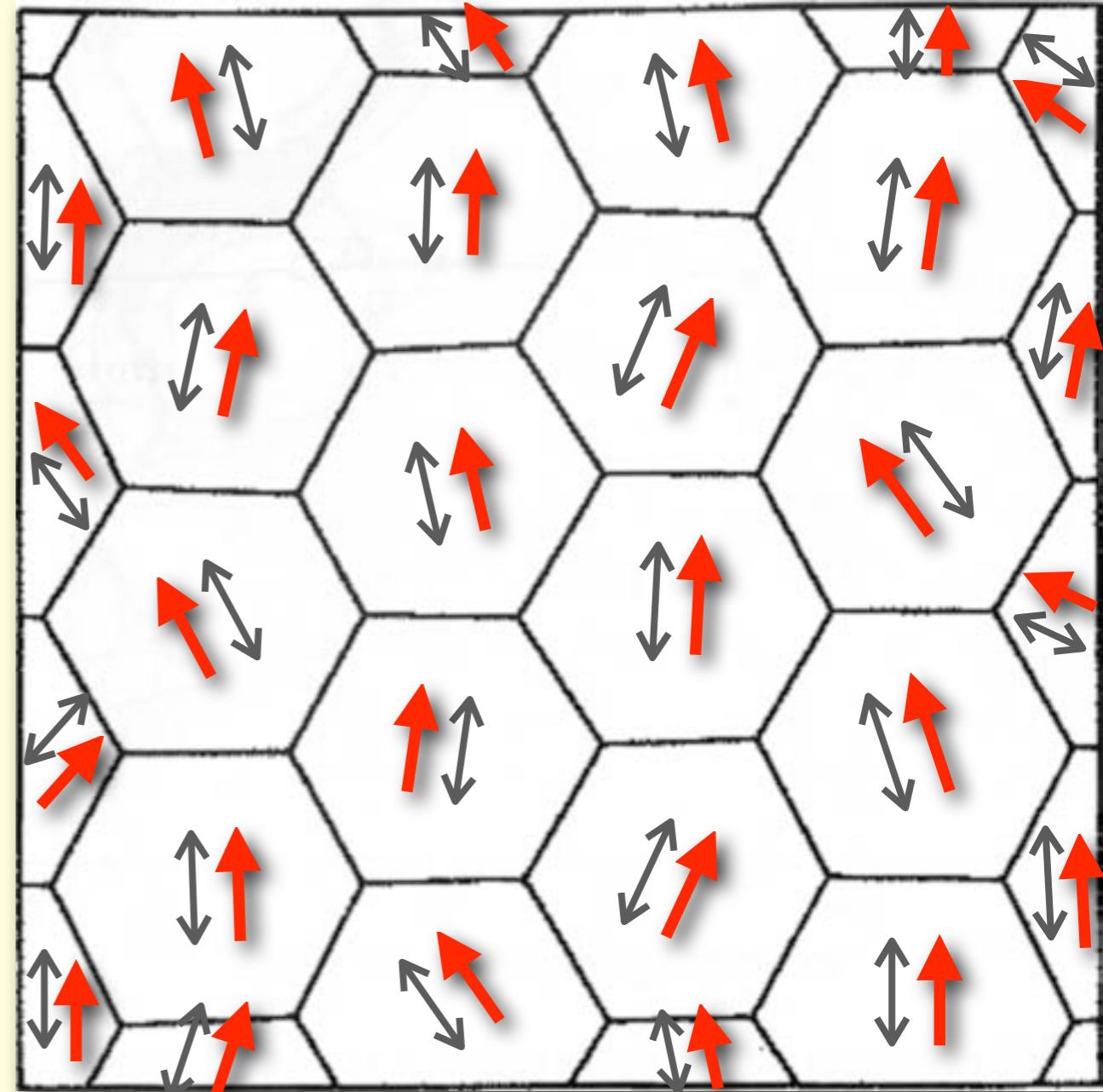
Permanent magnets, basics

isotropic



remanence = $0.5 M_s$

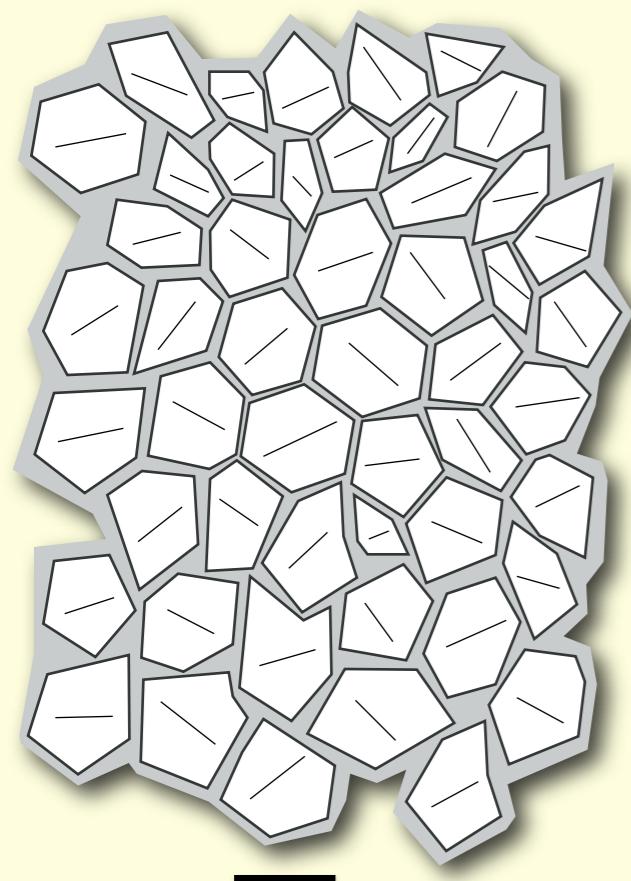
anisotropic (textured)



↑
field

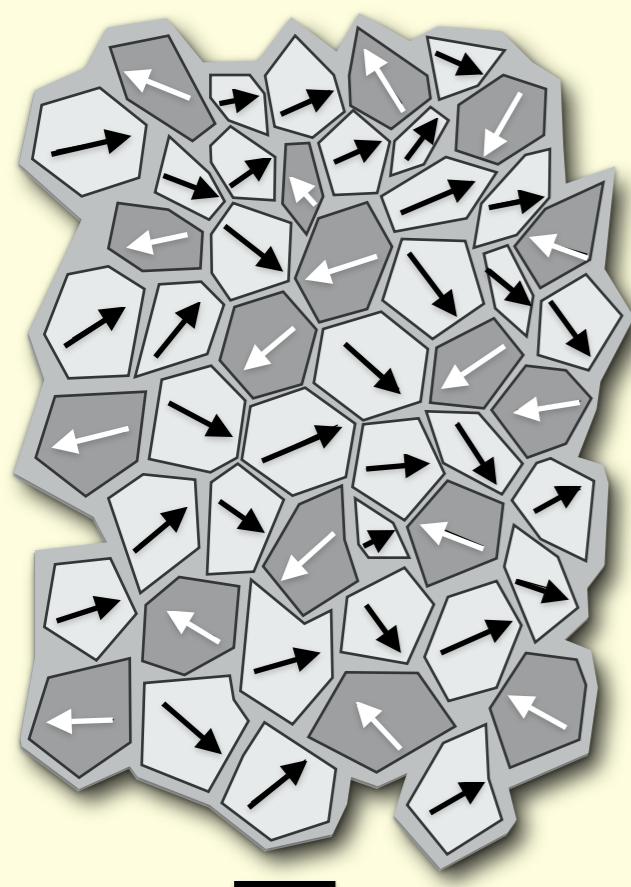
remanence > $0.5 M_s$

Nanostructured NdFeB: decoupled grains



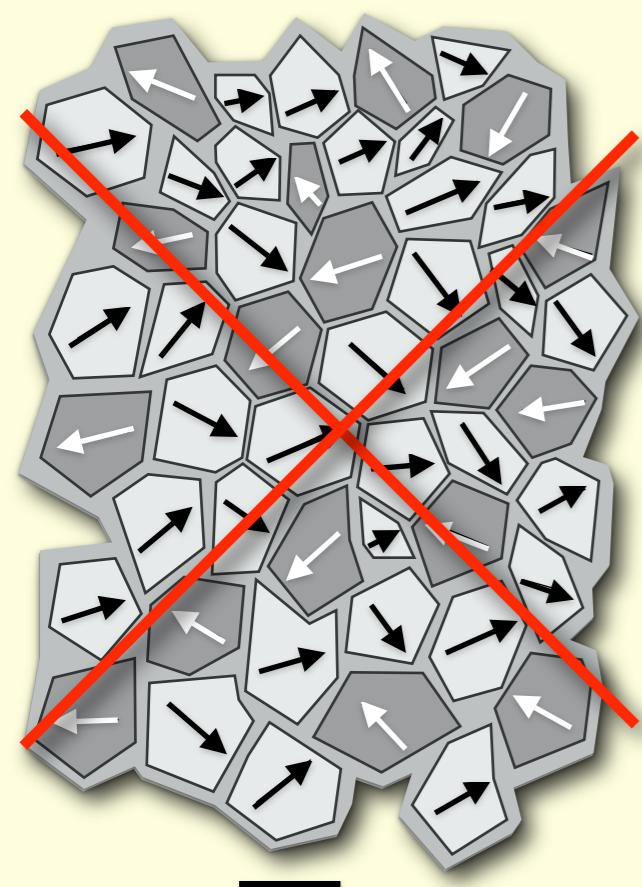
some 100 nm

Nanostructured NdFeB: decoupled grains



some 100 nm

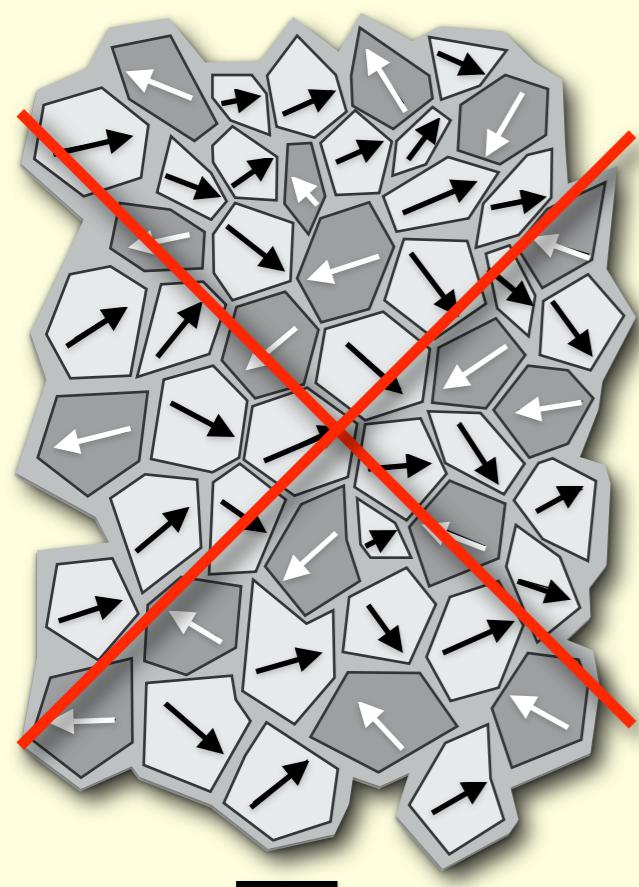
Nanostructured NdFeB: decoupled grains



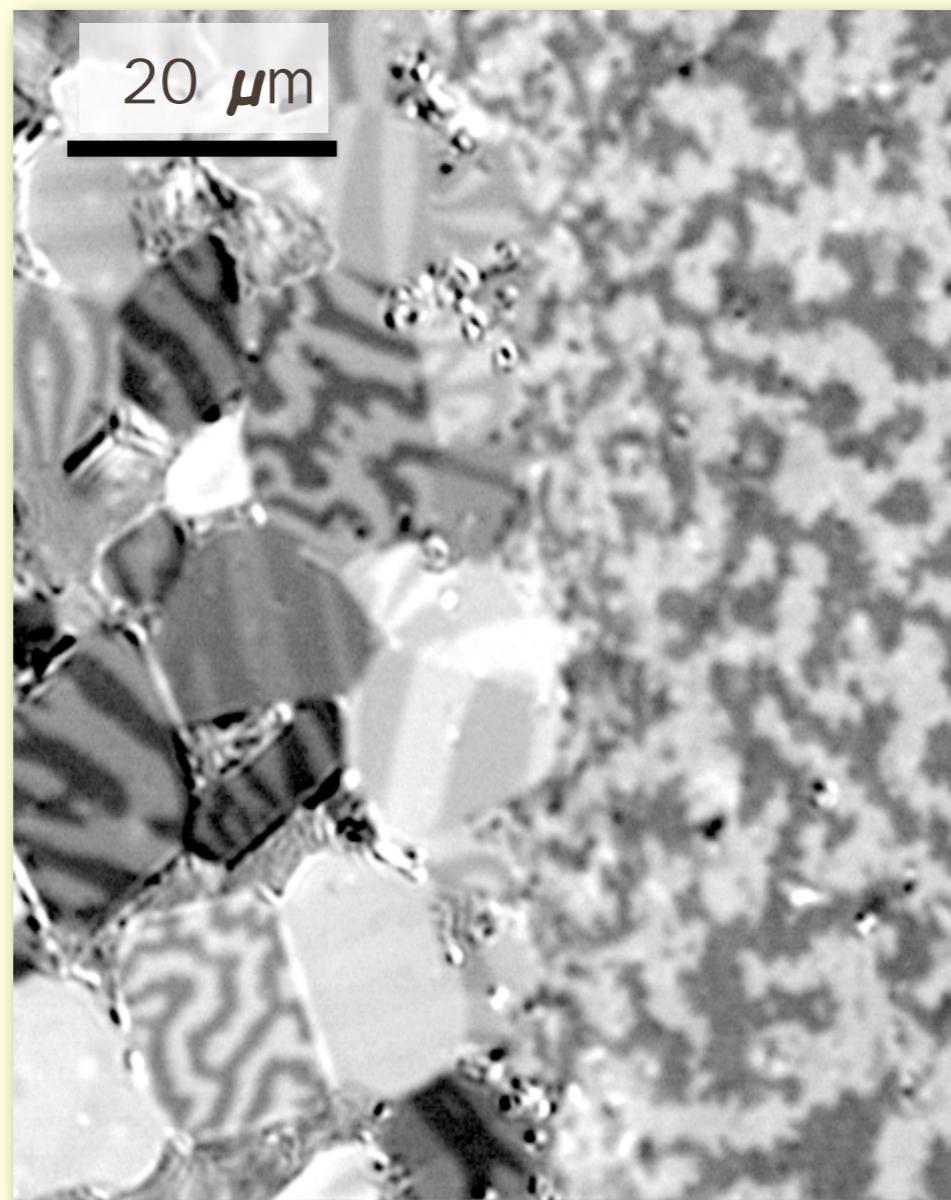
some 100 nm

Nanostructured NdFeB: decoupled grains

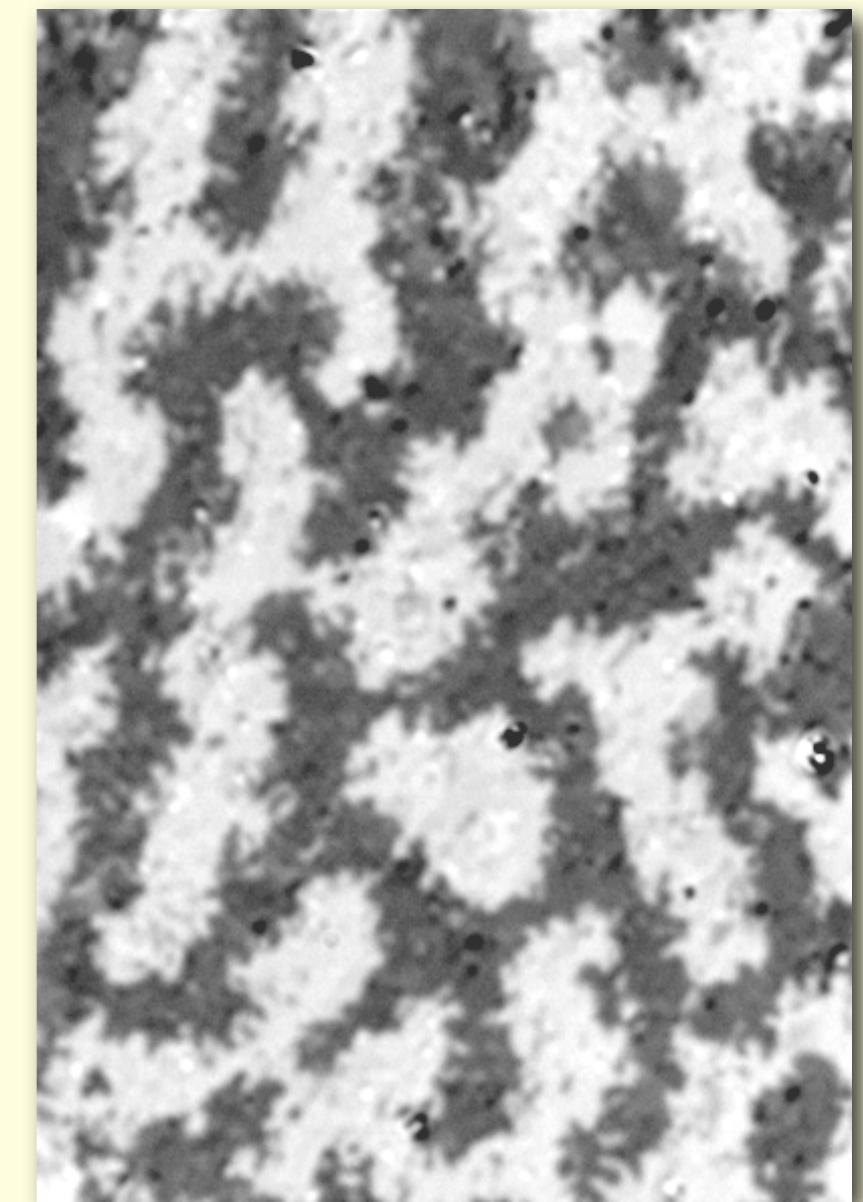
observation perpendicular to texture axis



some 100 nm



coarse
grains



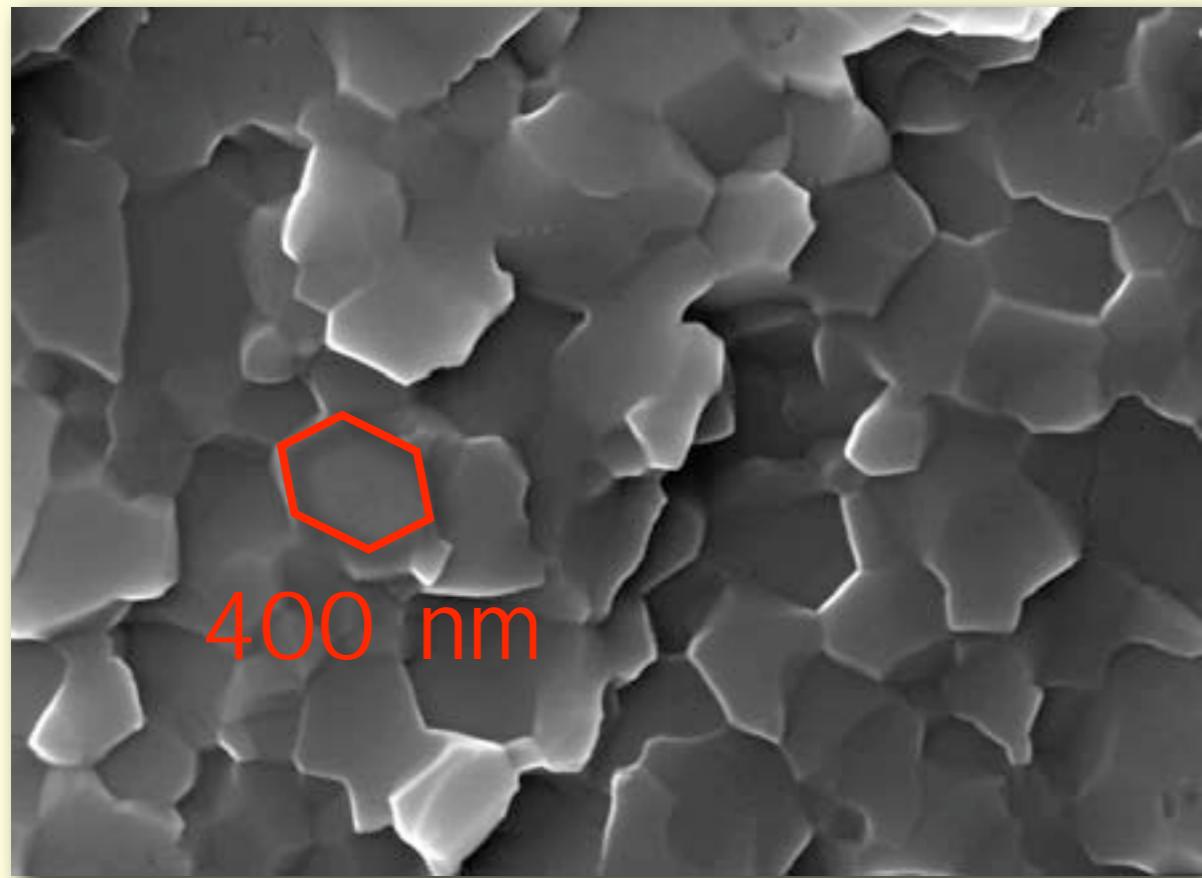
fine
grains



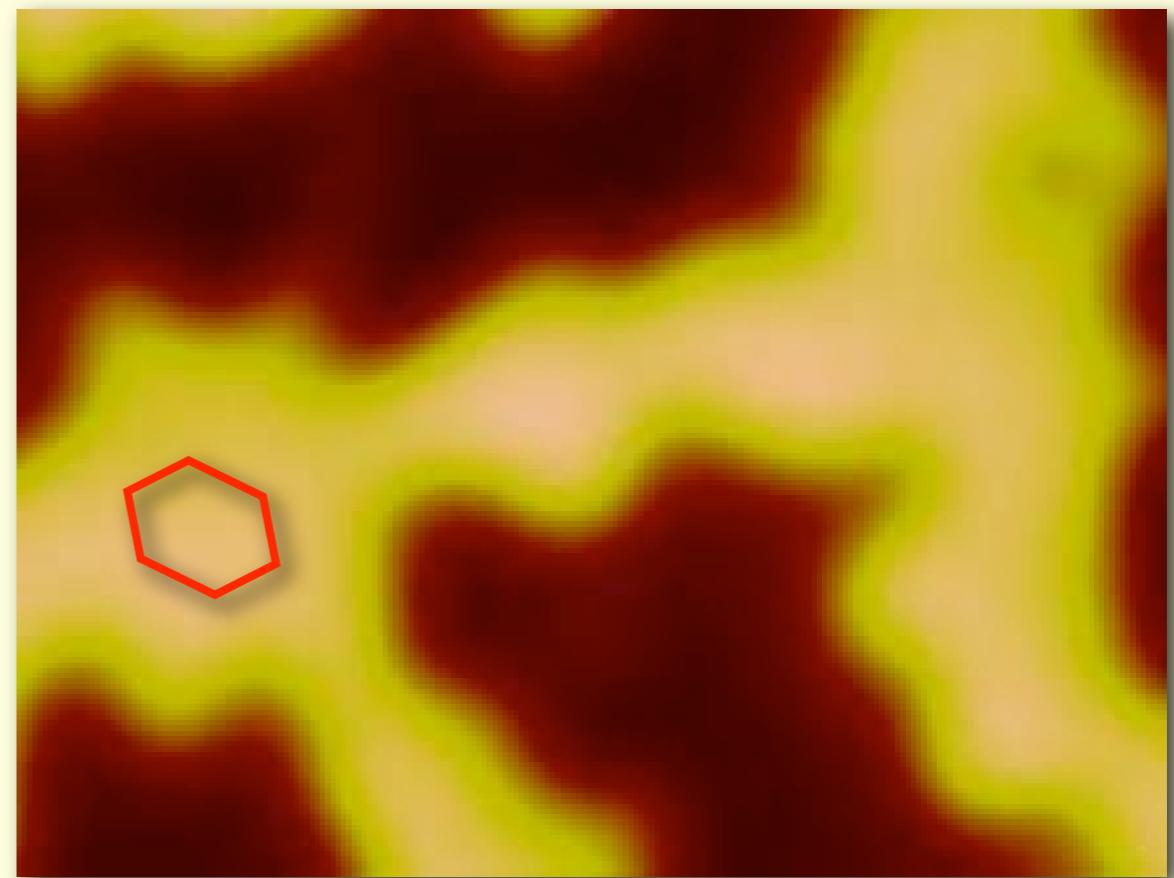
Nanostructured NdFeB: decoupled grains

Hot deformed NdFeB magnet (thermally demagnetized)
(deformation degree ~ 76%, texture parameter $(B_{r\parallel}-B_{r\perp})/B_{r\parallel} = 0.79$)
observed perpendicular to texture axis

grain structure

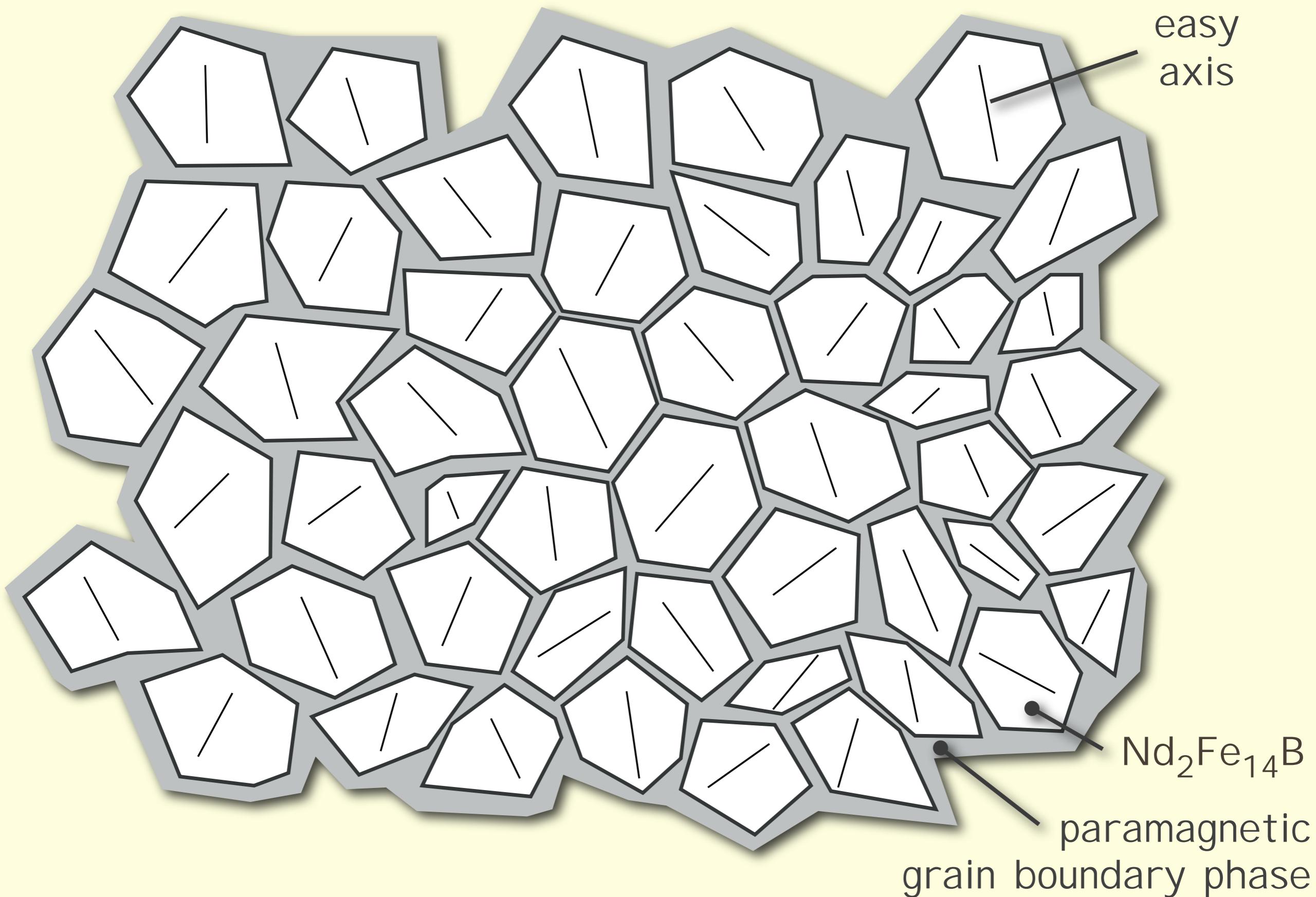


domains

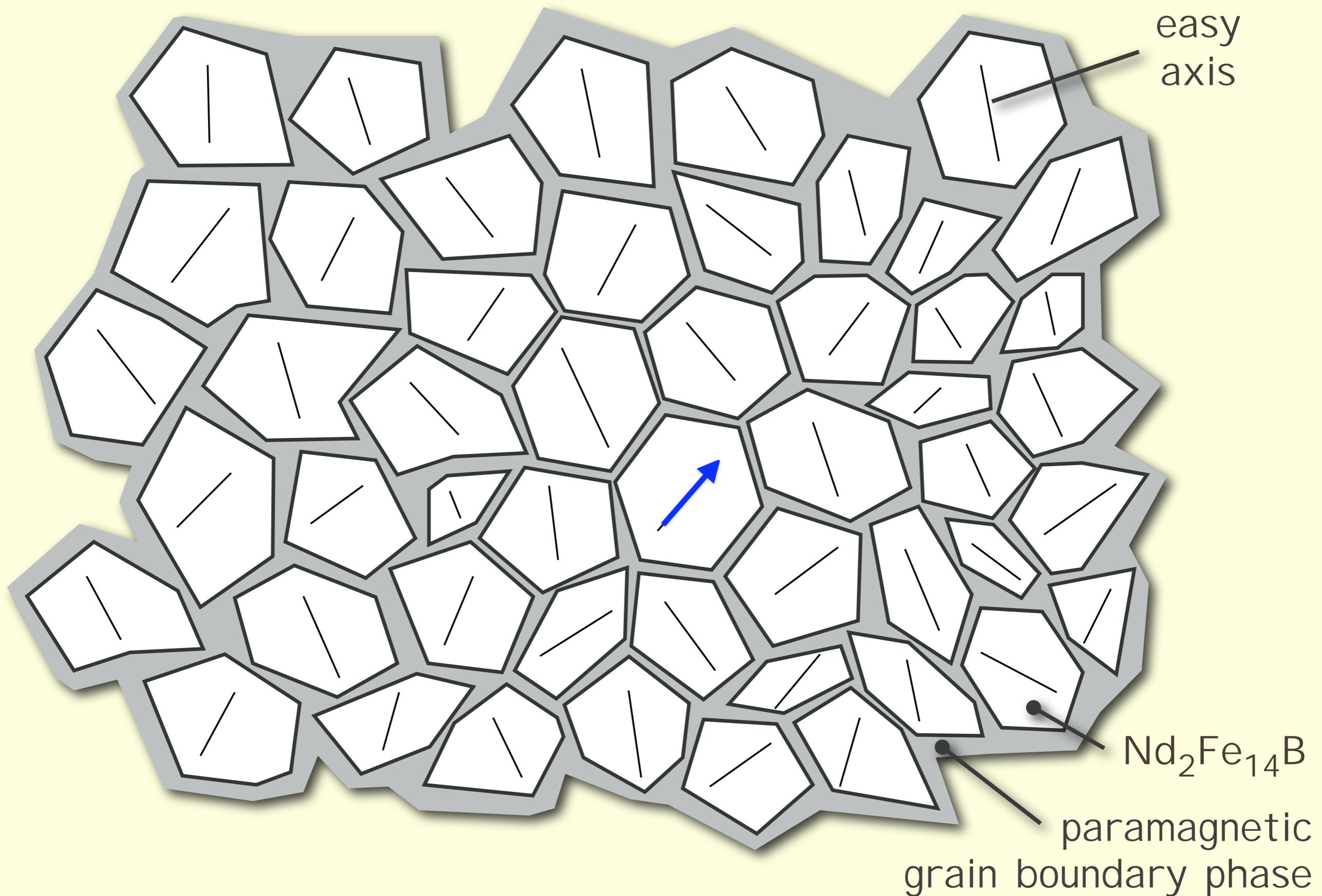


courtesy K. Khlopkov and O. Gutfleisch (IFW Dresden)

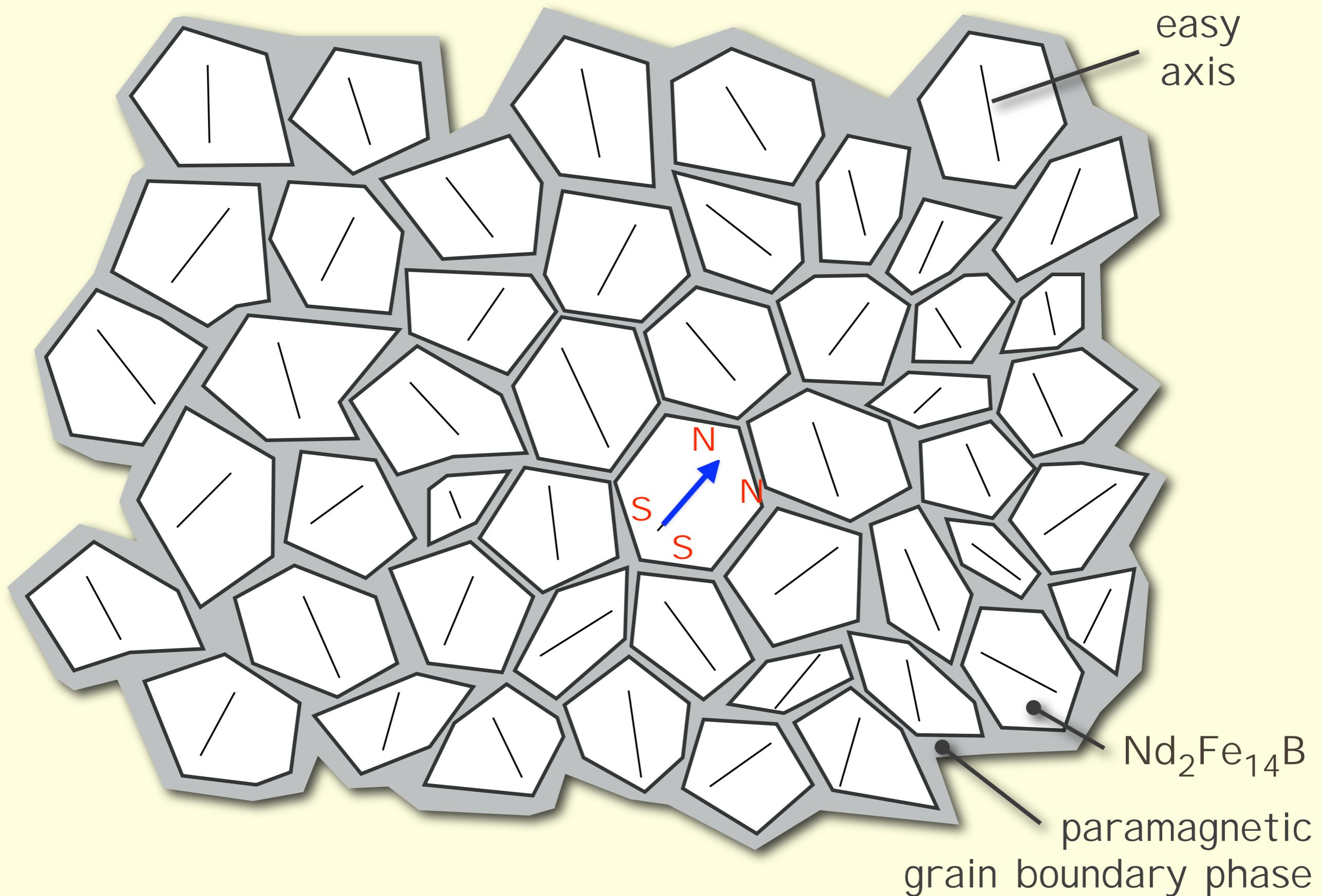
Nanostructured NdFeB: decoupled grains



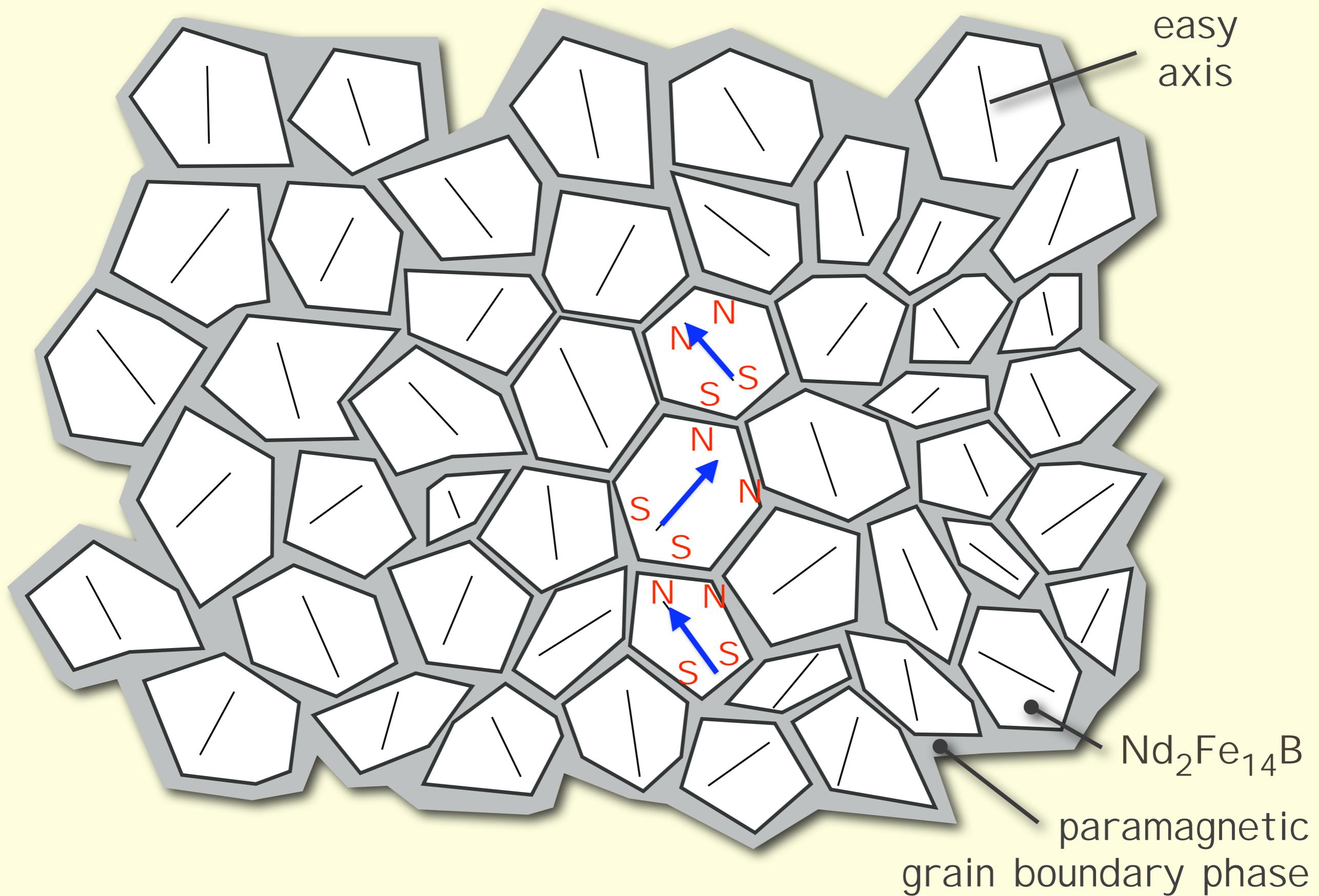
Nanostructured NdFeB: decoupled grains



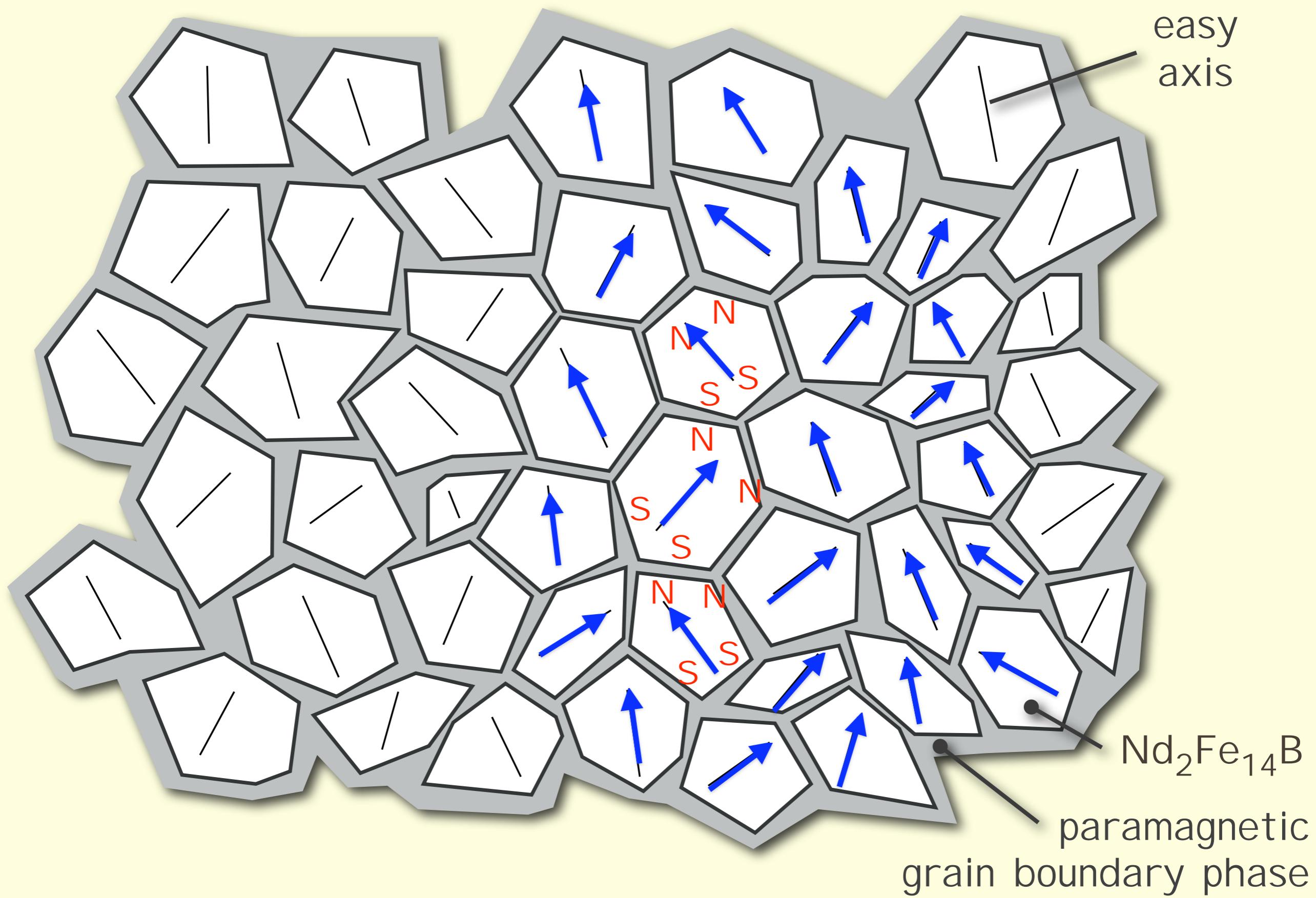
Nanostructured NdFeB: decoupled grains



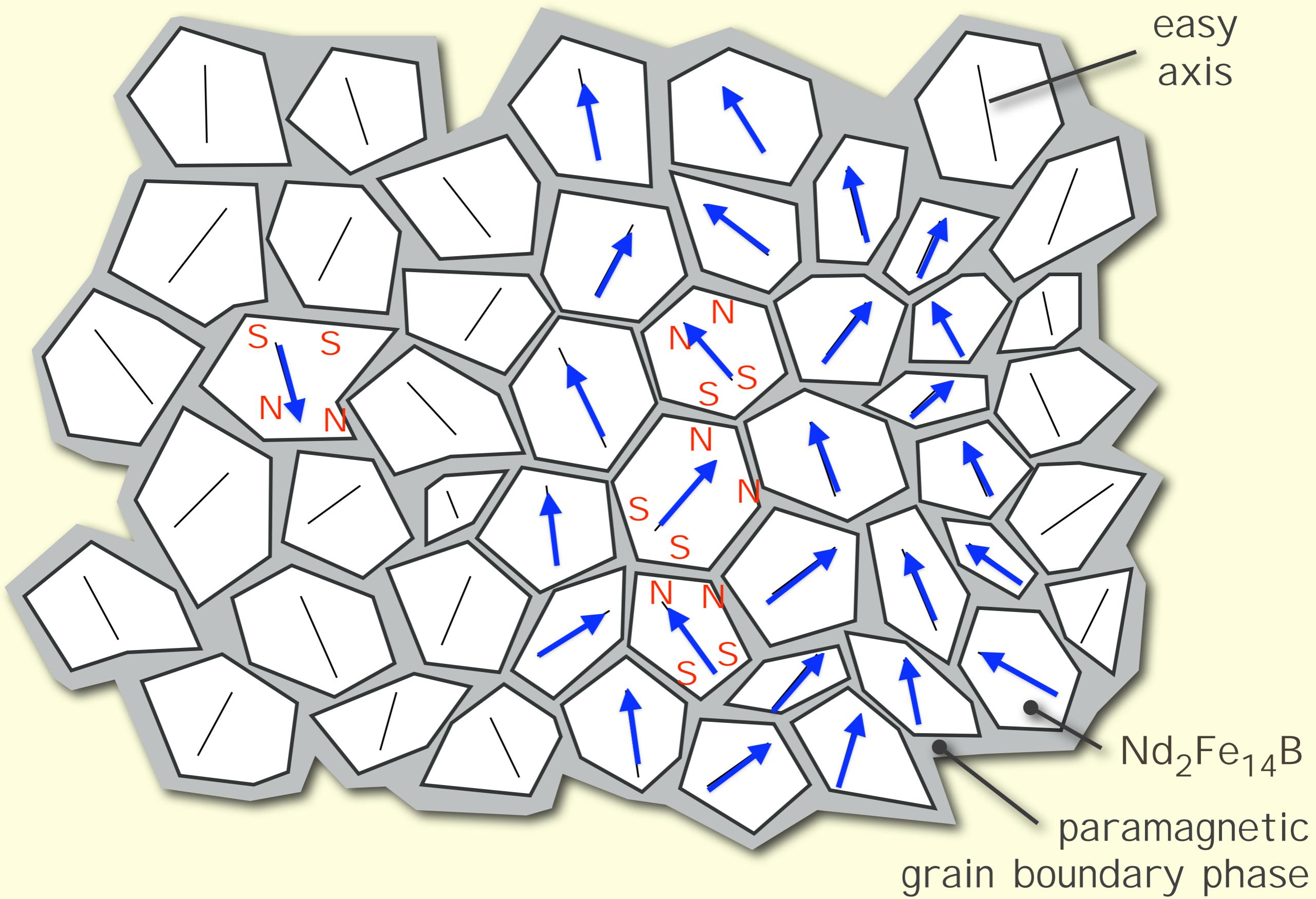
Nanostructured NdFeB: decoupled grains



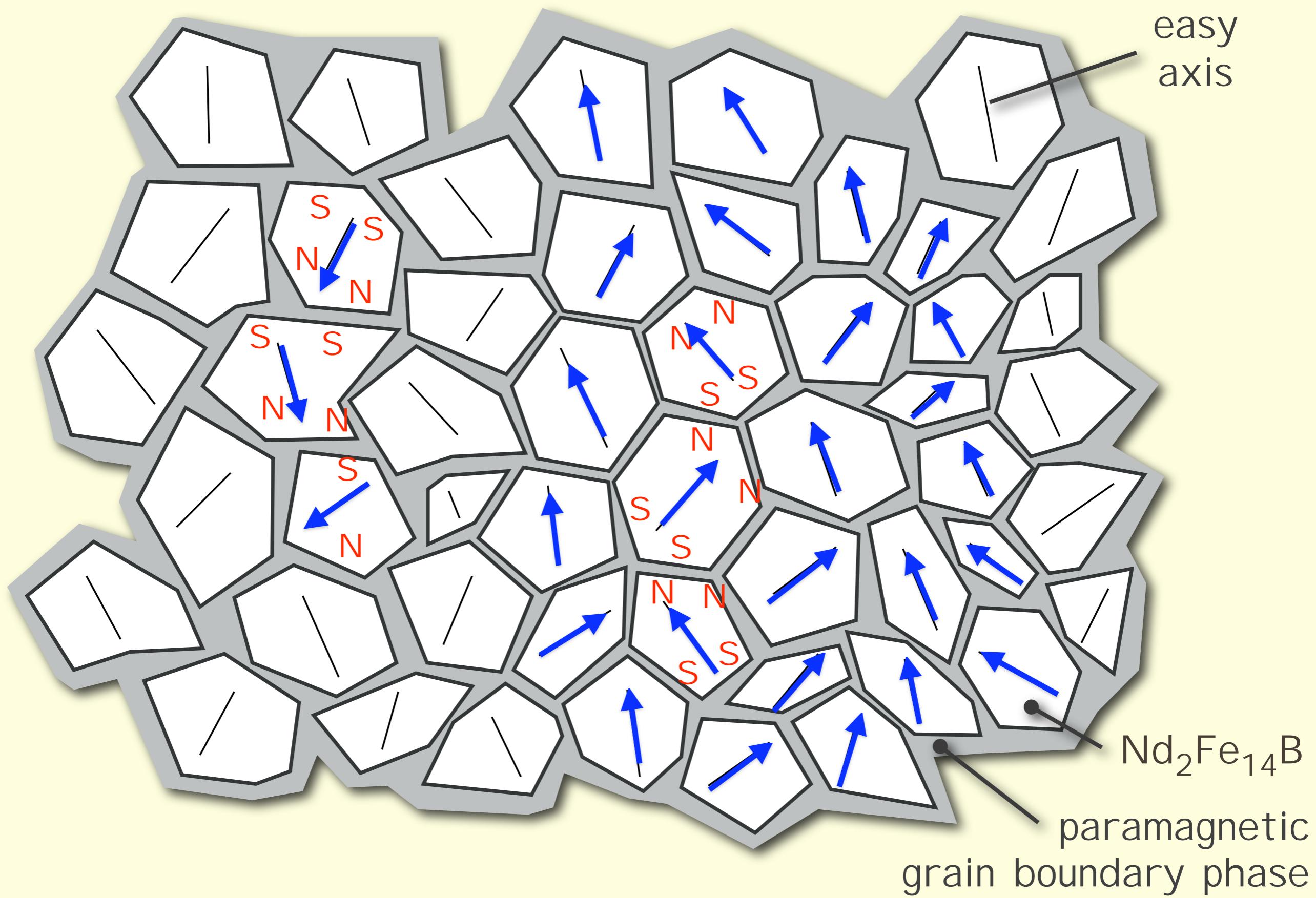
Nanostructured NdFeB: decoupled grains



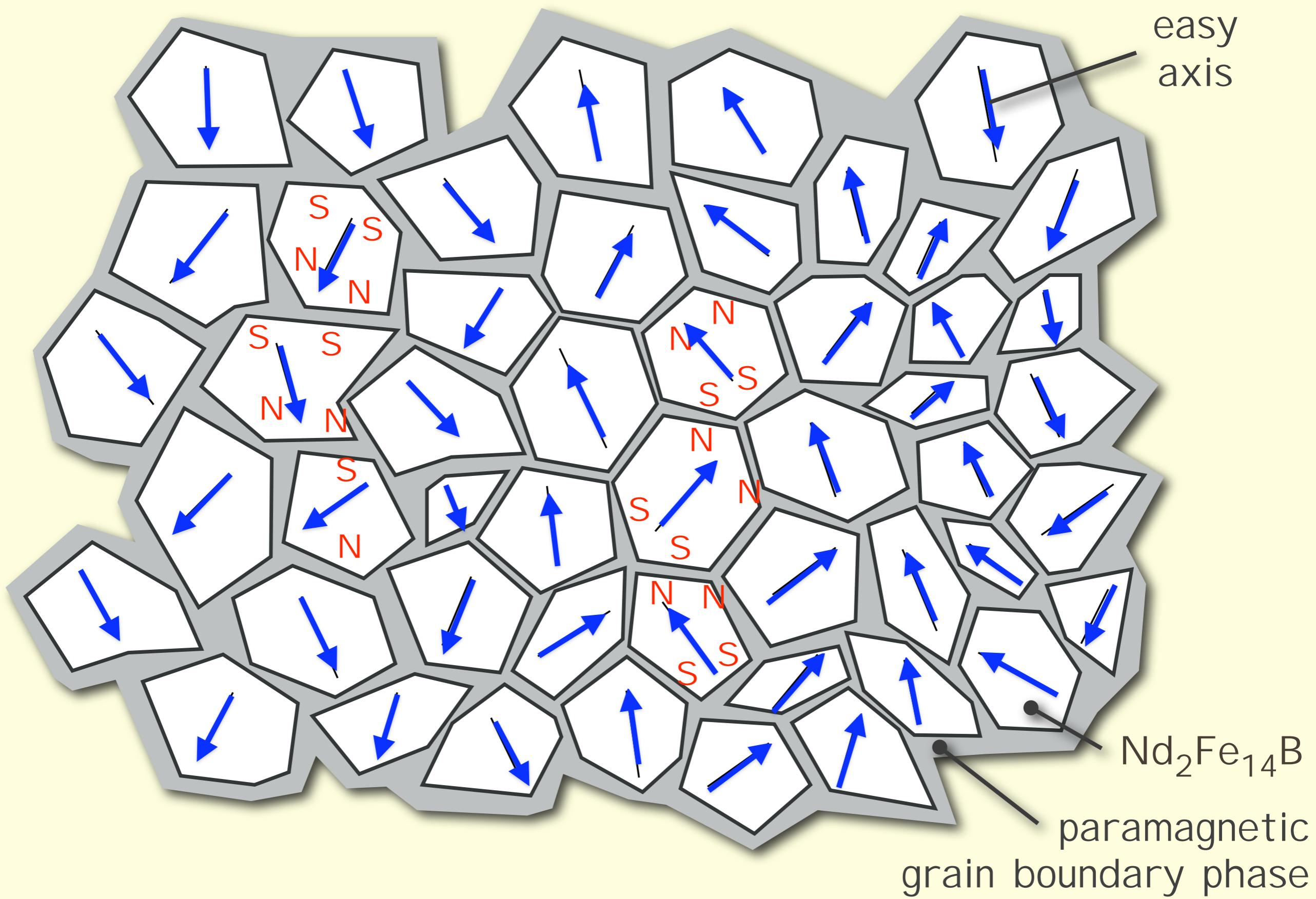
Nanostructured NdFeB: decoupled grains



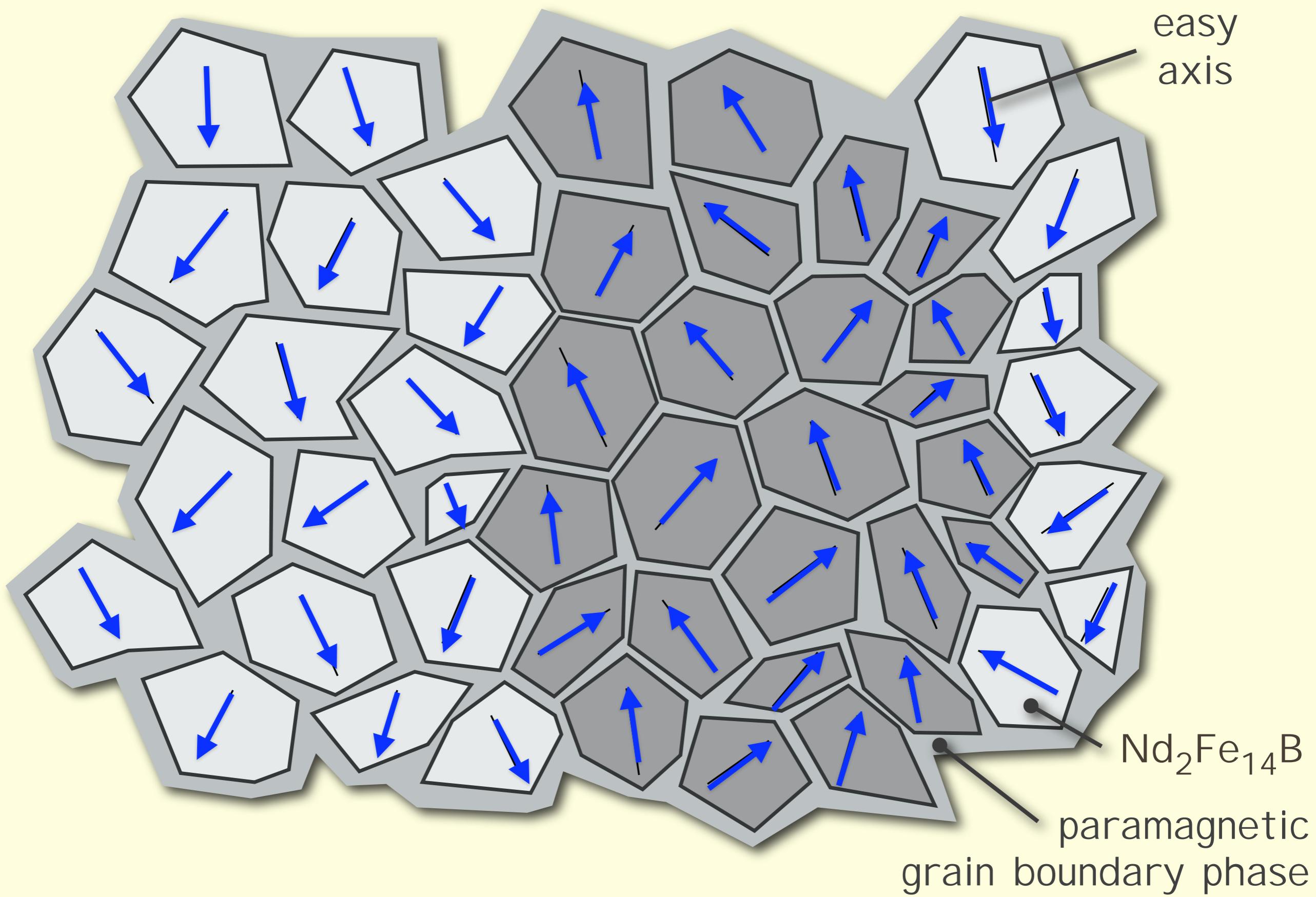
Nanostructured NdFeB: decoupled grains



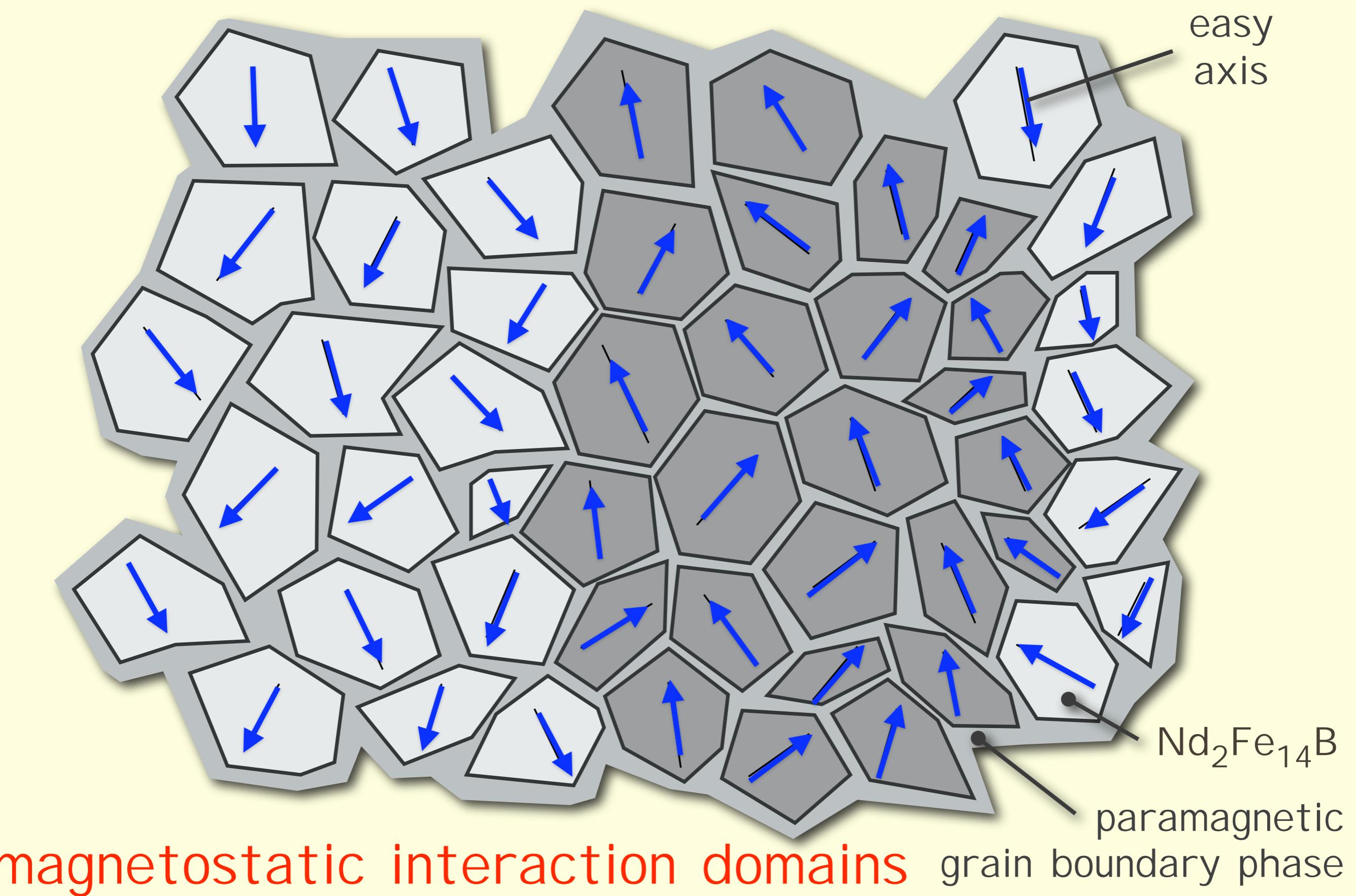
Nanostructured NdFeB: decoupled grains



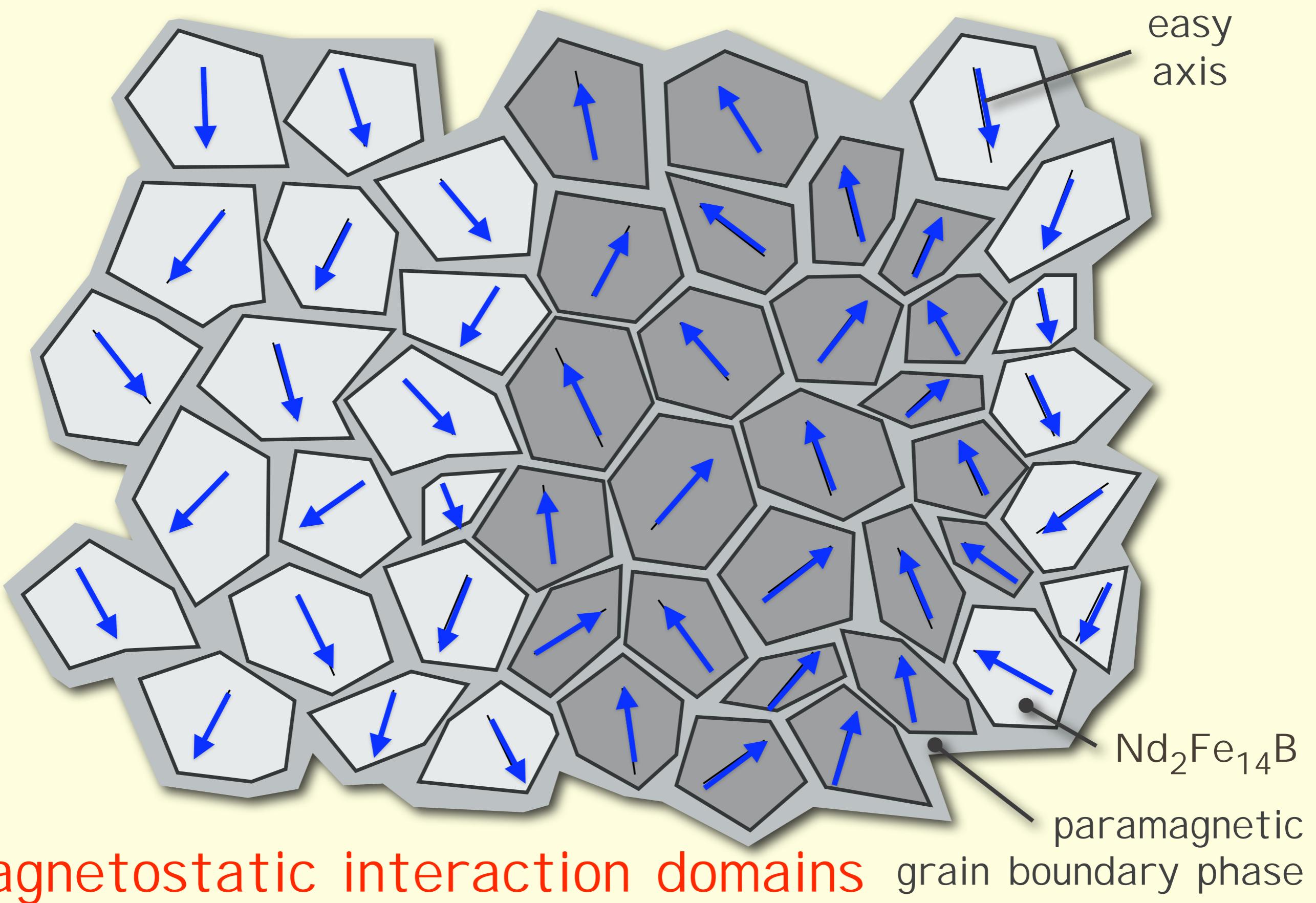
Nanostructured NdFeB: decoupled grains



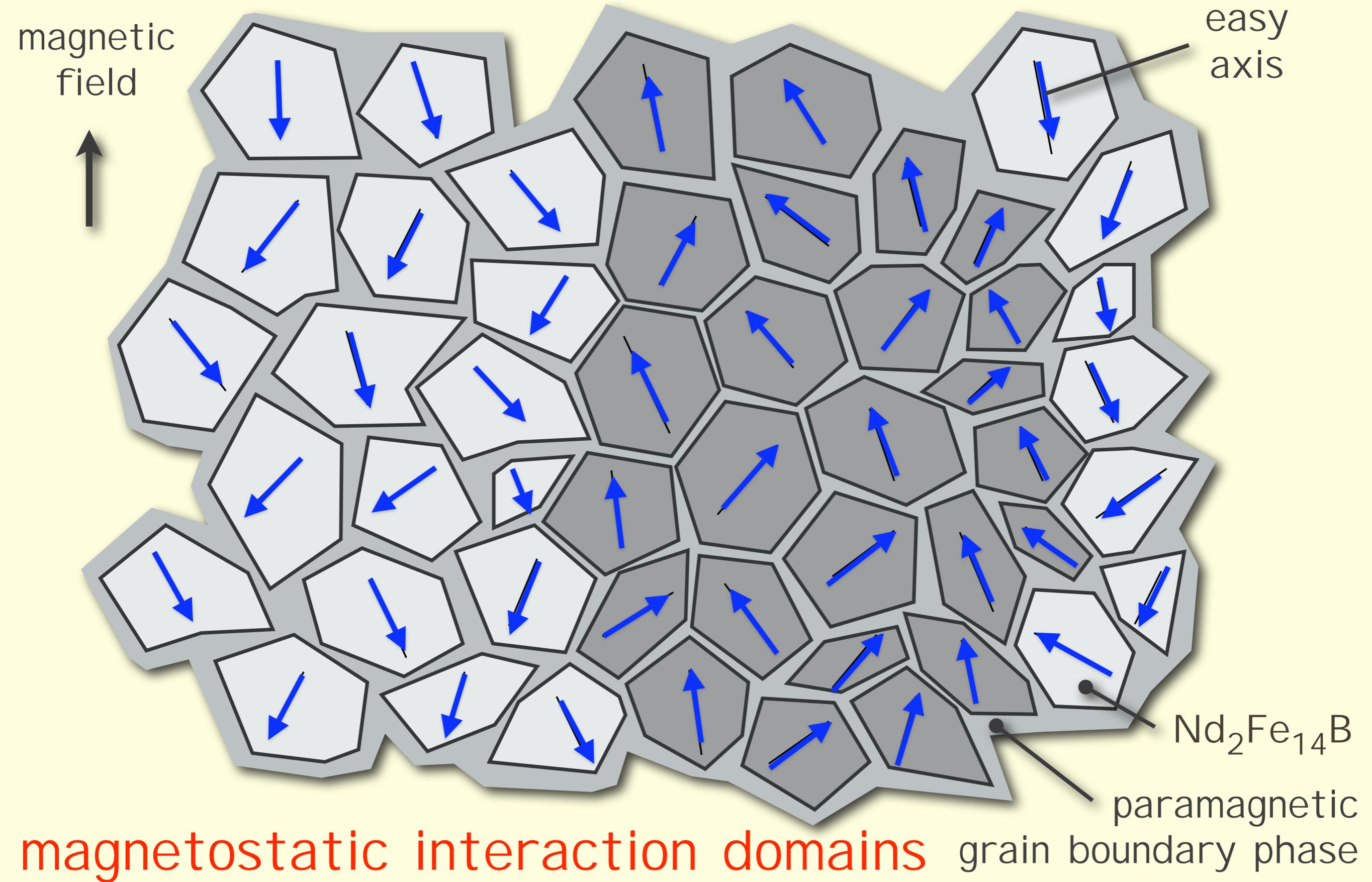
Nanostructured NdFeB: decoupled grains



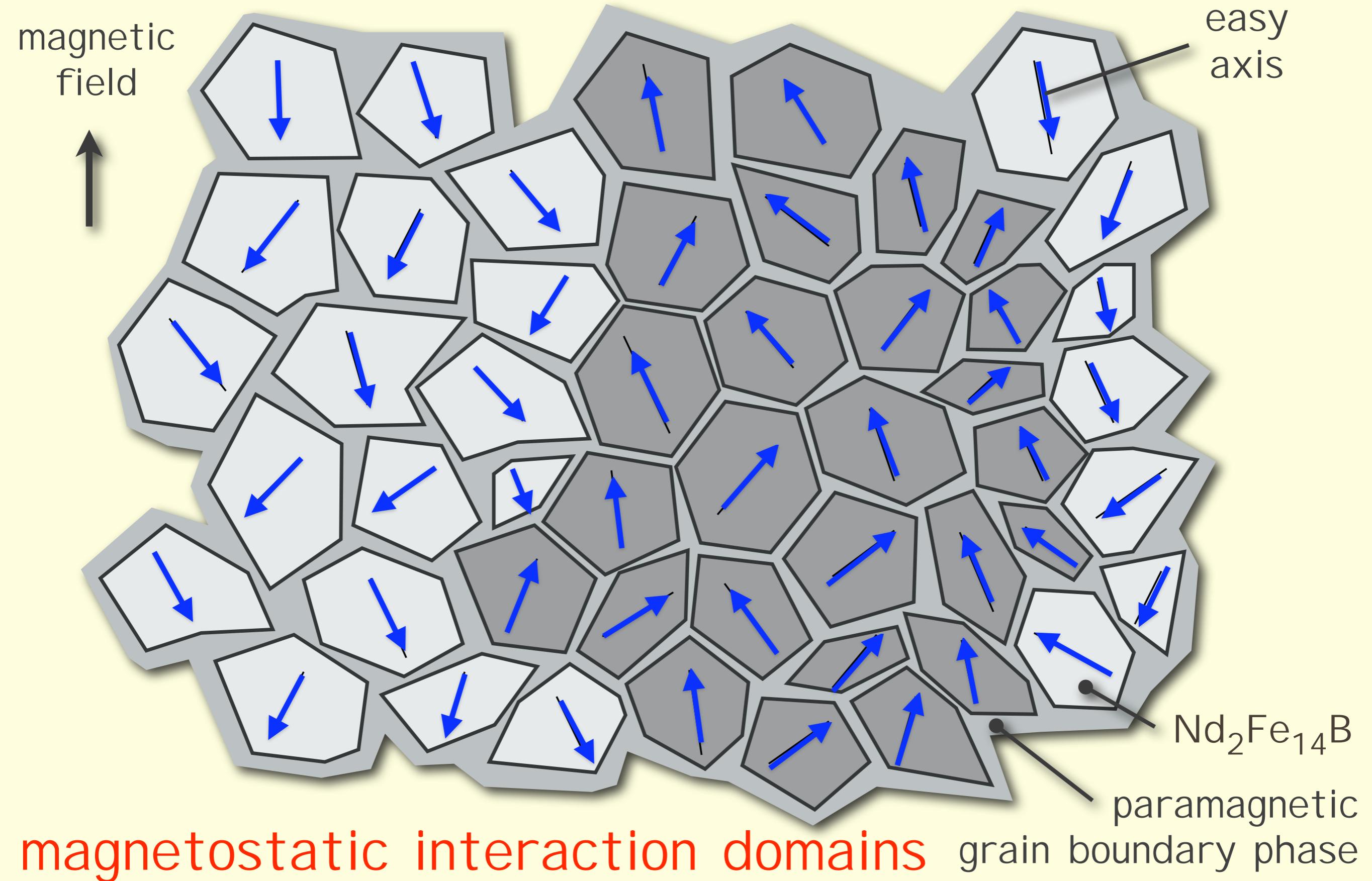
Nanostructured NdFeB: decoupled grains



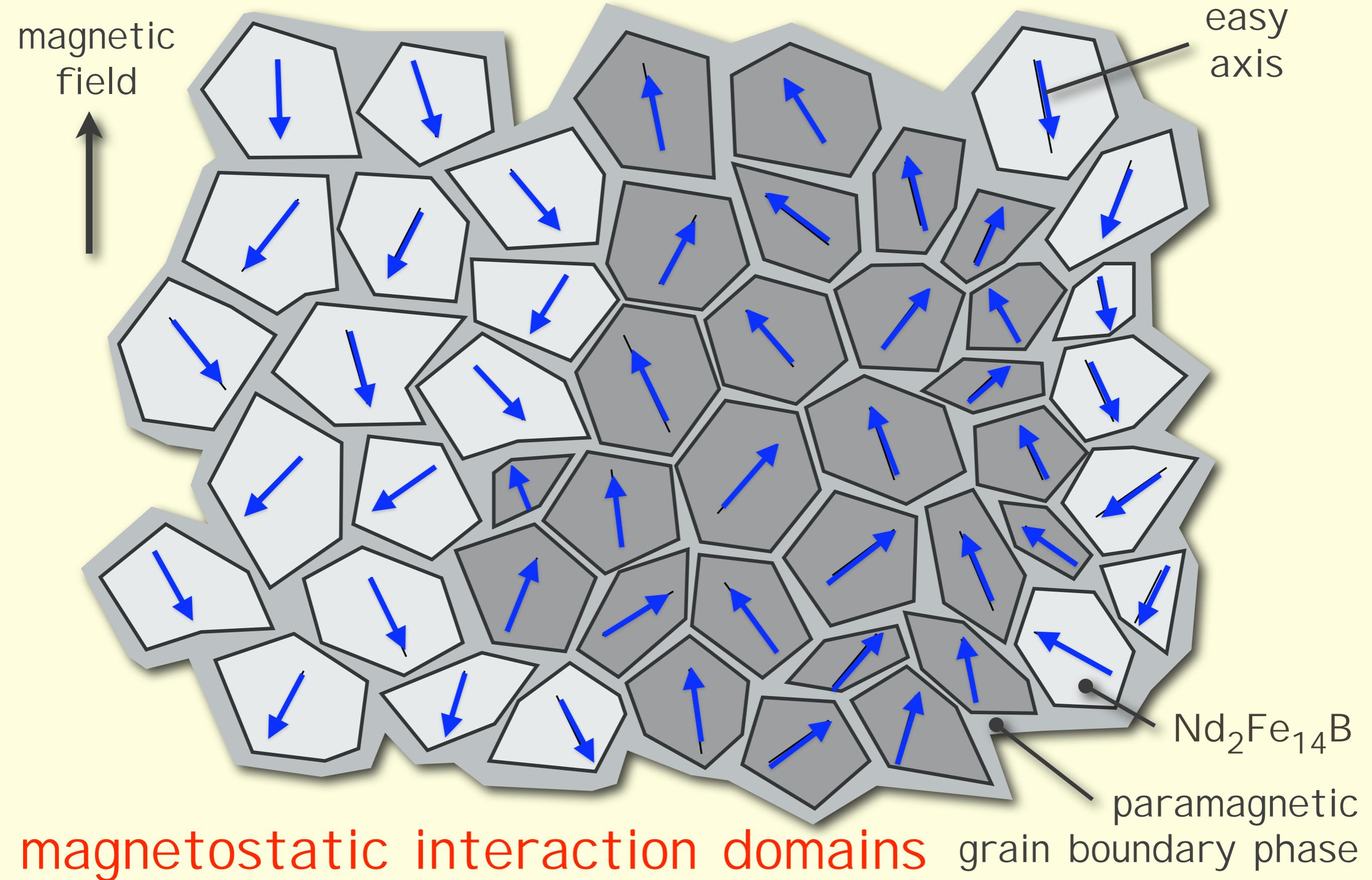
Nanostructured NdFeB: decoupled grains



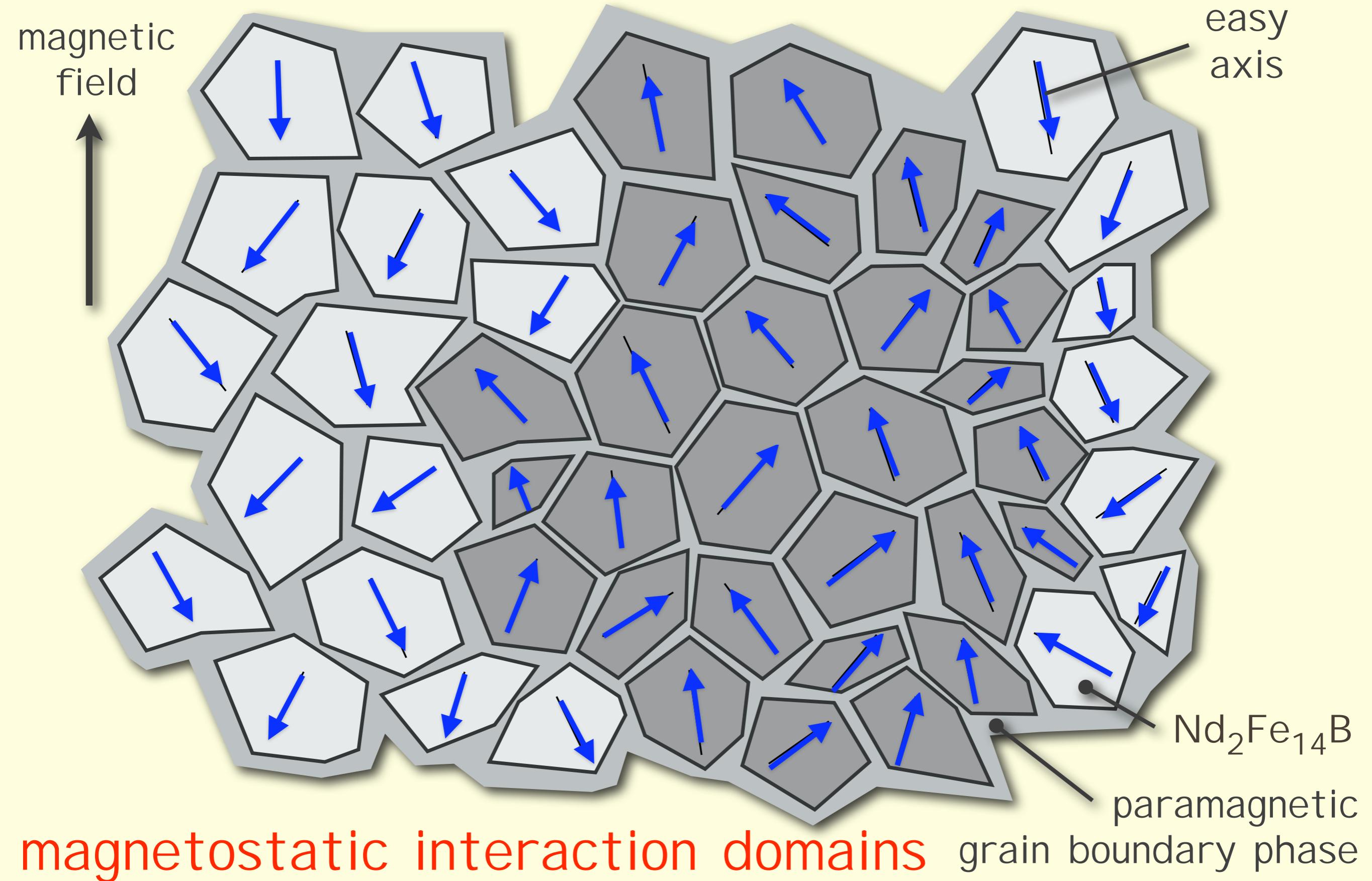
Nanostructured NdFeB: decoupled grains



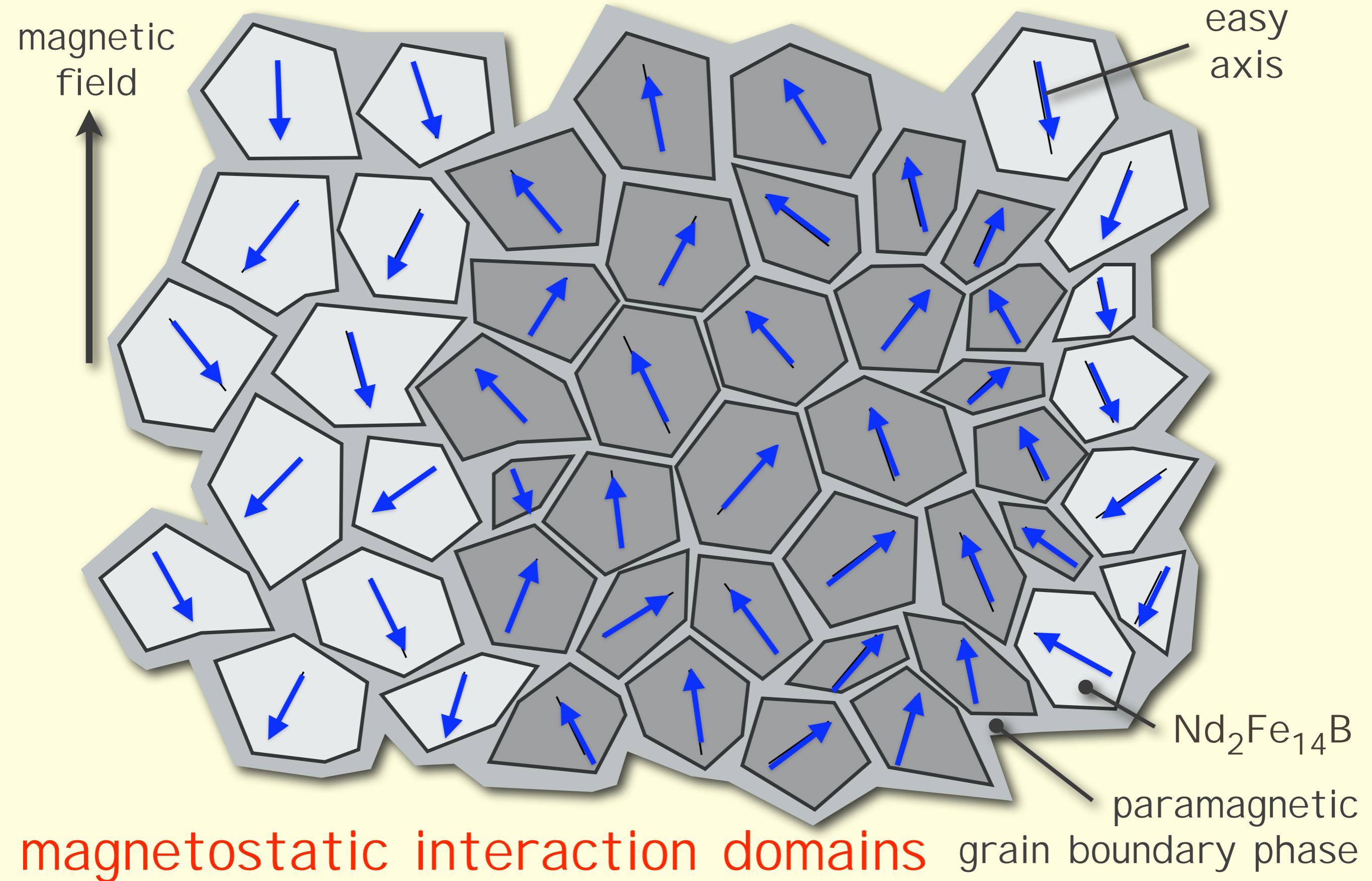
Nanostructured NdFeB: decoupled grains



Nanostructured NdFeB: decoupled grains

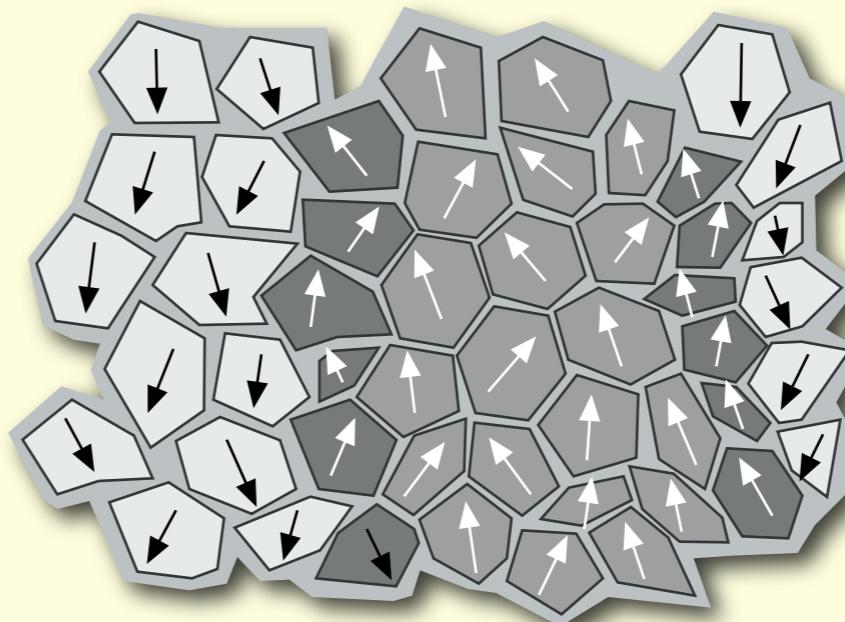
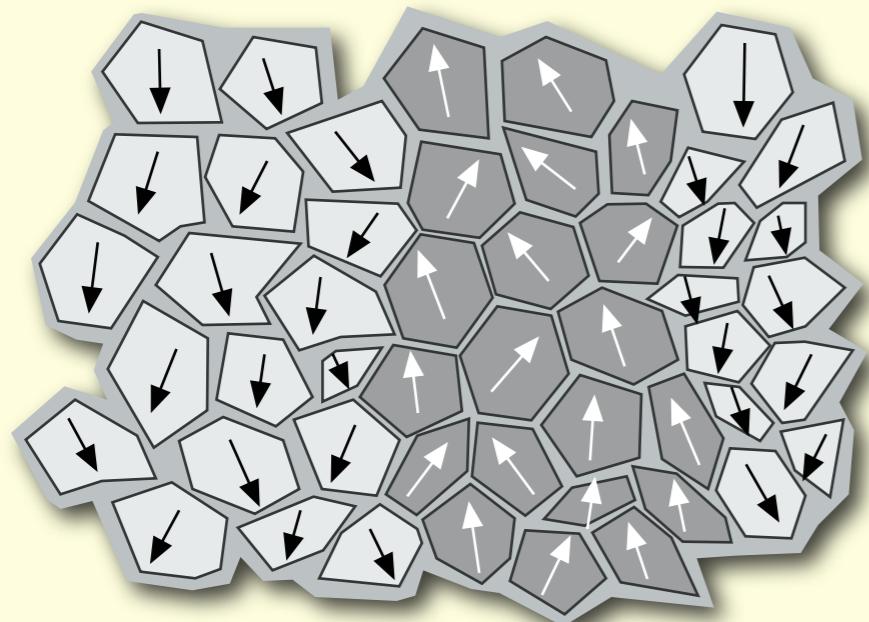


Nanostructured NdFeB: decoupled grains

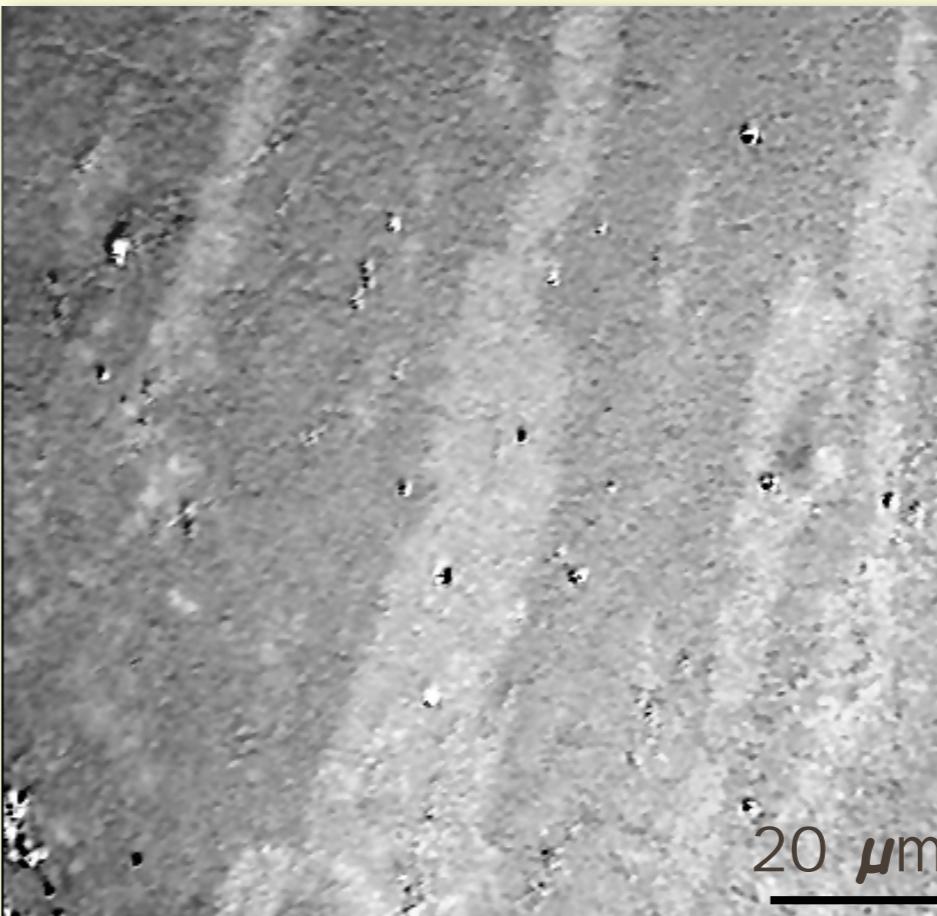
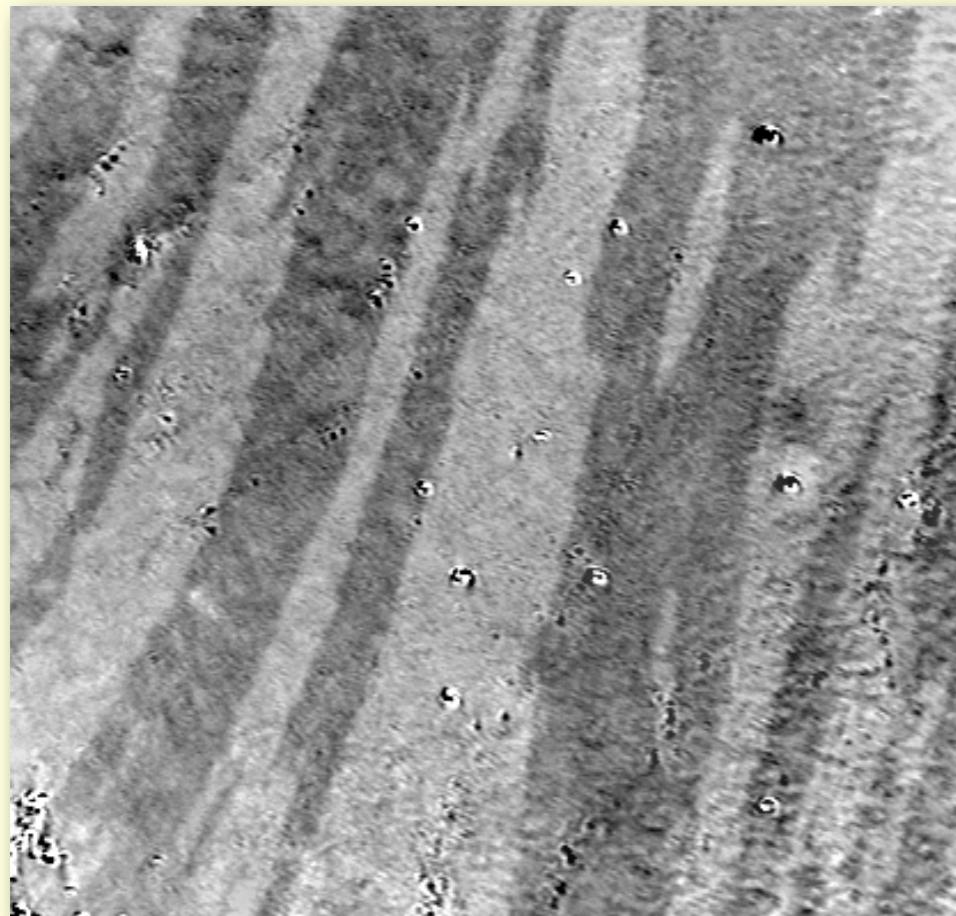


Nanostructured NdFeB: decoupled grains

magnetization process along preferred axis



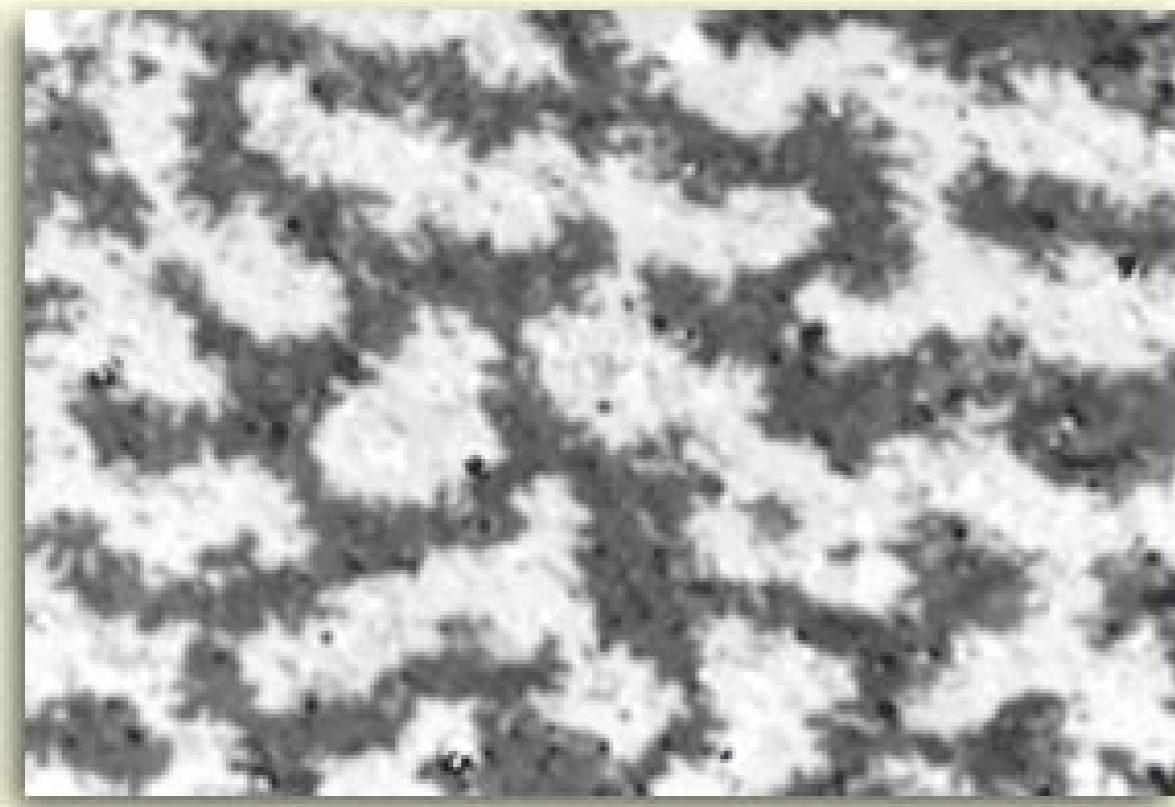
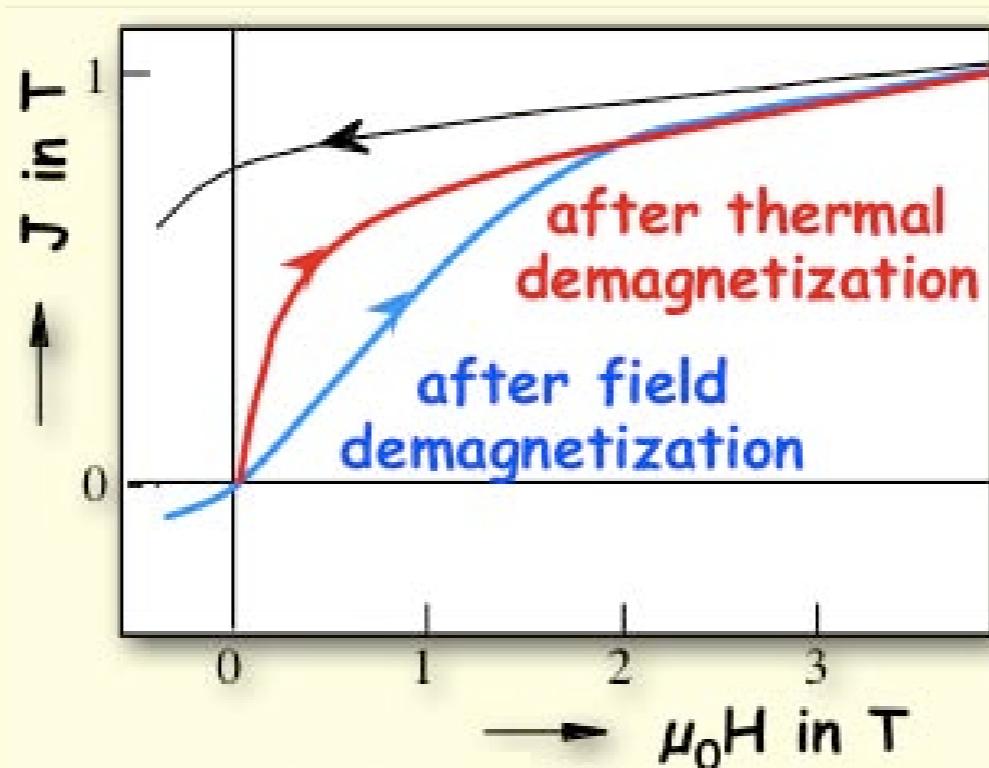
↑
field



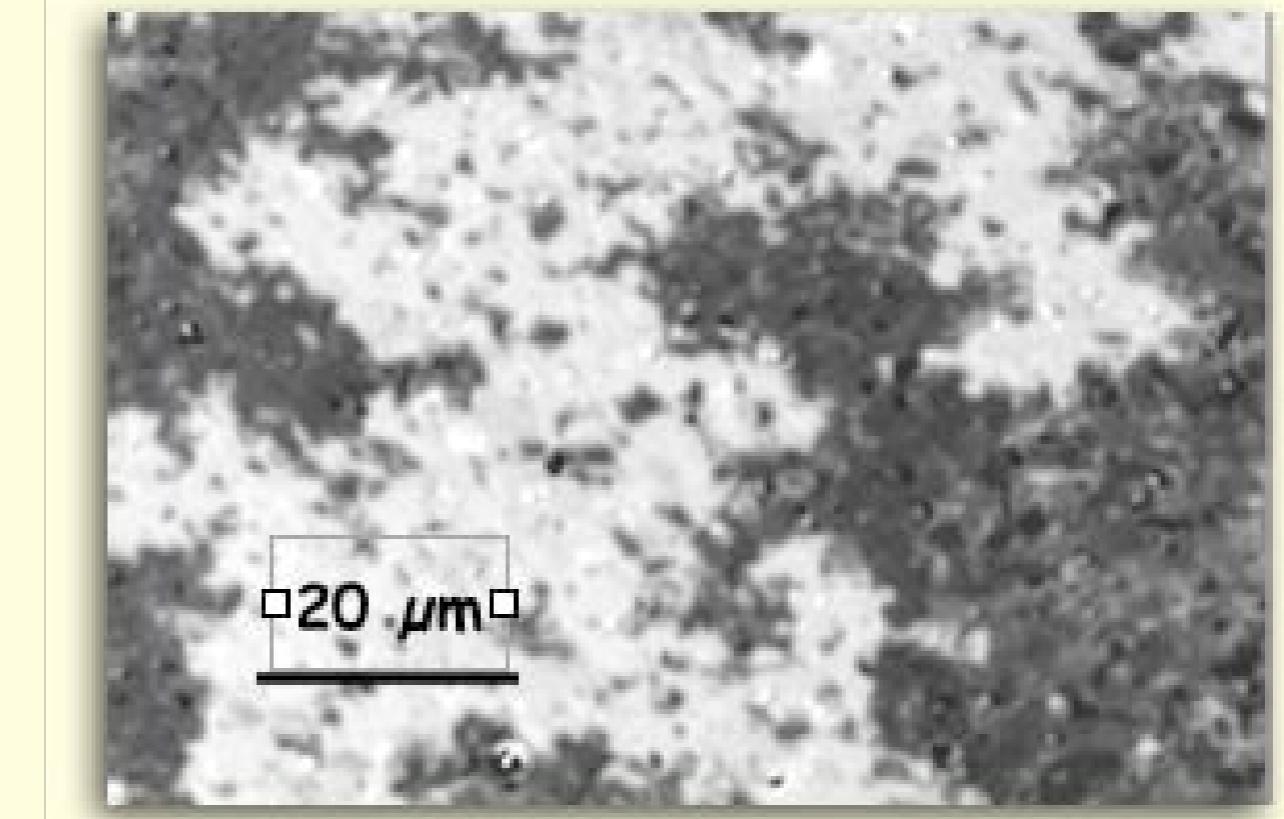
NdFeB
grain size
about 100 nm

20 μm

Nanostructured NdFeB: decoupled grains



after thermal demagnetization

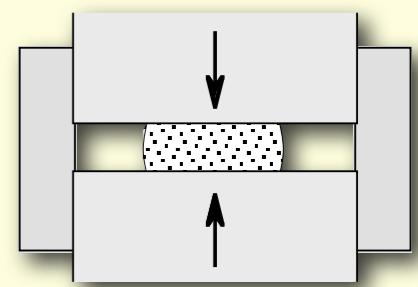


after field demagnetization

Nanostructured NdFeB: decoupled grains

Preparation: melt spinning, ball milling, hot-pressing, die-upsetting

degree of deformation: $\ln \frac{\text{initial thickness}}{\text{final thickness}}$



decreasing degree of deformation and texture

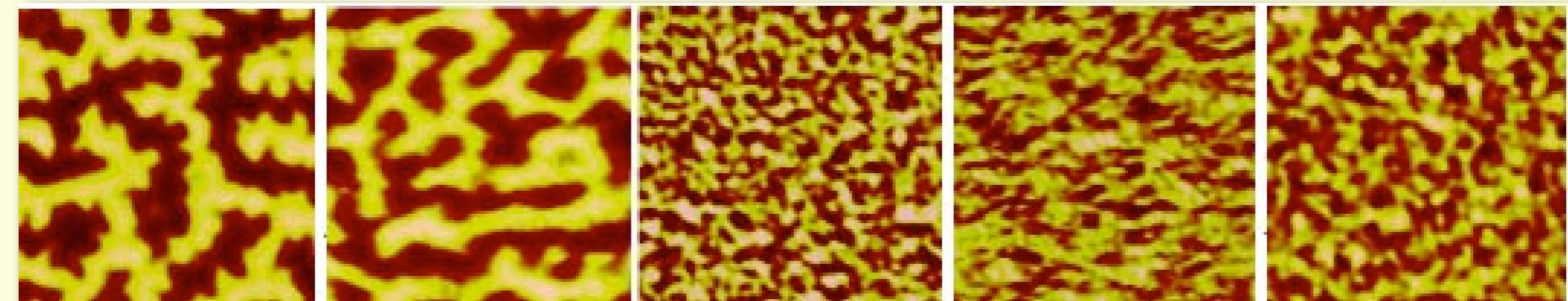
1.44

0.97

0.74

0.56

isotropic



10 μm

MFM observation

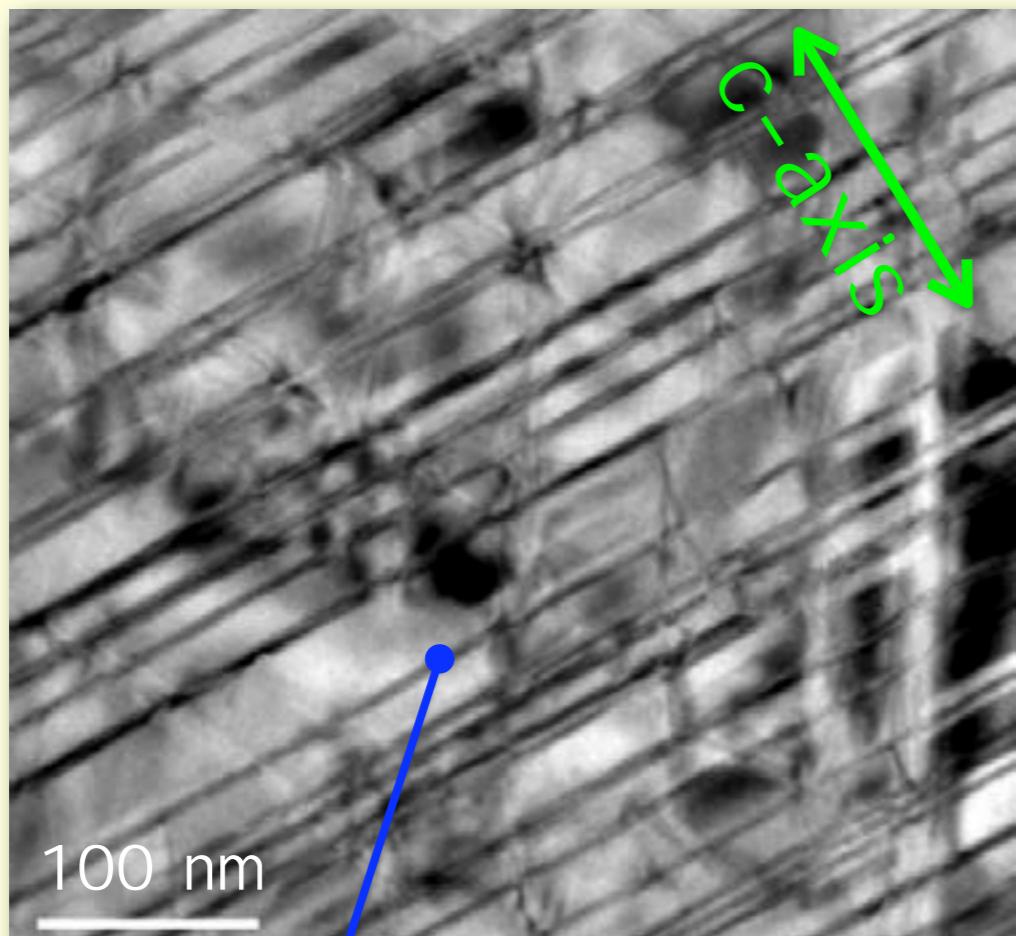
courtesy K. Khlopkov and O. Gutfleisch (IFW Dresden)

Domains in Sm₂Co₁₇ magnets

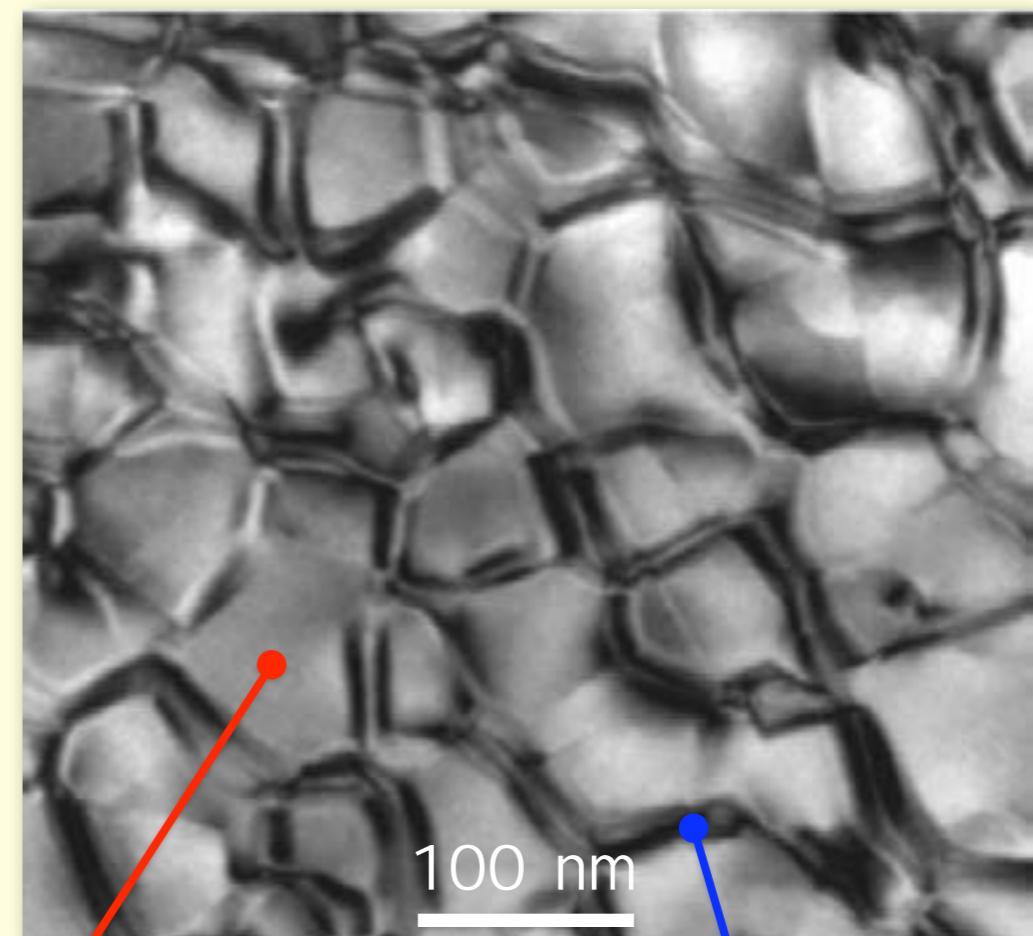
Sm(Co_{0.784}Fe_{0.1}Cu_{0.088}Zr_{0.028})_{7.19}

known as pinning magnet

c-axis parallel



c-axis perpendicular



Zr-rich
precipitation phase

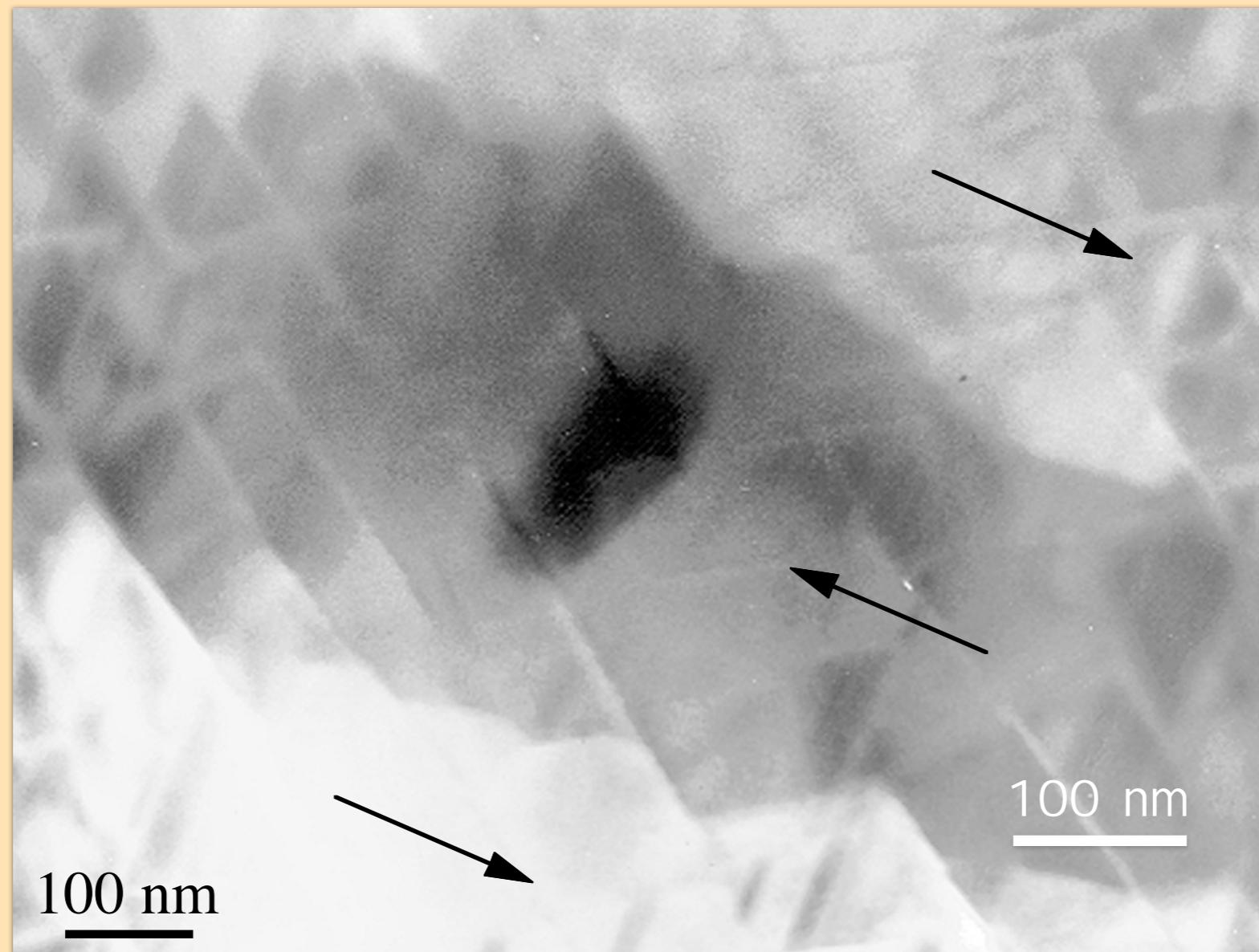
Sm₂(CoFe)₁₇
cells (100 nm)

Cu-rich
precip. phase

Domains in Sm₂Co₁₇ magnets

Sm(Co_{0.784}Fe_{0.1}Cu_{0.088}Zr_{0.028})_{7.19}

magnetic microstructure (Lorentz-TEM):



courtesy J. Fidler, Vienna

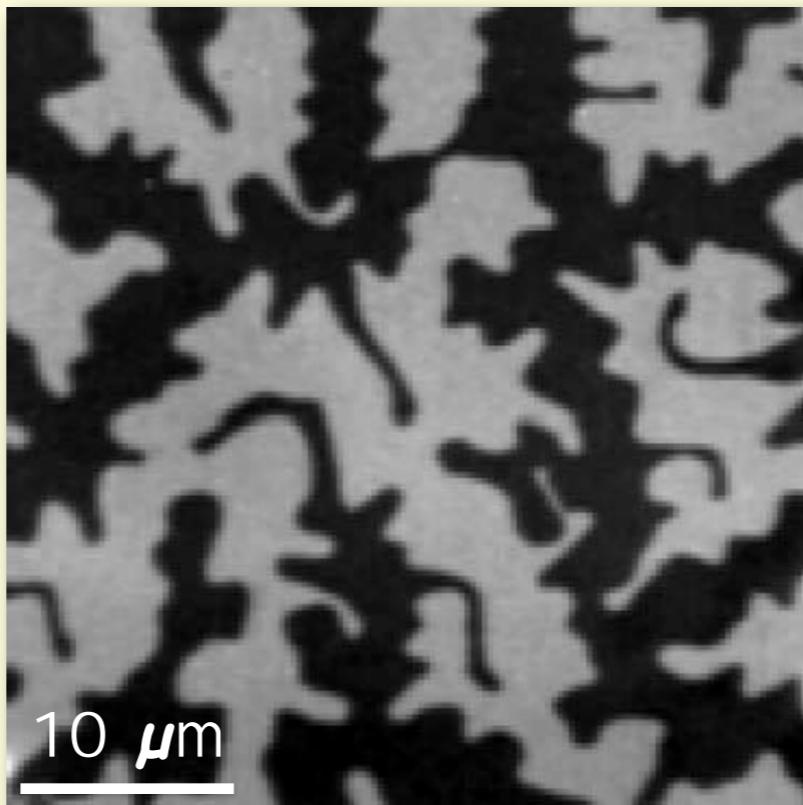
Domains in Sm₂Co₁₇ magnets

quenched from 850°C
(low coercive state)

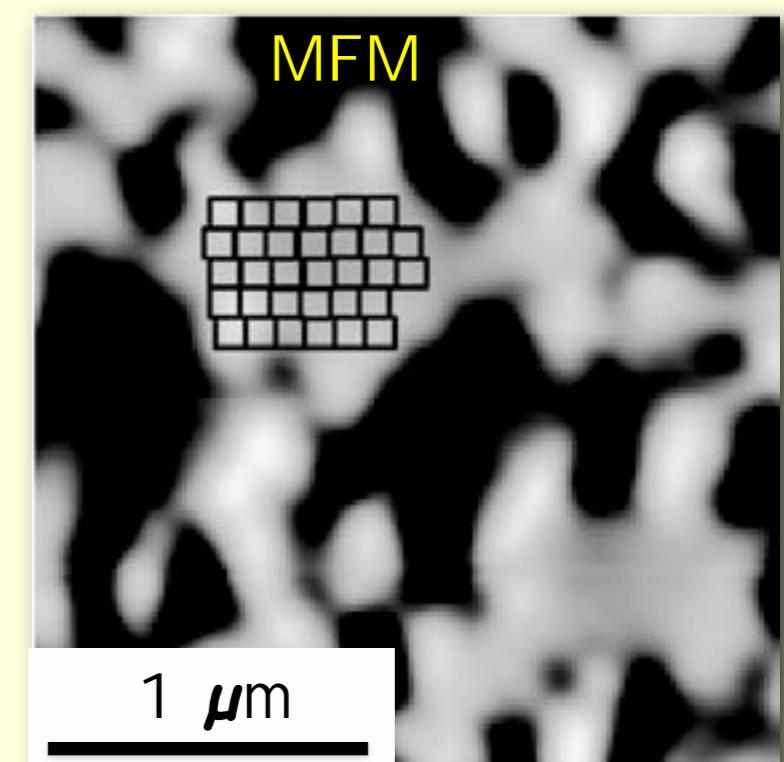
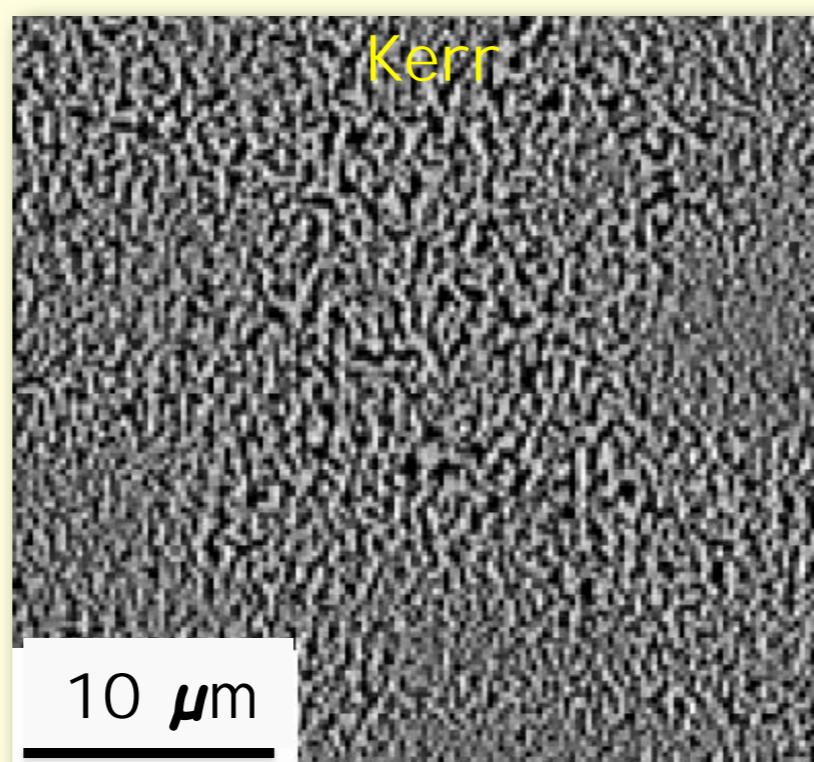
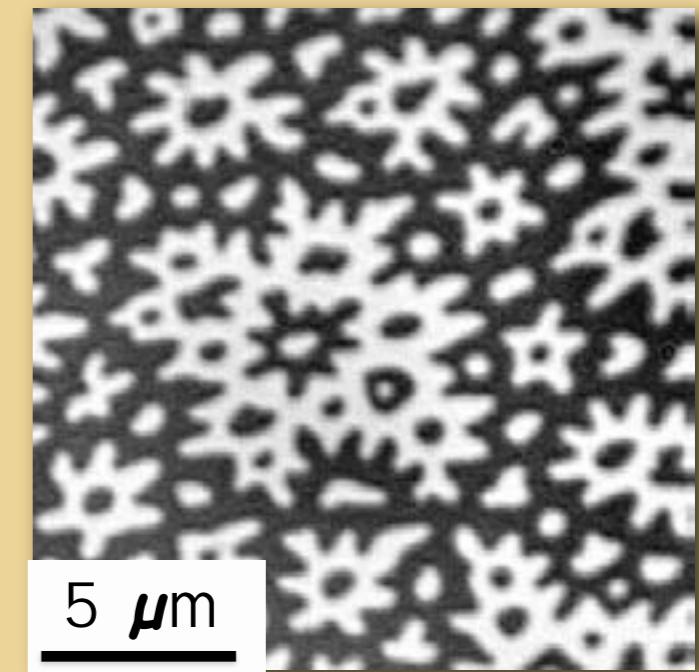
O. Gutfleisch et al.,
Acta Mater. 54 (2006)

slowly cooled to 400°C
(optimally processed,
high coercive state

$$\mu_0 H_c \approx 3T$$



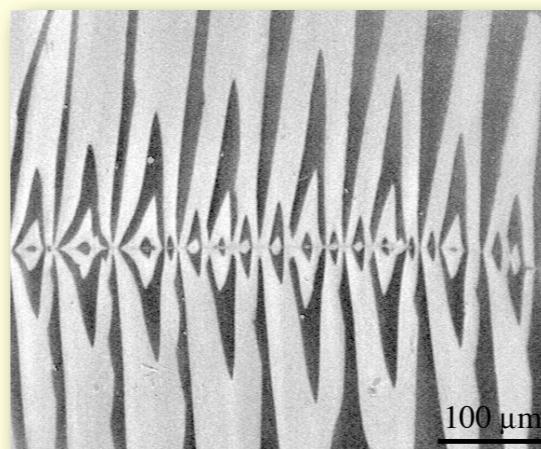
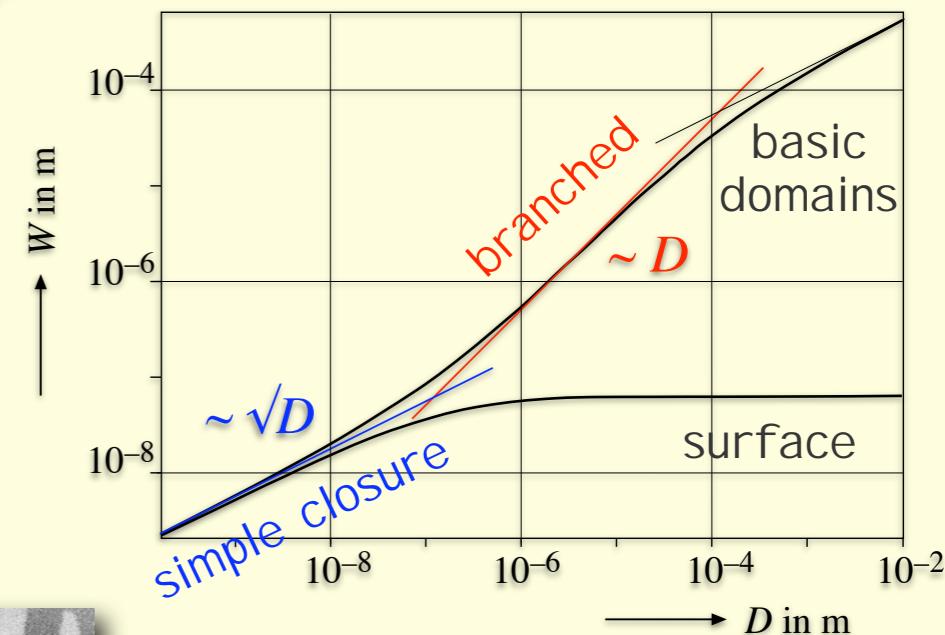
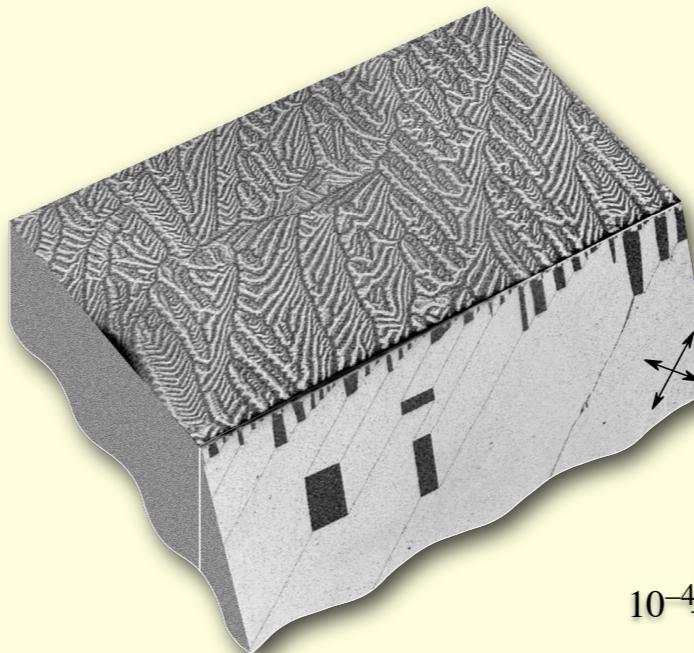
for comparison: NdFeB



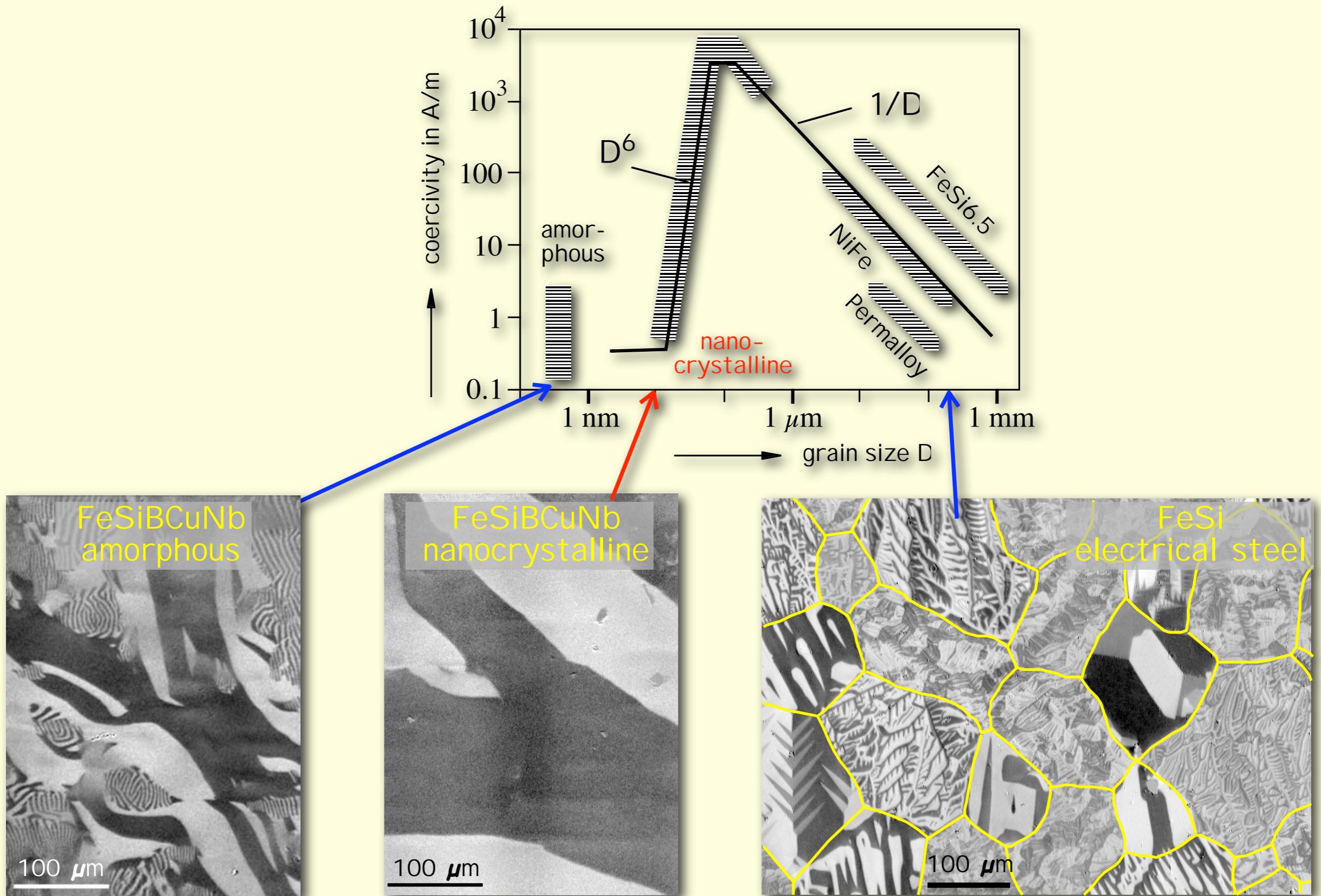
Summary

Domains in coarse-grained material

- wide volume domains
fine surface domains
- domain width increases linearly
with thickness (i.e. grain size)
- coercivity due to
grain boundary effects



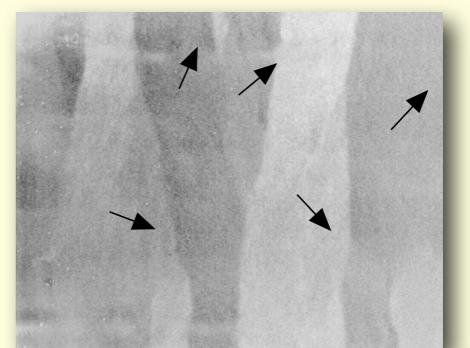
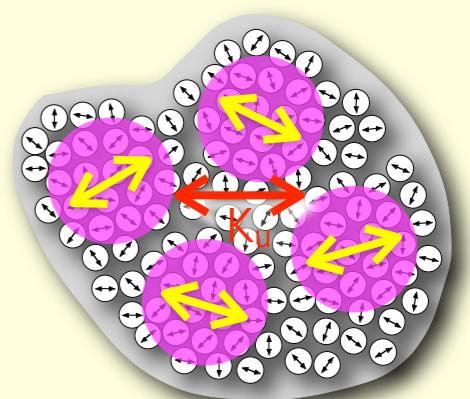
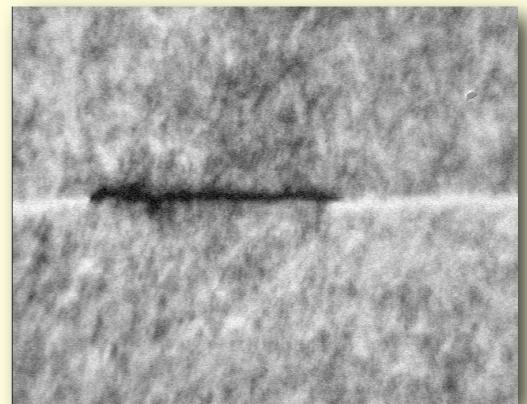
Summary



Summary

Domains in nanocrystalline ribbons

- patchy modulation (connection to ripple), depends on induced anisotropy
- counterplay uniform induced anisotropy/averaged magnetocrystalline anisotropy
- counterplay also explains:
 - patch domains for $T > T_c$, amorph
 - irregularities in hard- and easy-axis magnetization process
- nucleation-dominated domain refinement (patch domains) at high f



Summary

Domains in fine and nanostructured permanent magnets

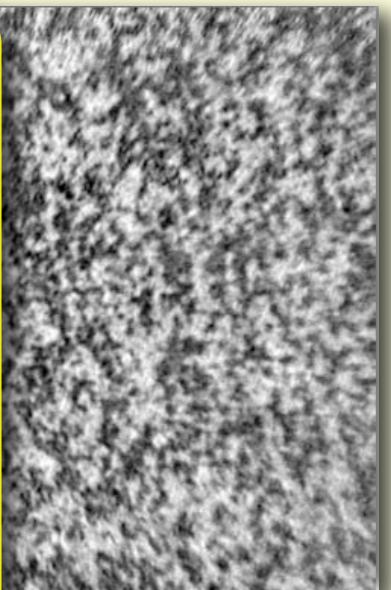
- highly inhomogeneous for exchange
- magnetostrictive for decoherence

typical grain sizes: 20 - 300 nm

$$\text{Nd}_2\text{Fe}_{14}\text{B}: \\ K_u = 4.3 \cdot 10^6 \text{ kJ/m}^3 \\ A = 8 \cdot 10^{-12} \text{ J/m}$$

$$\rightarrow L_{ex} = \sqrt{A/K_1} = 1.3 \text{ nm}$$

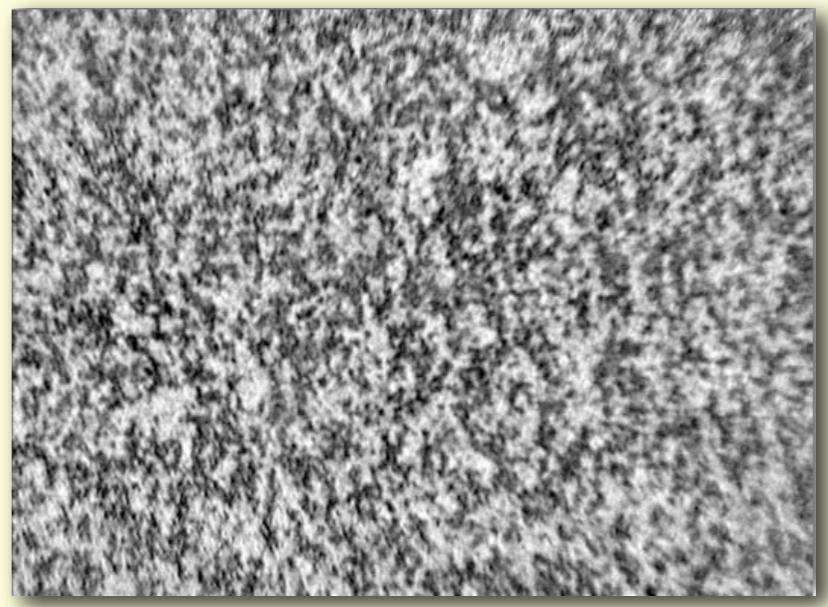
→ random anisotropy
model irrelevant



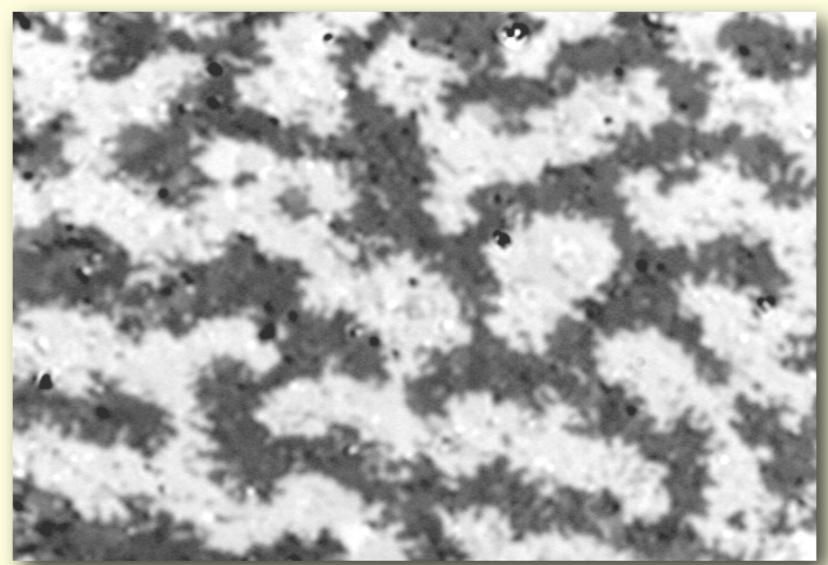
Summary

Domains in fine and nanostructured permanent magnets

- highly immobile patch domains
for exchange coupled materials



- magnetostatic interaction domains
for decoupled grains





Hierarchy of descriptive levels of magnetic materials

5. Magnetic Hysteresis, or Magnetization Curve

Describing the *average magnetization* vector of a sample as a function of the external field (always applicable)

4. Phase, or Magnetic Texture Analysis

Collecting domains of equal magnetization direction in “phases”. More generally, describing the distribution function (*texture*) of magnetization directions (> 0.1 mm)

3. Domain, or Magnetic Microstructure Analysis

Describing the *magnetic microstructure* of a sample, the shape and detailed spatial arrangement of domains and domain boundaries (1–1000 µm)

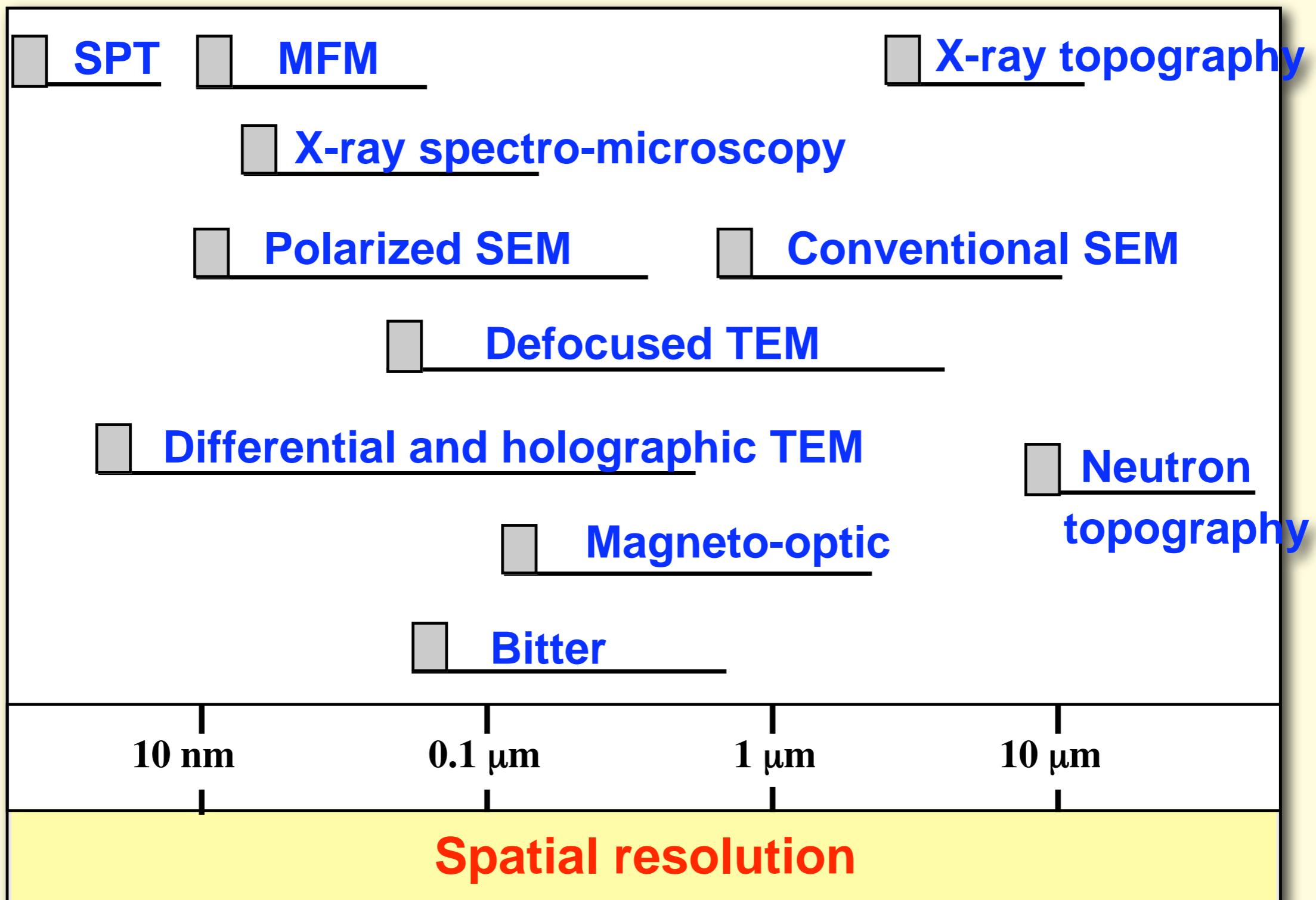
2. Micromagnetic Analysis

Describing the *internal structure of domain walls* and their substructures in terms of a continuum theory of a classical magnetization vector field (1–1000 nm)

1. Atomic Level Theory

Describing the origin, the interactions, the mutual arrangement and the statistical thermodynamics of elementary magnetic moments (< 1 nm)

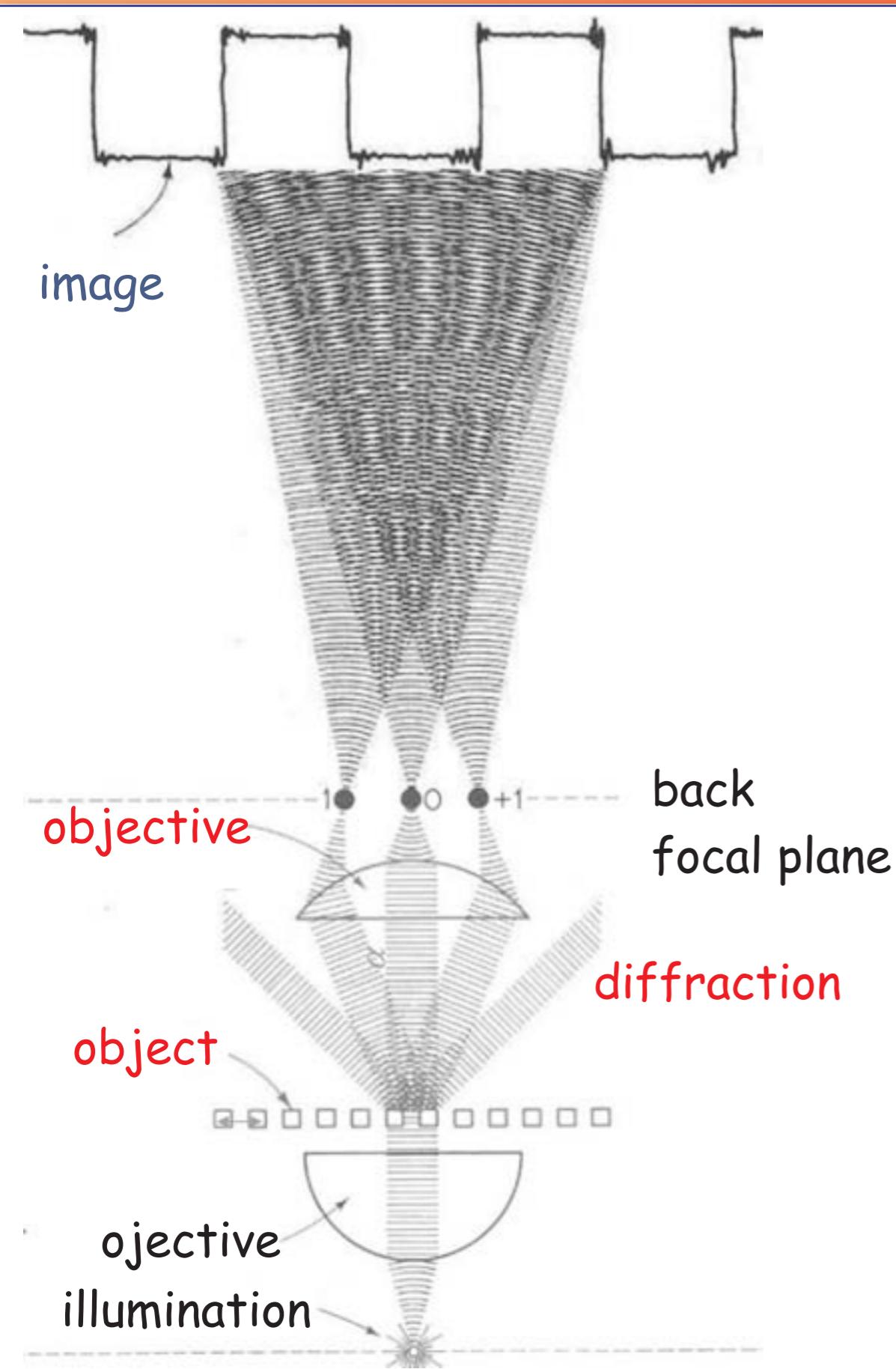
Comparison of Domain Observation Techniques



MFM: Magnetic Force Microscopy
SPT: Spin-Polarized Tunneling
MO: Magnoptic Method

SEM: Scanning (reflection) Electron Microscopy
TEM: Transmission Electron Microscopy

Resolution of optical microscopy (E. Abbe 1840 - 1905)



resolution determined by
constructive interference

diffraction limited image formation

$$\text{Rayleigh equation: } d = \frac{0.5 \lambda}{\text{NA}}$$

d = separation between particles,
still allowing to see them

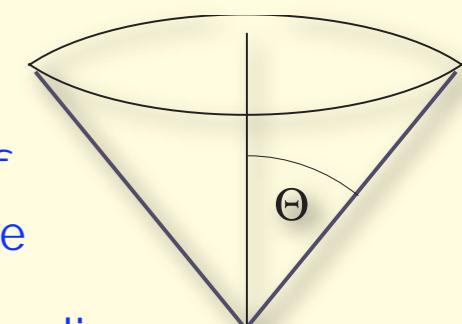
λ = wavelength

NA = numerical aperture of objective

$$\text{NA} = n \sin \theta$$

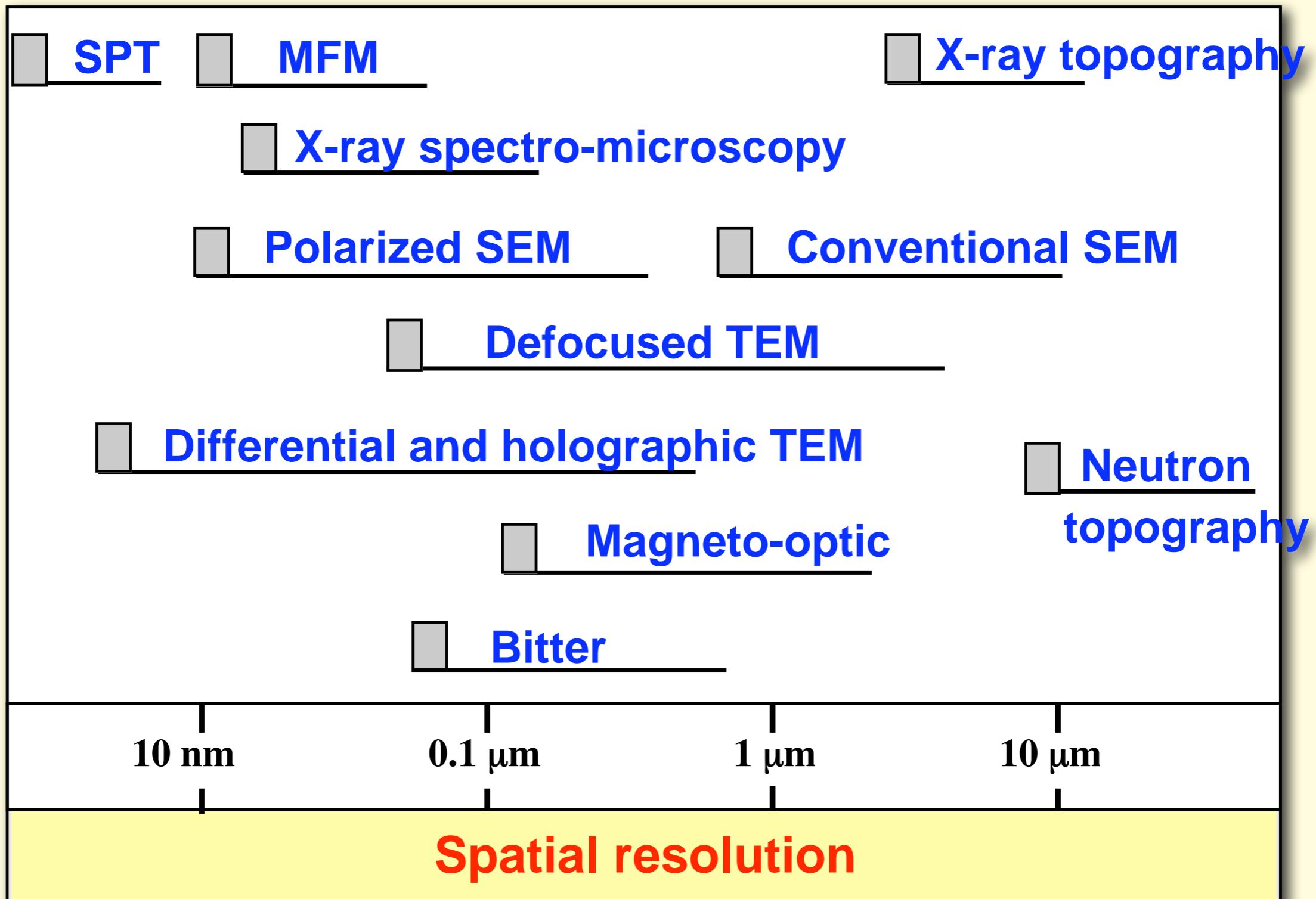
θ = half the cone angle of
light accepted by objective

n = refraction index of medium
between sample and objective



best around 200 nm

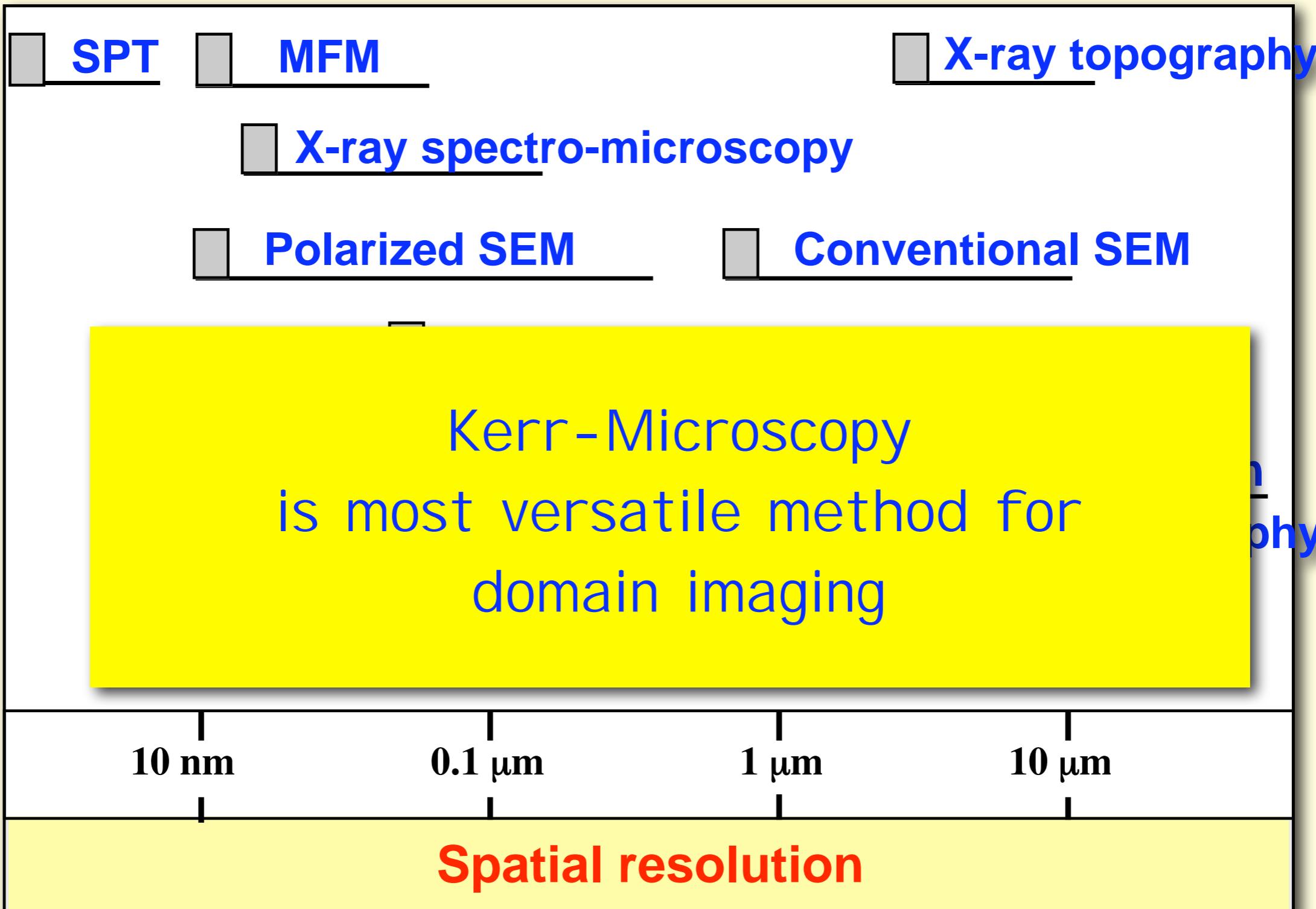
Comparison of Domain Observation Techniques



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Comparison of Domain Observation Techniques



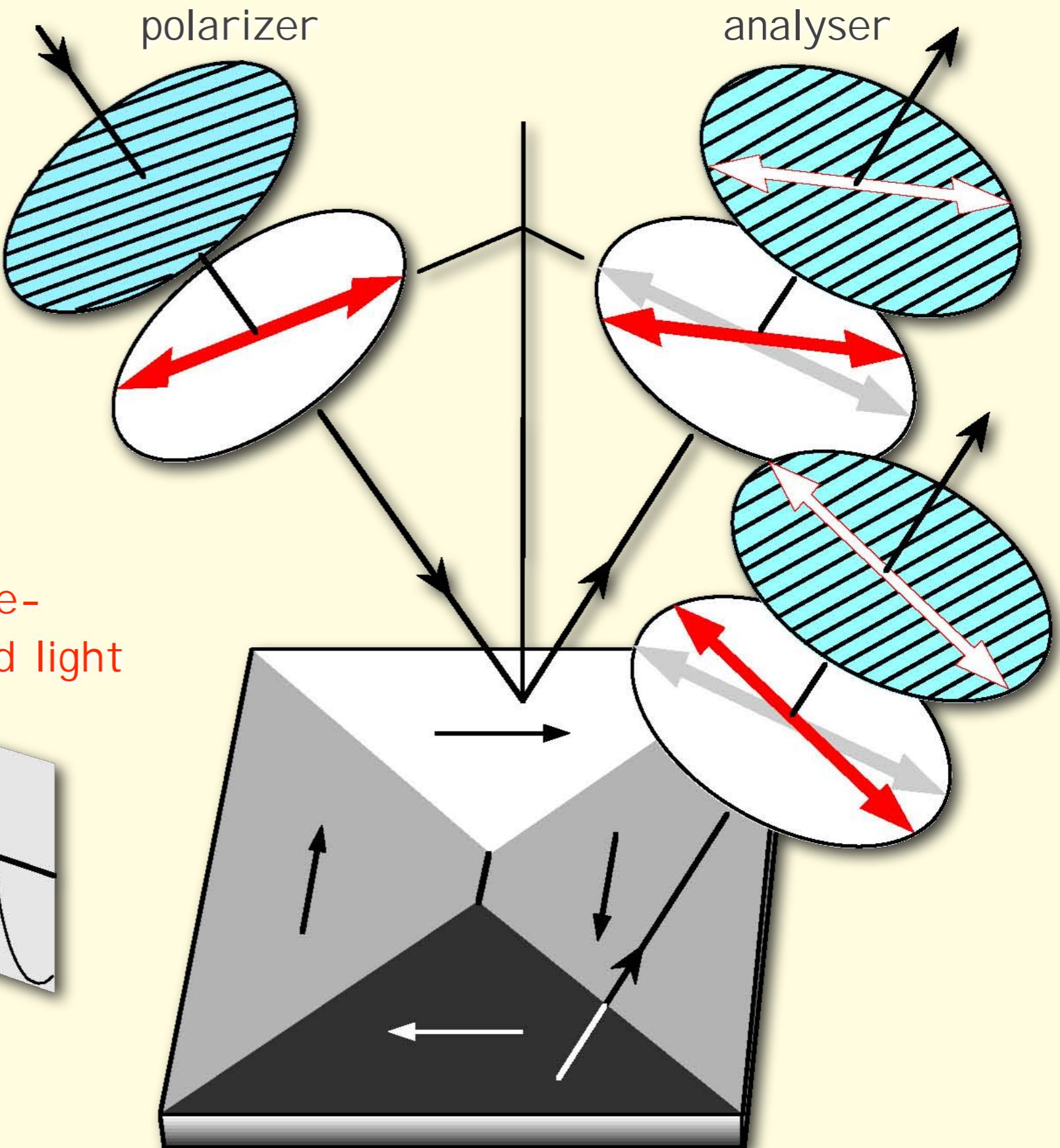
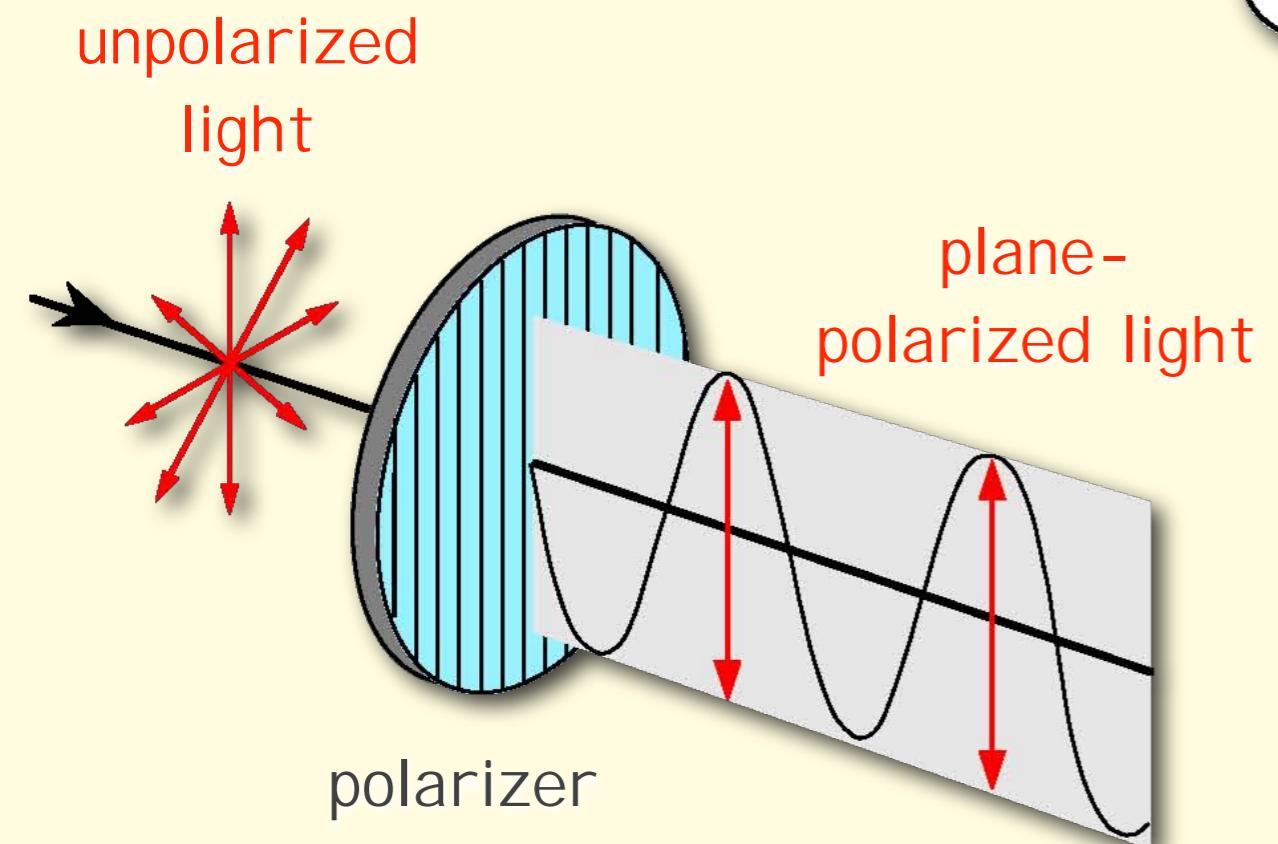
MFM: Magnetic Force Microscopy
SPT: Spin-Polarized Tunneling
MO: Magneto-optic Method

SEM: Scanning (reflection) Electron Microscopy
TEM: Transmission Electron Microscopy

Kerr microscopy

Kerr effect

Kerr-effect:
rotation of
polarized light



Wide-field Kerr microscope

Video camera



Analyser



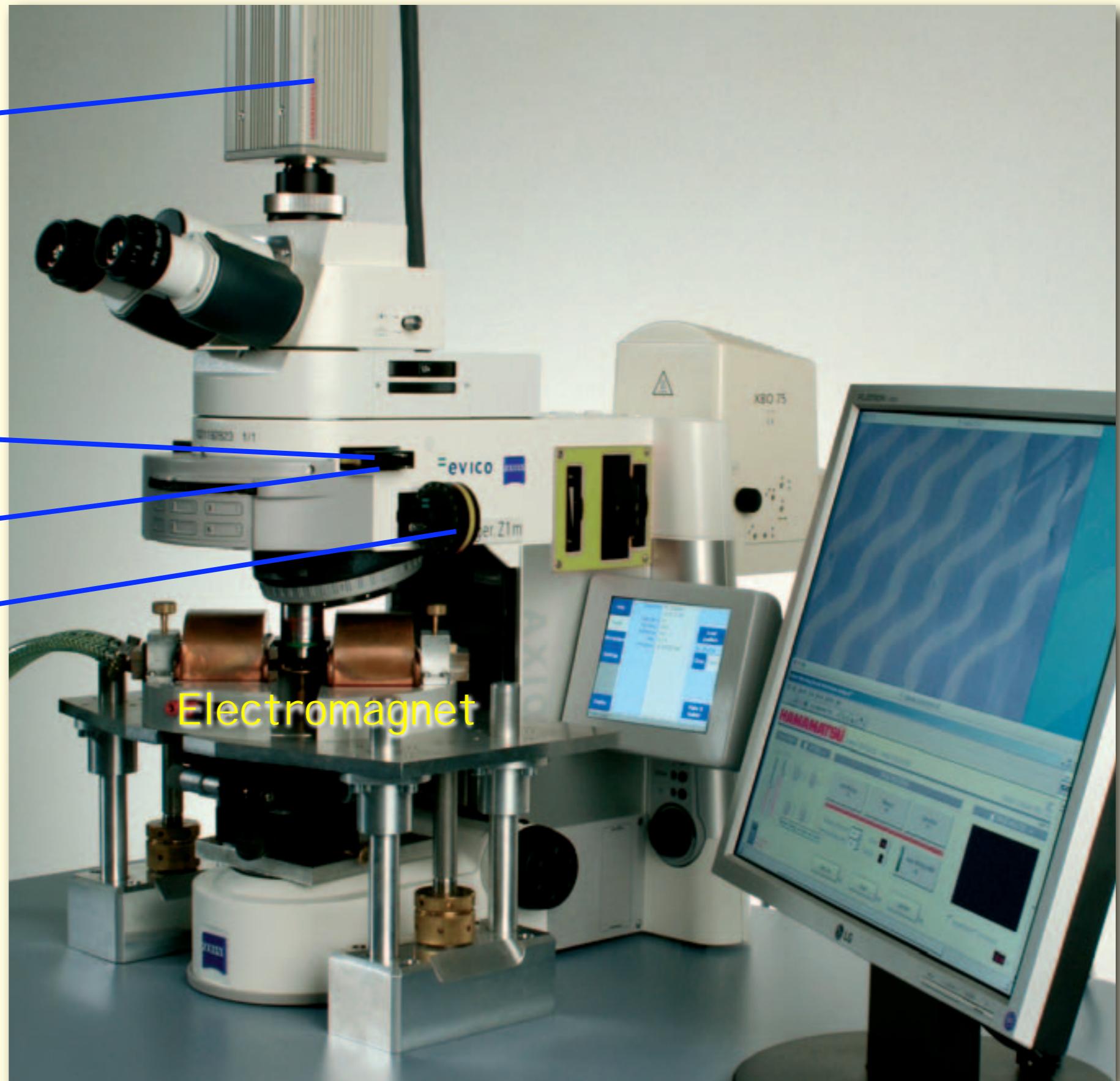
Compensator



Polarizer



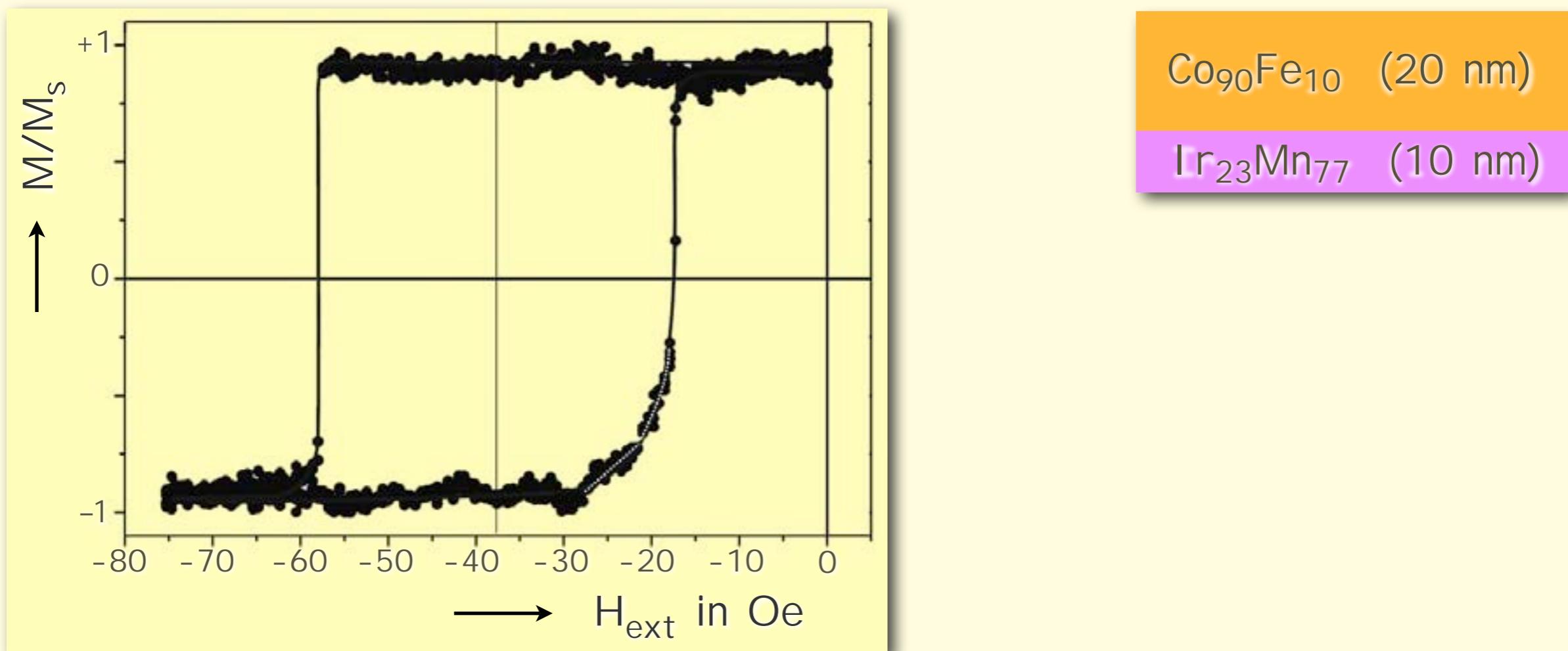
Electromagnet



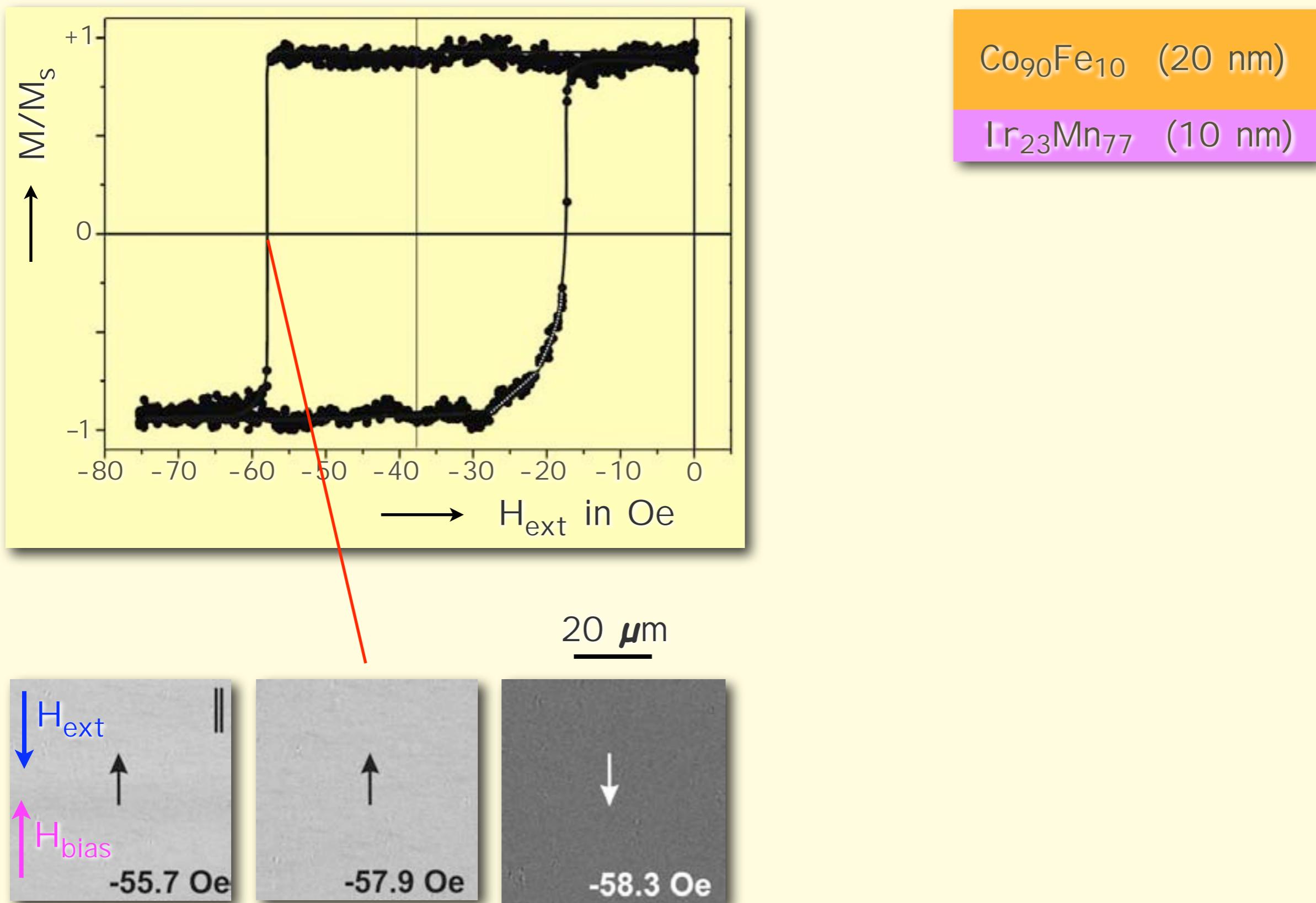
Kerr microscopy: advantages

Hysteresis curve
and
magnetization process

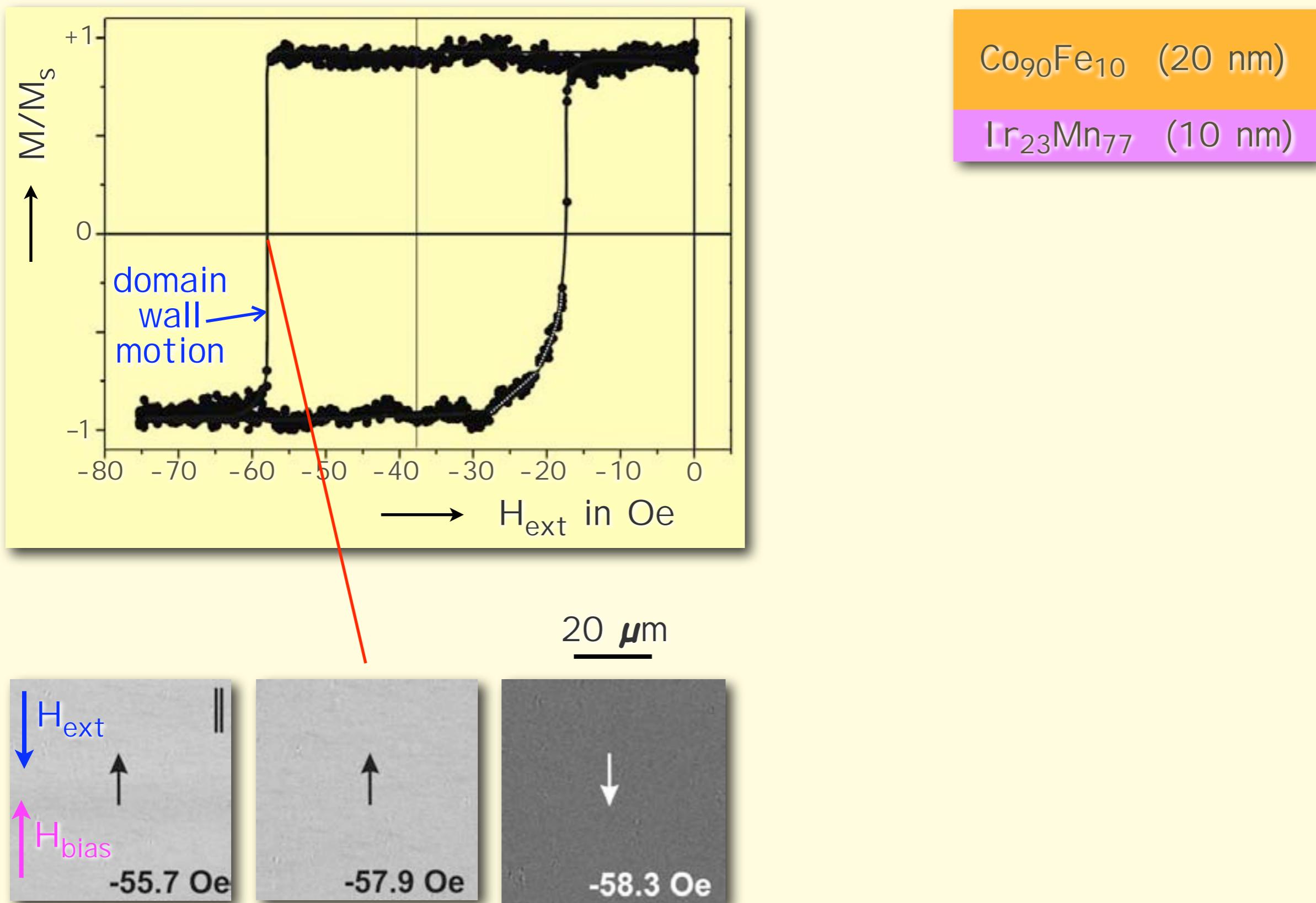
Asymmetric reversal in exchange biased CoFe/IrMn



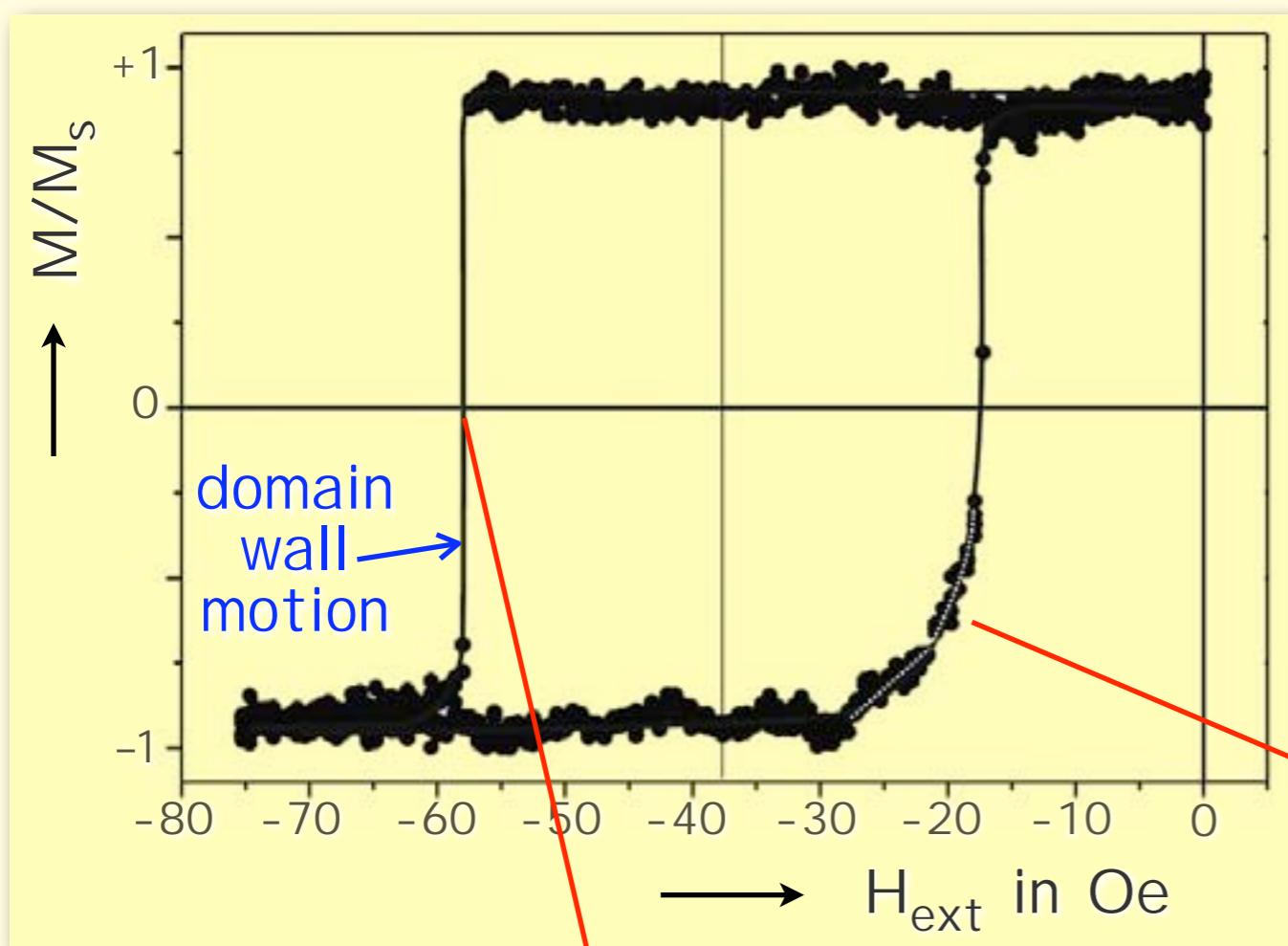
Asymmetric reversal in exchange biased CoFe/IrMn



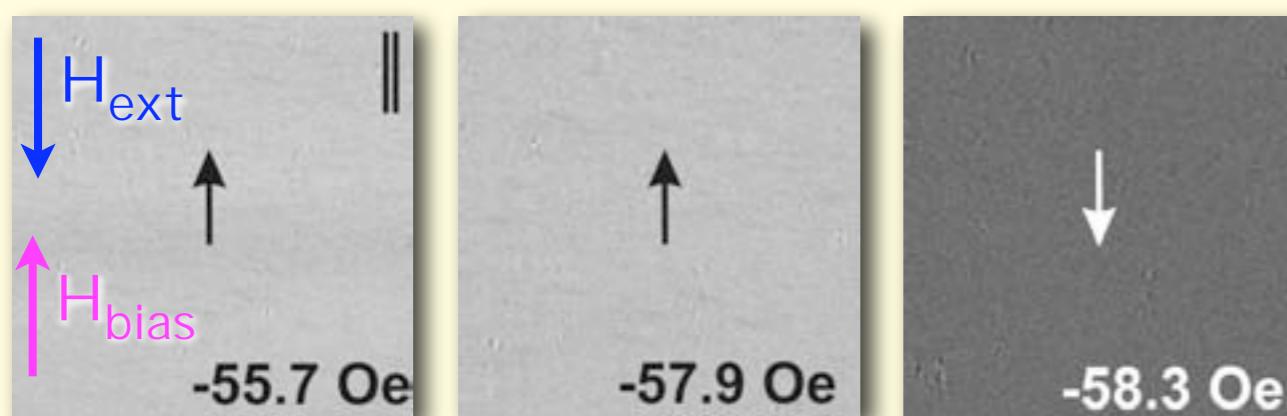
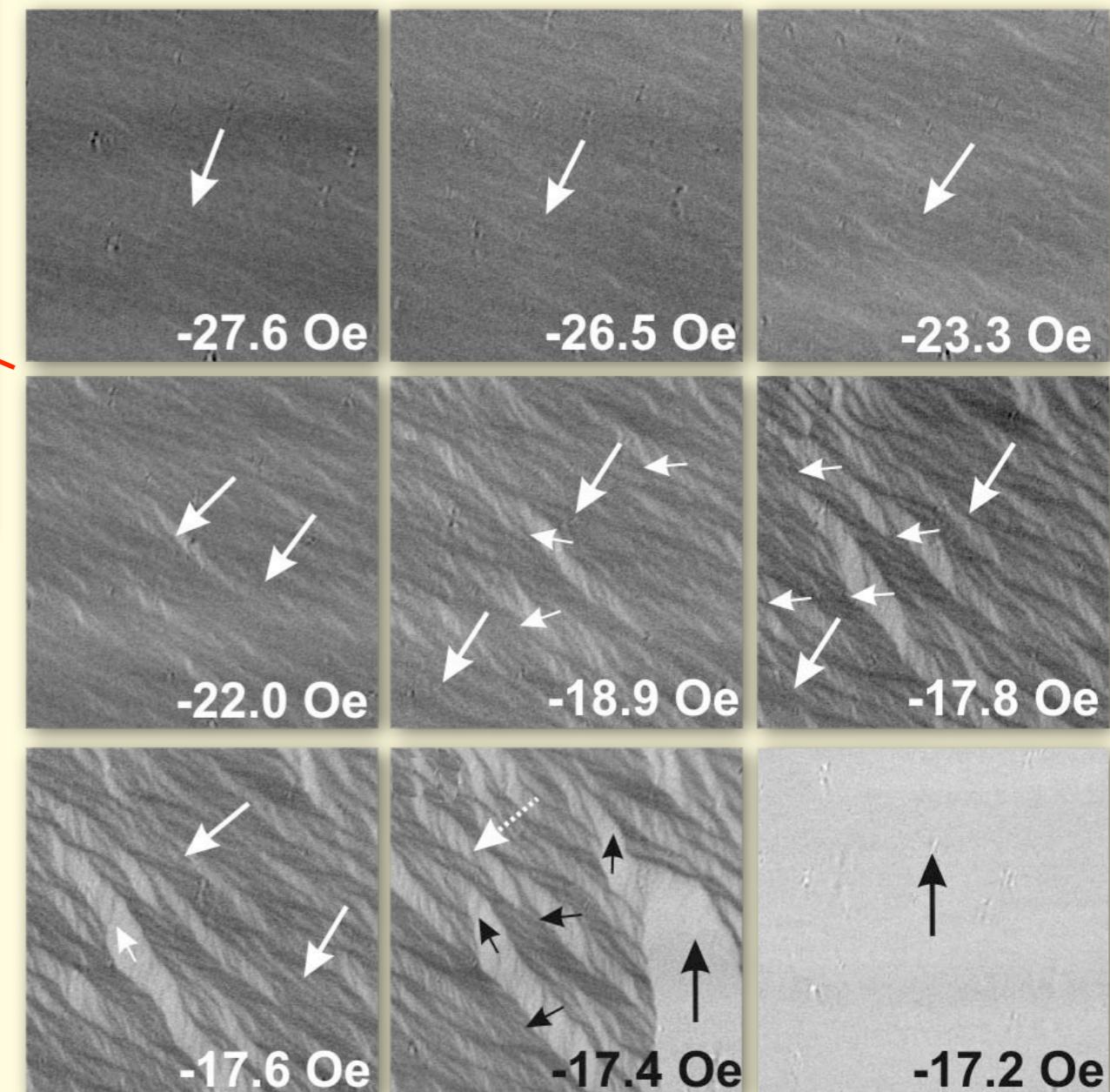
Asymmetric reversal in exchange biased CoFe/IrMn



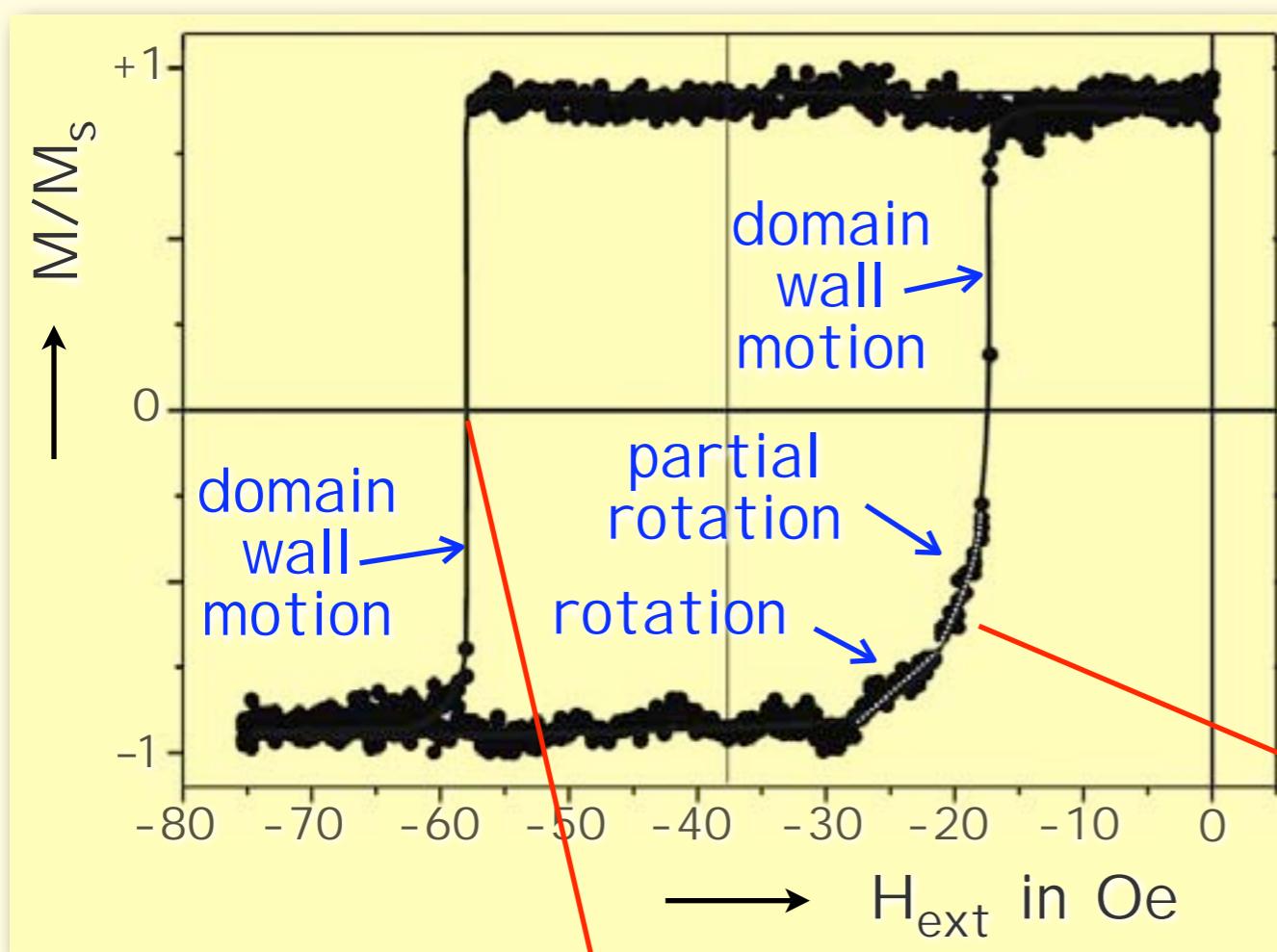
Asymmetric reversal in exchange biased CoFe/IrMn



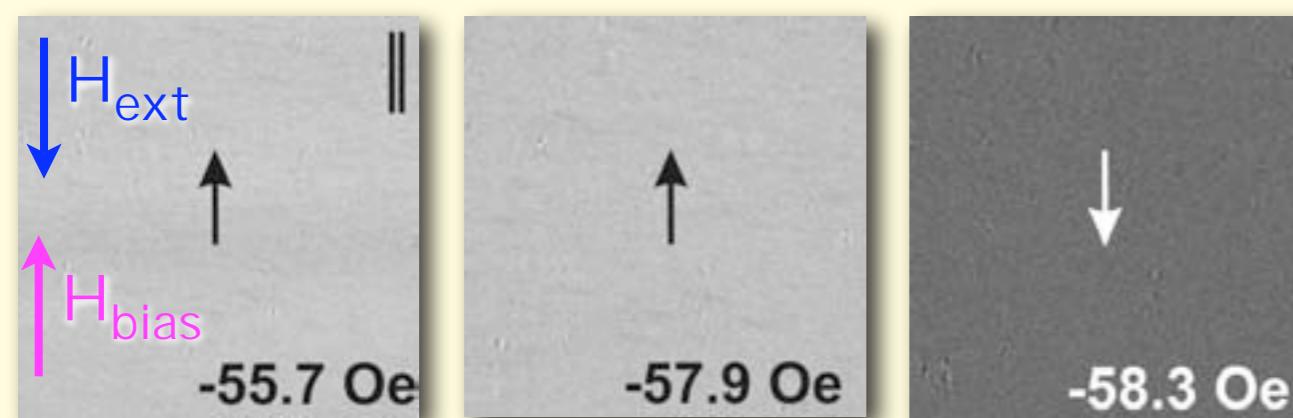
$\text{Co}_{90}\text{Fe}_{10}$ (20 nm)
 $\text{Ir}_{23}\text{Mn}_{77}$ (10 nm)



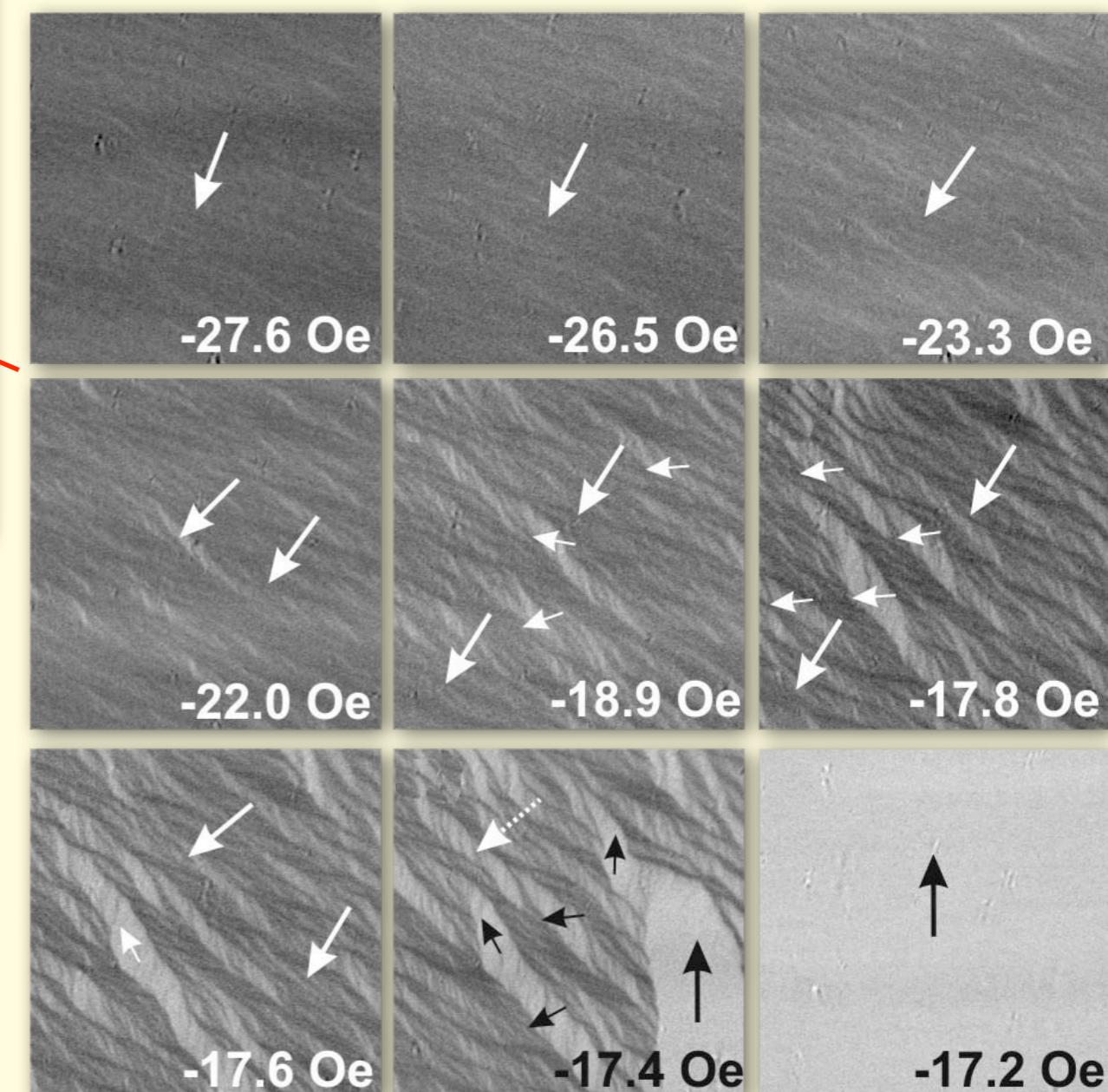
Asymmetric reversal in exchange biased CoFe/IrMn



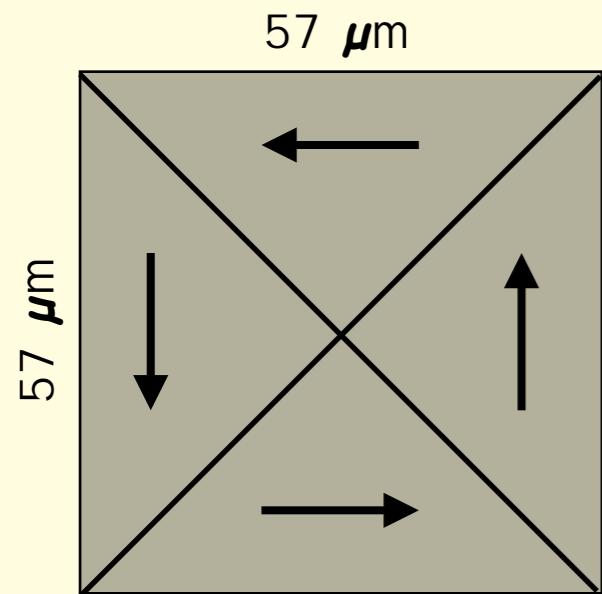
20 μm



$\text{Co}_{90}\text{Fe}_{10}$ (20 nm)
 $\text{Ir}_{23}\text{Mn}_{77}$ (10 nm)

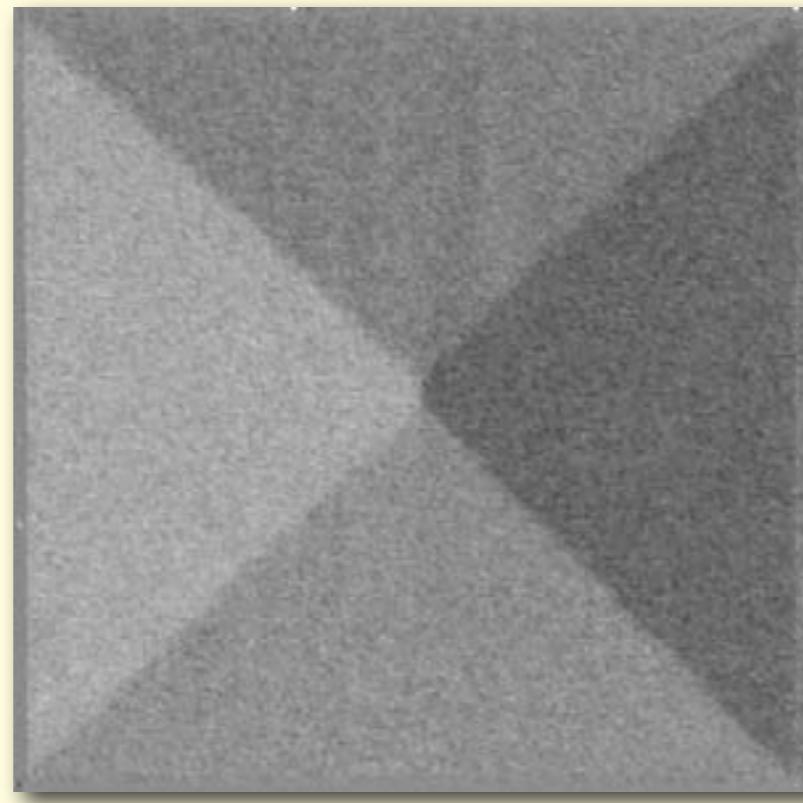


Concertina decay and hysteresis

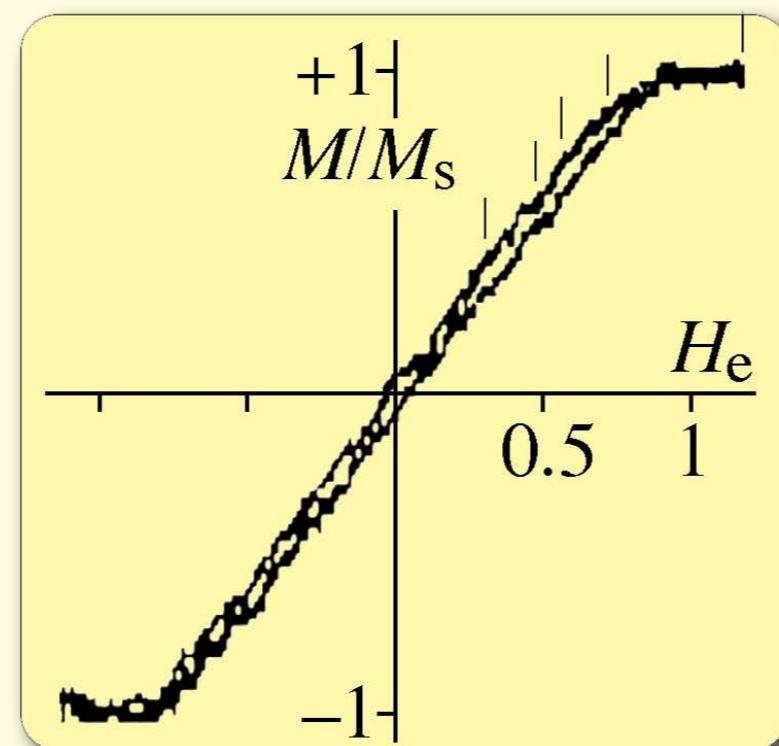


► magnetic-field

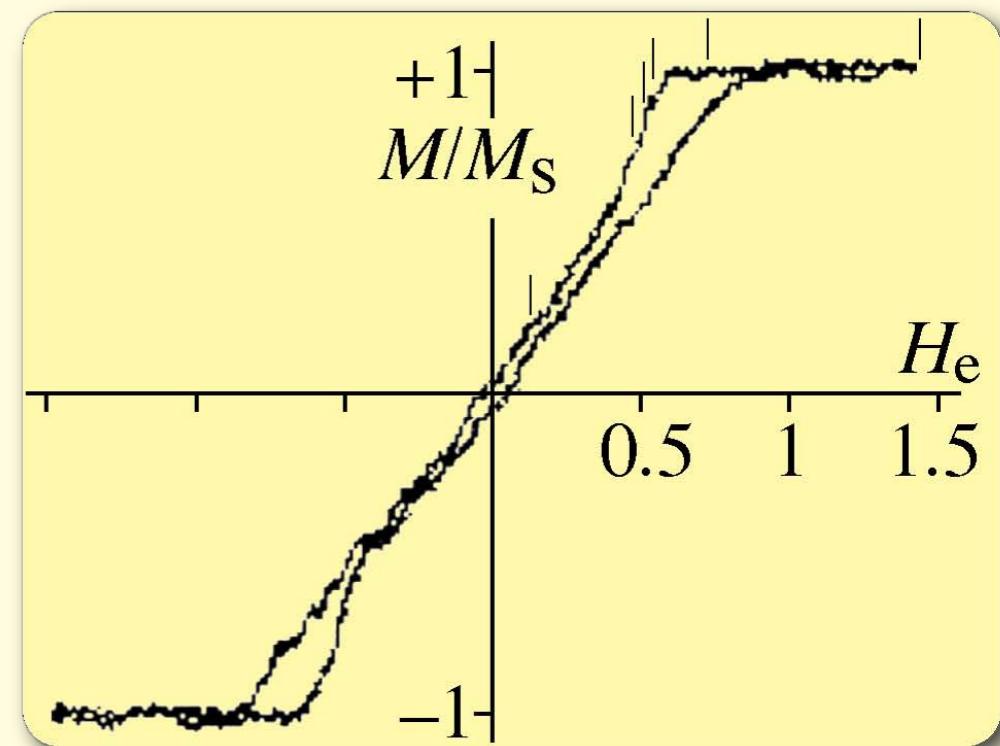
NiFe film
207 nm thick



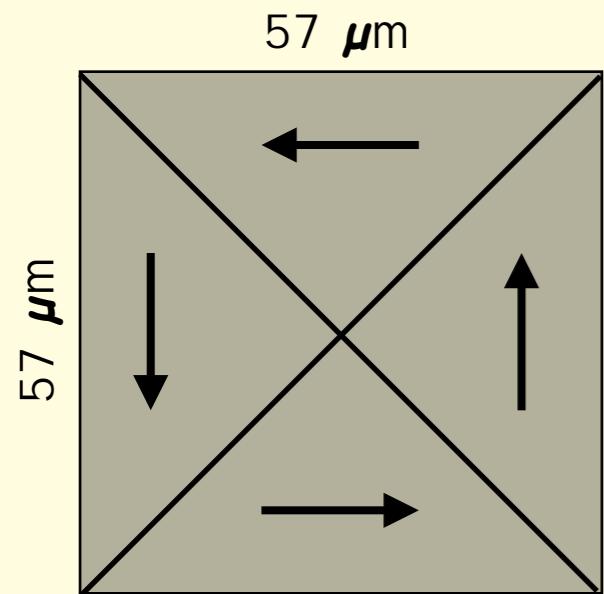
small field



large field

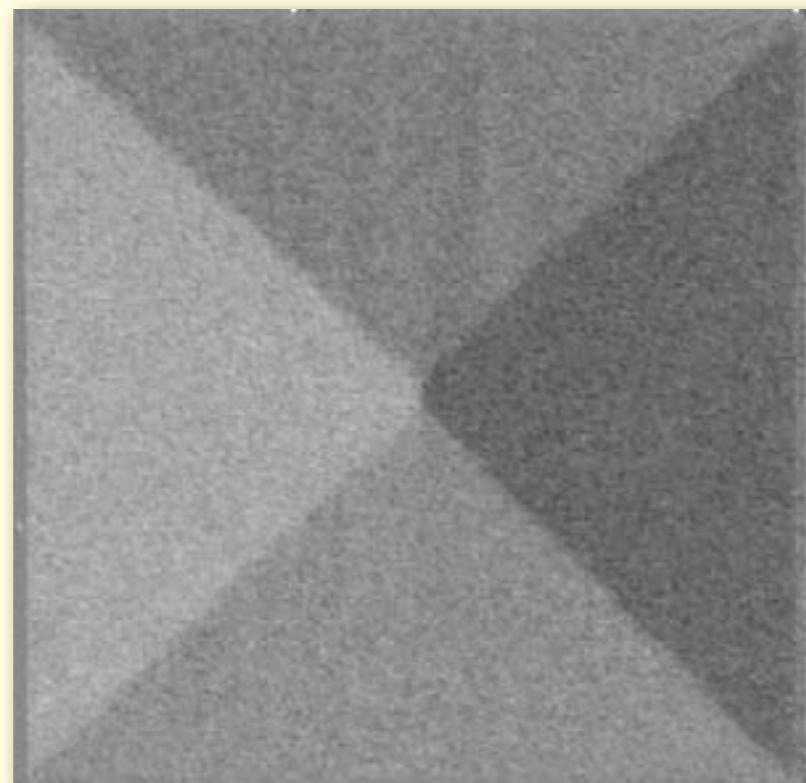


Concertina decay and hysteresis

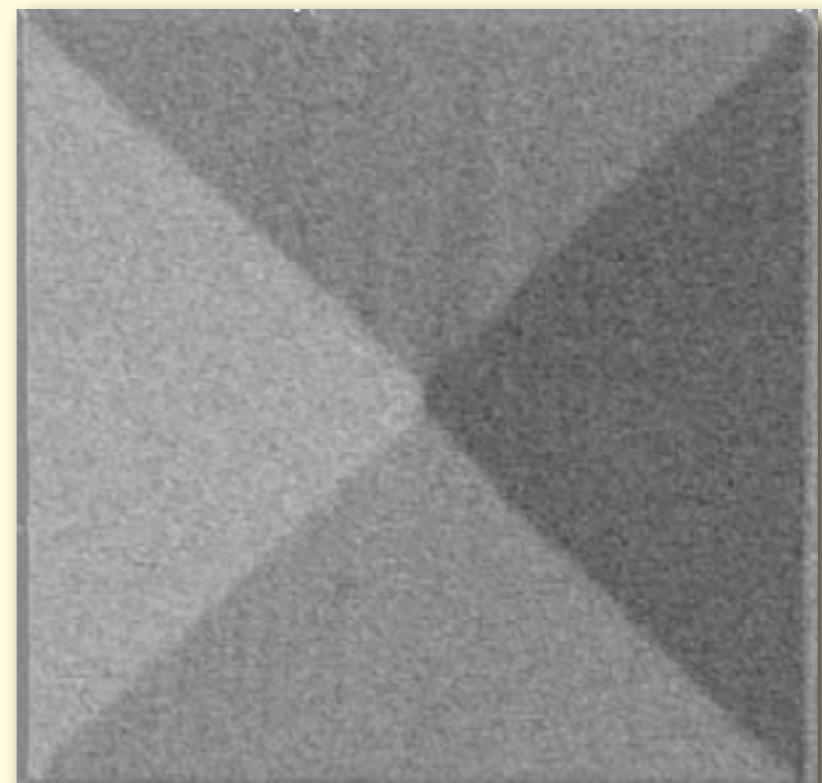


► magnetic-field

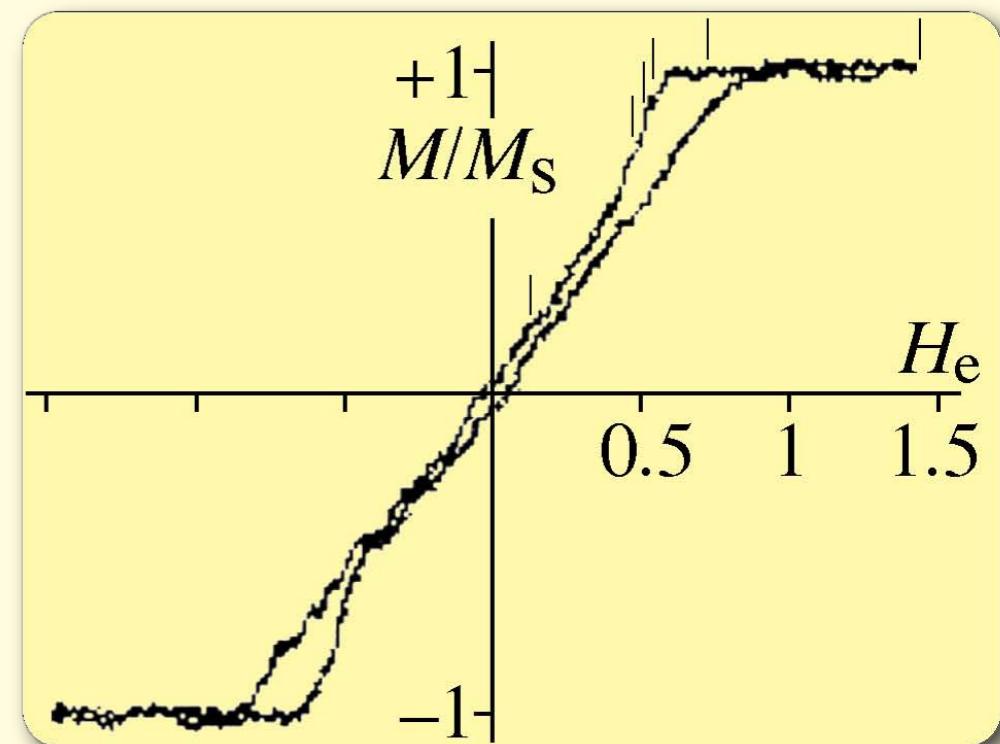
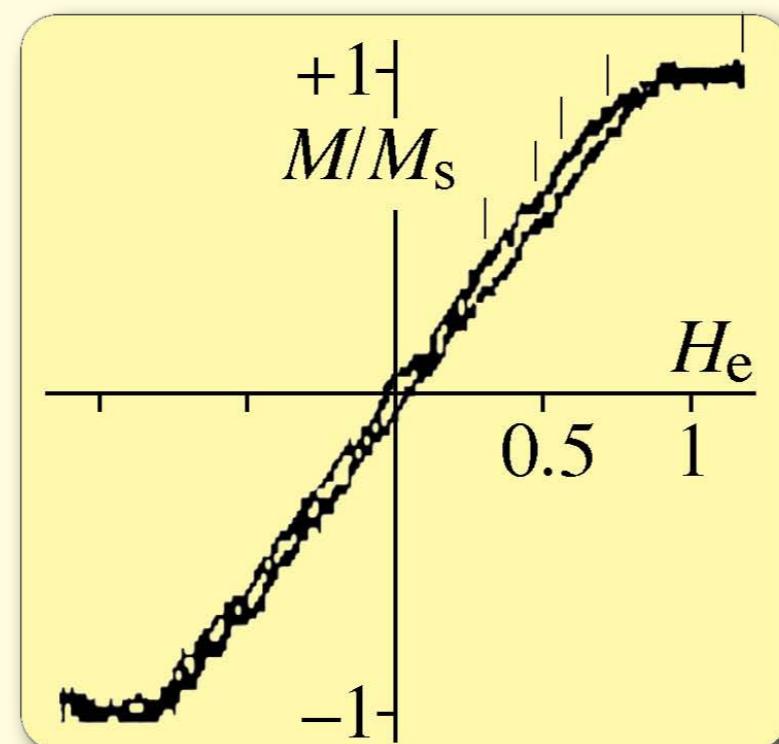
NiFe film
207 nm thick



small field



large field



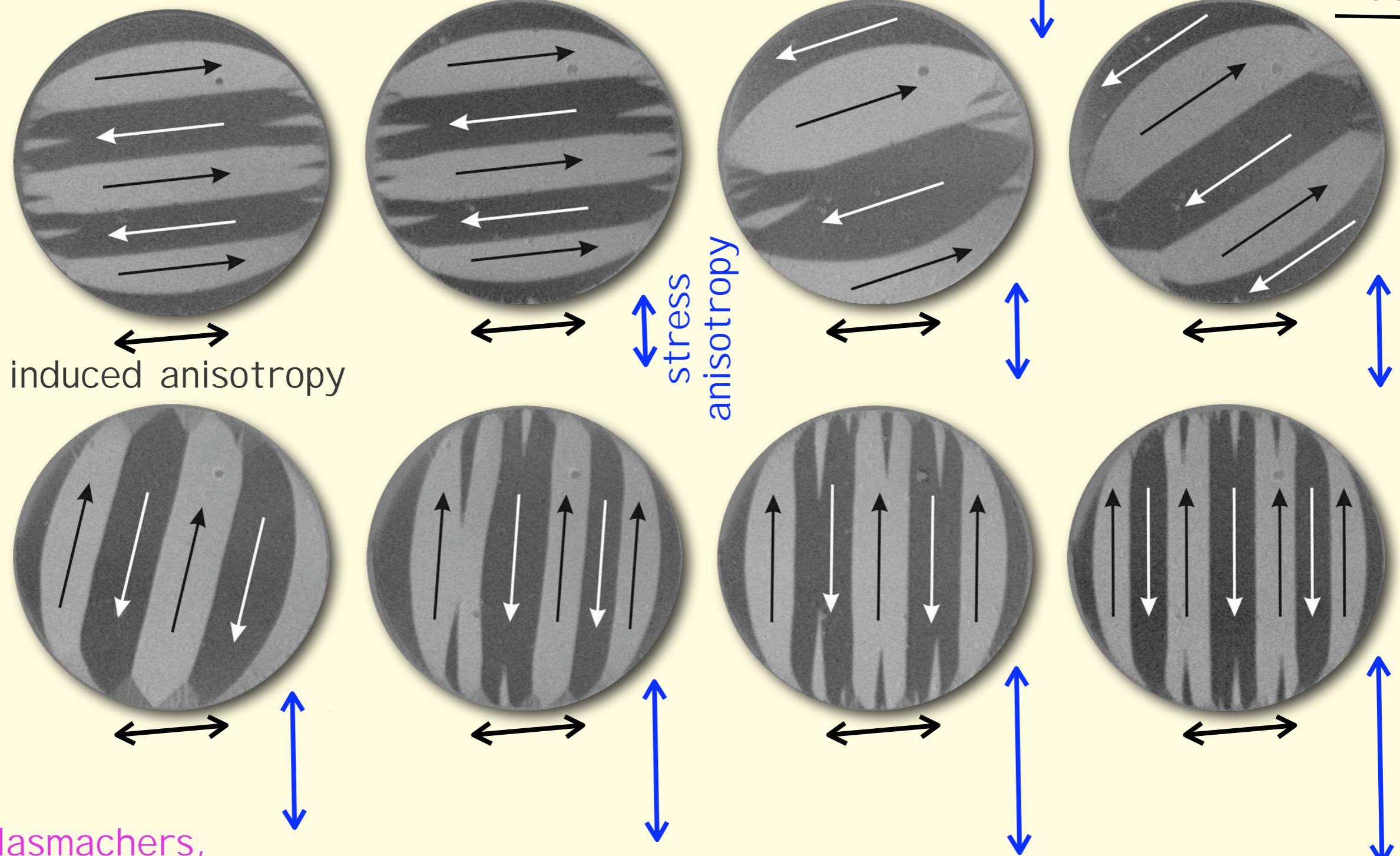
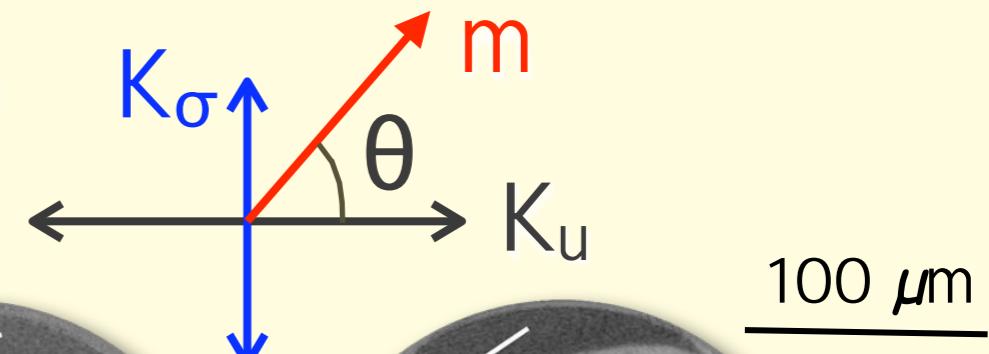
Kerr microscopy: advantages

Sample manipulation

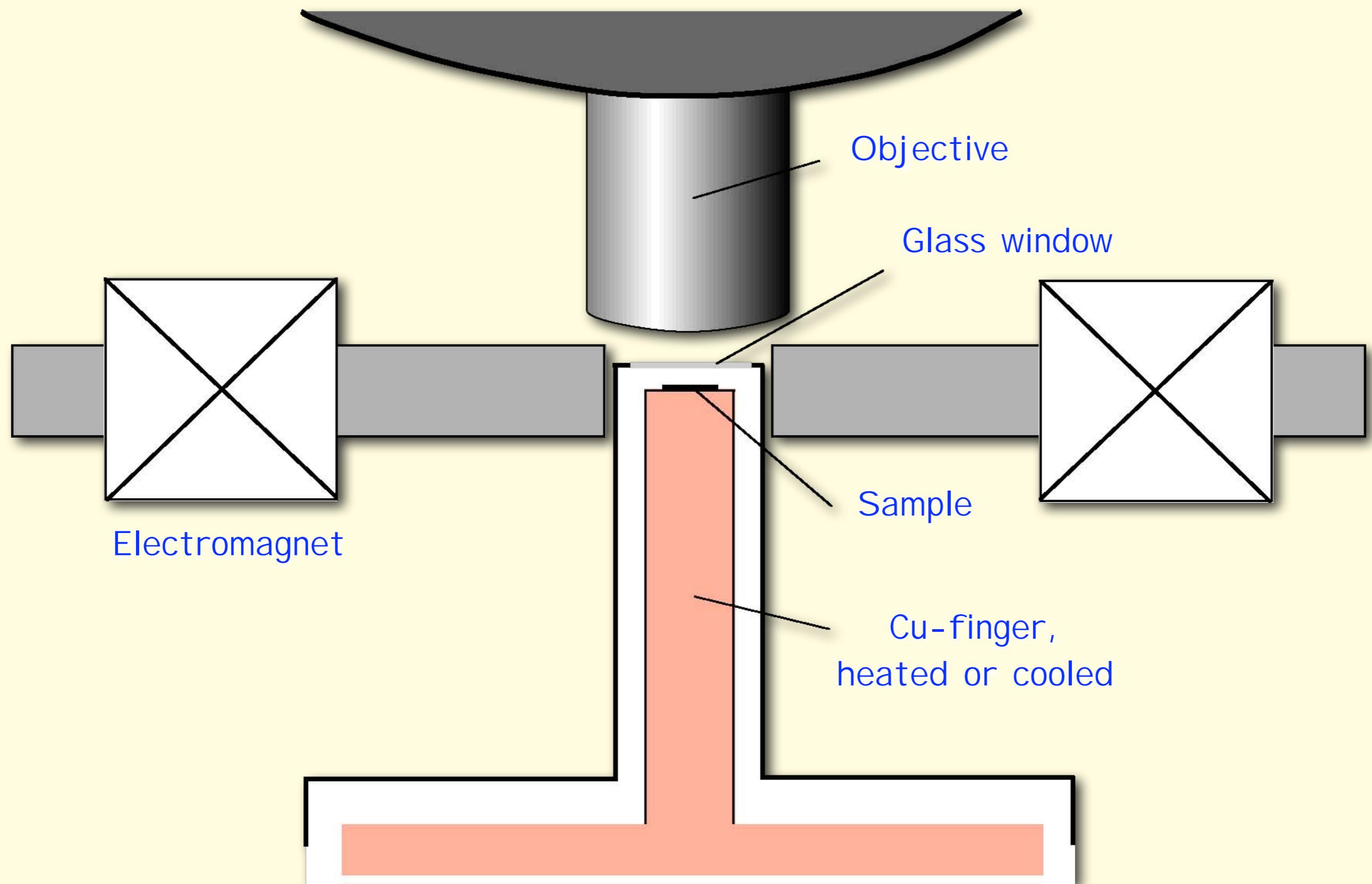
Sample manipulation by mechanical stress

CoFeBSi amorphous film (500 nm thick)

$$e_K = K_u \sin^2\theta + K_\sigma \cos^2\theta$$



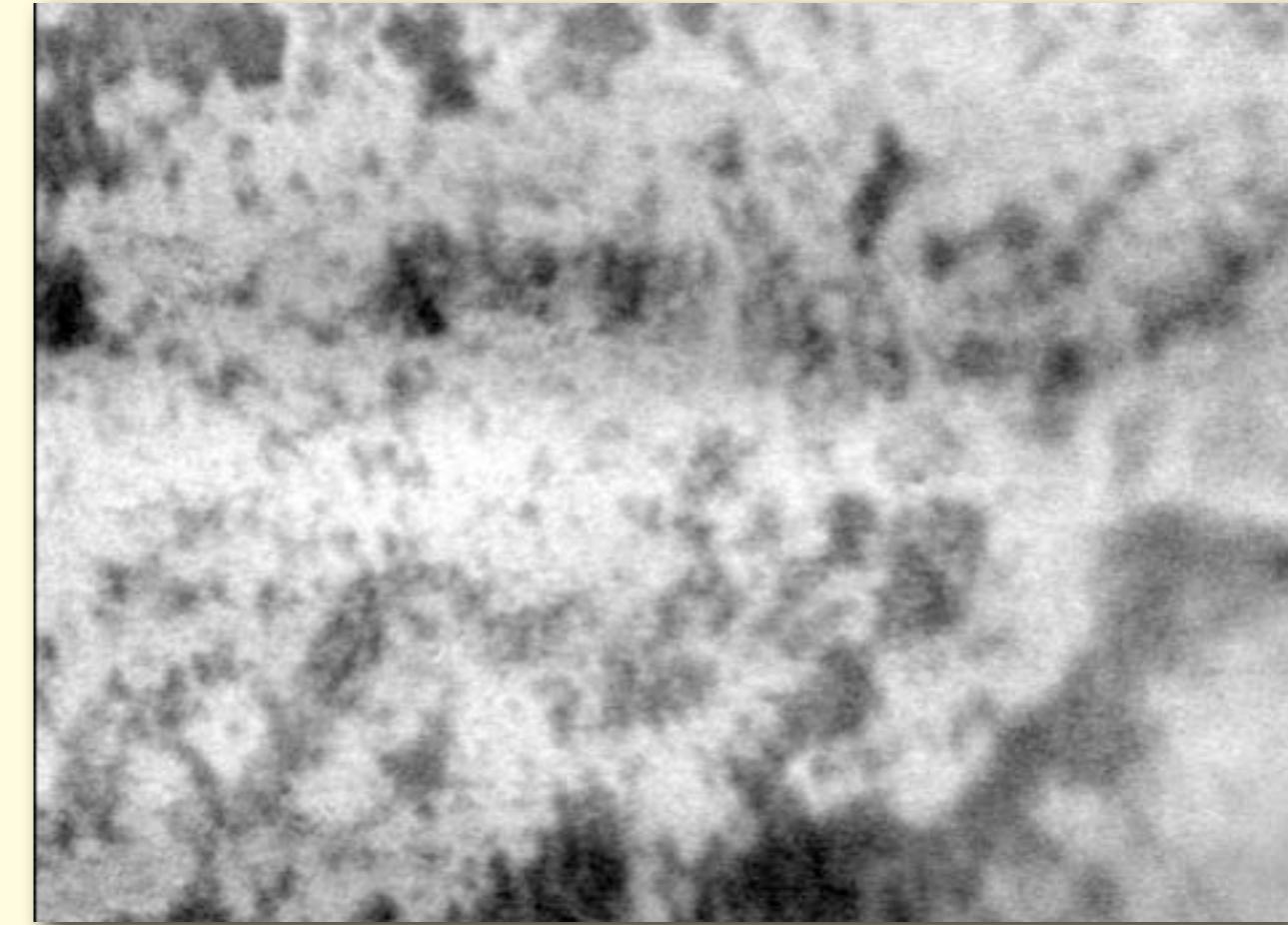
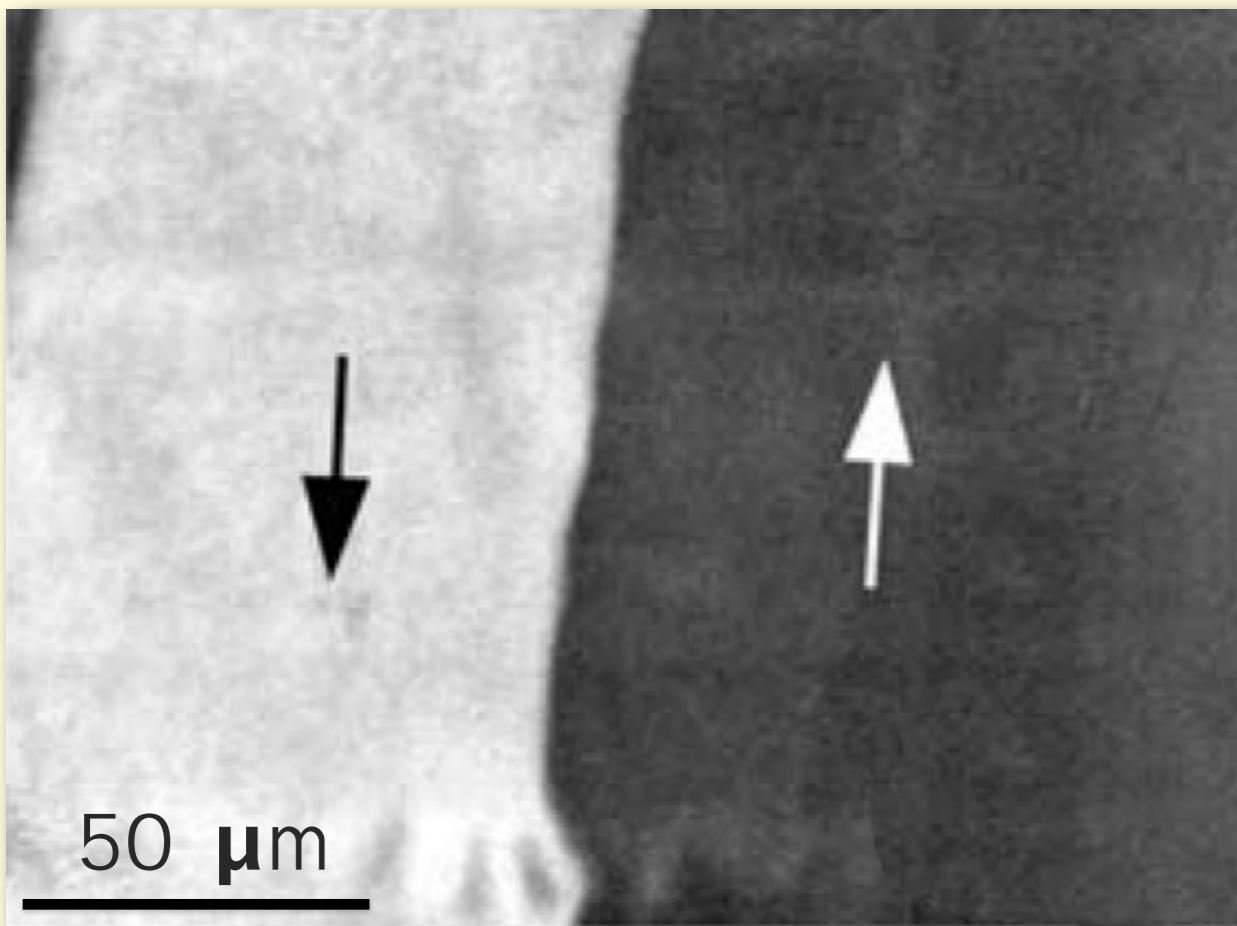
Kerr microscopy: high/low temperature observation



Heating above T_{Curie} of amorphous phase

$$\langle K_1 \rangle \sim \frac{K_1}{\sqrt{N}}$$

N: number of exchange-coupled grains within correlation volume



room temperature

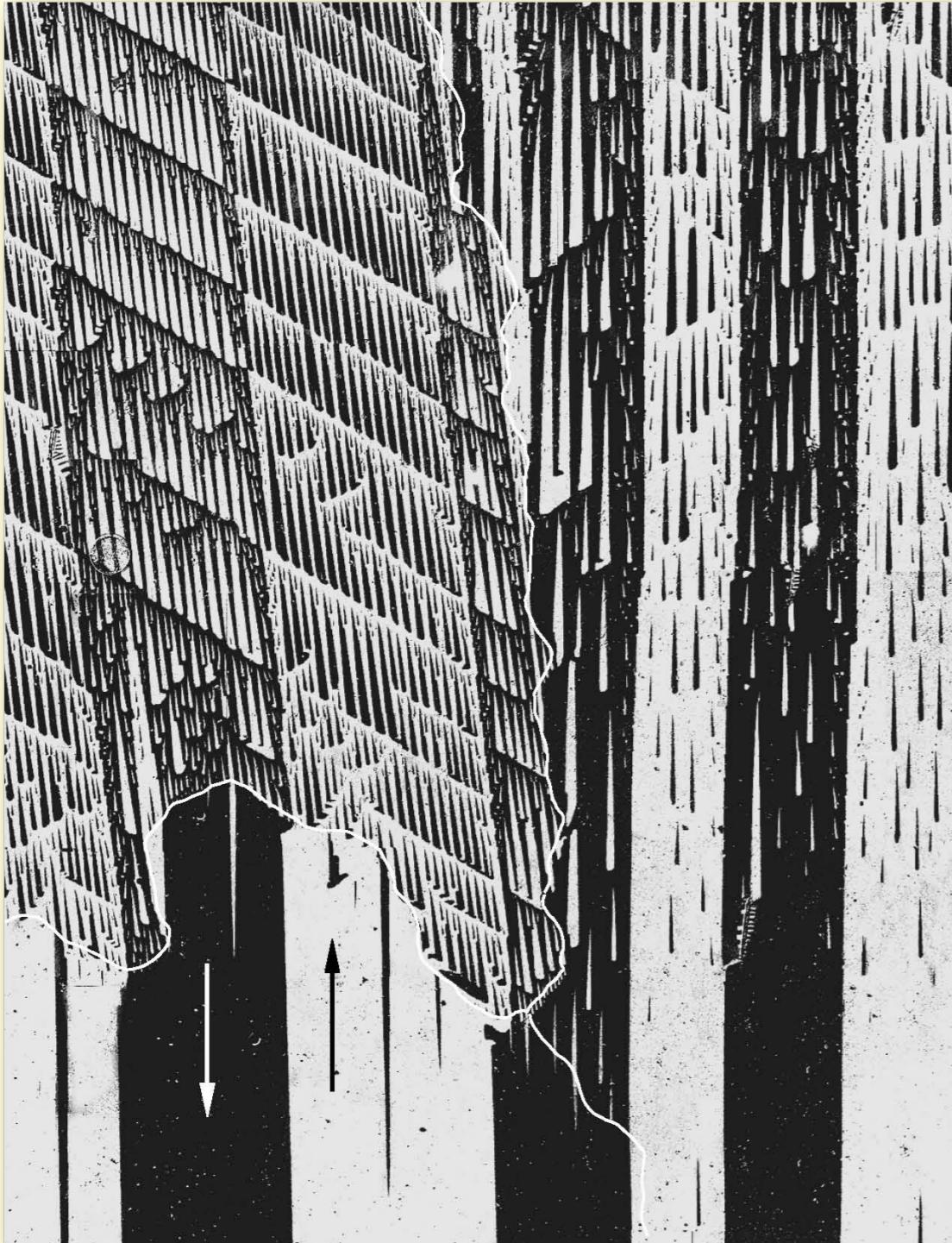
350°C

Kerr microscopy: advantages

Variable magnification

Stress effects in trafo steel

initial state



transformer steel

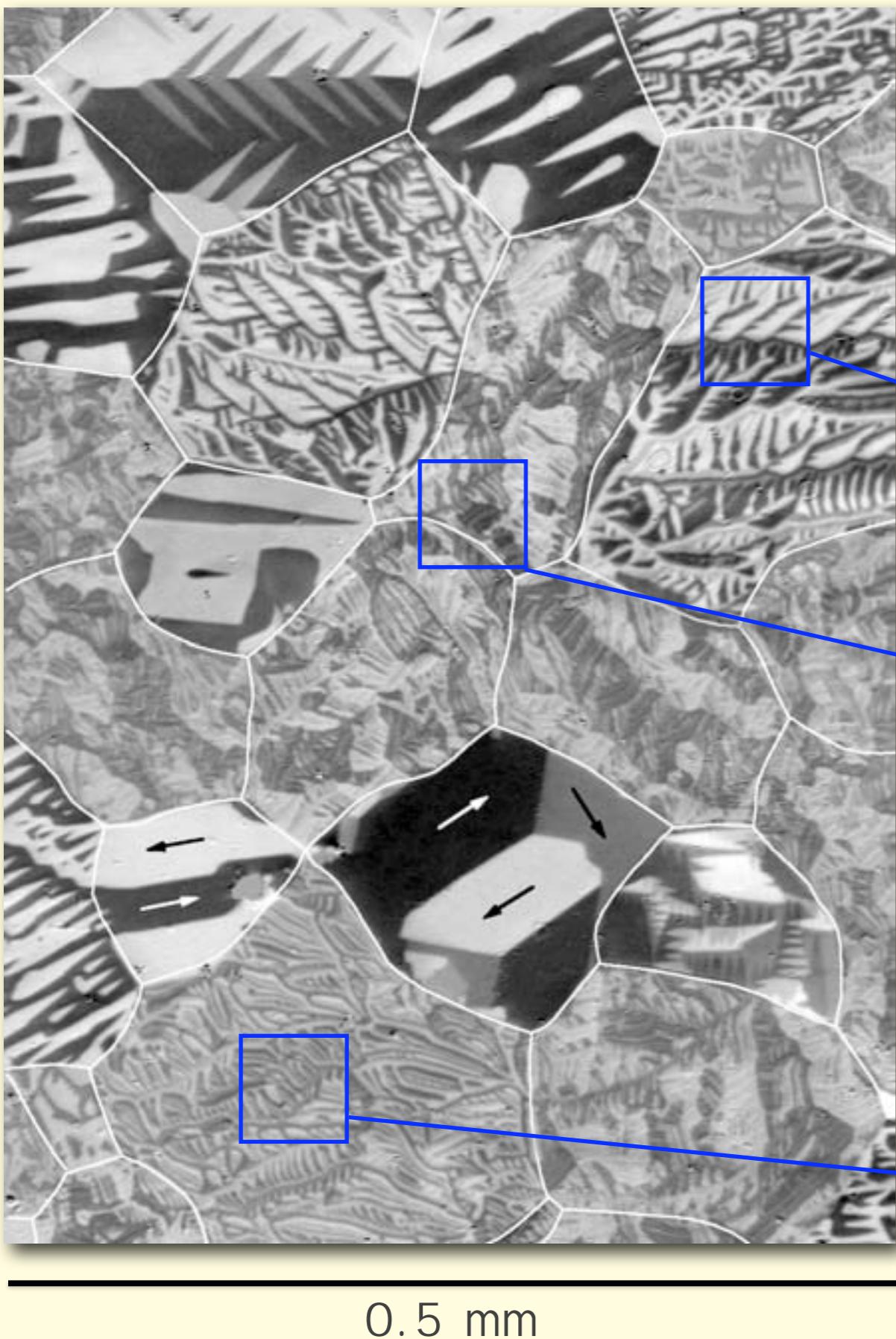
under tensile stress



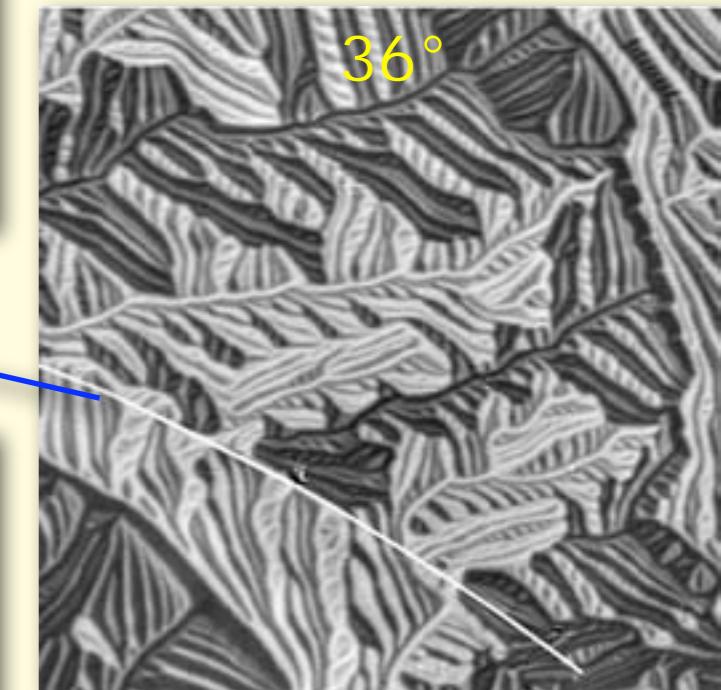
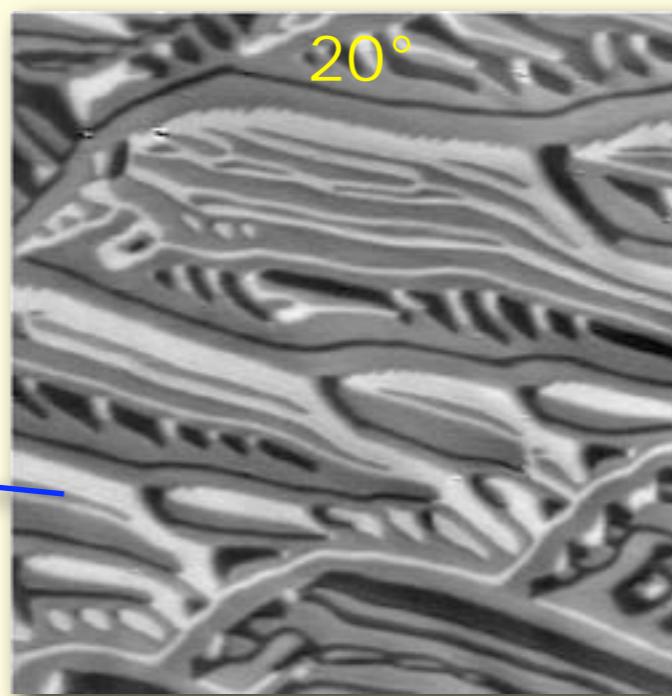
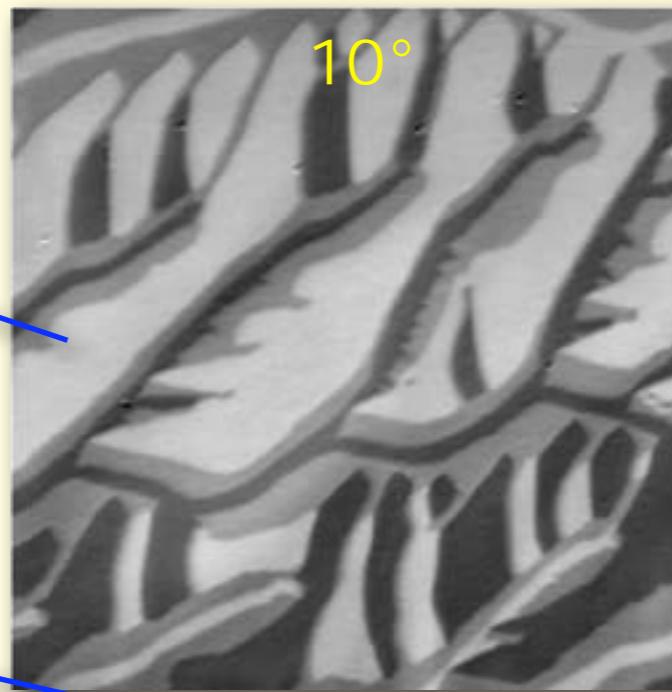
1 mm

stress

Change of magnification



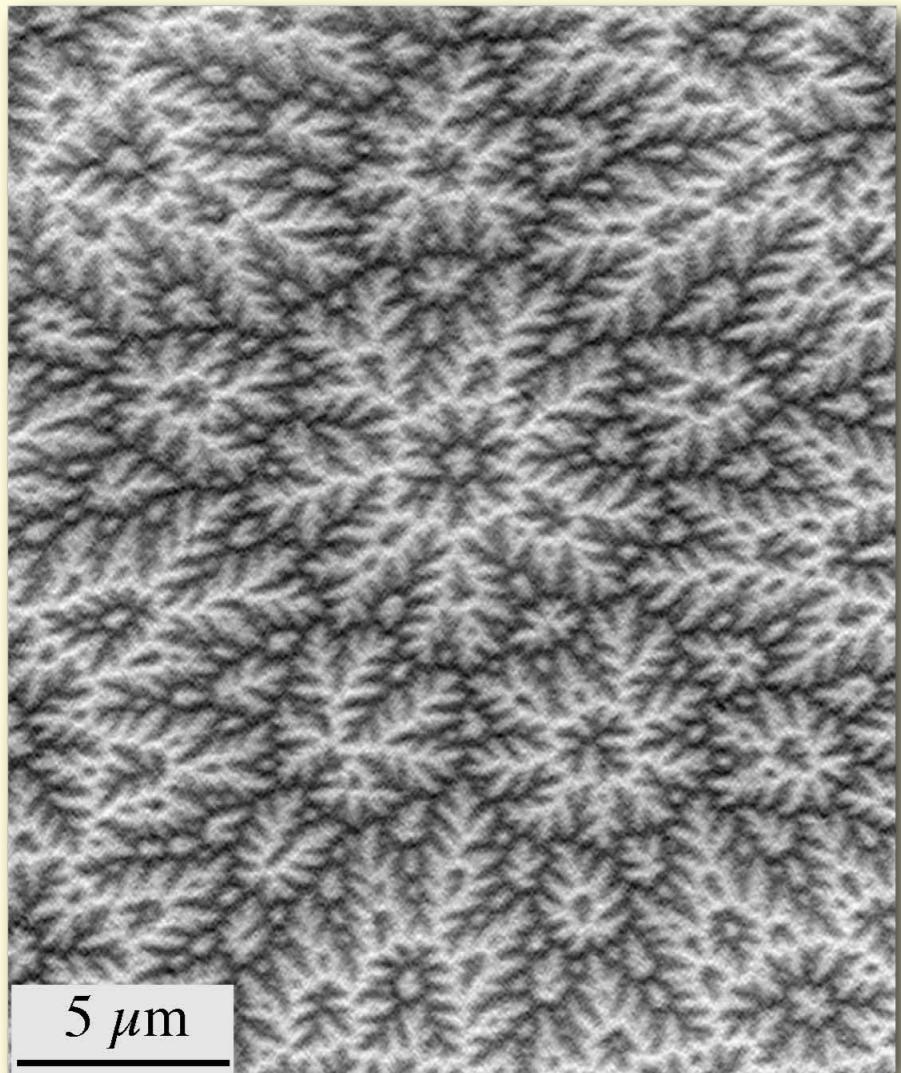
Non-oriented electrical steel
(0.5 mm thick)



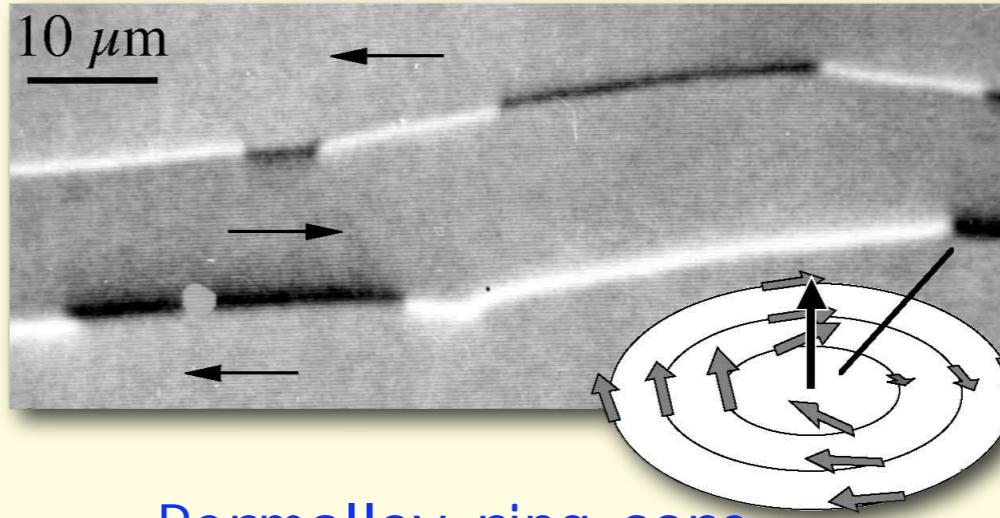
(111)-surface

High-resolution observations

Co basal plane

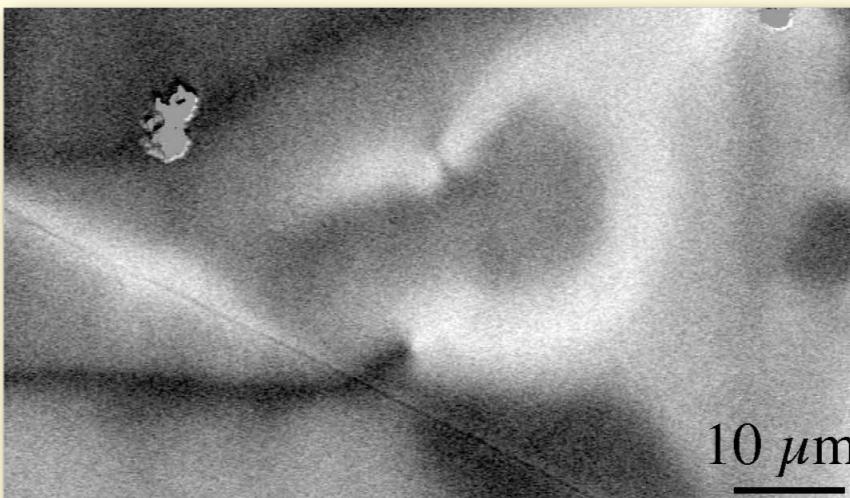


asymmetric Bloch wall (met. Glass)

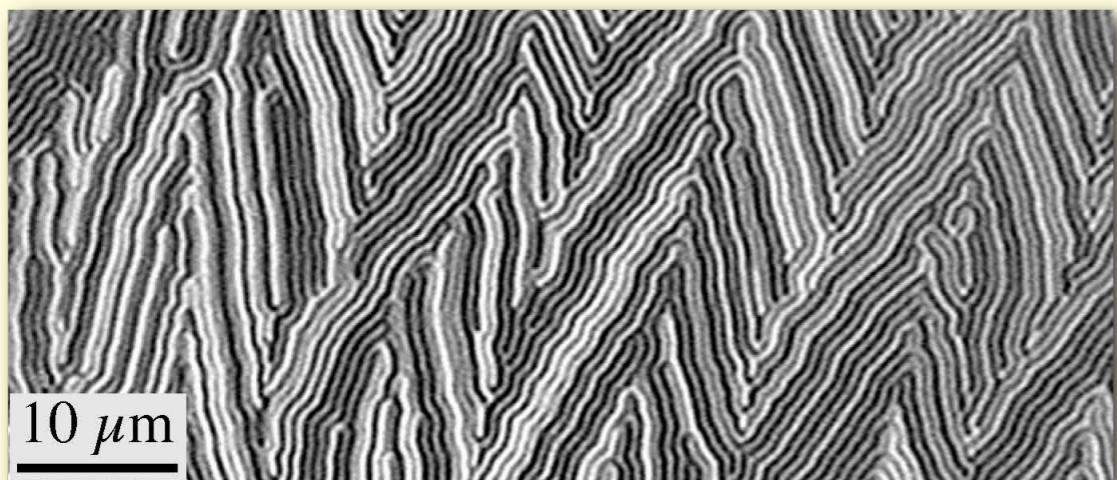


Surface swirl

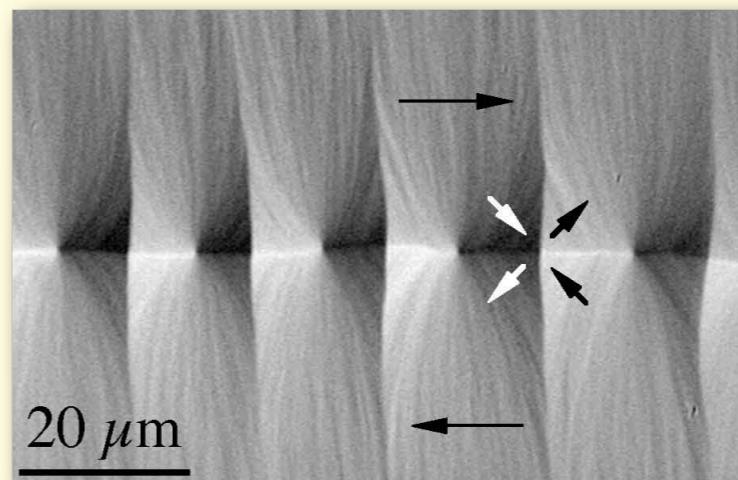
Permalloy ring core



amorphous layer (1 μm thick)



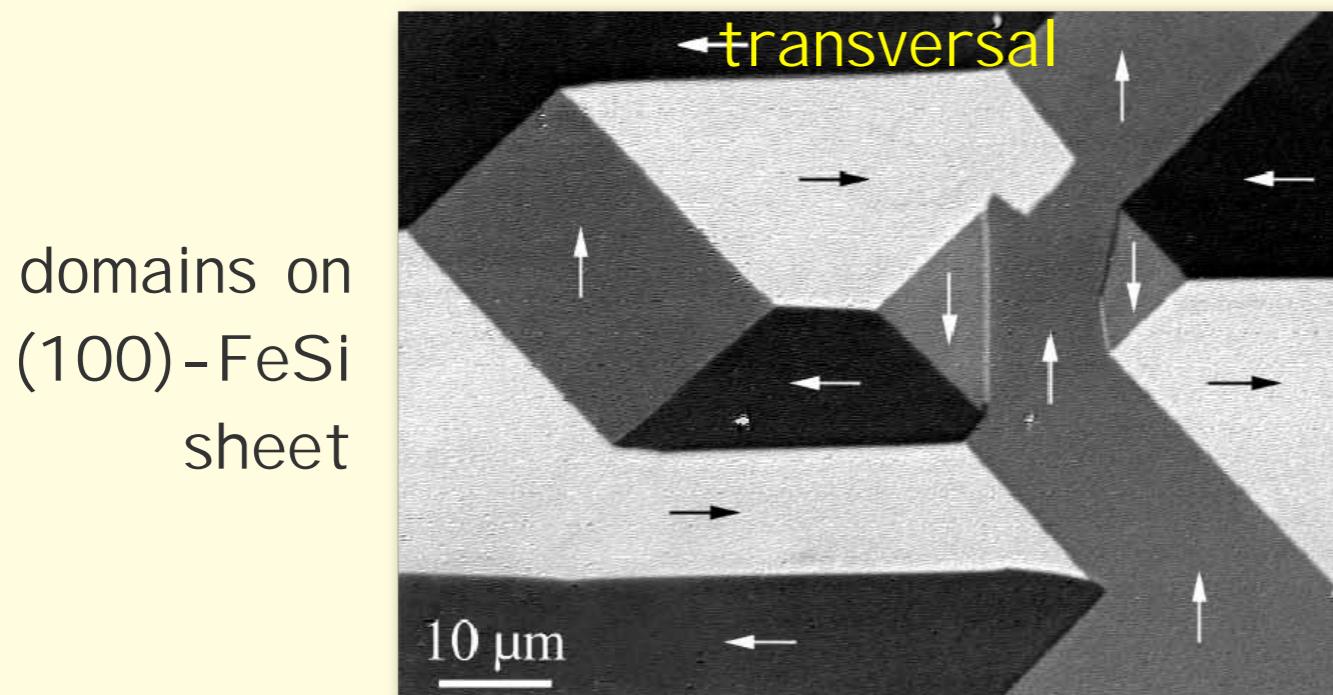
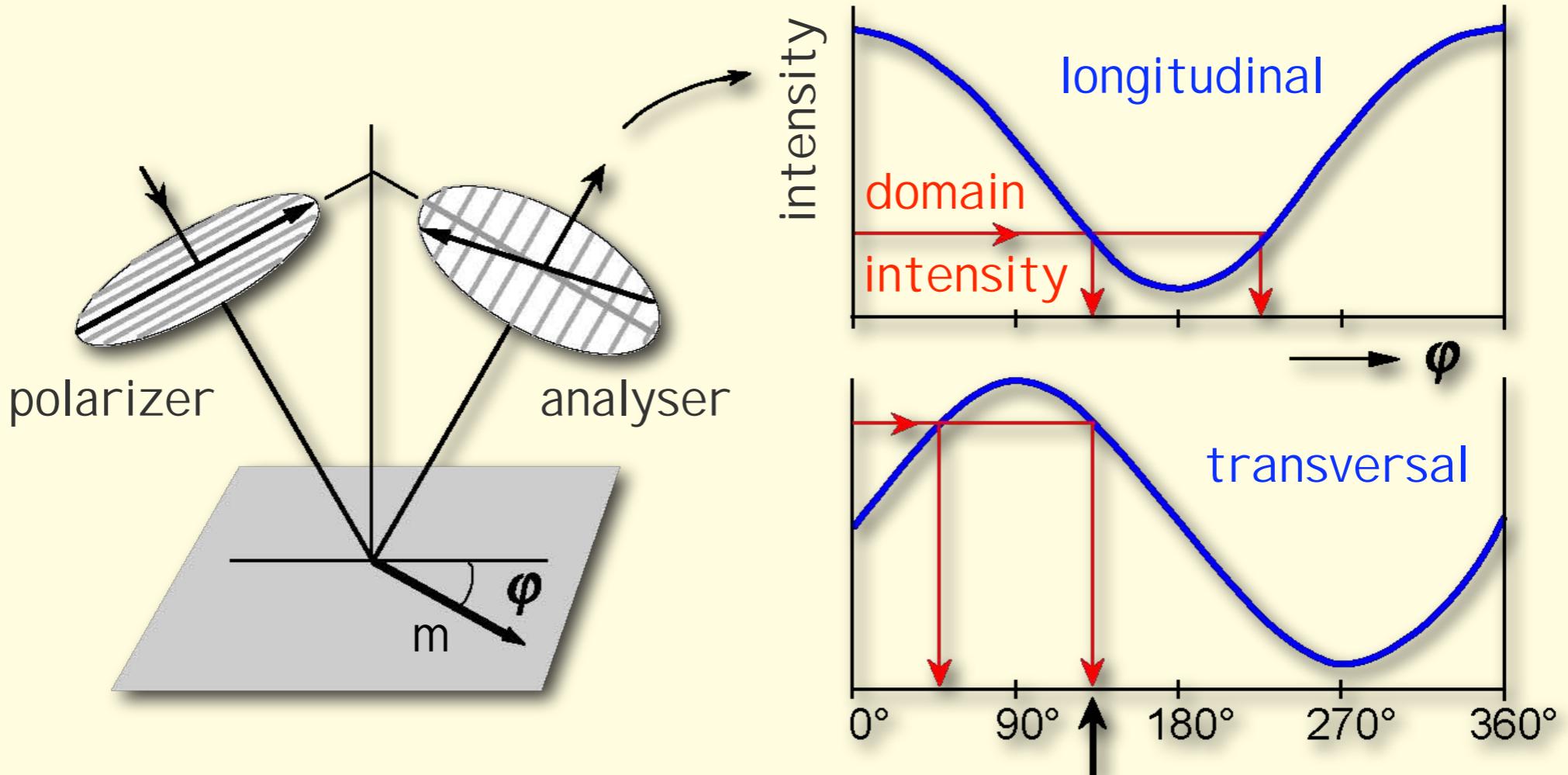
Crosstie wall (Permalloy)



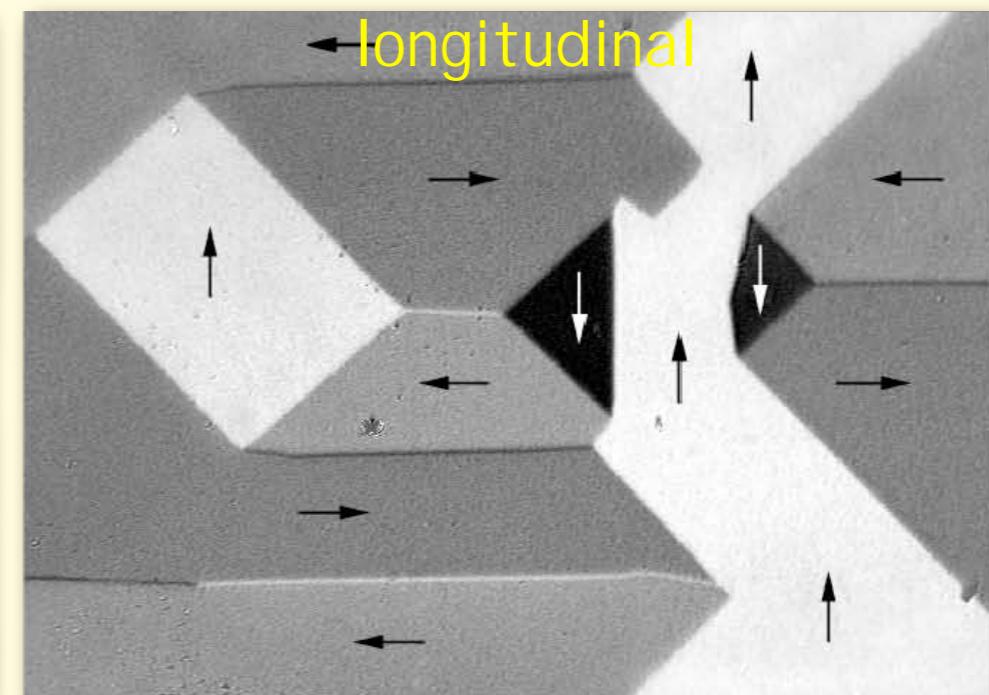
Kerr microscopy: advantages

Quantitative Kerr microscopy

Quantitative Kerr microscopy: principle



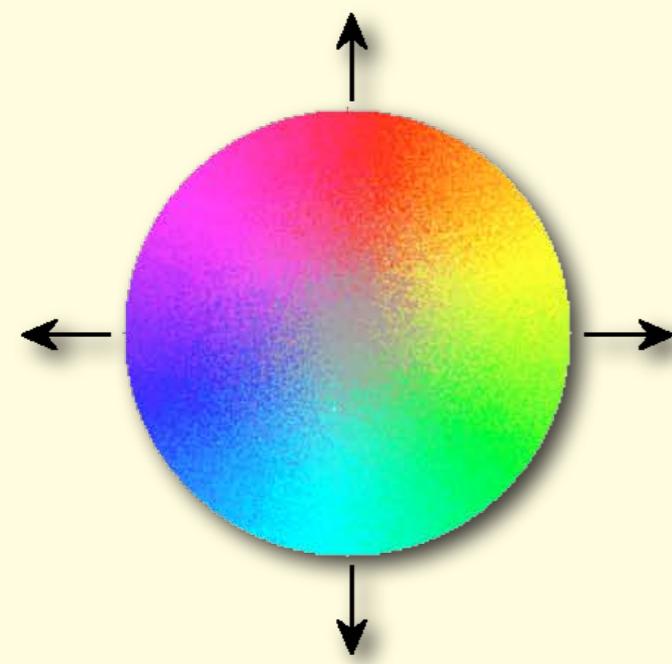
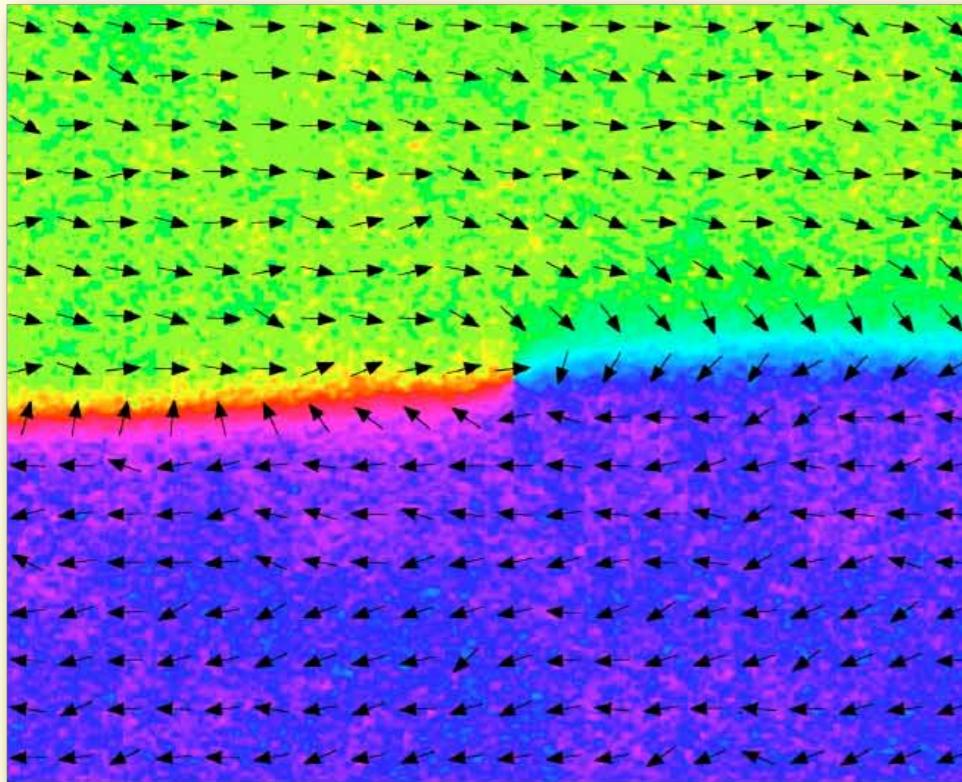
domains on
(100)-FeSi
sheet



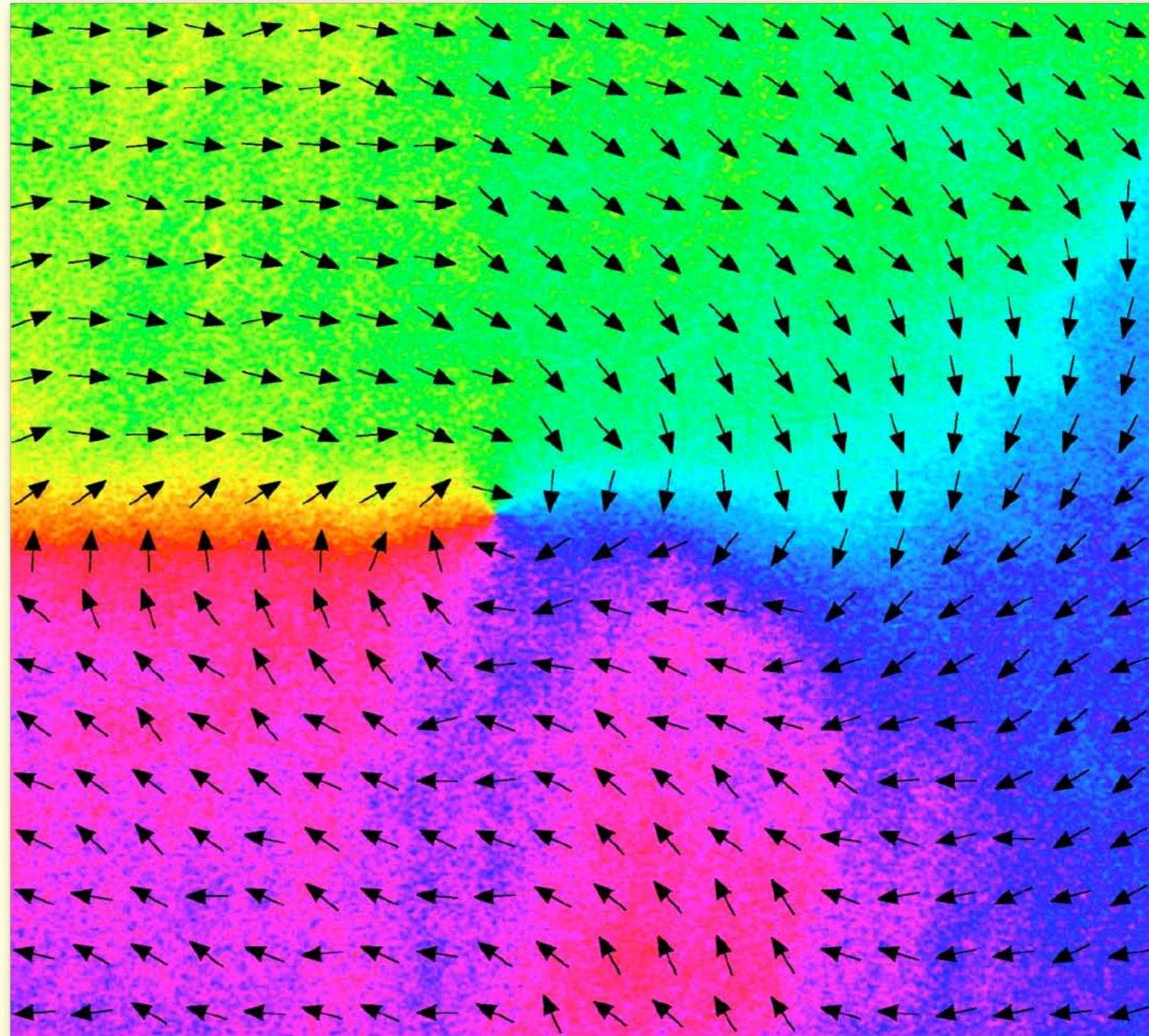
Quantitative Kerr microscopy: example

Domains in magnetostriction-free amorphous ribbon

as-quenched state



after annealing in rotating field



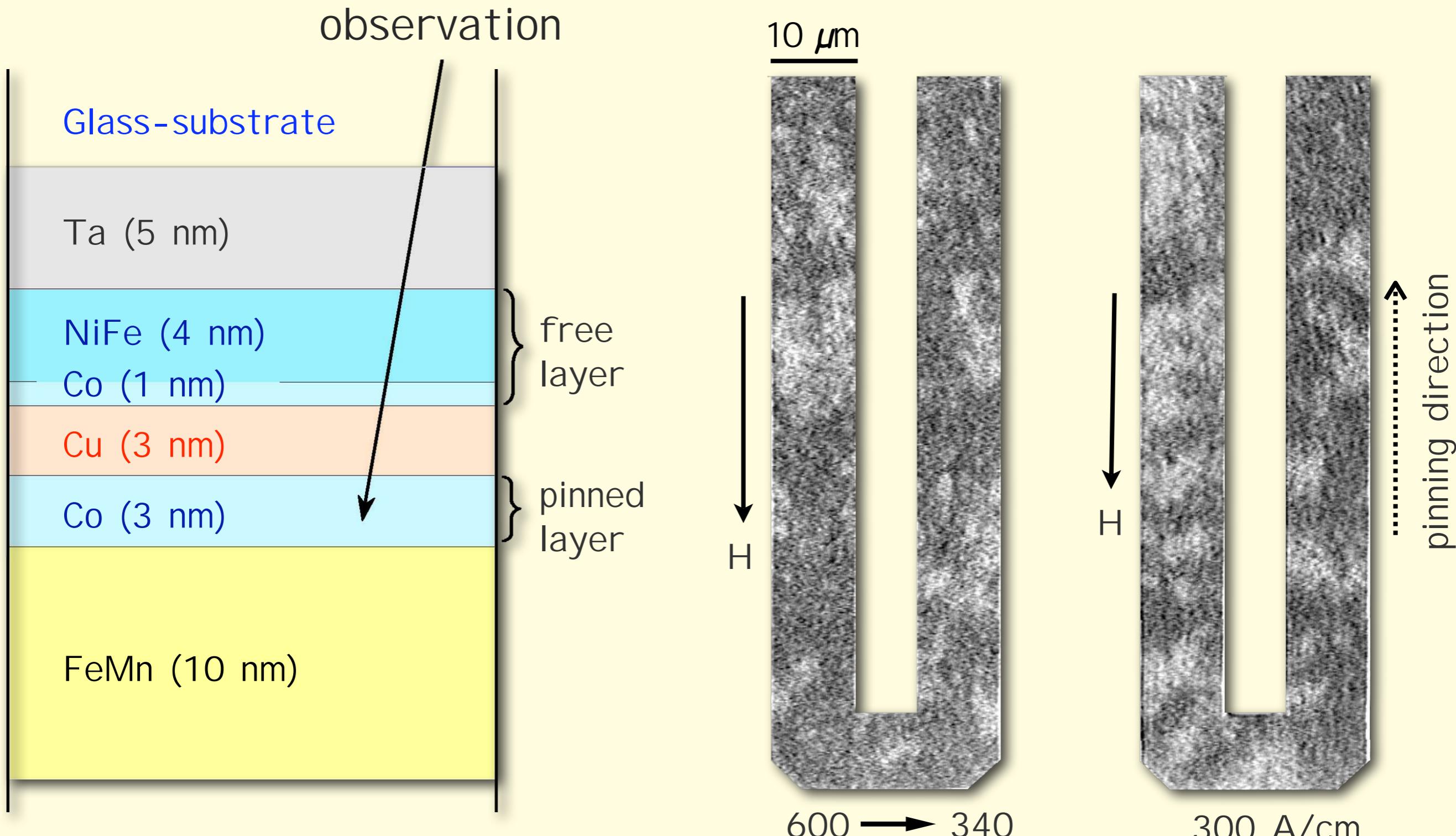
5 μm

Kerr microscopy: advantages

Depth sensitivity

Depth sensitivity of Kerr microscopy

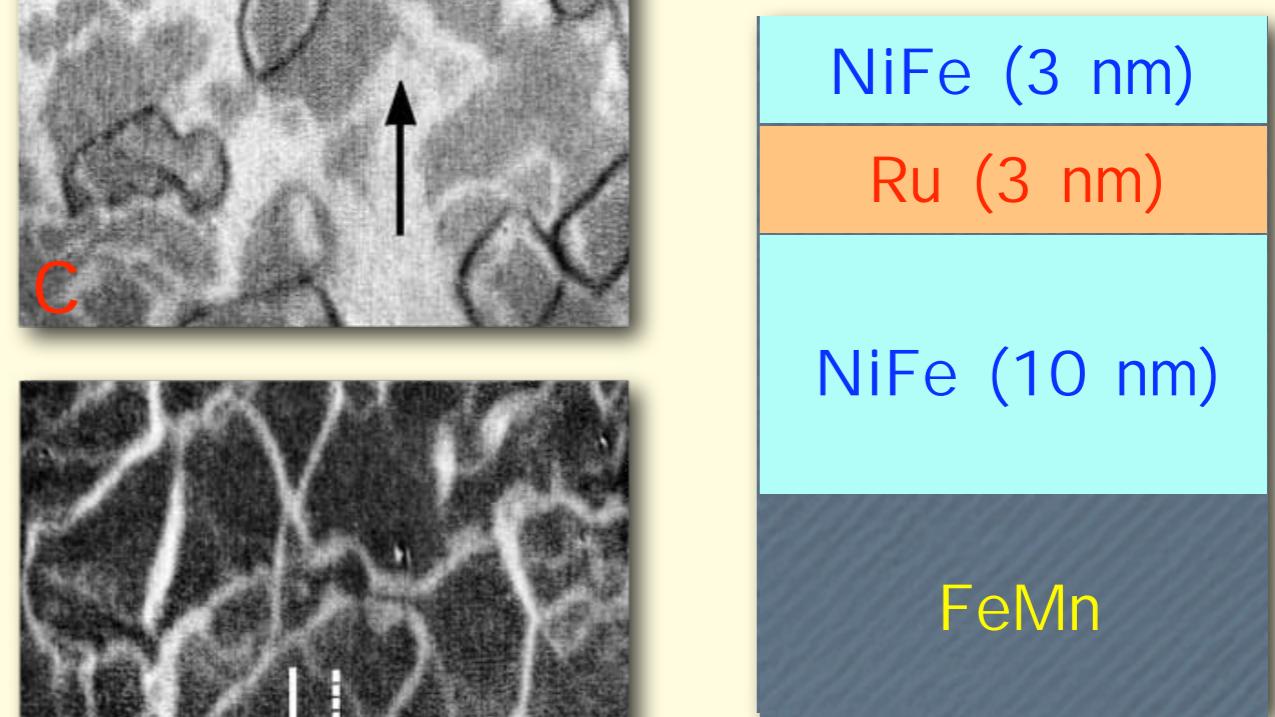
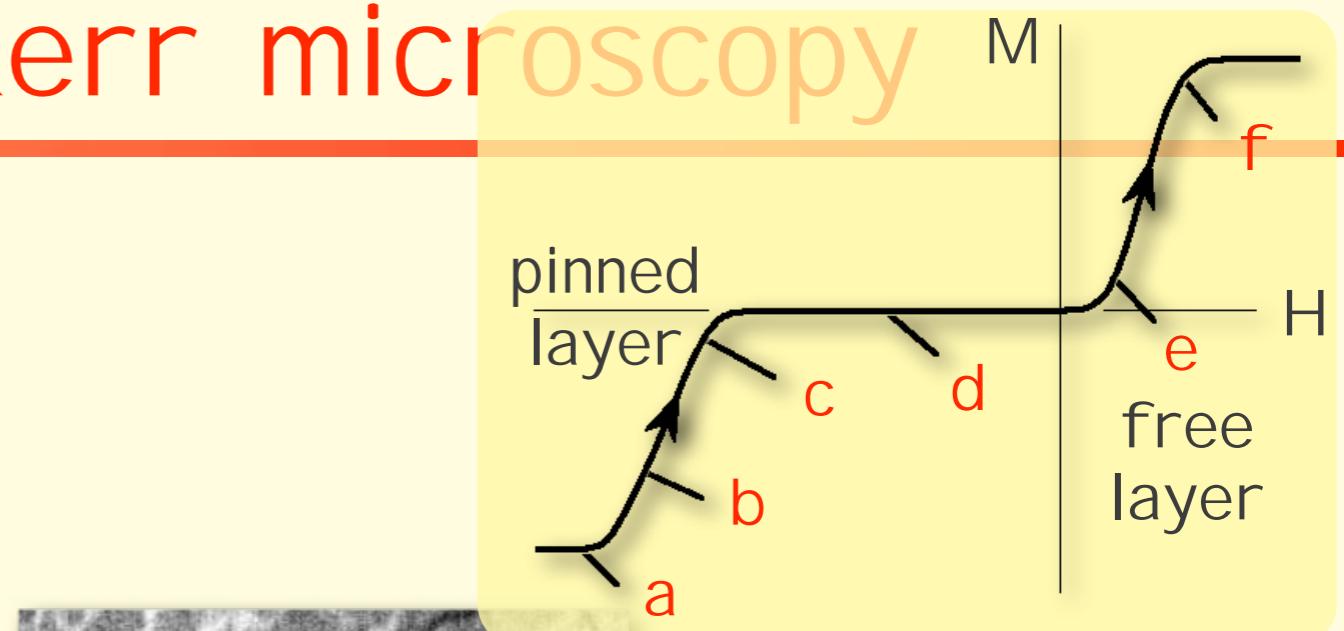
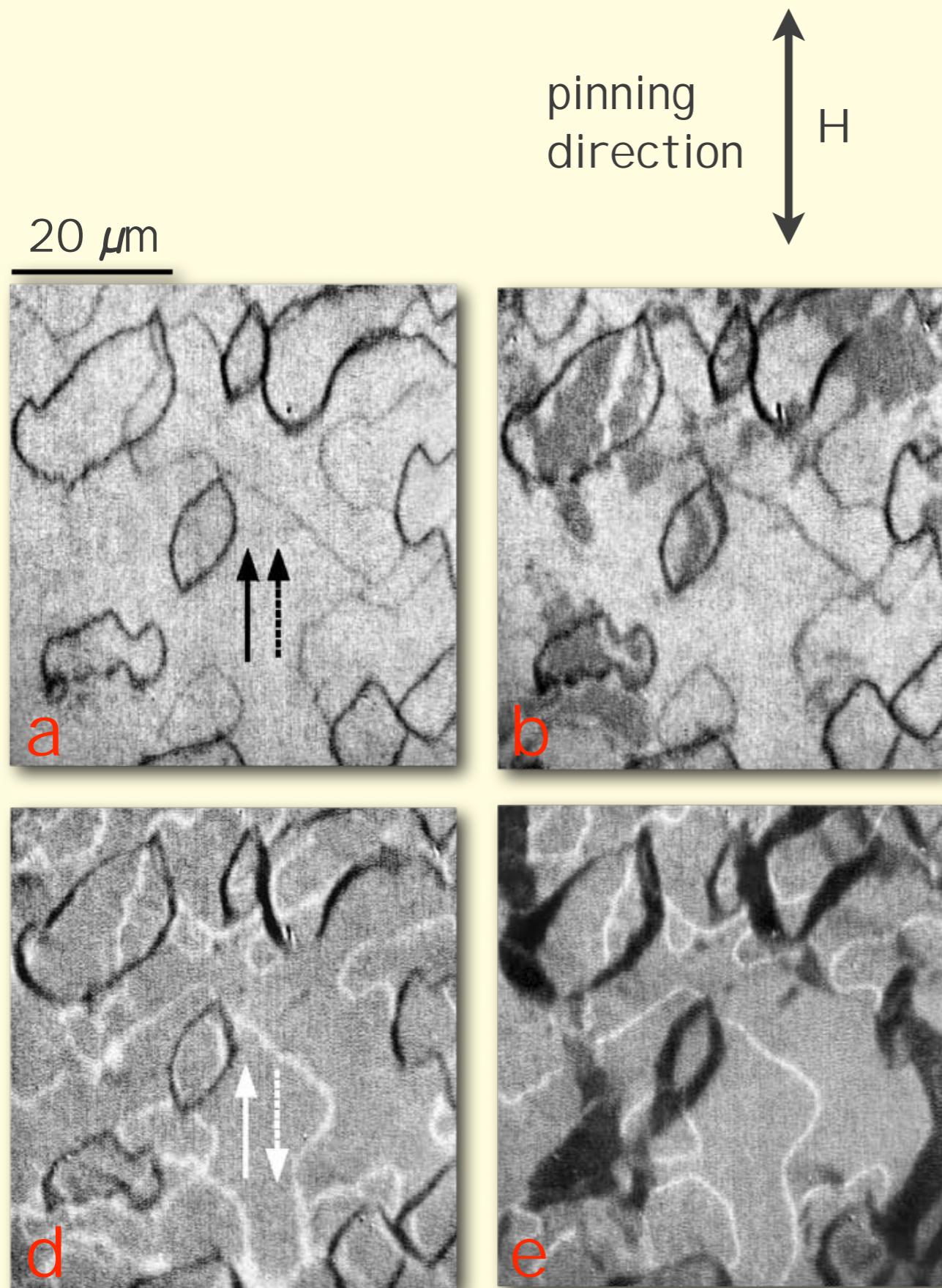
Spin-valve system



R.S., et al.,
IEEE Trans. Magn. 39, 2089 (2003)

together with
U. Barholz, R. Mattheis (IPHT Jena)

Depth sensitivity of Kerr microscopy



Sample:
S. Parkin, IBM

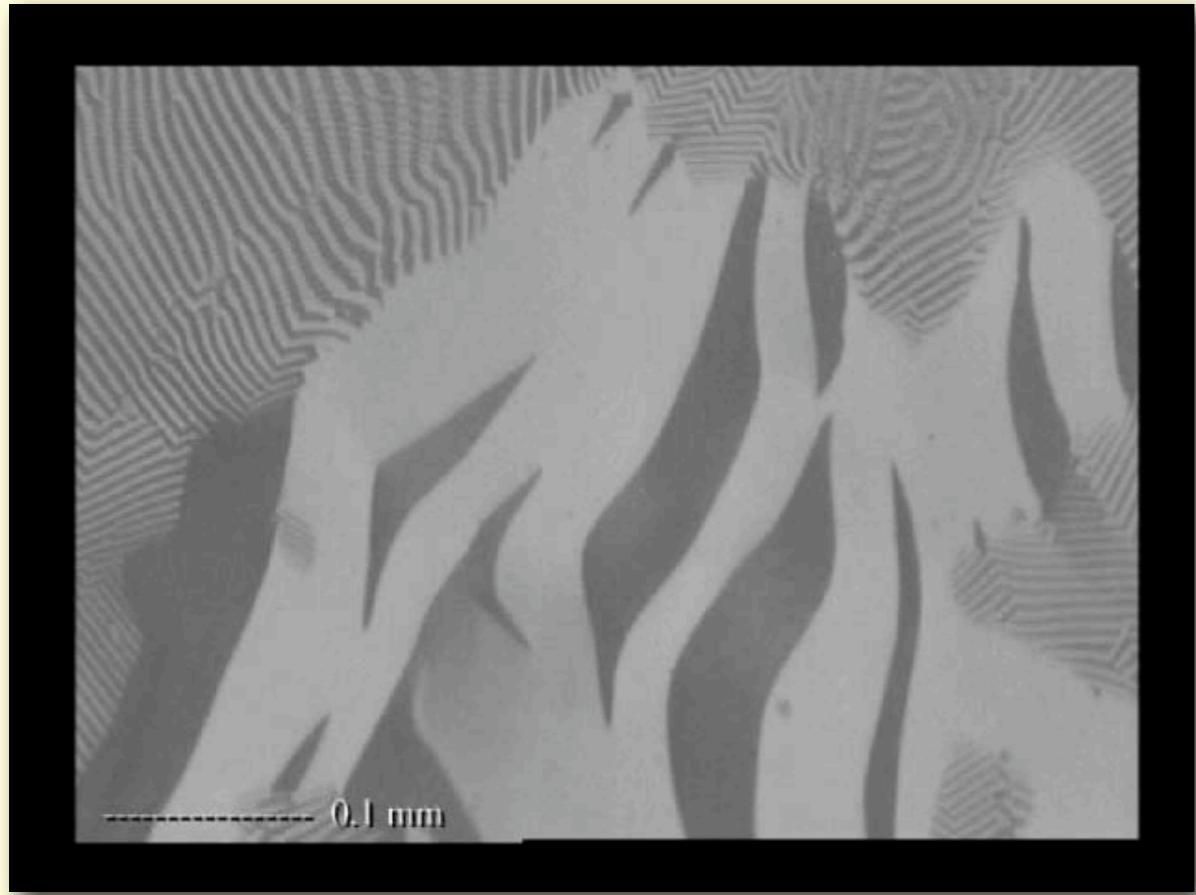
Kerr microscopy: advantages

Dynamic and time-resolved
Kerr microscopy

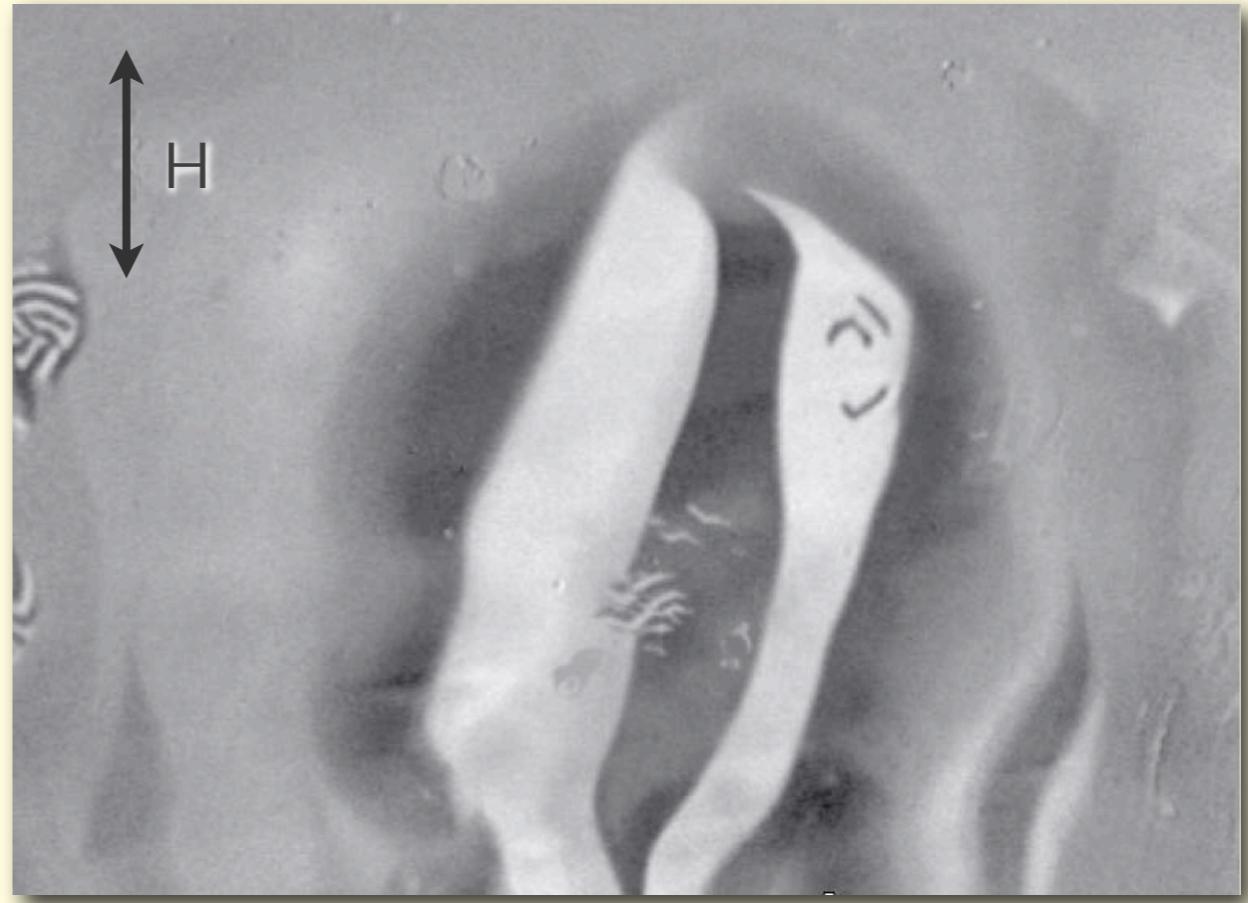
Dynamic observations

FeSiB amorphous ribbon,
as-quenched

0.2 mm



Slow dynamics

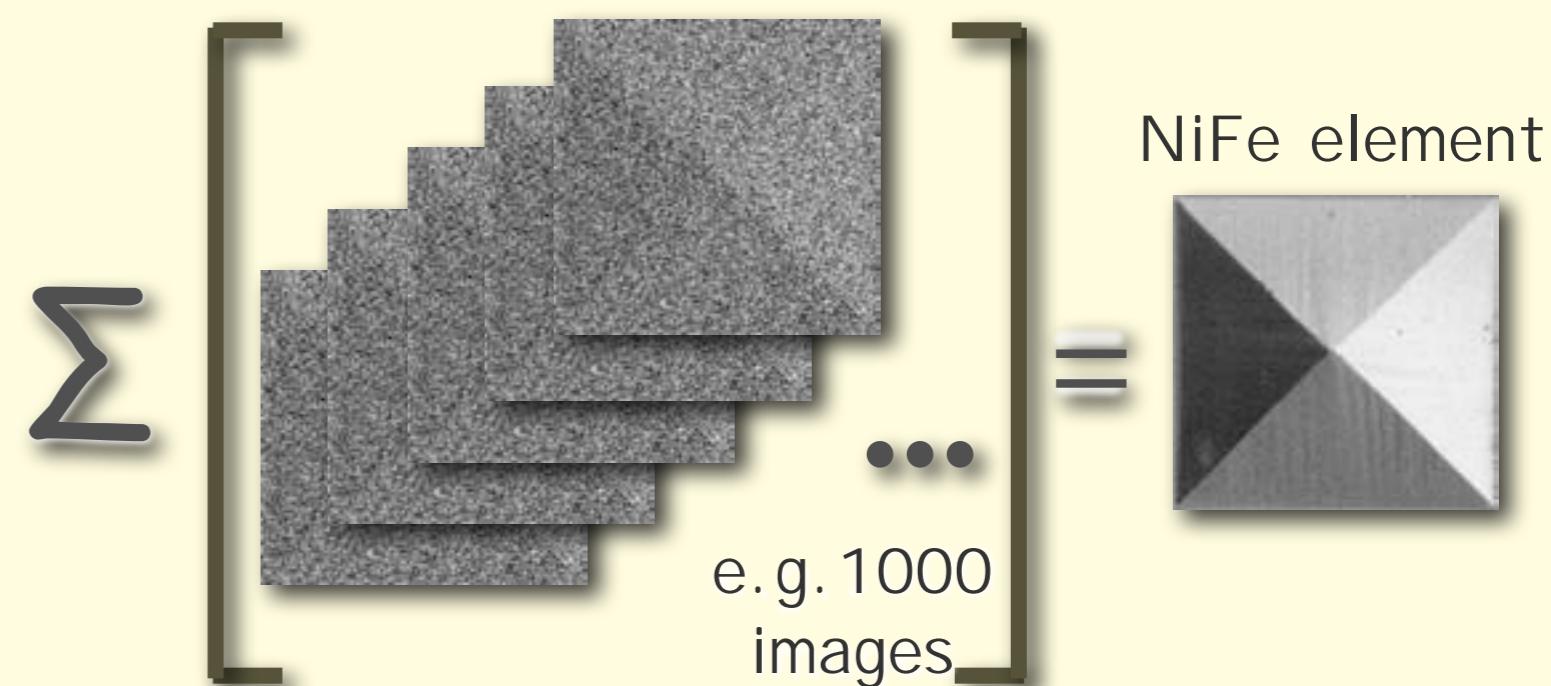


25 Hz sinusoidal field

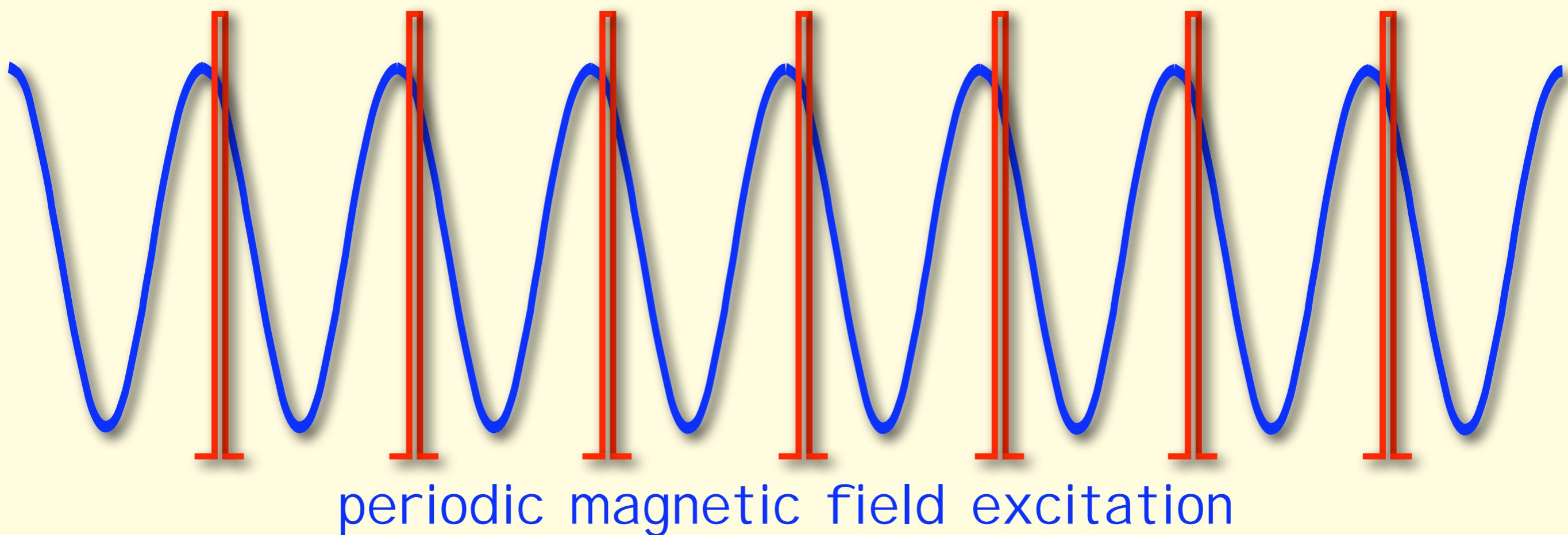
Time-resolved imaging: Stroboscopic mode

illumination intensity and repetition rate are limited

- no single-shot imaging possible
- accumulation of large number of independent events necessary (at fixed time delay)
- requires repetitive magnetization processes !!



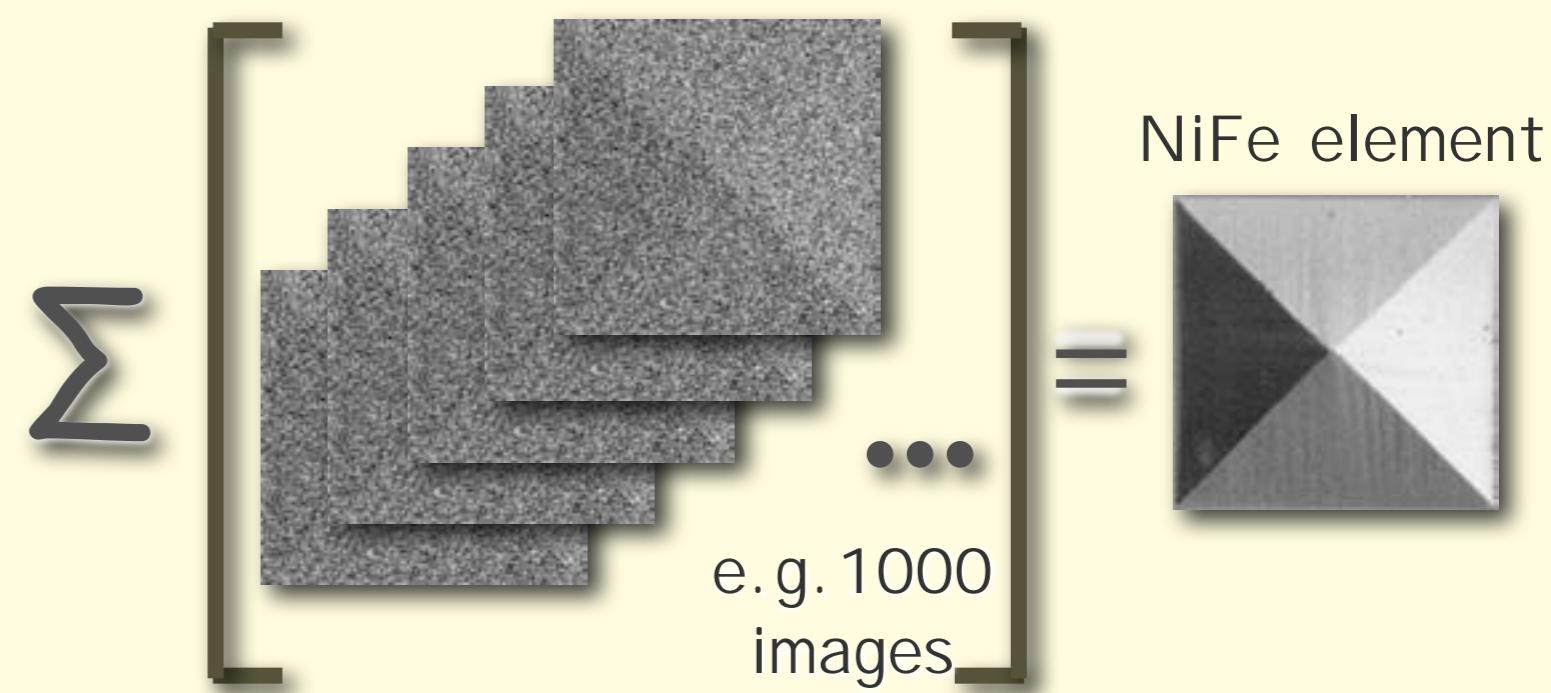
probing with defined time delay



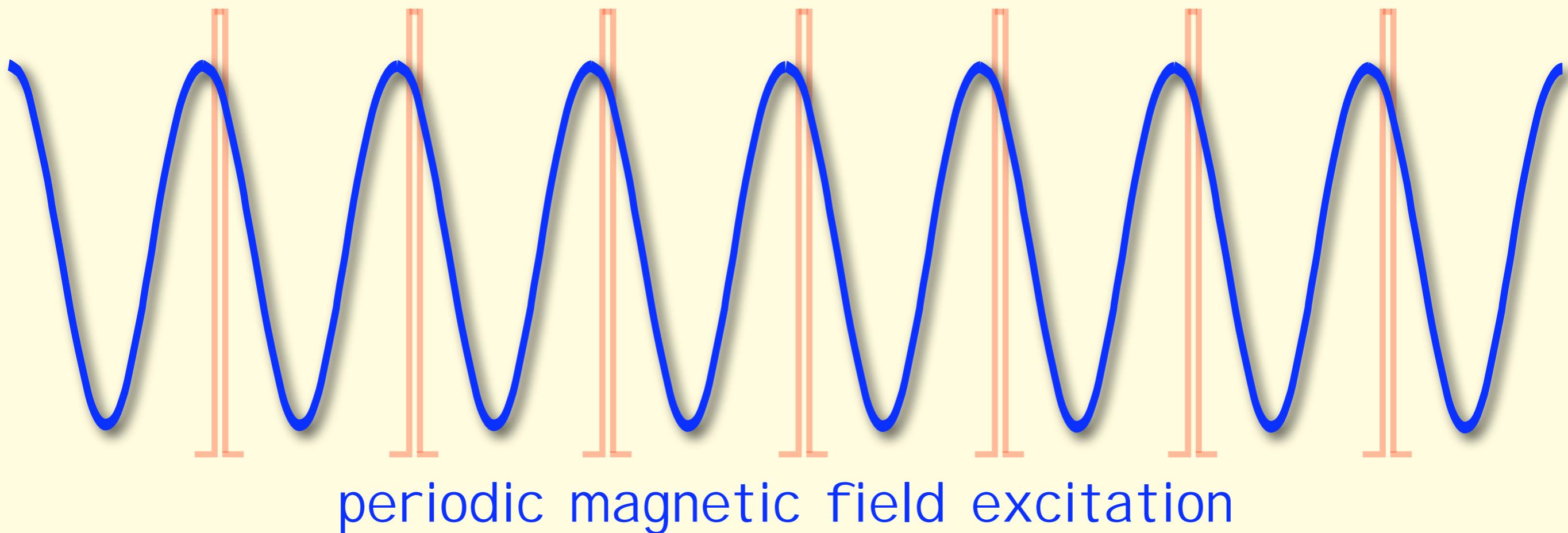
Time-resolved imaging: Stroboscopic mode

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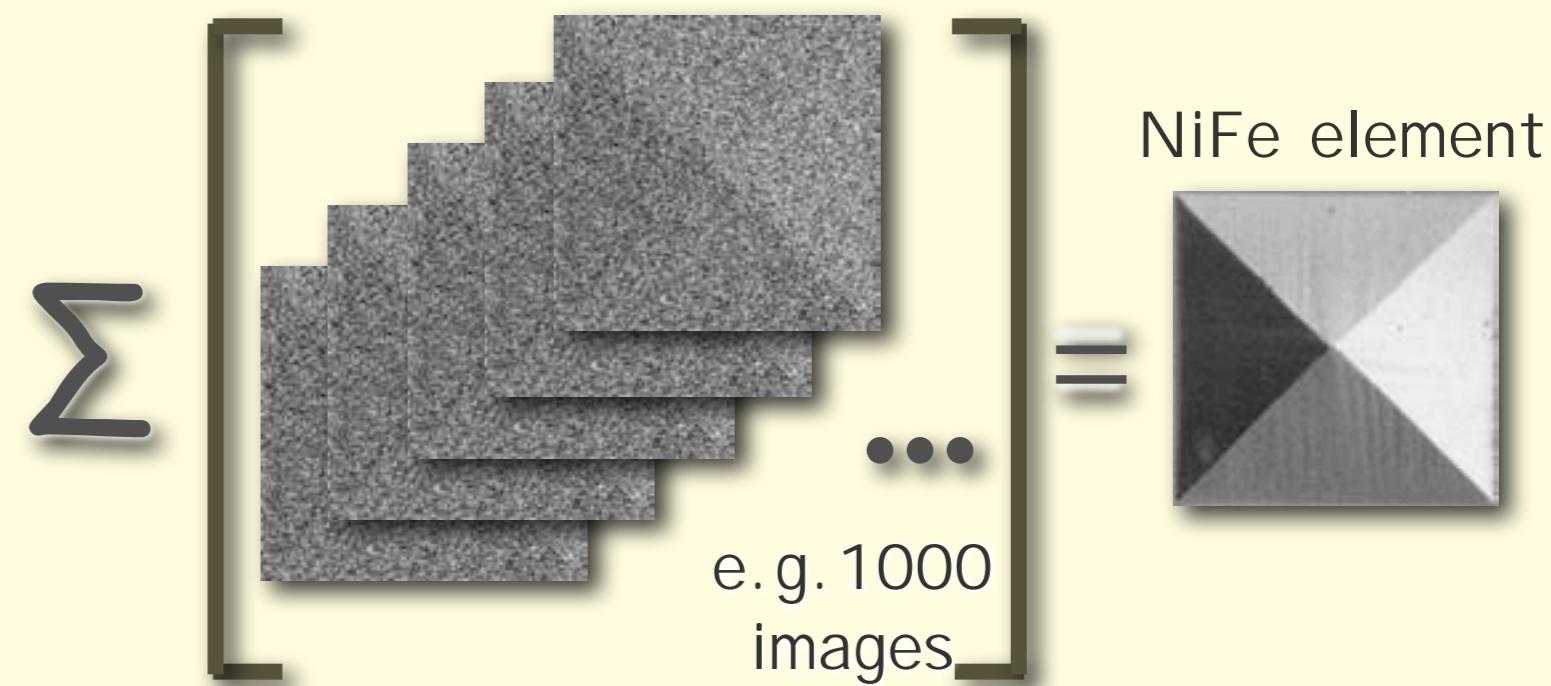
probing with defined time delay



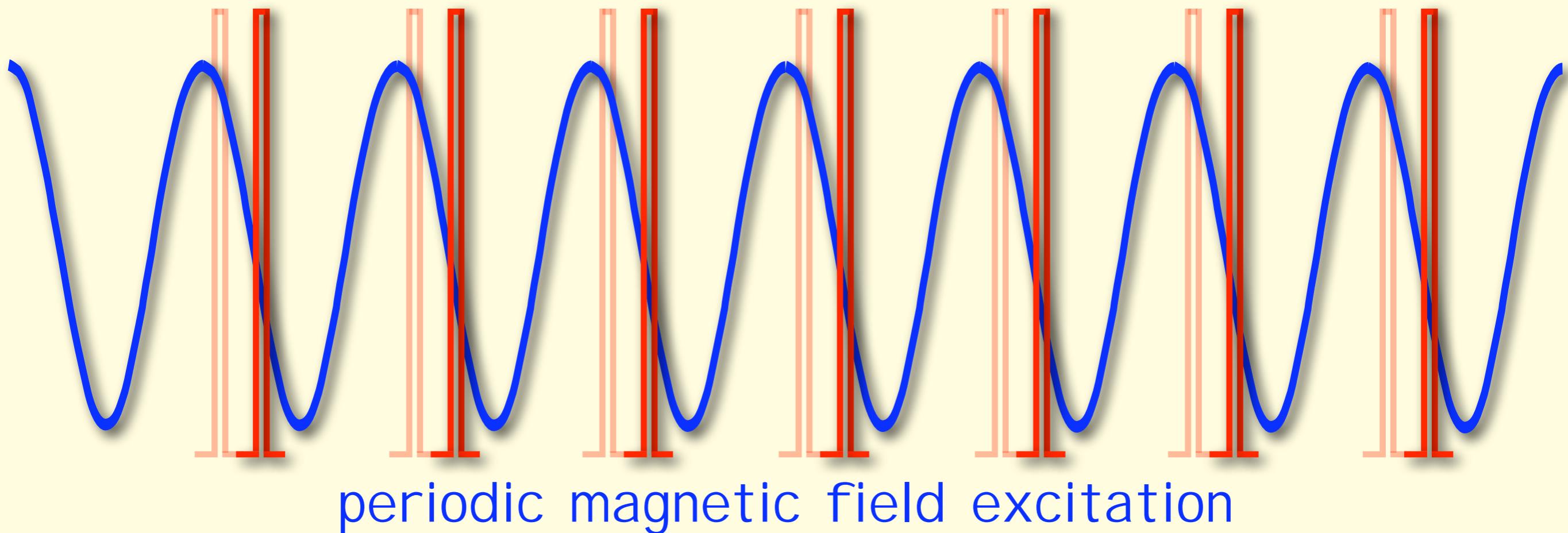
Time-resolved imaging: Stroboscopic mode

illumination intensity and repetition rate are limited

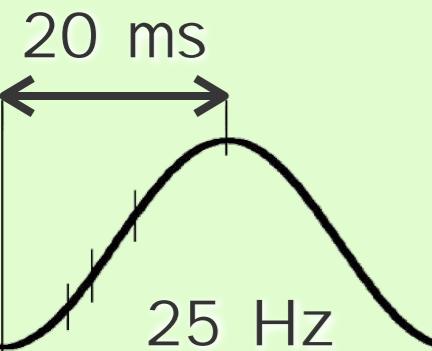
- no single-shot imaging possible
- accumulation of large number of independent events necessary (at fixed time delay)
- requires repetitive magnetization processes !!



probing with defined time delay



Low-frequency dynamics in amorphous ribbon



Stroboscopic
images

$\Delta t = 0.4 \text{ ms}$
800 images

Fe₇₈Si₉B₁₃ amorphous ribbon, 20 μm thick

6 ms



8 ms



12 ms



slowly
changing
field
(< Hz)

H



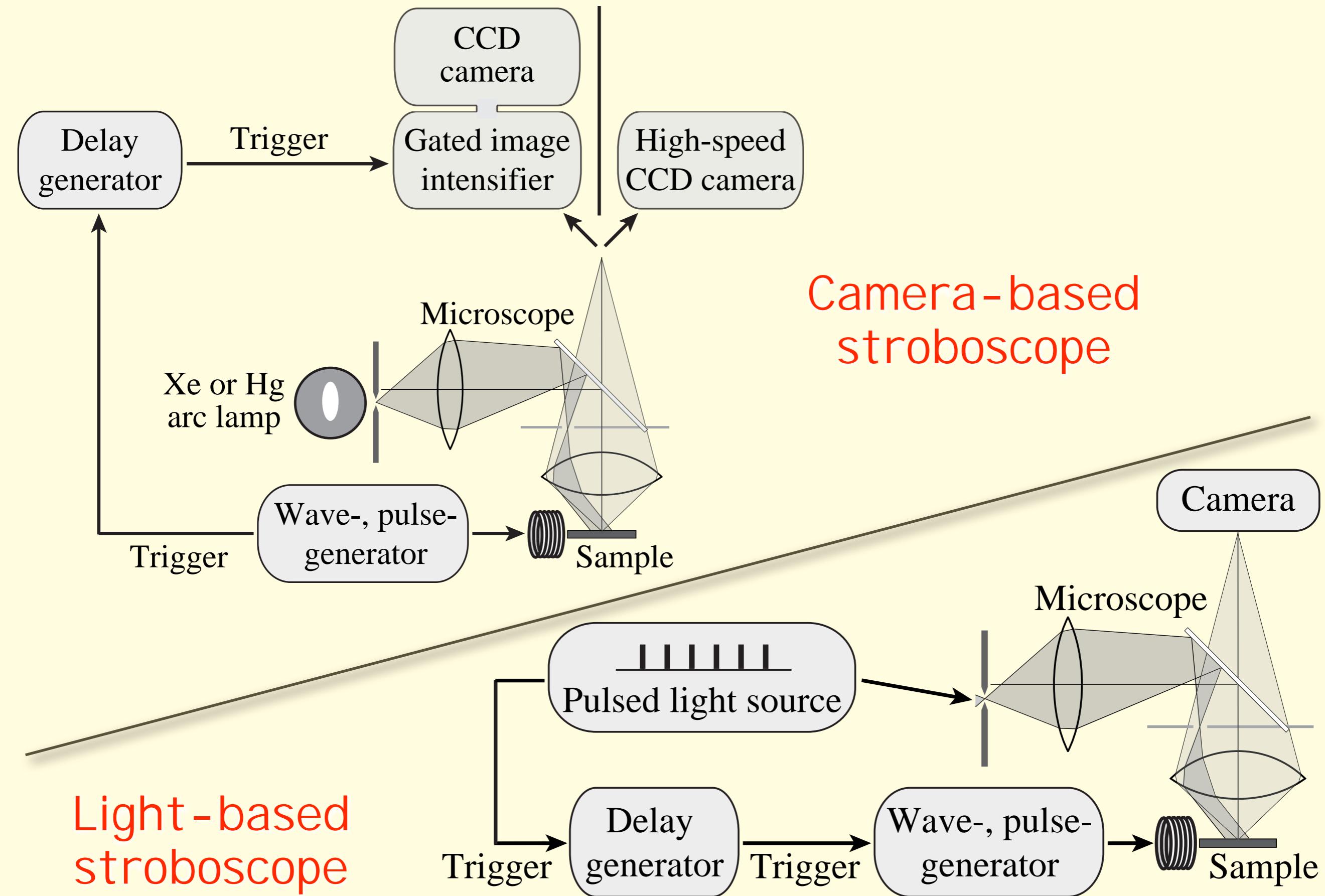
decreasing field



remanence

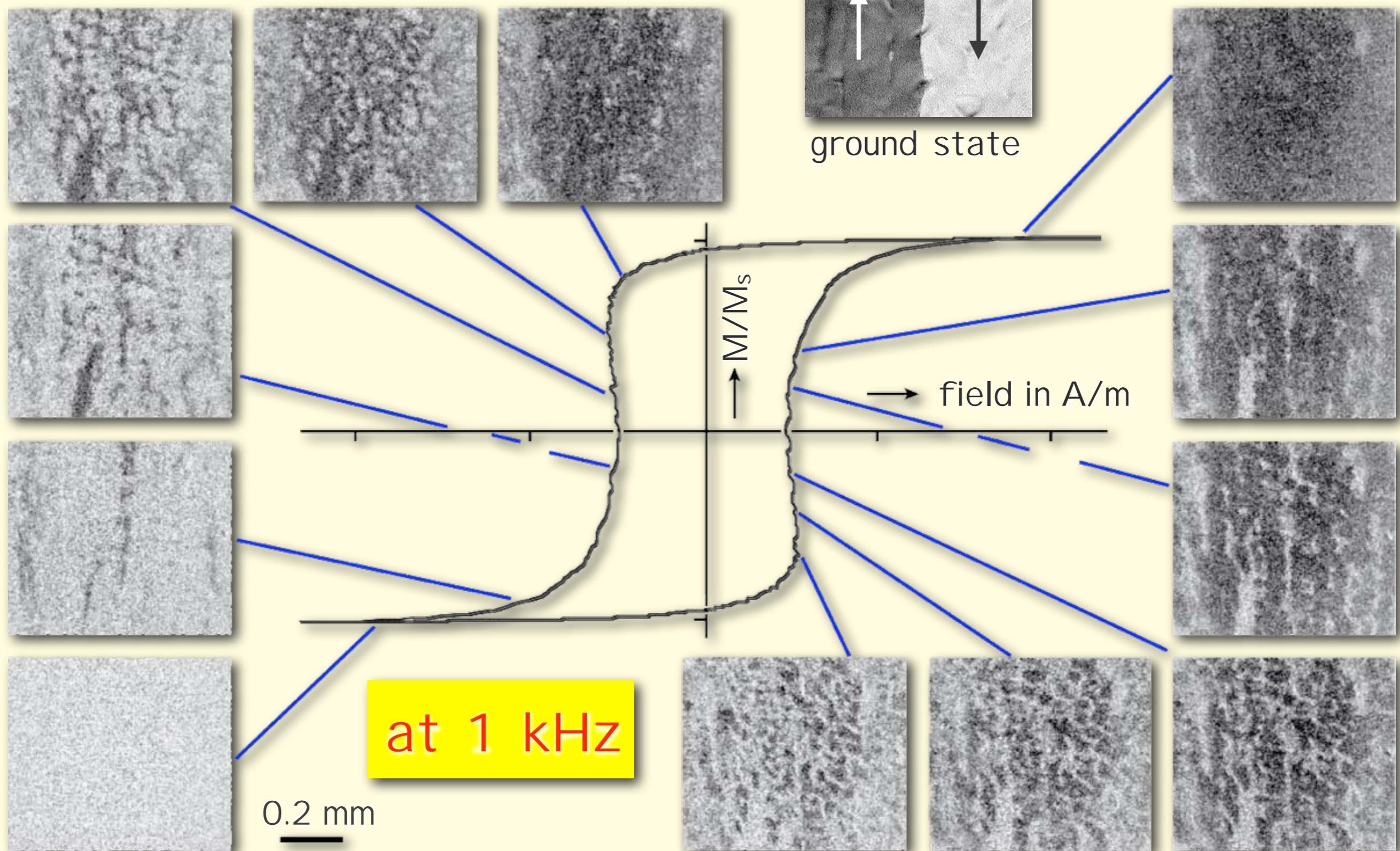
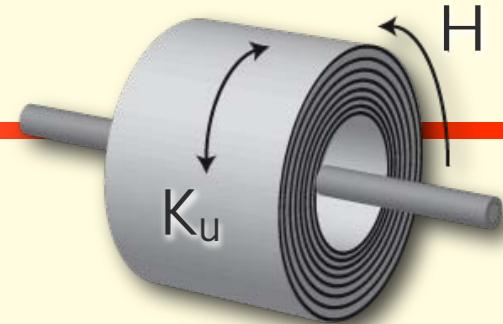
0.2 mm

Stroboscopic wide-field microscopes



Nanocrystalline core with weak K_u

S. Flohrer et al., Acta Mat. (2006)



Summary: limitations of dynamics

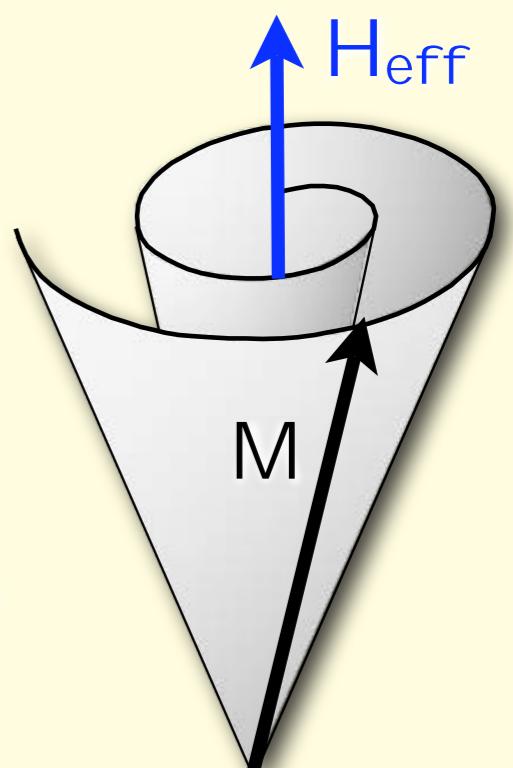
Bulk metallic ferromagnets:
eddy current effects dominate

Thick metallic films ($1 \mu\text{m}$):
eddy currents dominate

Thin metallic films ($<100 \text{ nm}$)
or non-conducting materials
eddy currents negligible



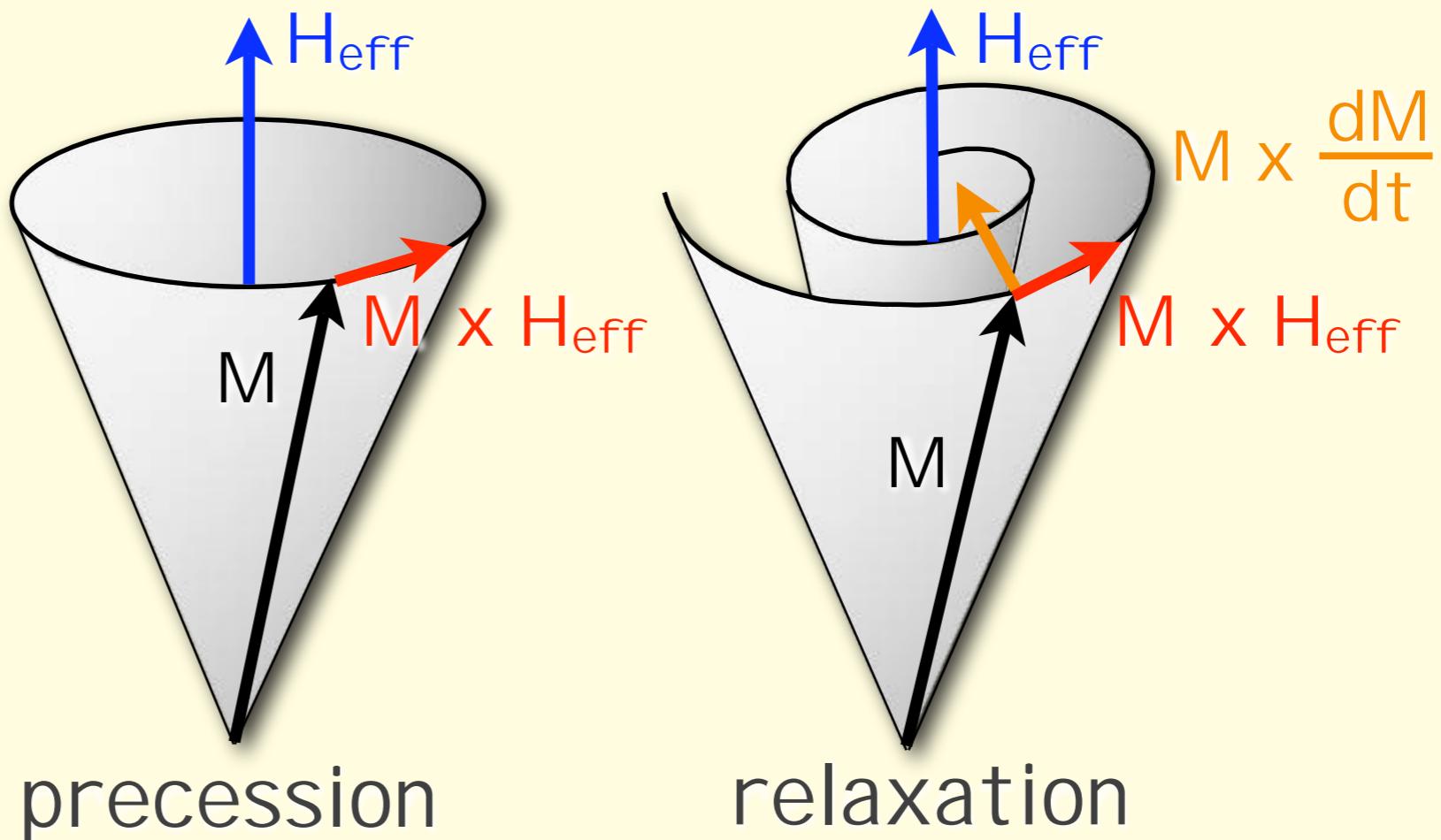
spin precession
(for frequency in GHz regime)



Landau-Lifshitz-Gilbert dynamics

$$\frac{dM}{dt} = -\gamma_0 [M \times H_{\text{eff}}] + \frac{\alpha}{M_s} [M \times \frac{dM}{dt}]$$

magnetic moment
↓
angular momentum
↓
gyrotropic reaction



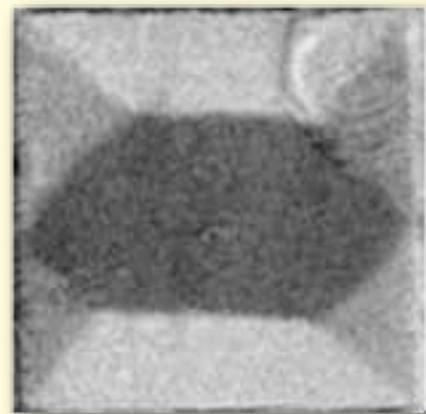
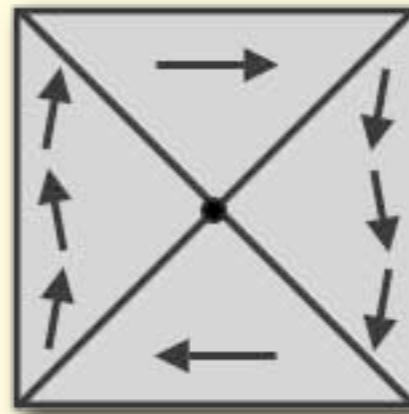
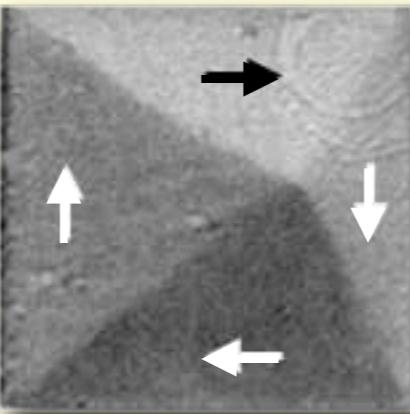
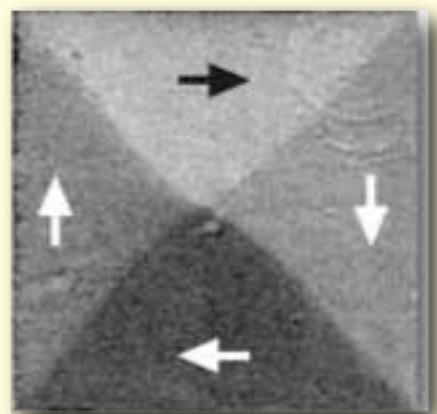
H_{eff} : acting magnetic field (embedding pulse field)

α : damping parameter

γ_0 : gyromagnetic ratio

Permalloy element ($40 \times 40 \mu\text{m}^2$, 50 nm thick)

static



↔
anisotropy

dynamic

0 ns



0.28 ns



0.38 ns



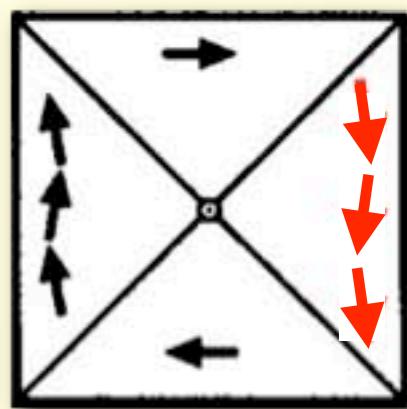
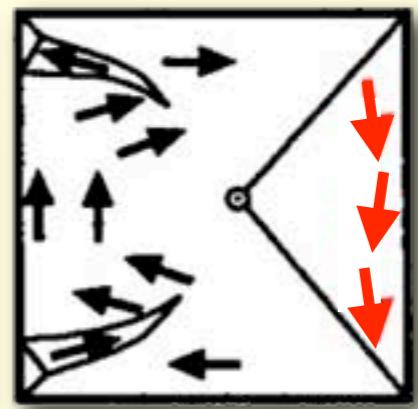
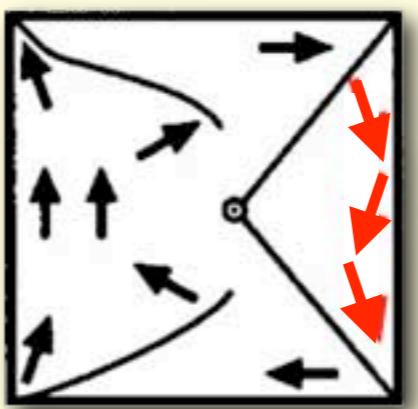
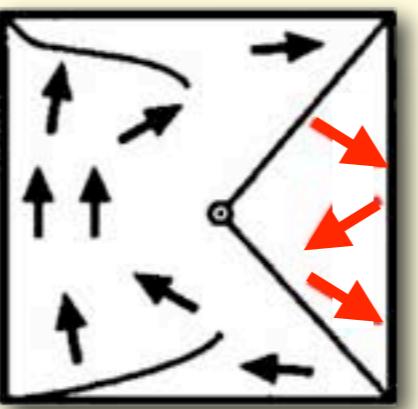
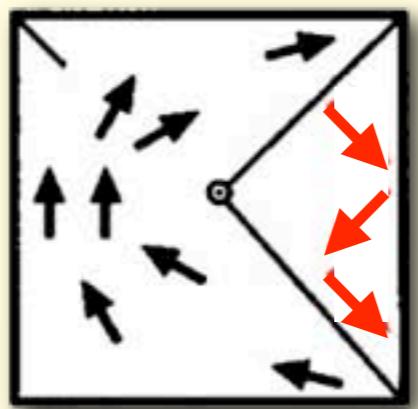
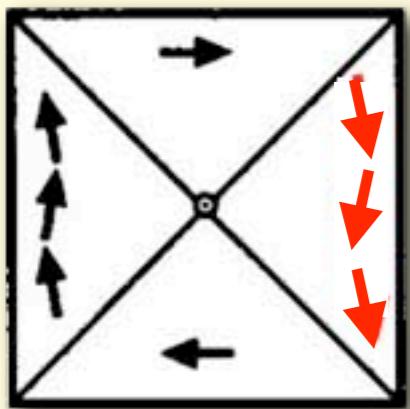
0.64 ns



0.93 ns

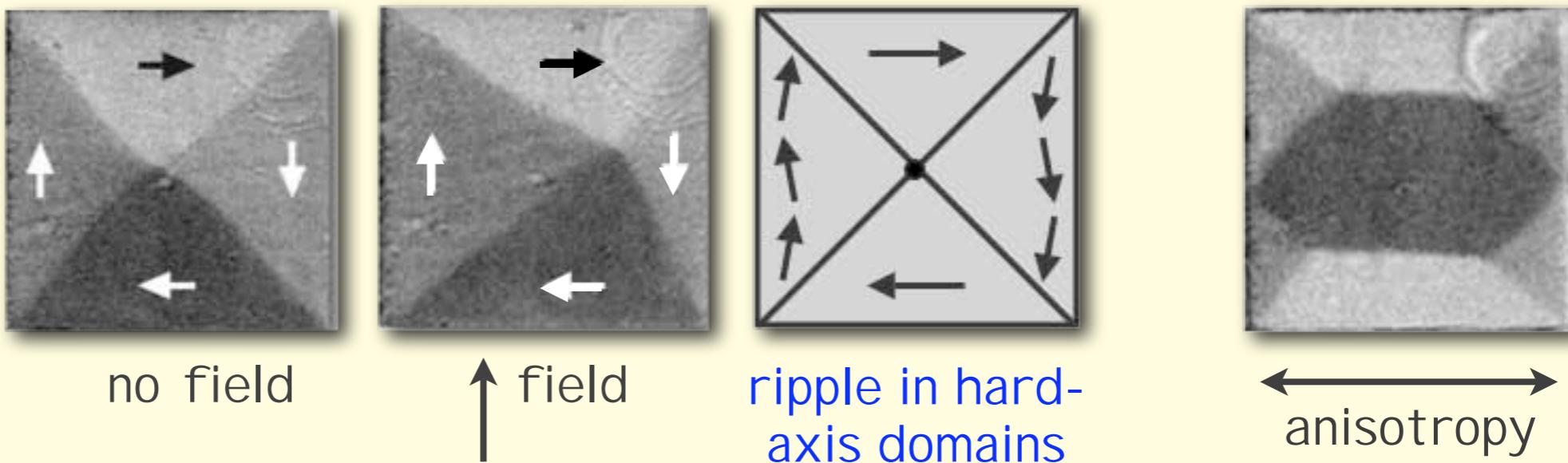


15.76 ns



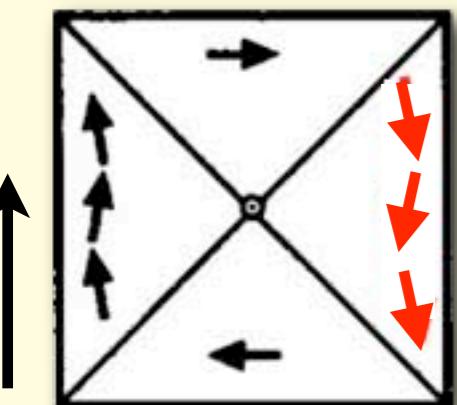
Permalloy element ($40 \times 40 \mu\text{m}^2$, 50 nm thick)

static

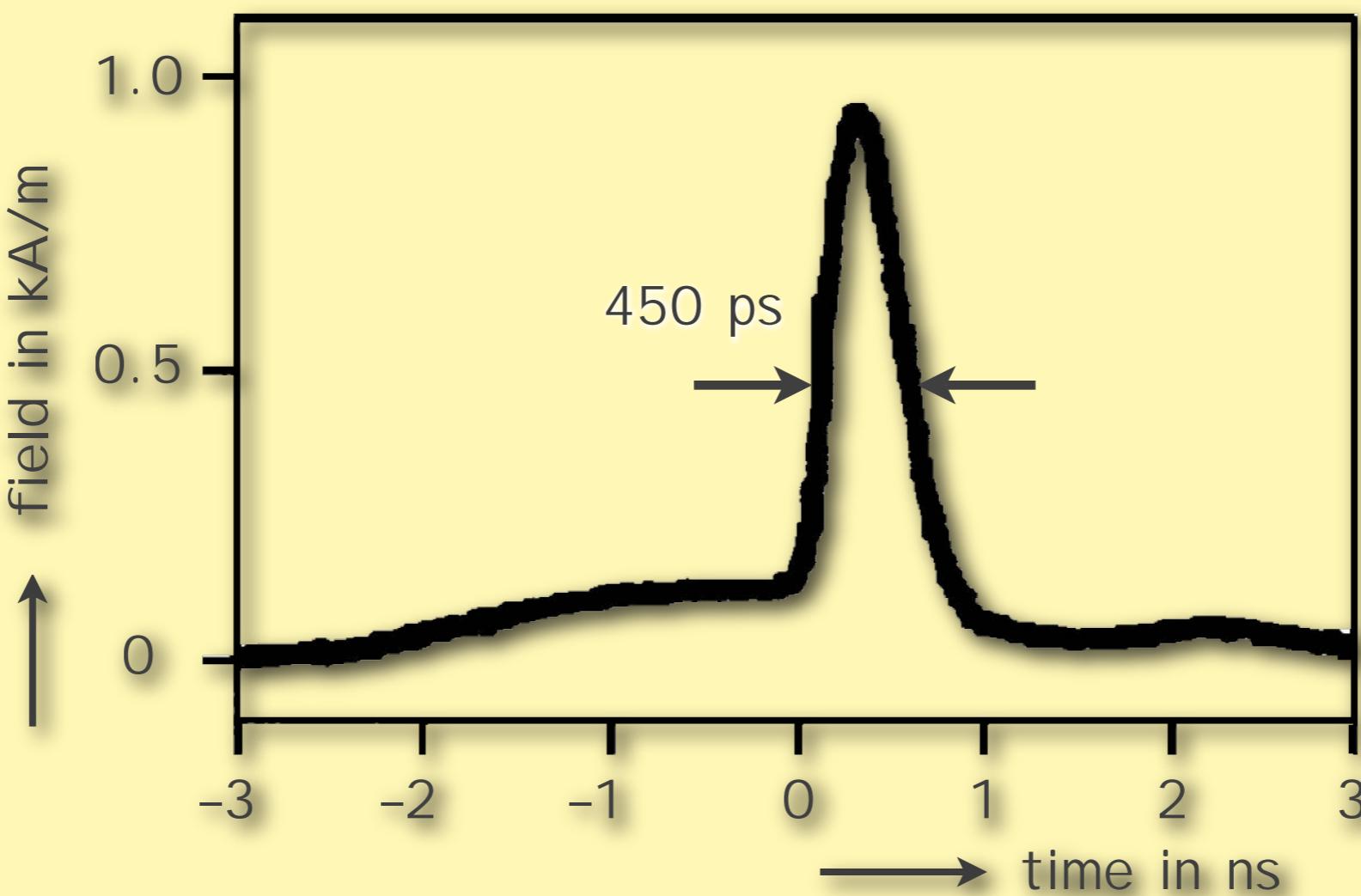


dynamic

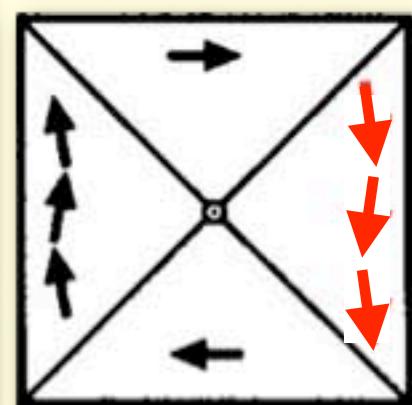
0 ns



H_{pulse}



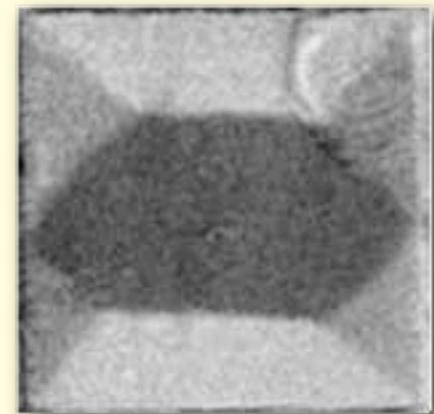
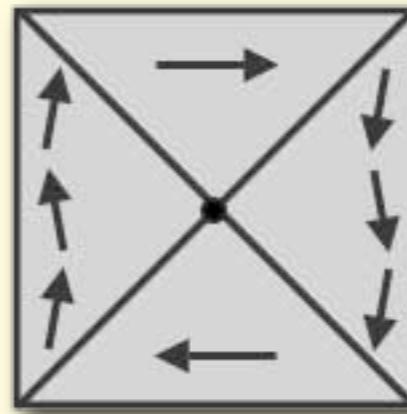
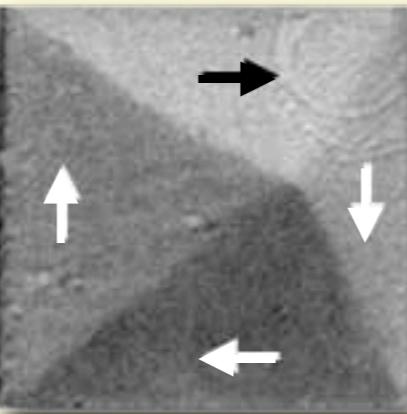
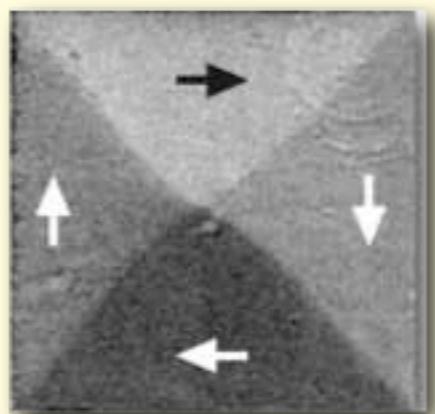
15.76 ns



34405 (2005)

Permalloy element ($40 \times 40 \mu\text{m}^2$, 50 nm thick)

static



↔
anisotropy

dynamic

0 ns



0.28 ns



0.38 ns



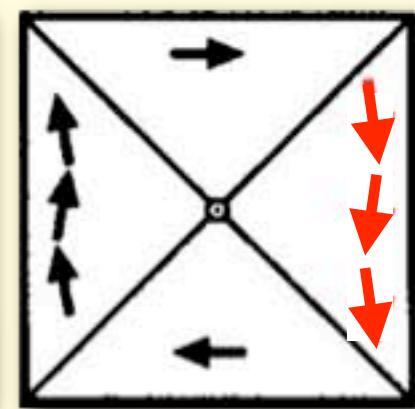
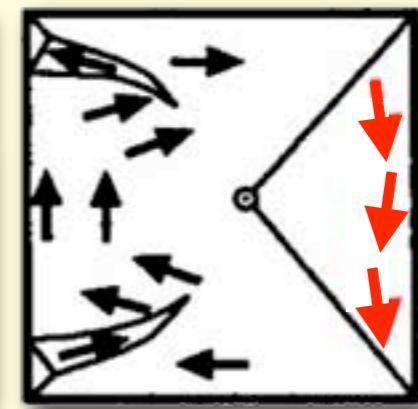
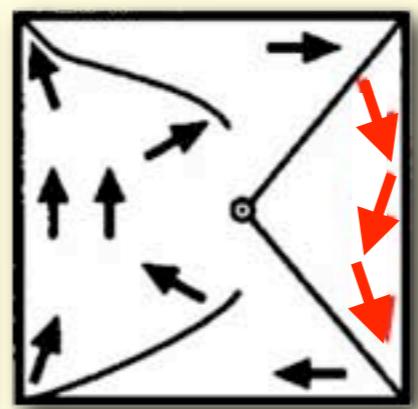
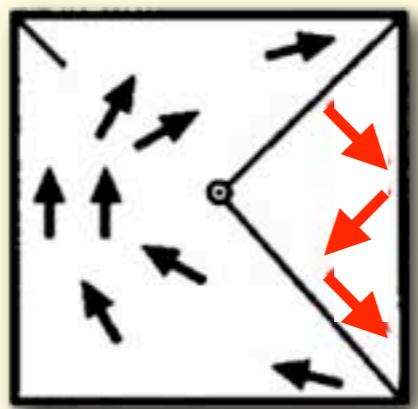
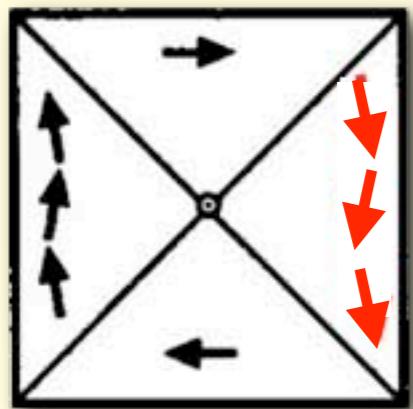
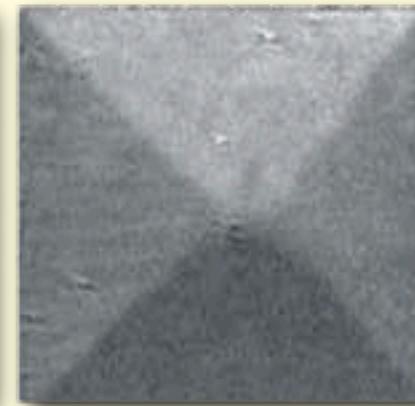
0.64 ns

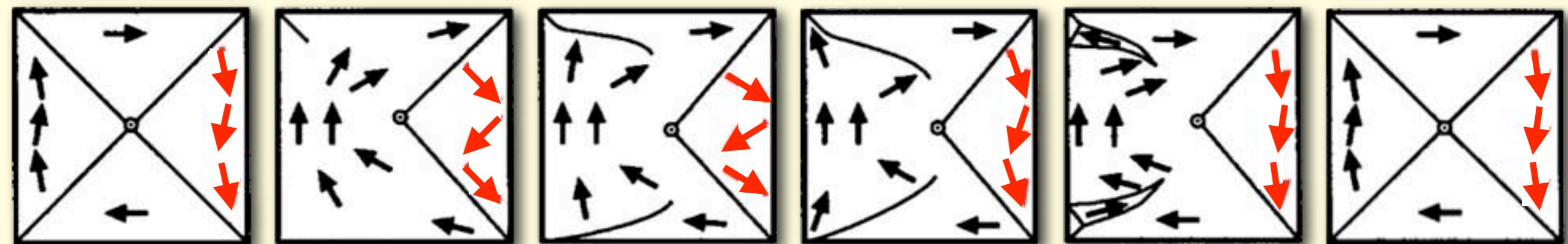
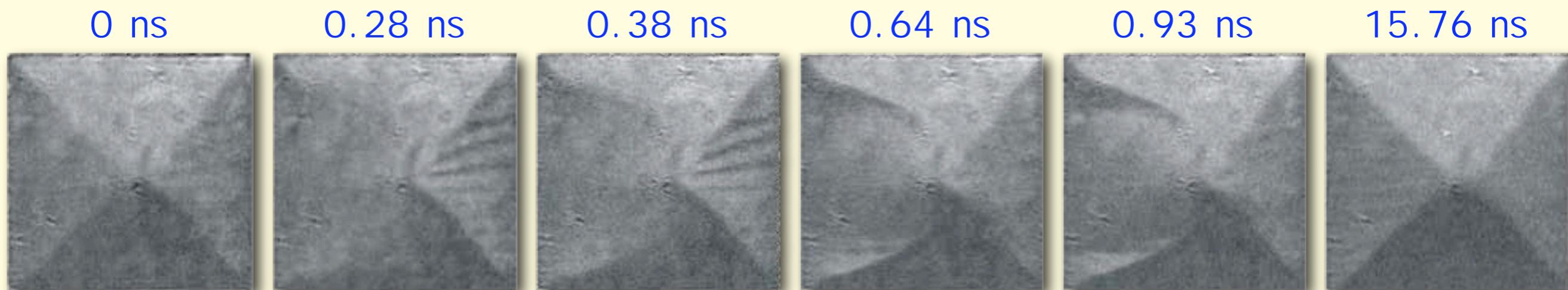
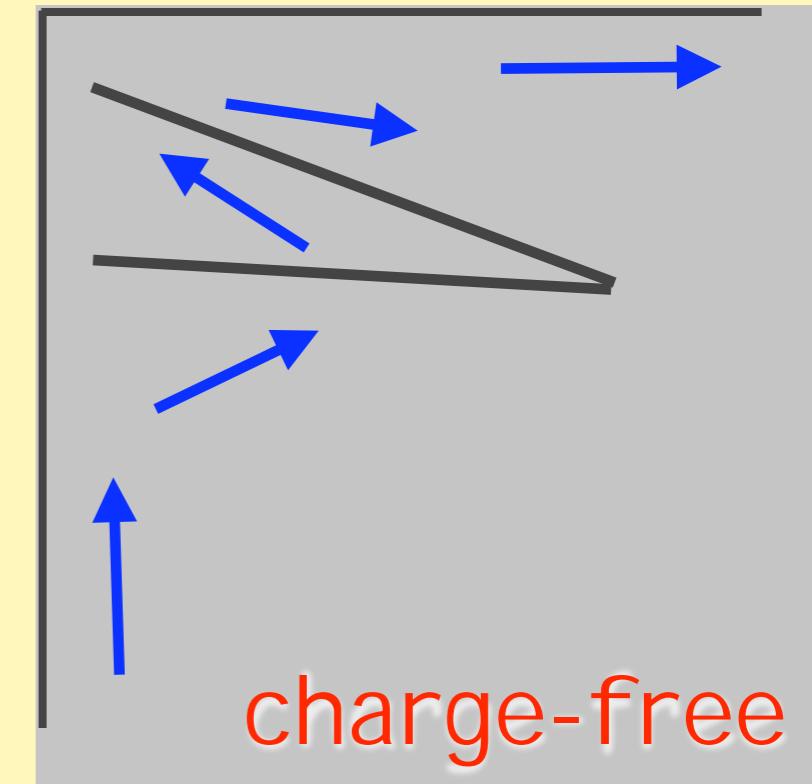
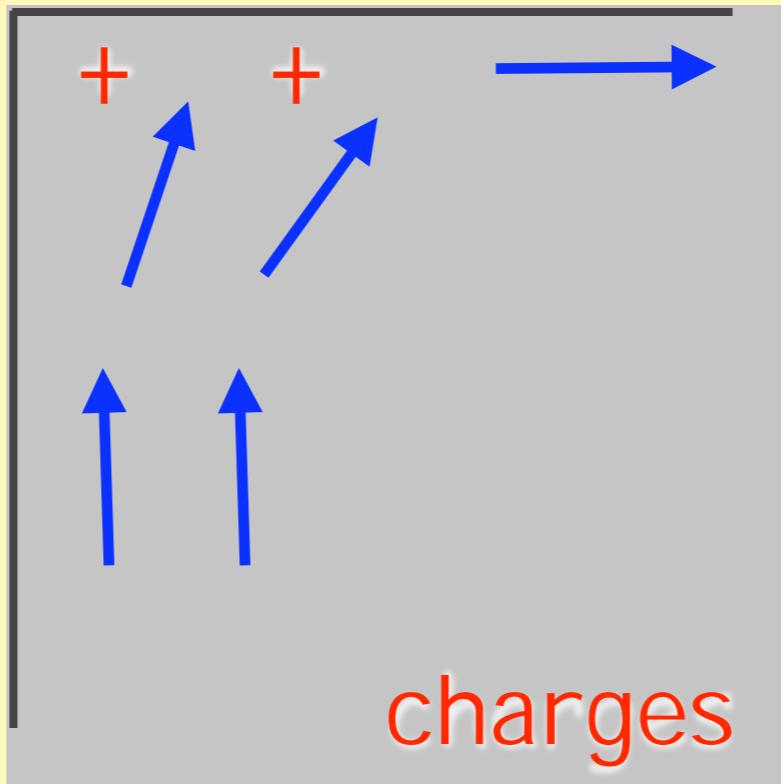
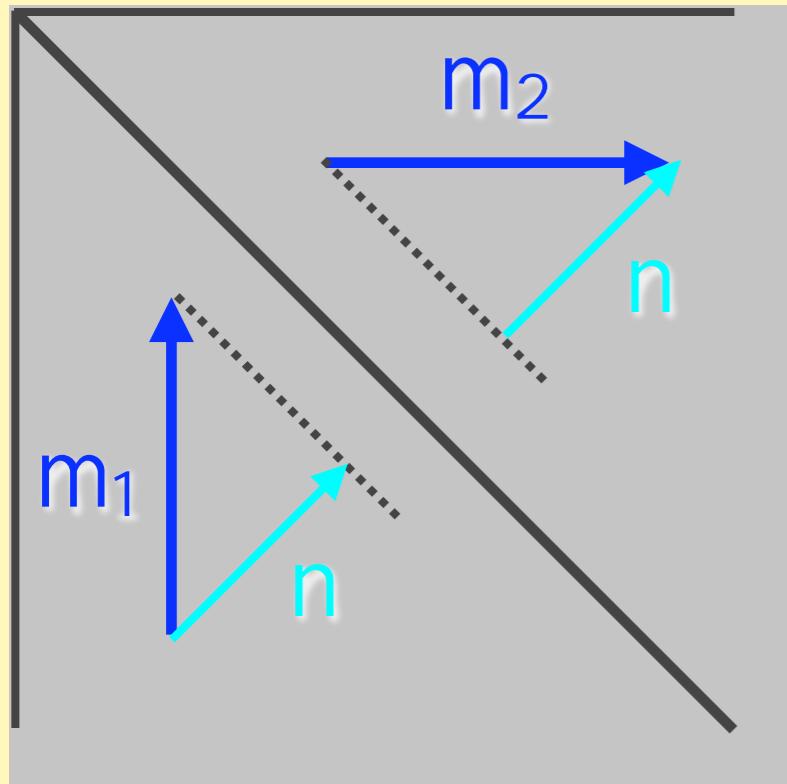


0.93 ns



15.76 ns



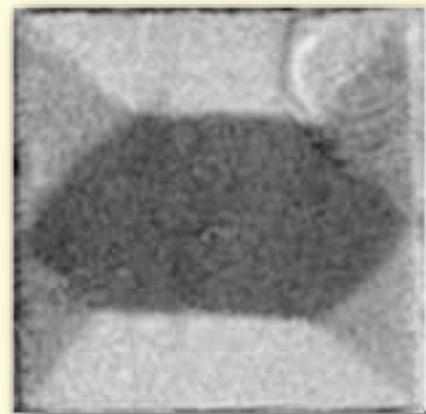
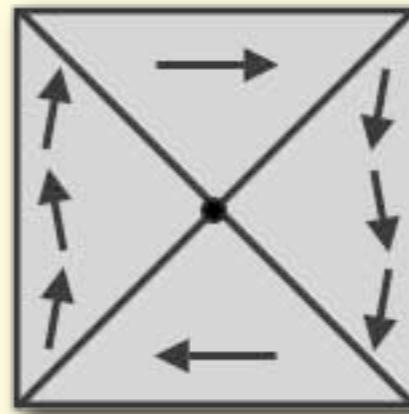
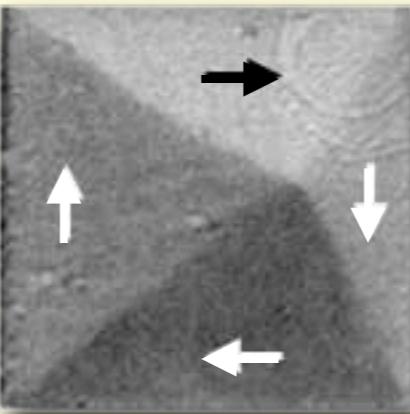
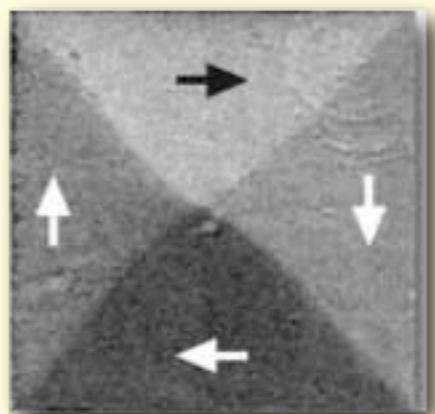


A. Neudert et al., Phys. Rev. B 71, 134405 (2005)

H_{pulse}

Permalloy element ($40 \times 40 \mu\text{m}^2$, 50 nm thick)

static



↔
anisotropy

dynamic

0 ns



0.28 ns



0.38 ns



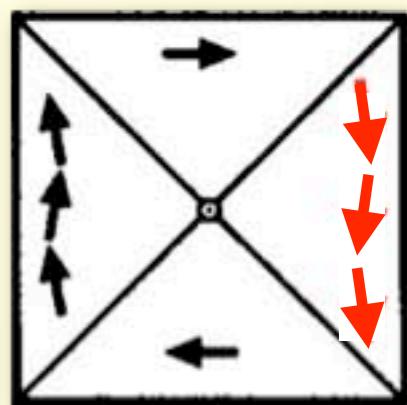
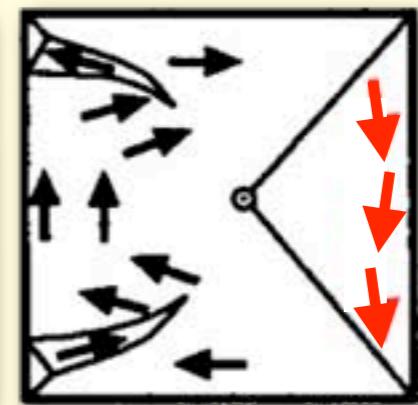
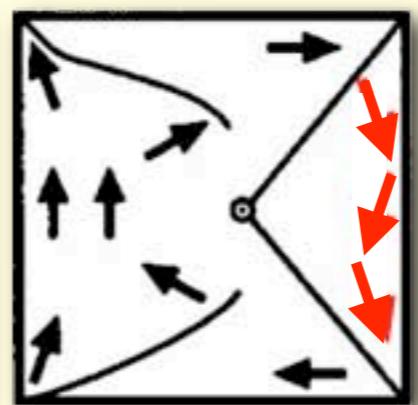
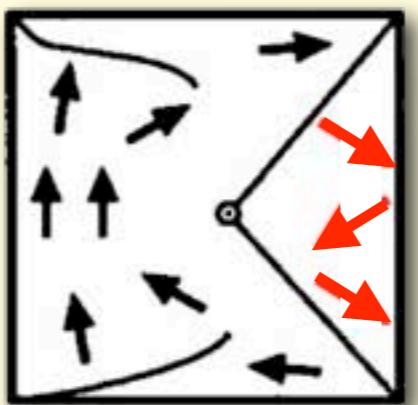
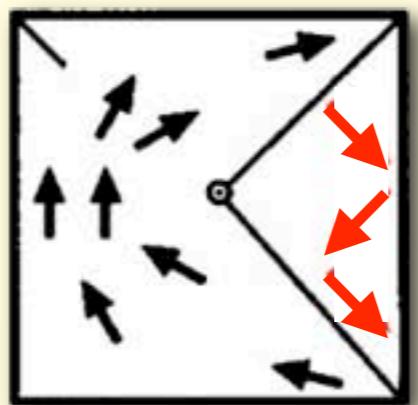
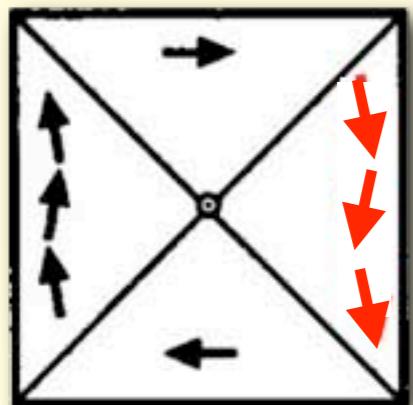
0.64 ns



0.93 ns



15.76 ns



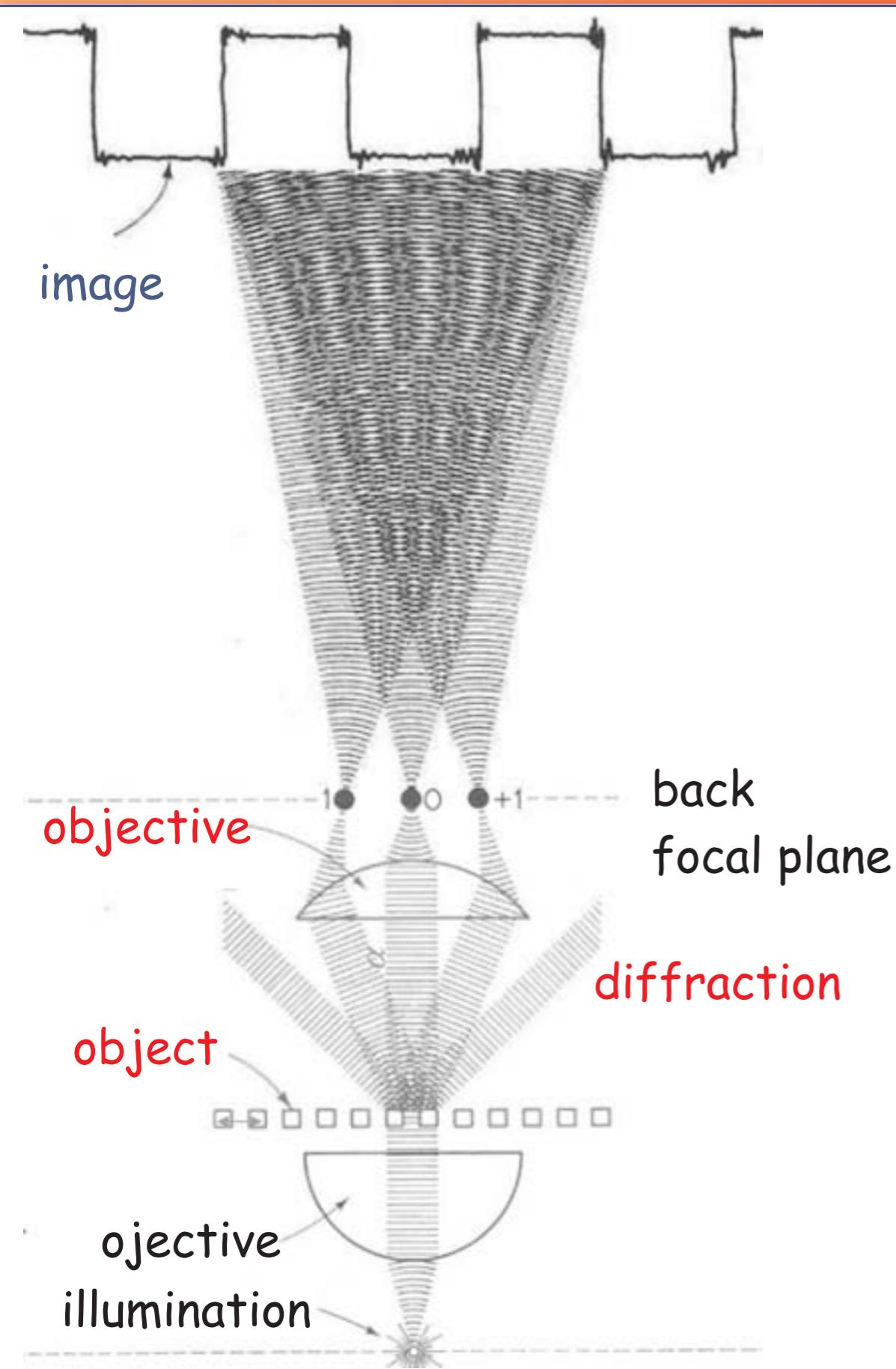
H_{pulse}

A. Neudert et al., Phys. Rev. B 71, 134405 (2005)

Kerr microscopy: drawbacks

Small objects?

Resolution of optical microscopy (E. Abbe 1840 - 1905)



resolution determined by
constructive interference

diffraction limited image formation

$$\text{Rayleigh equation: } d = \frac{0.5 \lambda}{\text{NA}}$$

d = separation between particles,
still allowing to see them

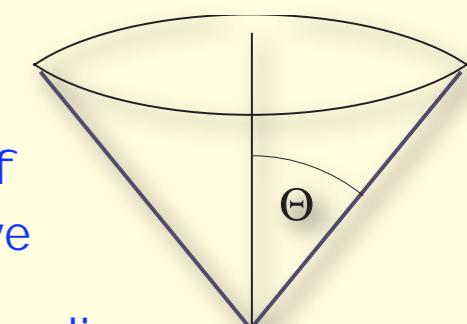
λ = wavelength

NA = numerical aperture of objective

$$\text{NA} = n \sin \theta$$

θ = half the cone angle of
light accepted by objective

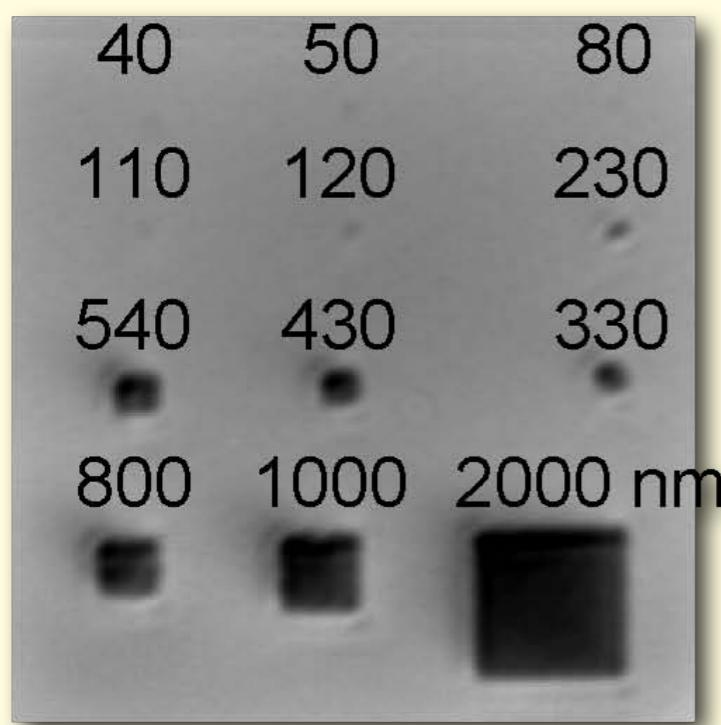
n = refraction index of medium
between sample and objective



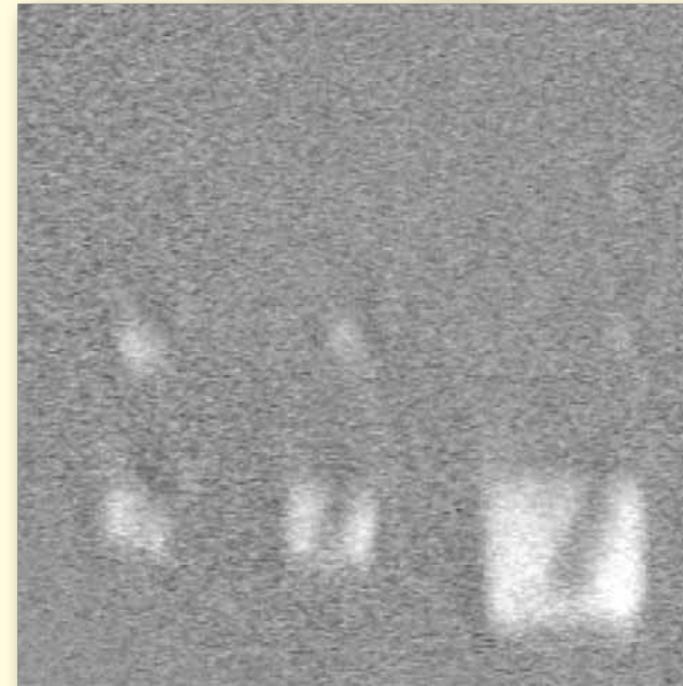
best around 200 nm

About resolution

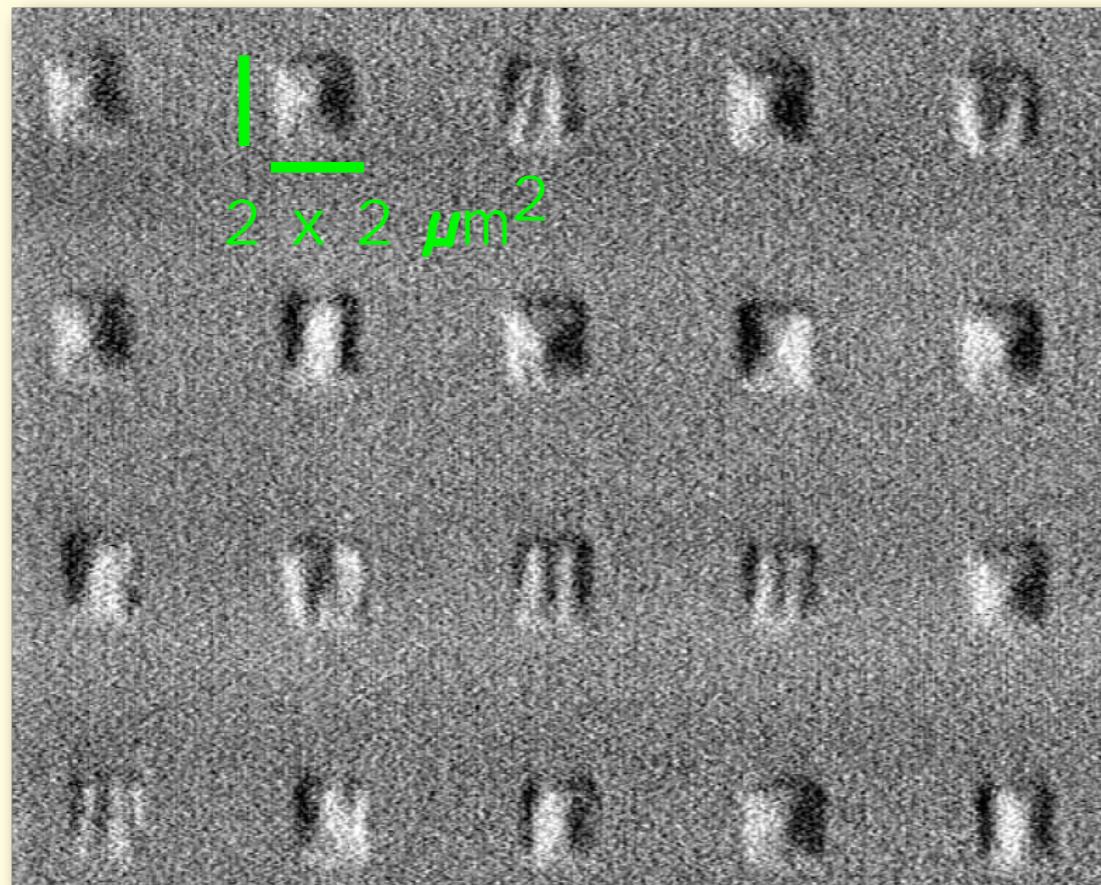
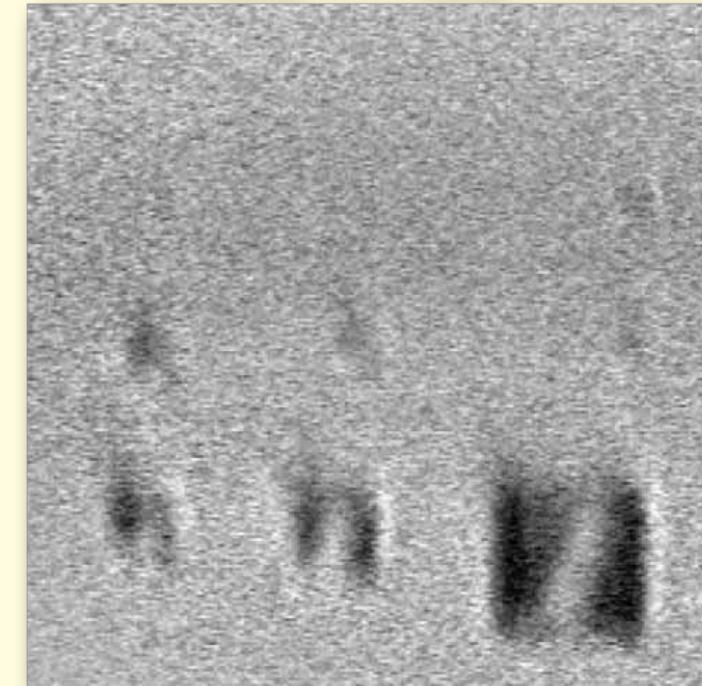
Co elements (sample: Axel Carl)



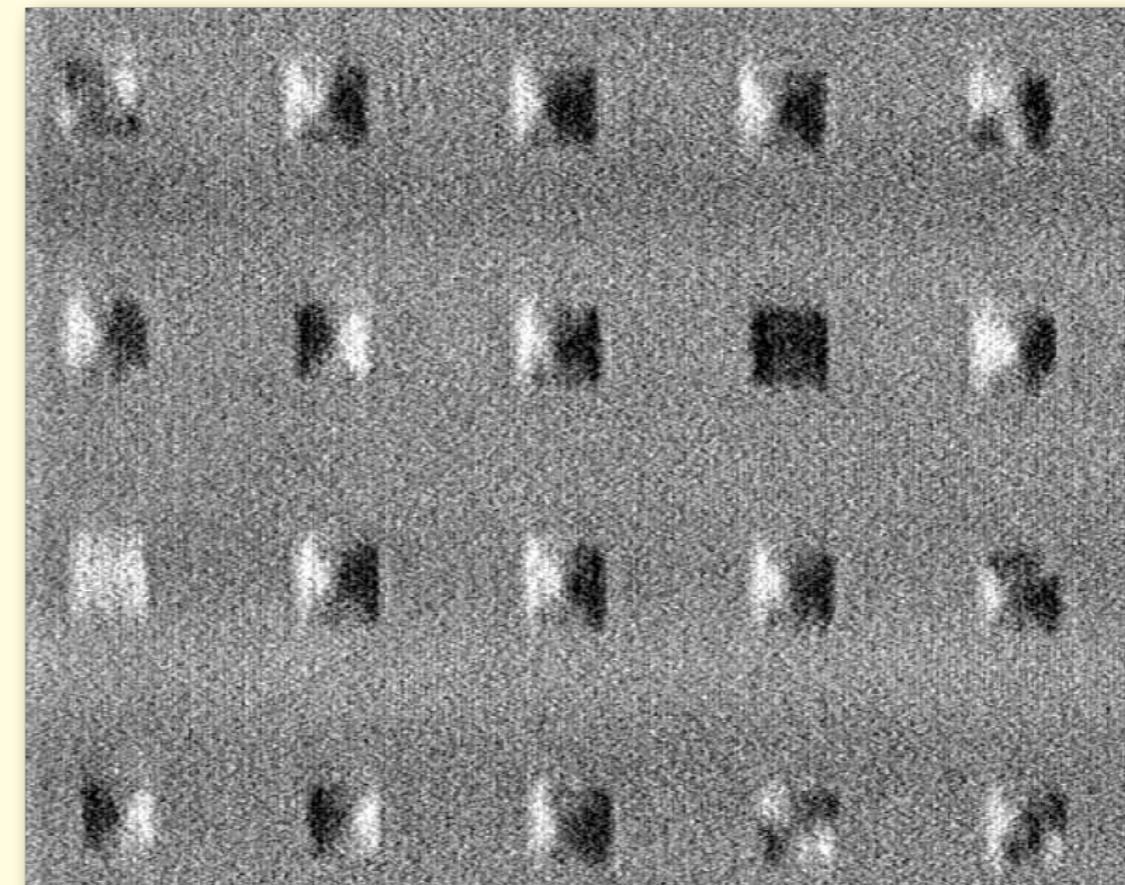
$M_r^+ - M_r^-$



$M_r^- - M_r^+$

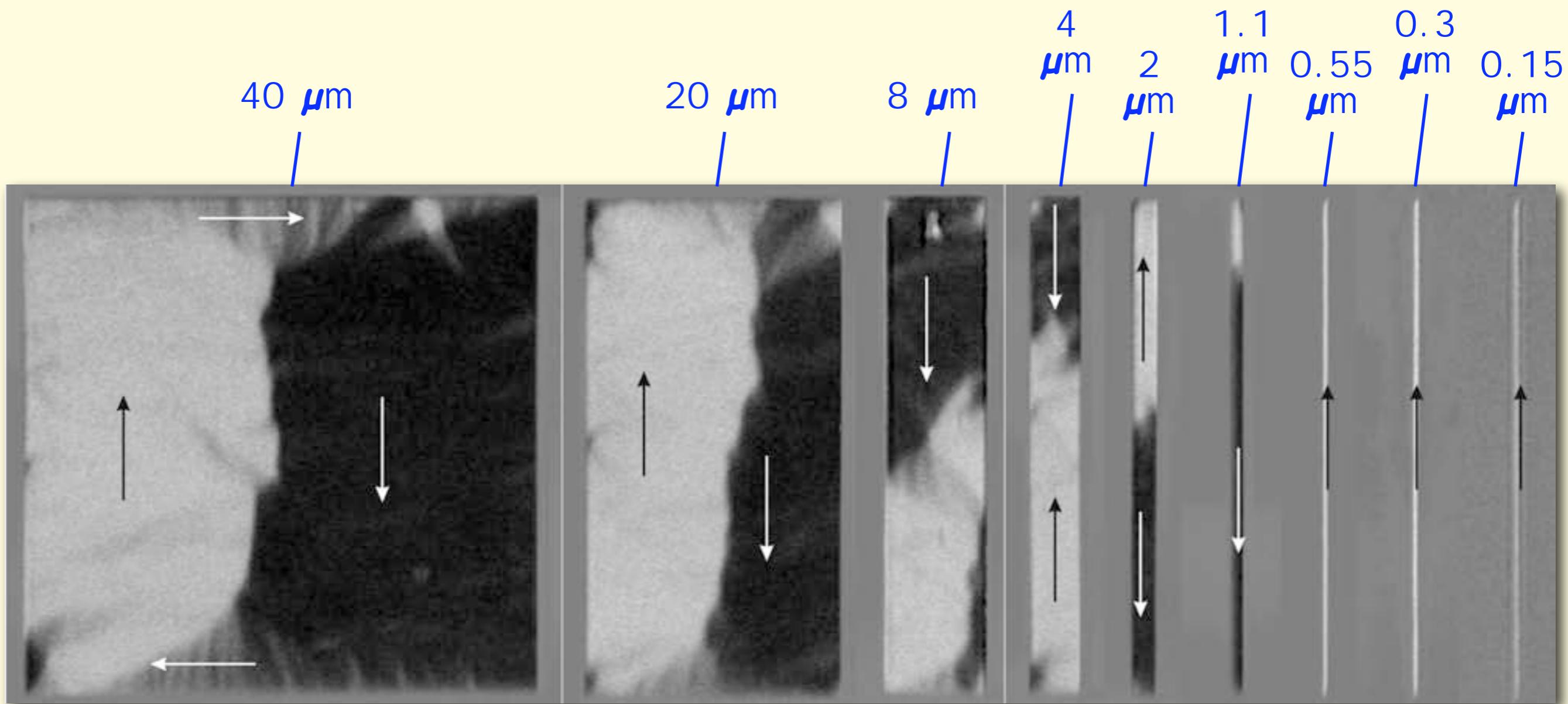


$\longleftrightarrow H_{\text{demag}}$



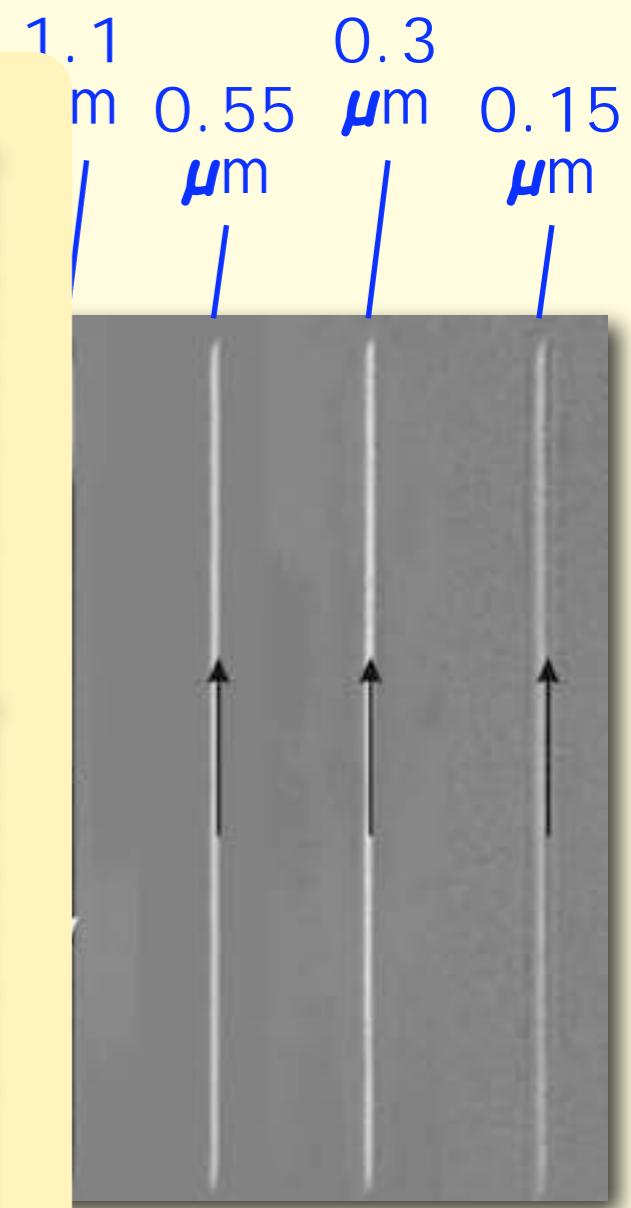
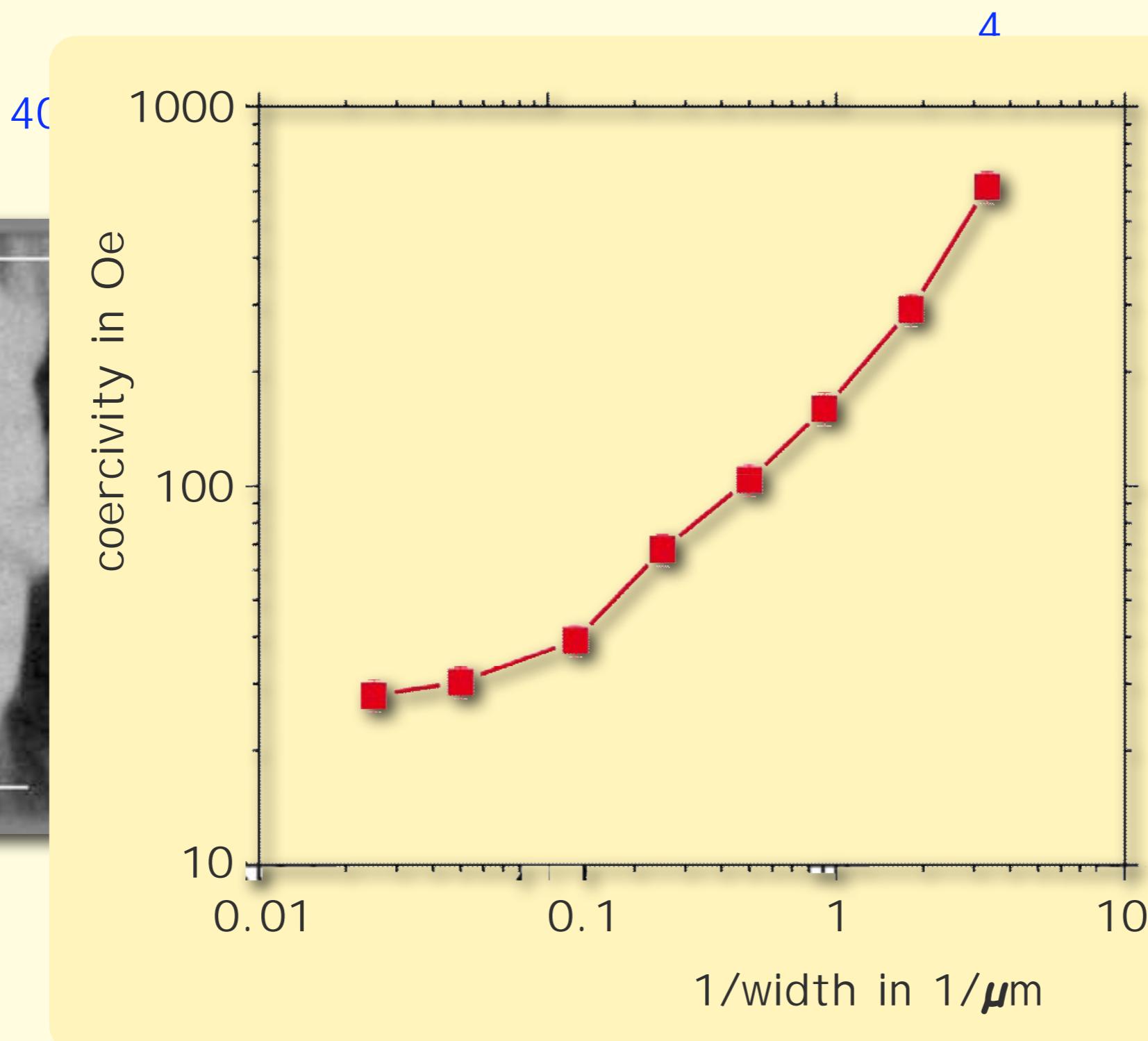
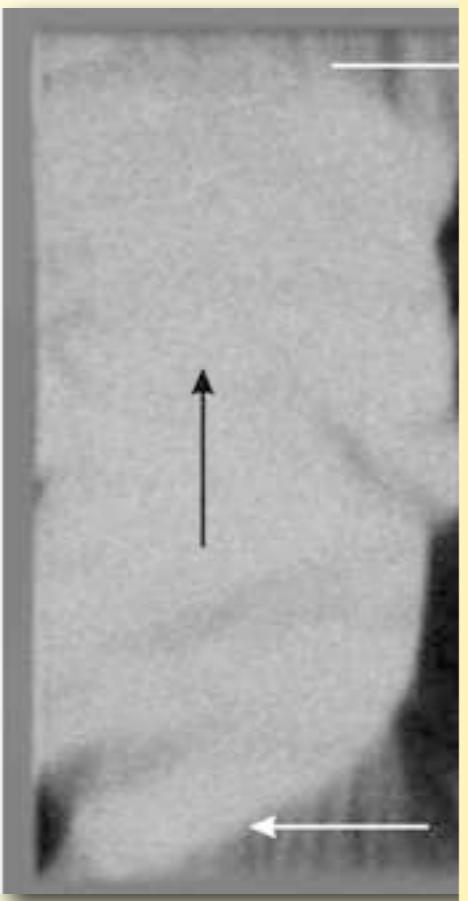
H_{demag}

Magnetization reversal of Co-wires



courtesy J. McCord (IFW Dresden),
sample: B. Hausmanns (Duisburg)

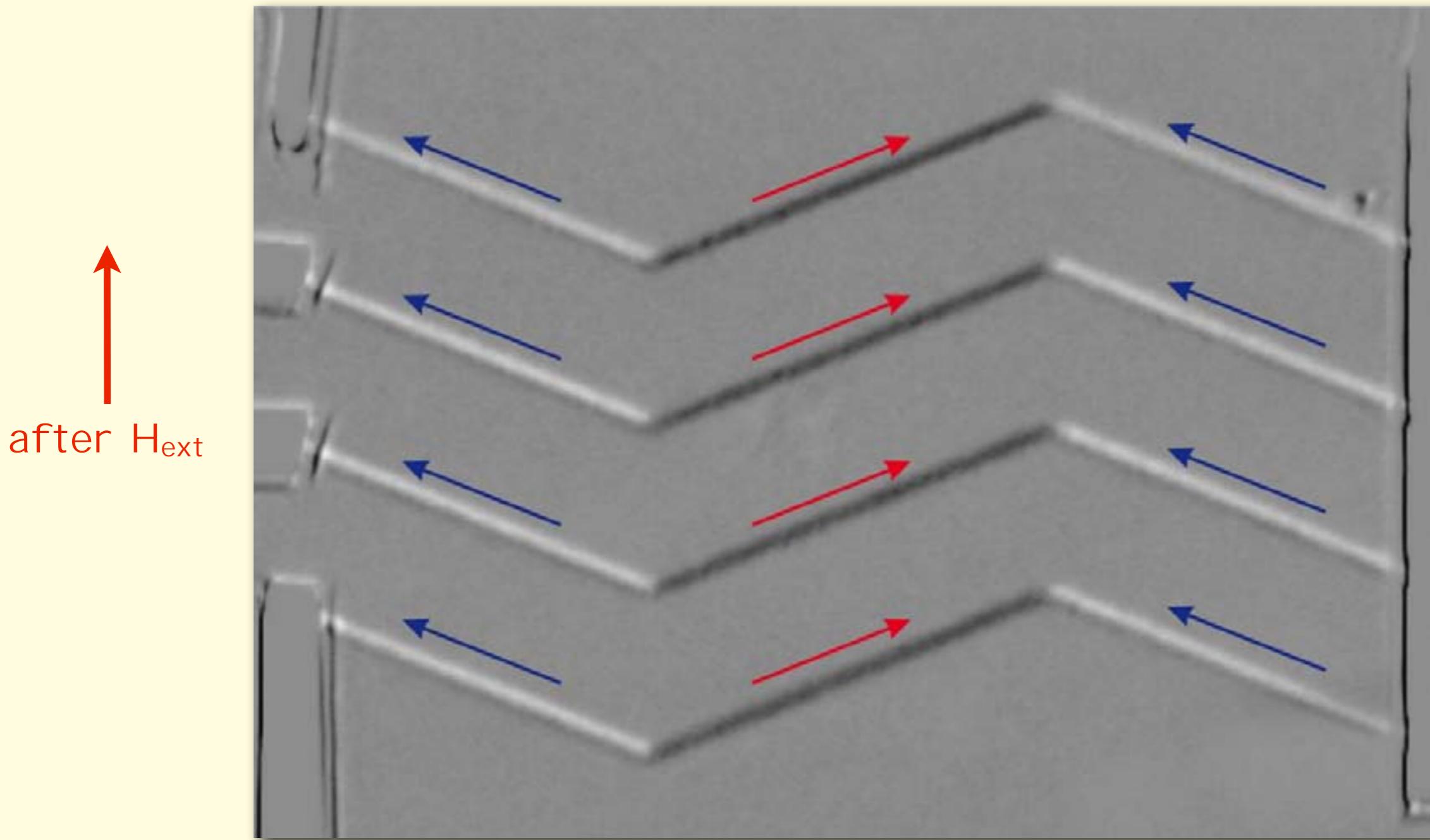
Magnetization reversal of Co-wires



courtesy J. McCord (IFW Dresden),
sample: B. Hausmanns (Duisburg)

Sub-micrometer imaging

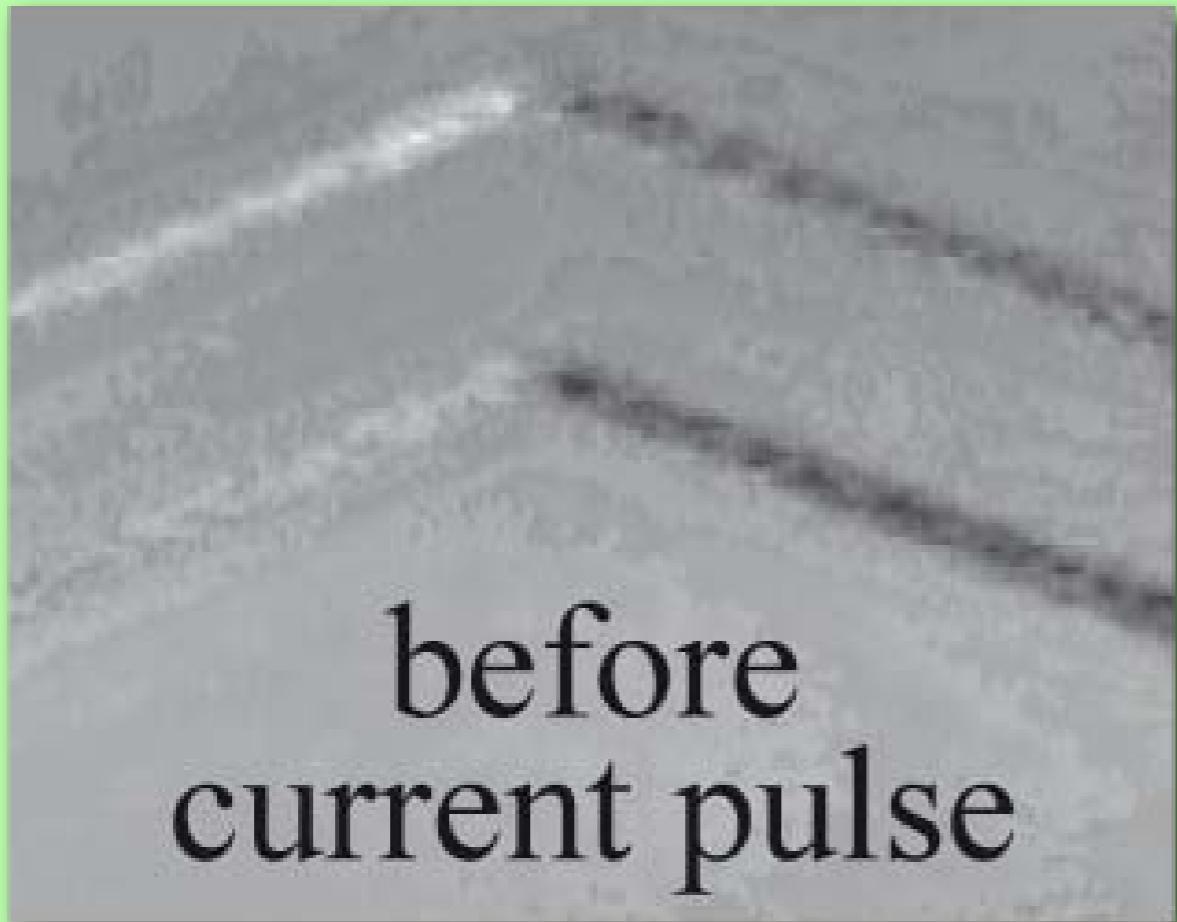
NiFe wires, $0.5 \mu\text{m}$ wide, 20 nm thick



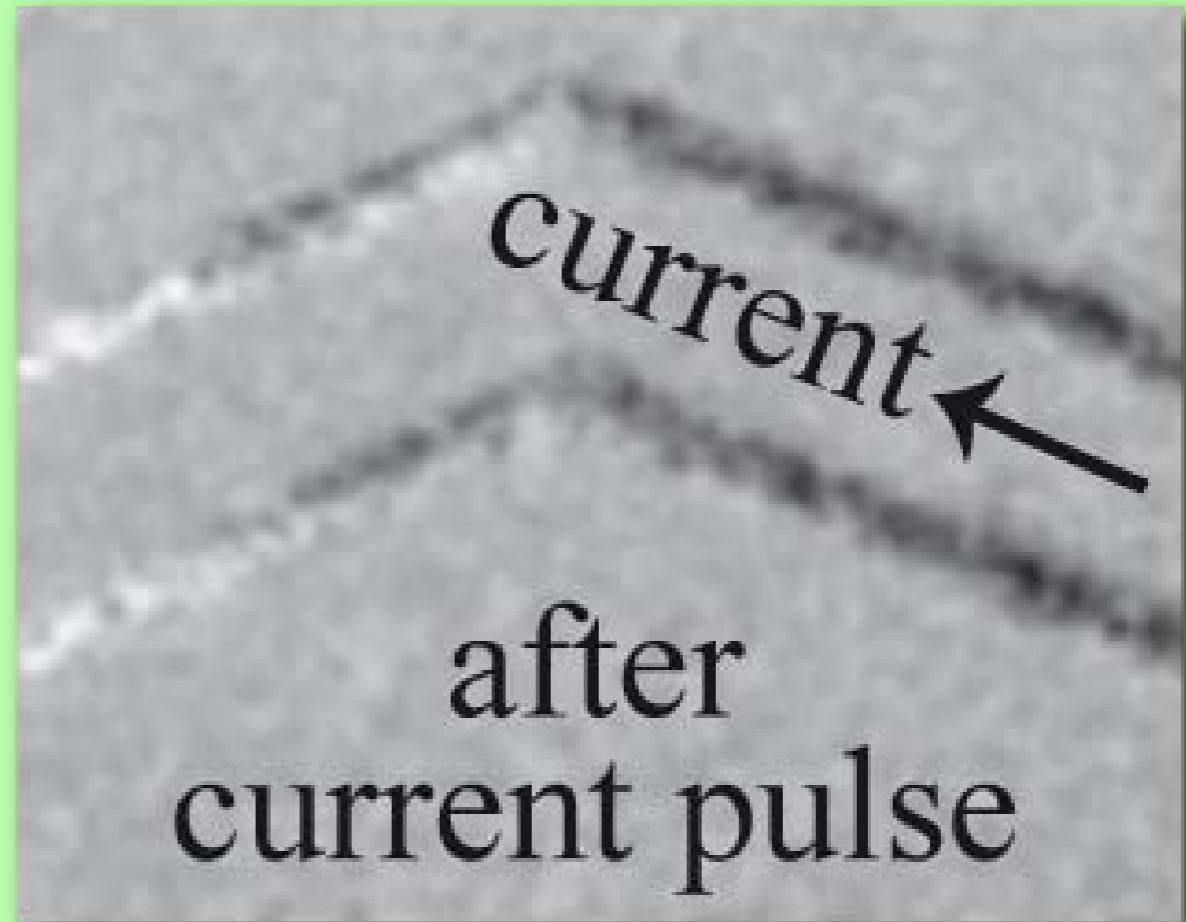
together with: M. Kläui, T. Moore, U. Rüdiger (Konstanz),
J. McCord (IFW Dresden),

Sub-micrometer imaging

NiFe wires, 0.5 μm wide, 20 nm thick



before
current pulse



after
current pulse



together with: M. Kläui, T. Moore, U. Rüdiger (Konstanz),
J. McCord (IFW Dresden),

Some Magneto-optics

Kerr effect: dielectric law

$$\begin{aligned} \mathbf{D} &= \epsilon \mathbf{E} = \epsilon \begin{pmatrix} 1 & -i Q m_3 & i Q m_2 \\ i Q m_3 & 1 & -i Q m_1 \\ -i Q m_2 & i Q m_1 & 1 \end{pmatrix} \mathbf{E} \\ &= \epsilon \mathbf{E} + i \epsilon Q \mathbf{m} \times \mathbf{E} \end{aligned}$$

\mathbf{E} : electric vector of light wave

\mathbf{D} : dielectric displacement vector
(= vector of light after reflection)

m_i : components of magnetization vector (cubic crystal)

ϵ : dielectric tensor

Q: material constant ($\sim M_s$, complex, determines strength of rotation)

Kerr effect: dielectric law

$$\mathbf{D} = \epsilon \mathbf{E} = \epsilon \begin{pmatrix} 1 & -i Q m_3 & i Q m_2 \\ i Q m_3 & 1 & -i Q m_1 \\ -i Q m_2 & i Q m_1 & 1 \end{pmatrix} \mathbf{E}$$
$$= \epsilon \mathbf{E} + i \epsilon Q \mathbf{m} \times \mathbf{E} \quad \longrightarrow \text{concept of Lorentz force}$$

\mathbf{E} : electric vector of light wave

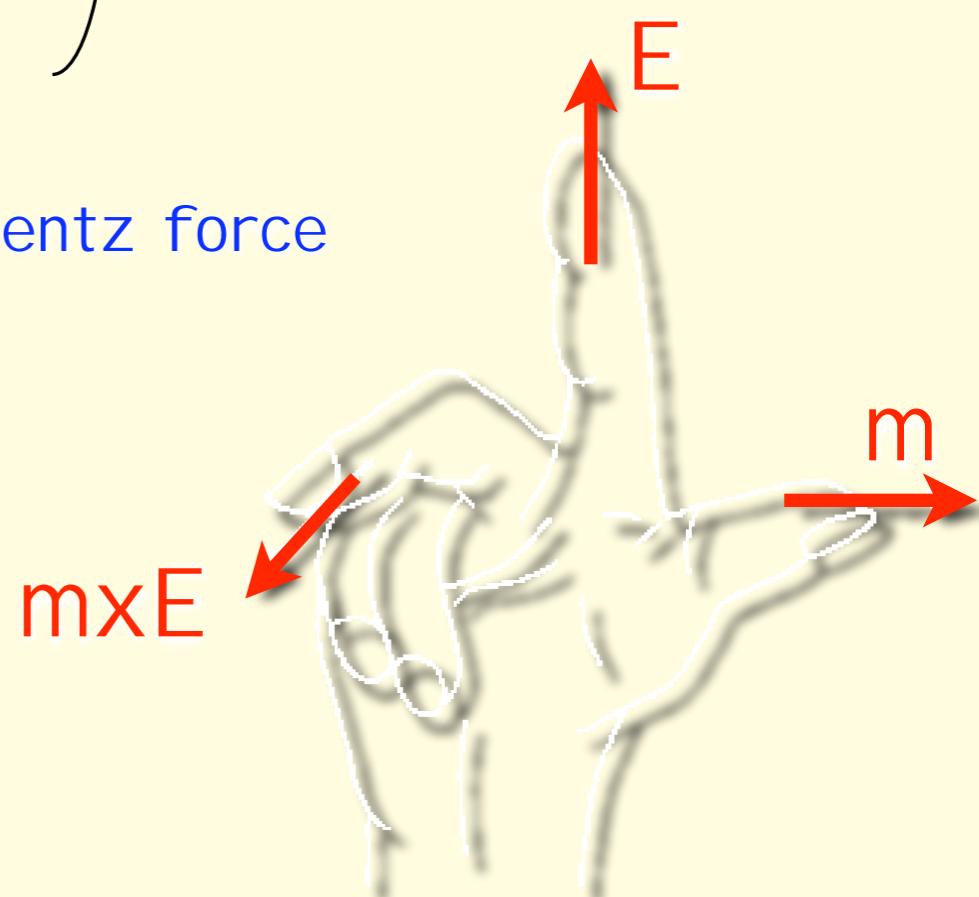
\mathbf{D} : dielectric displacement vector

(= vector of light after reflection)

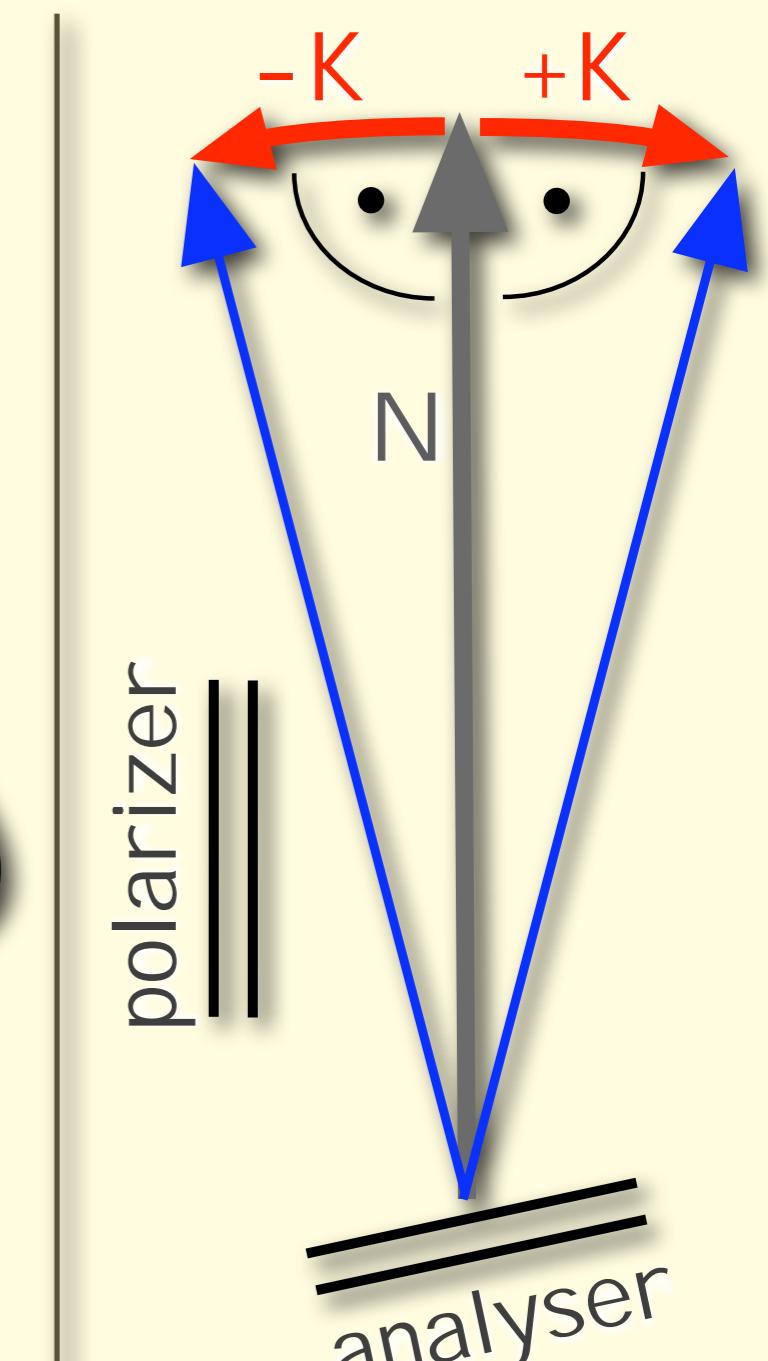
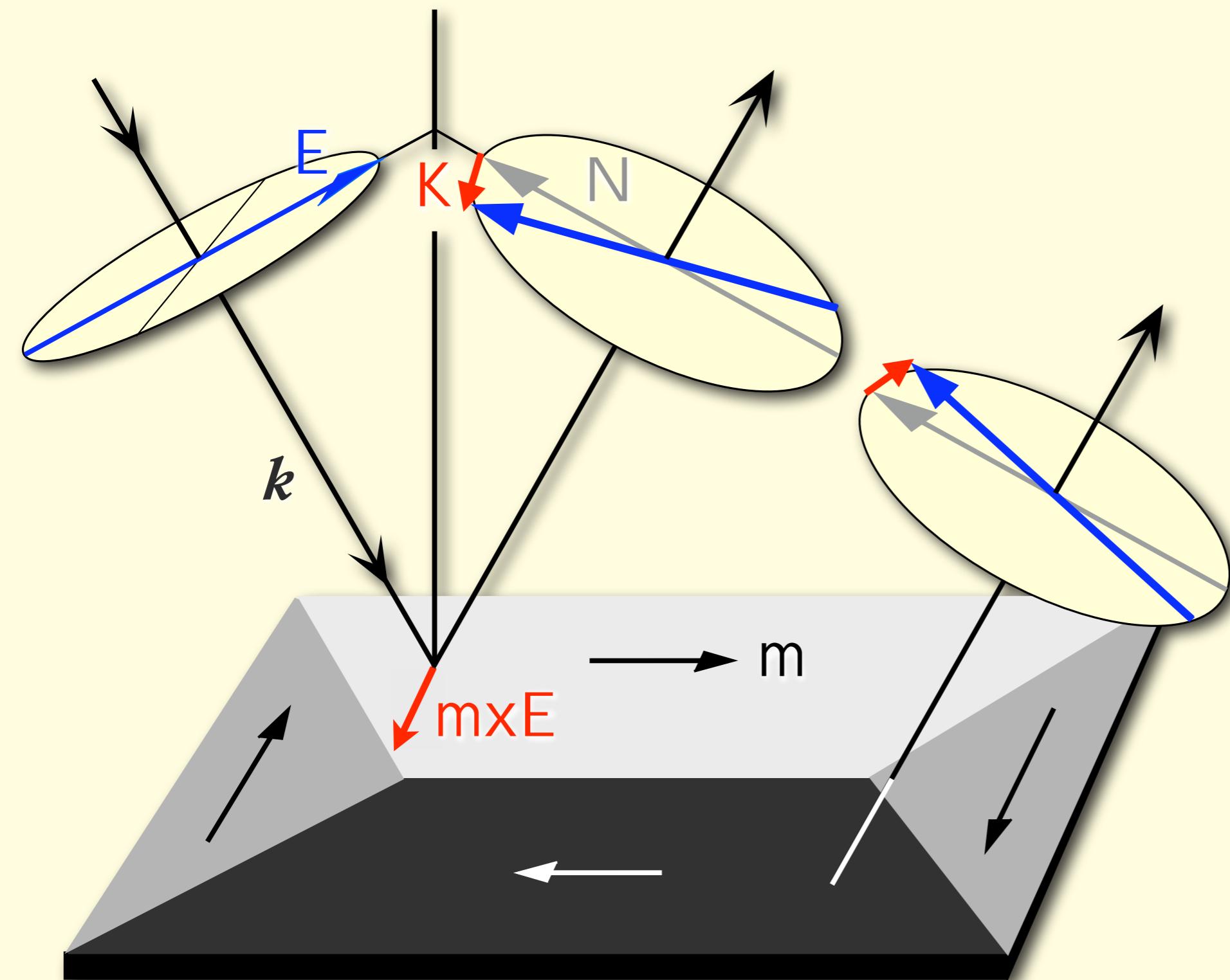
m_i : components of magnetization vector (cubic crystal)

ϵ : dielectric tensor

Q : material constant ($\sim M_s$, complex, determines strength of rotation)

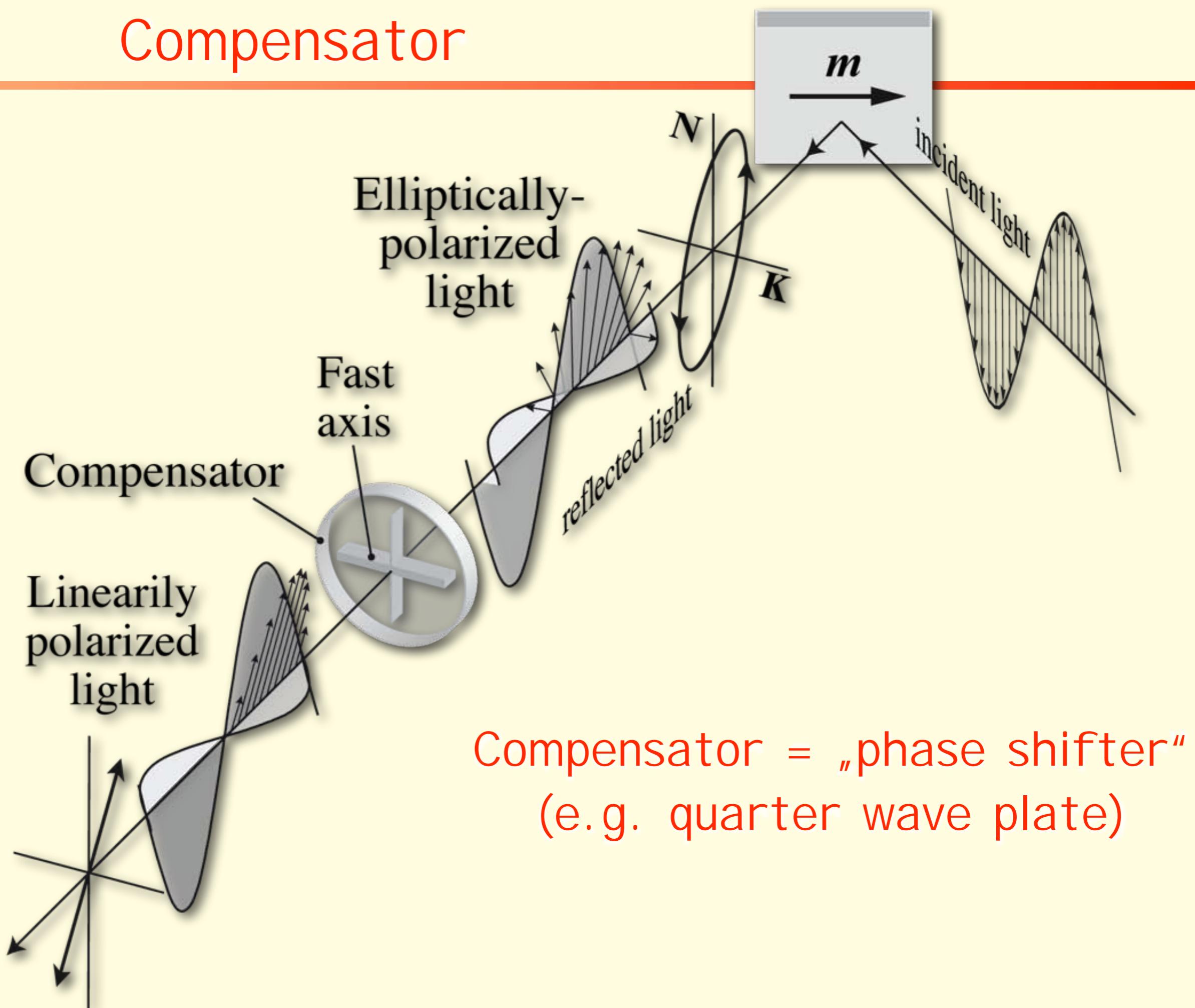


Kerr effect: Lorentz concept

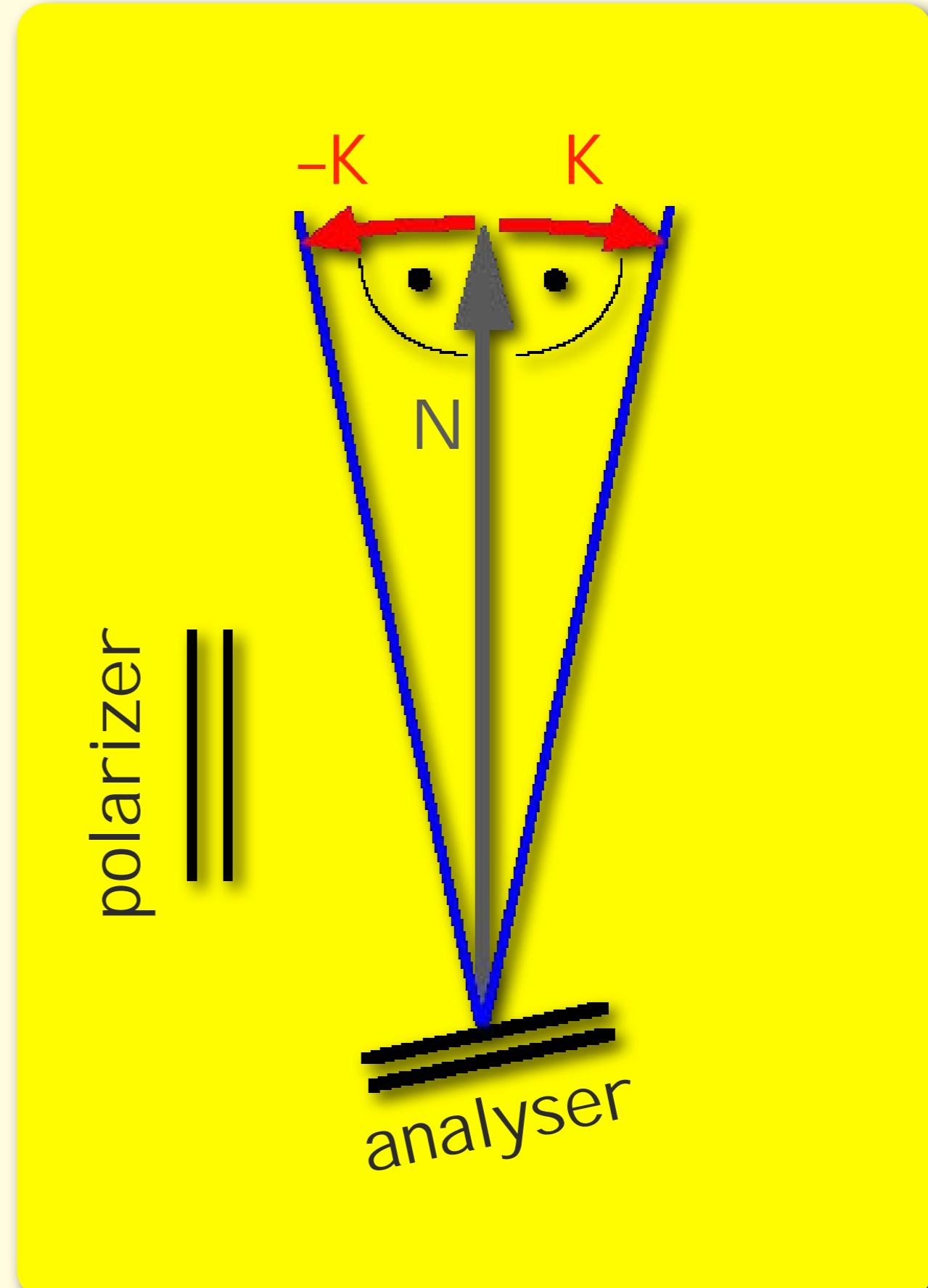
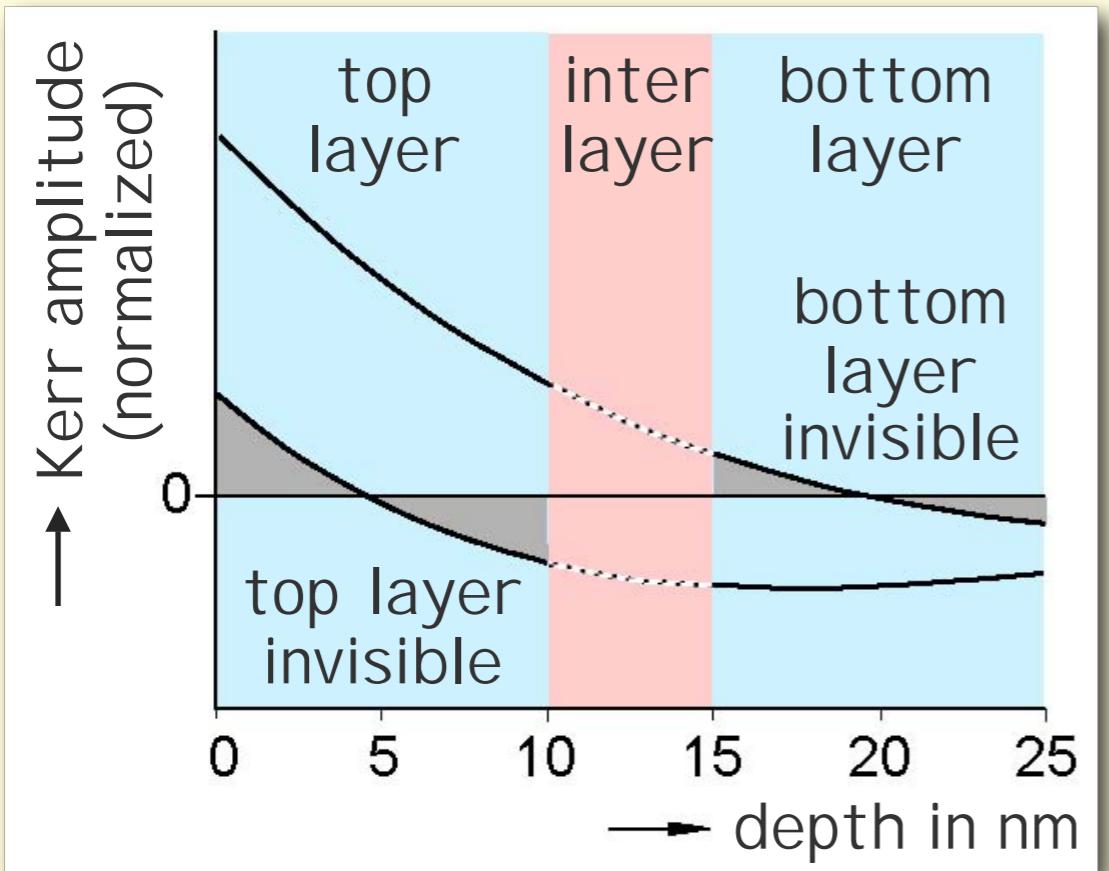
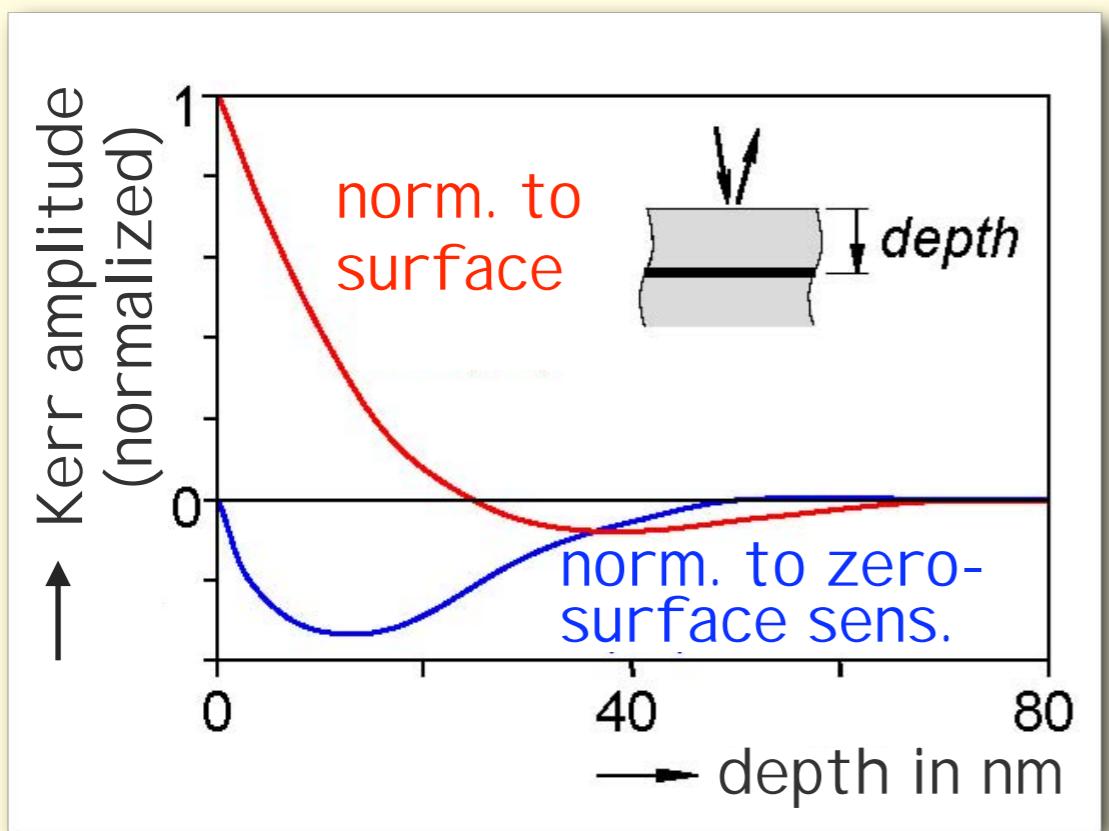


Kerr rotation
= K/N

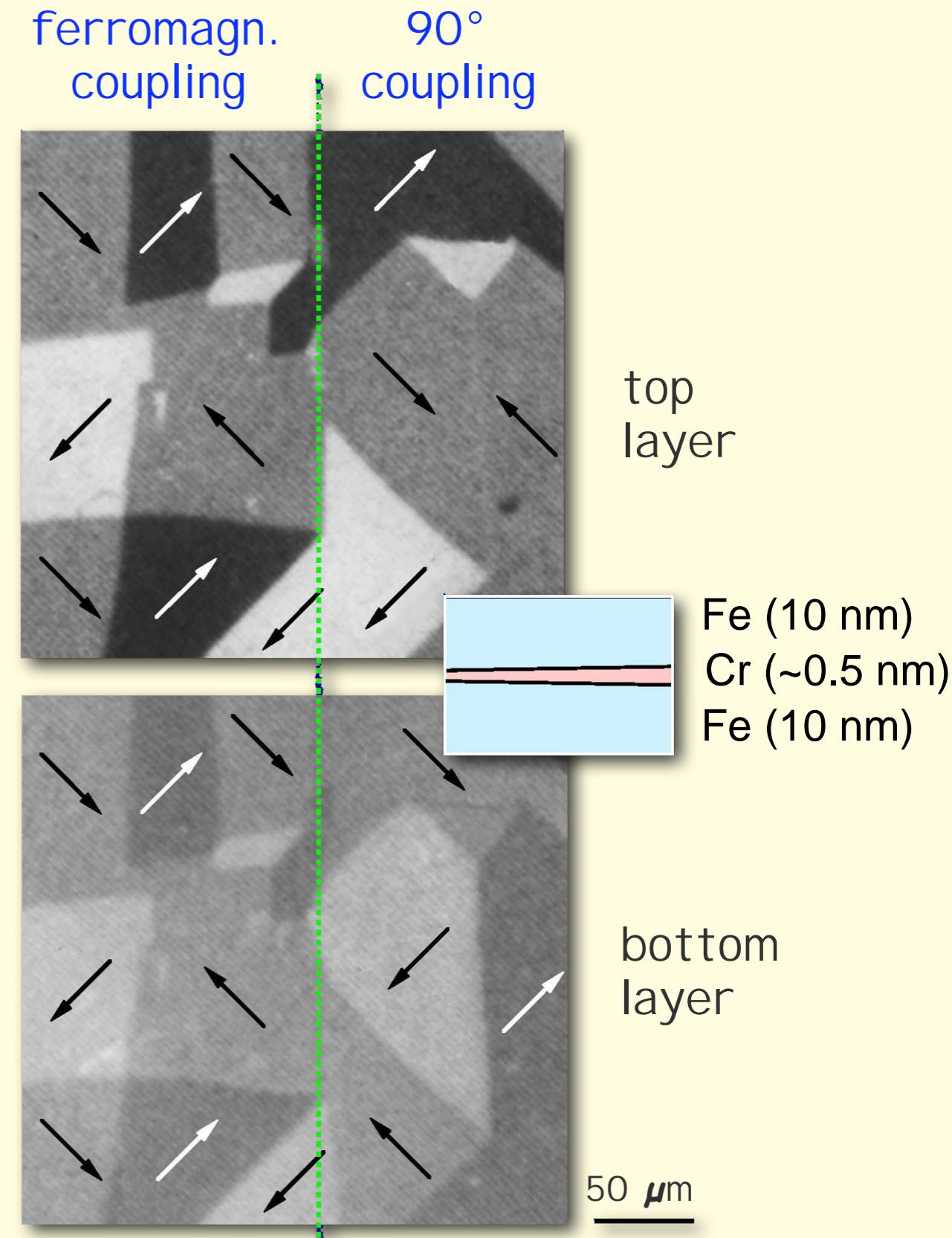
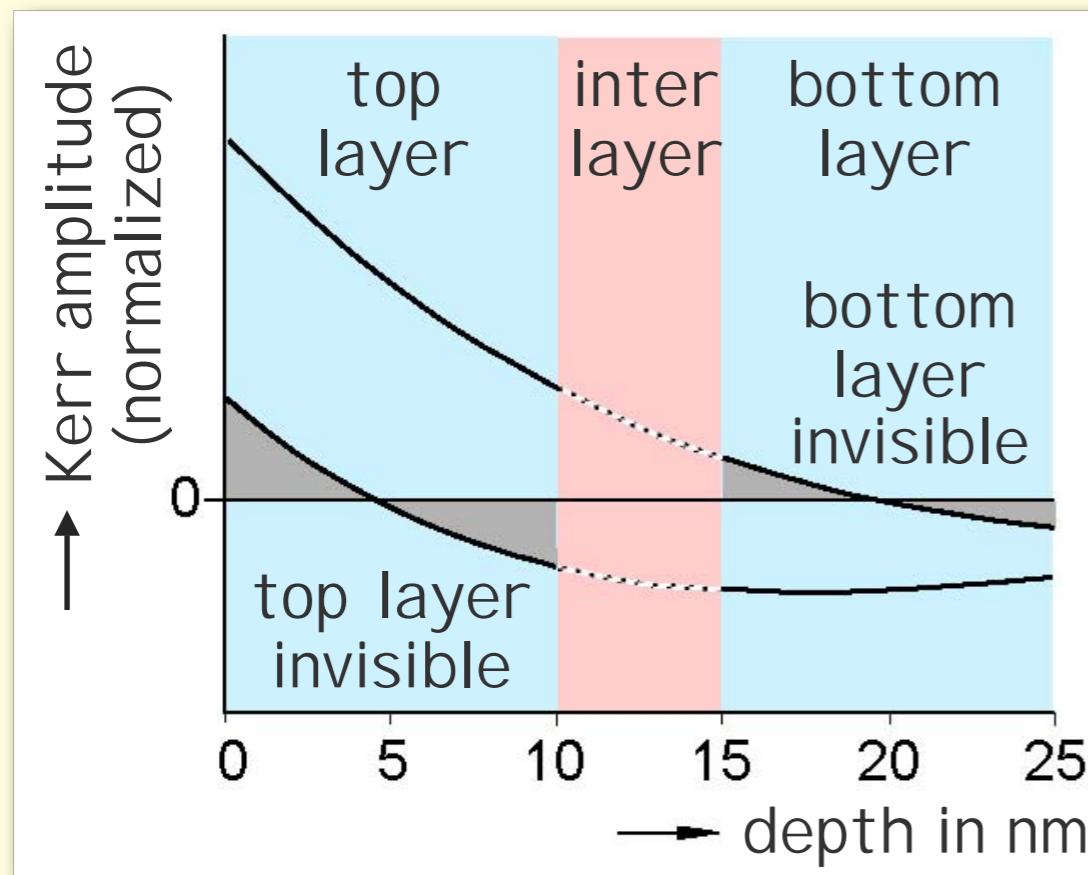
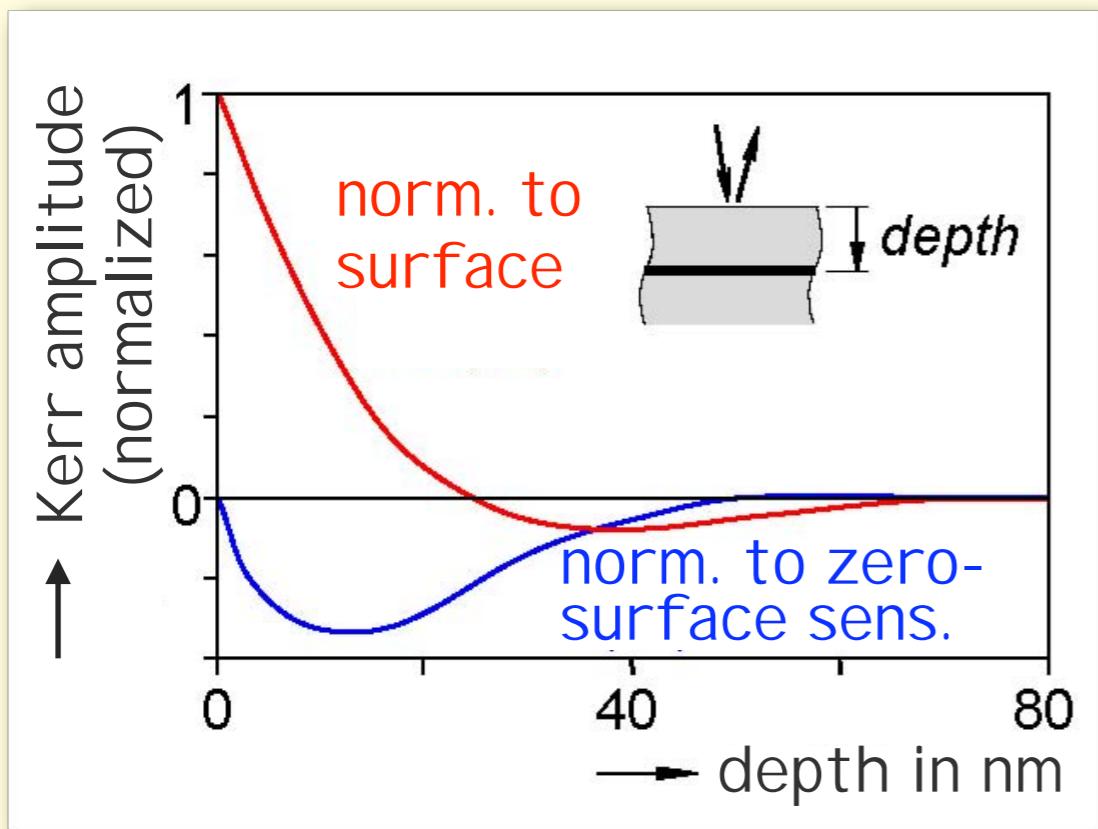
Compensator



Depth selective Kerr microscopy



Depth selective Kerr microscopy



Magneto-optical microscopy: history



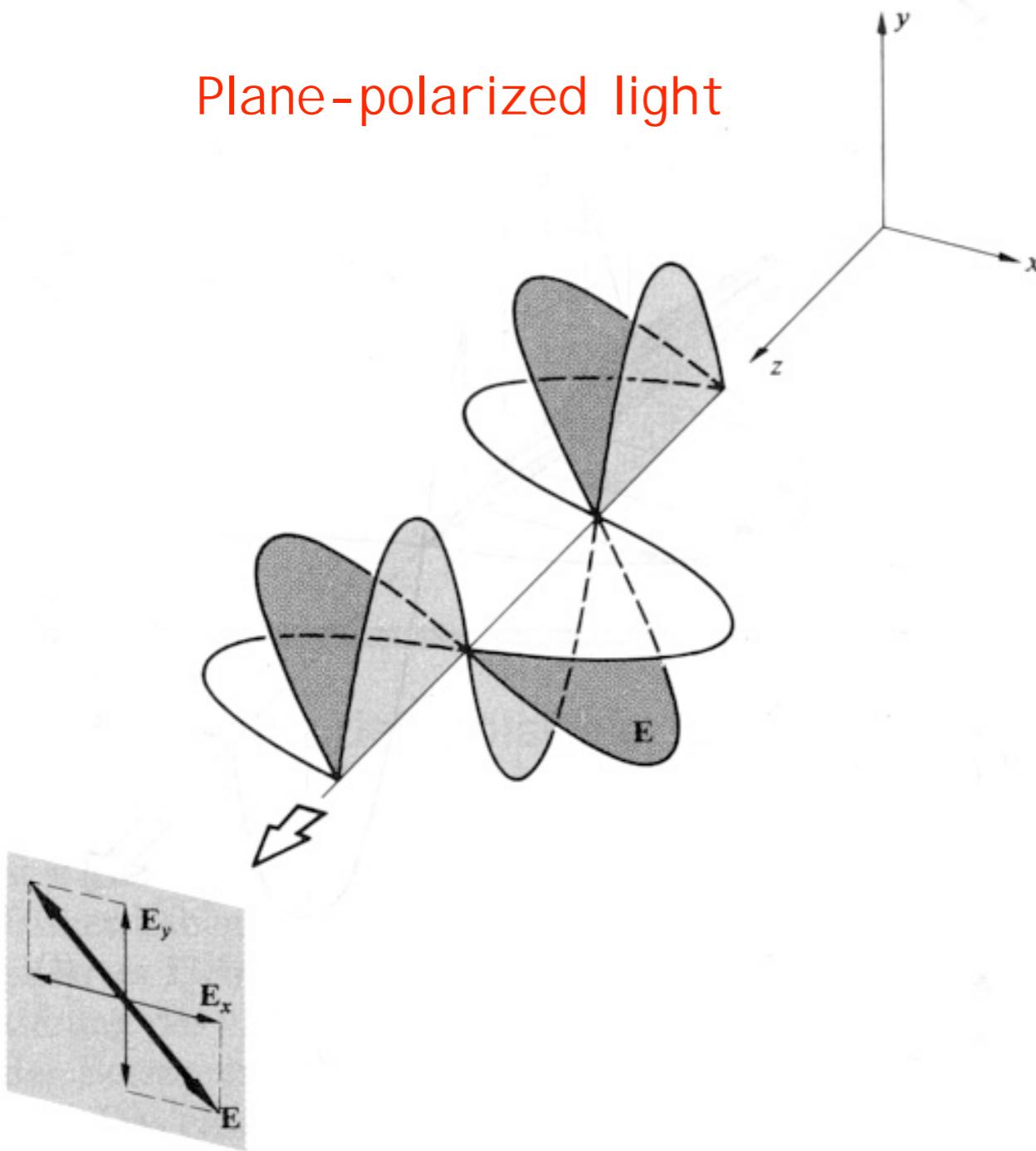
Michael Faraday
(1791-1867)

small change of polarization plane due to
magneto-optic interaction in transmission,
circular birefringence, $\sim M$

Fowler and Fryer,
1956

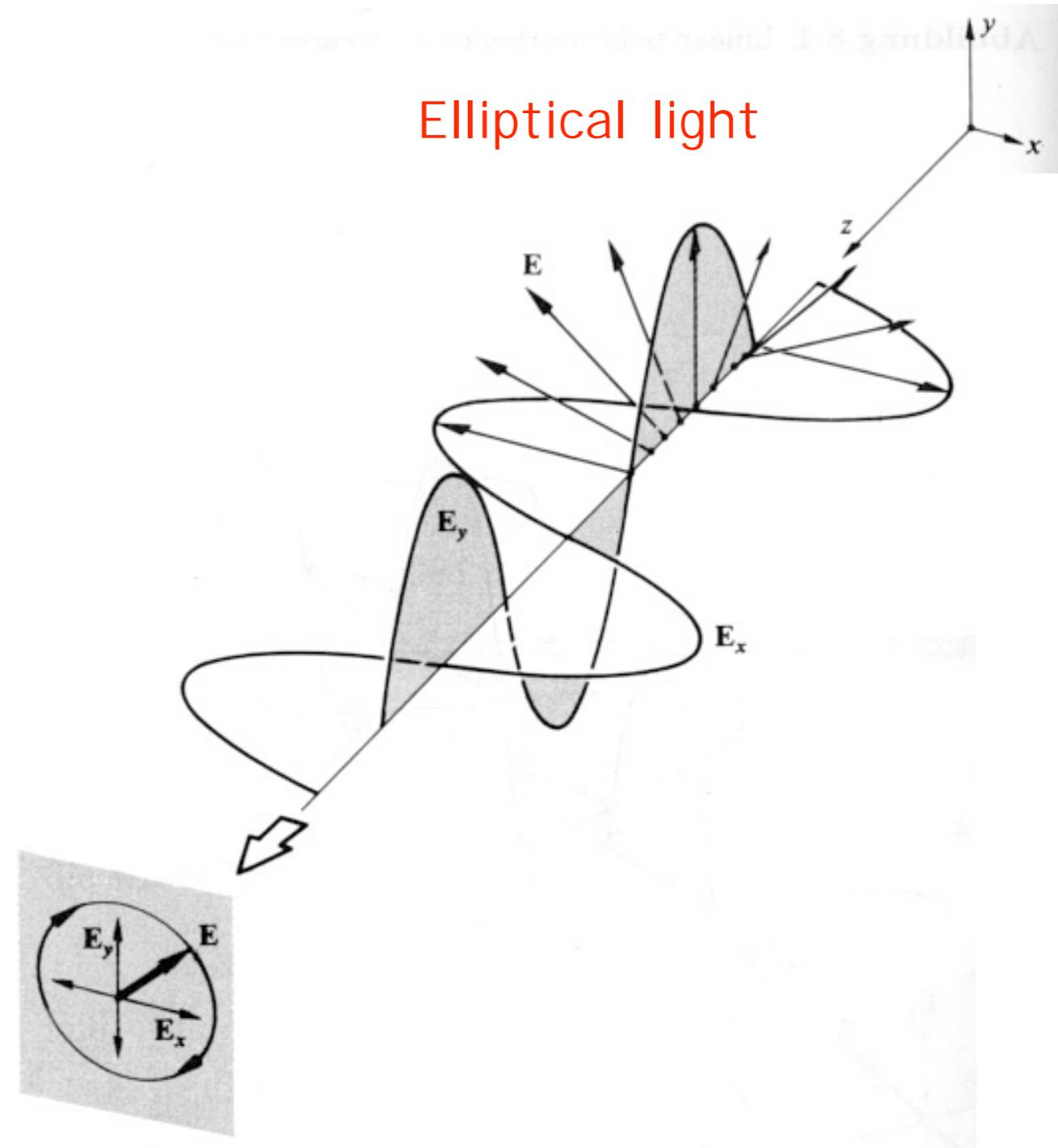
About polarized light

Plane-polarized light



superposition of two orthogonal transverse waves of equal phase

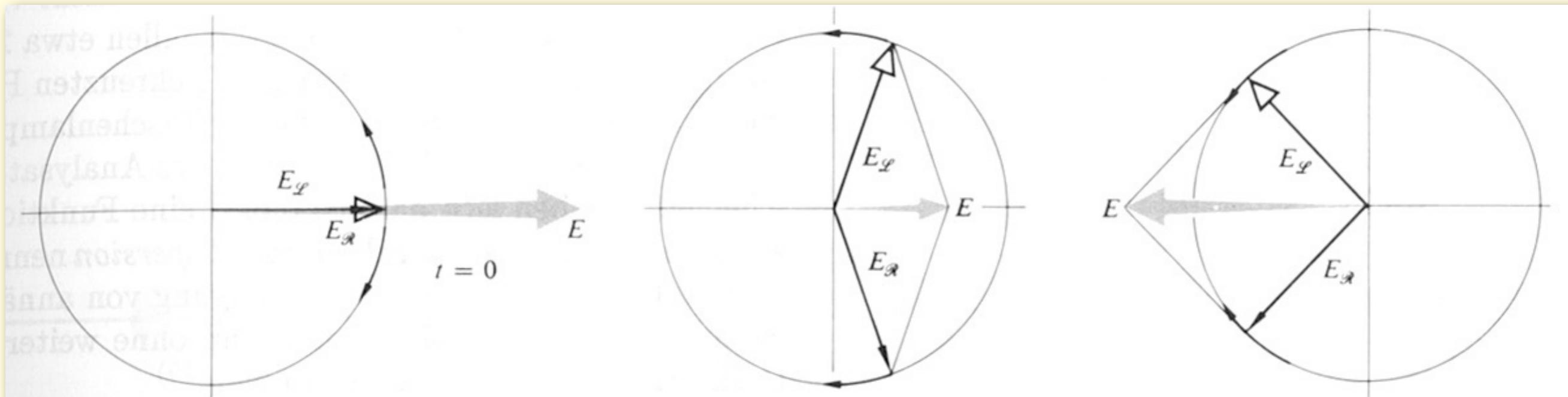
Elliptical light



superposition of two orthogonal transverse waves of different phase

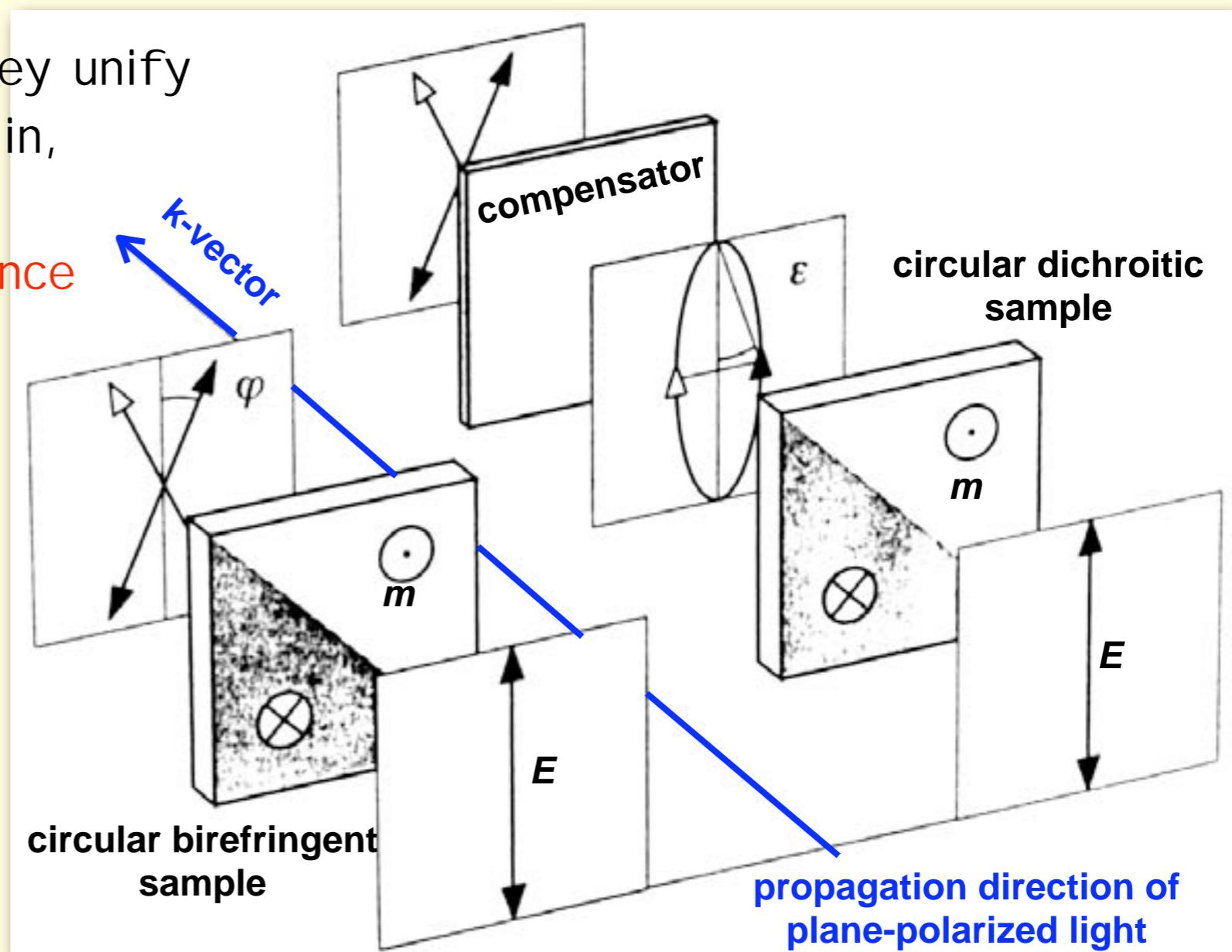
About polarized light

Linearly polarized light =
superposition of two circular waves of opposite rotation sense
and equal frequency

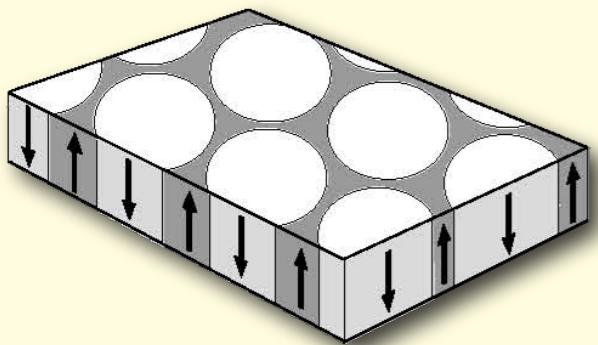


Circular birefringence

- if sample is illuminated parallel to the magnetization vector ($k \parallel m$), the light wave can only propagate in two circularly polarized modes of opposite rotation sense
- due to the magnetization, both circular modes feel different refraction indices
 - both modes propagate with different velocities
 - modes are shifted in phase
 - after leaving the sample they unify to plane-polarized wave again, which is rotated
 - **circular magnetic birefringence** (Faraday rotation)
- if also absorption:
 - both modes are damped differently
 - elliptical wave
 - **circular magnetic dichroism** (Faraday ellipticity)

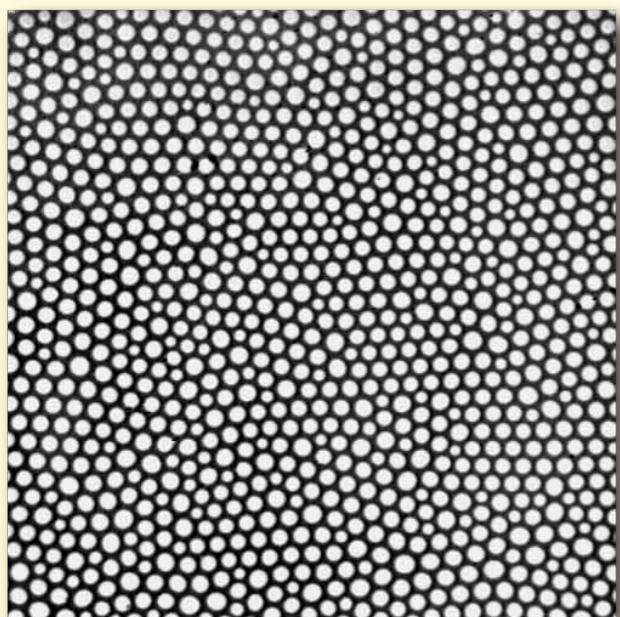


Faraday microscopy in transparent films

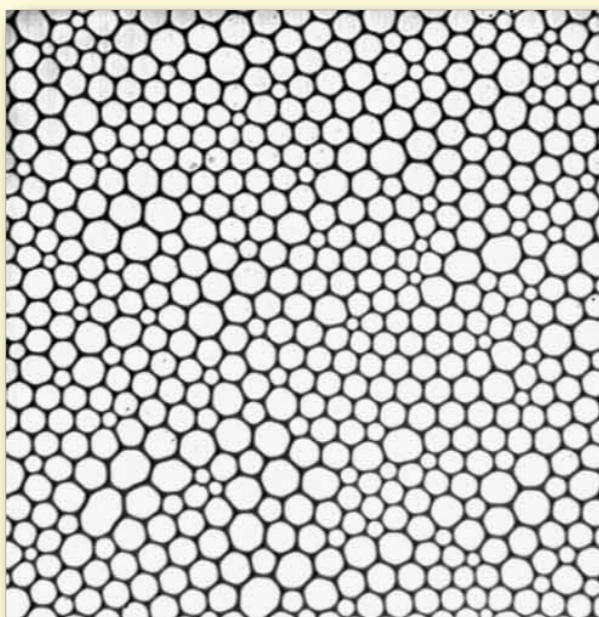


Yttrium iron garnet film
5 μm thick

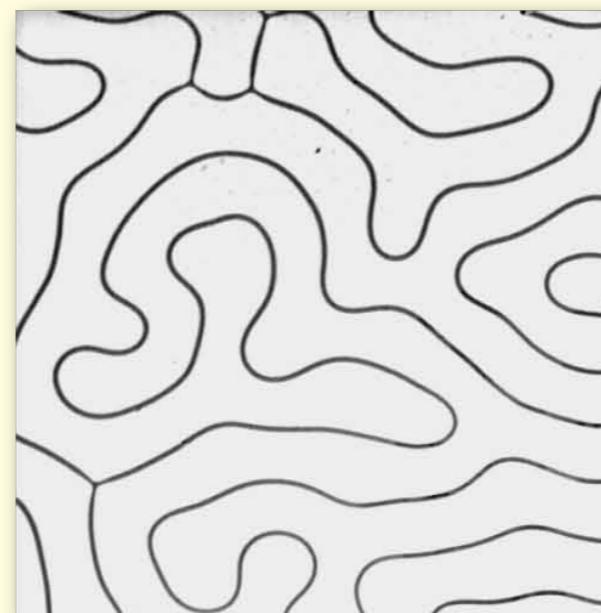
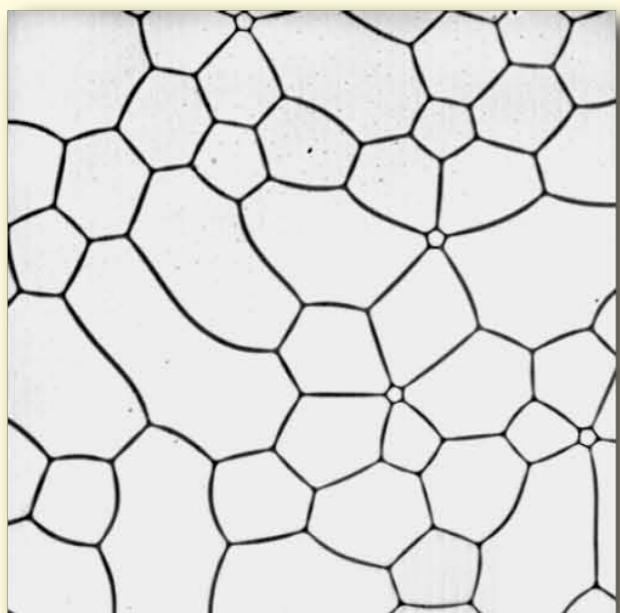
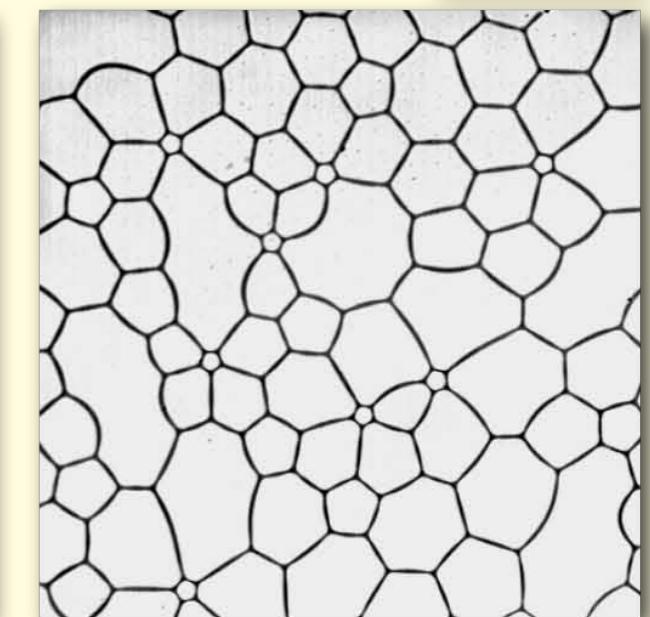
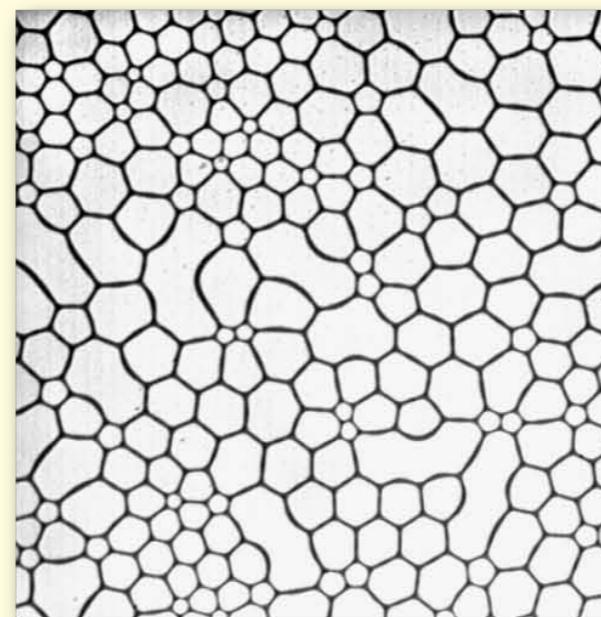
50 μm



zero field



increasing field



decreasing field

zero field

Magneto-optical microscopy: history



Michael Faraday
(1791-1867)

small change of polarization plane due to magneto-optic interaction in transmission,
circular birefringence, $\sim M$

Fowler and Fryer,
1956



John Kerr
(1824-1907)

small change of polarization plane due to magneto-optic interaction in reflection,
circular birefringence, $\sim M$

Williams et al.,
1951;

Fowler and Fryer,
1952



W. Voigt
(1850-1919)

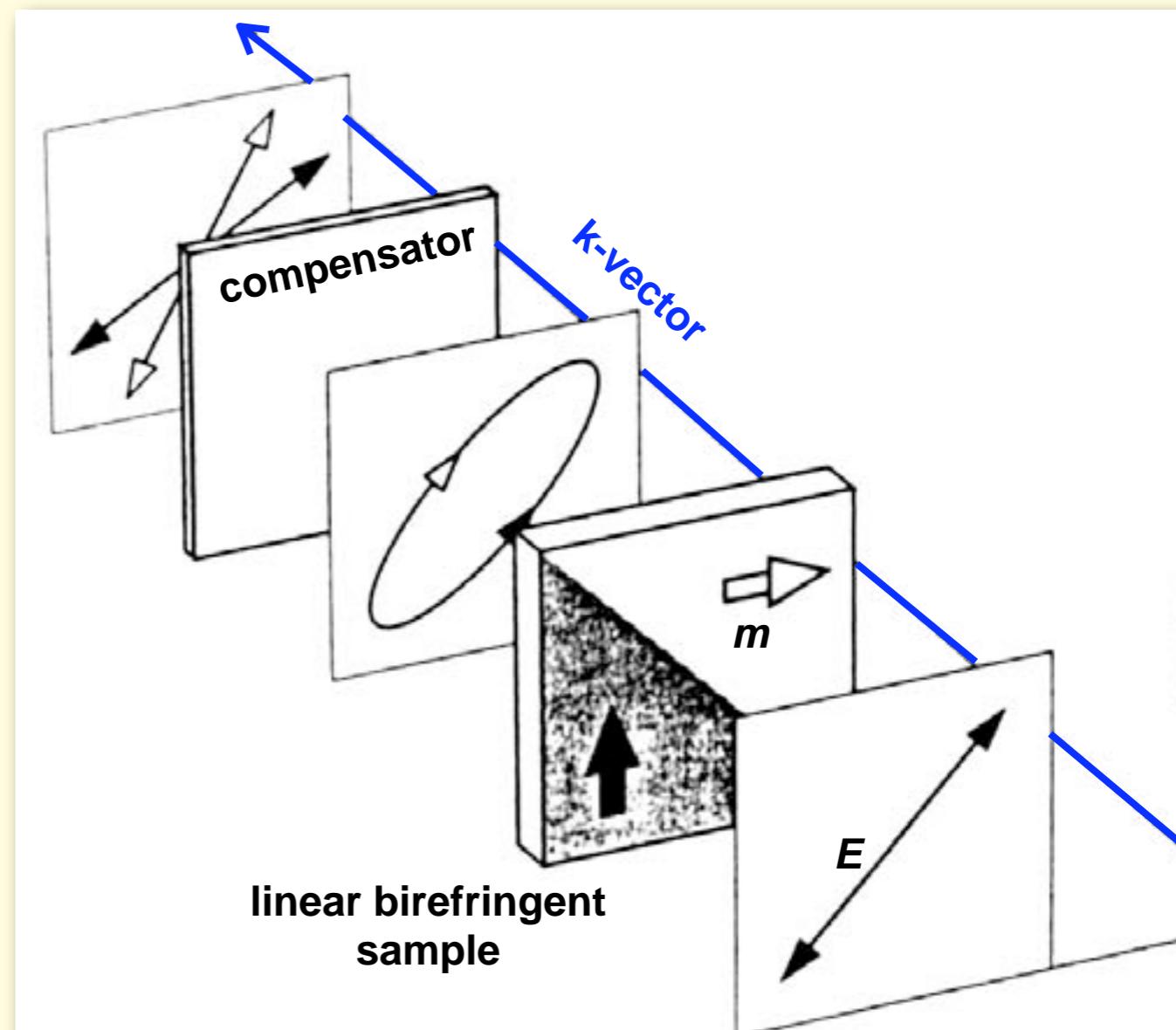
small change of polarization state due to magneto-optic interaction in reflection,
linear birefringence, $\sim M^2$

Dillon,
1958

Schäfer and Hubert,
1990

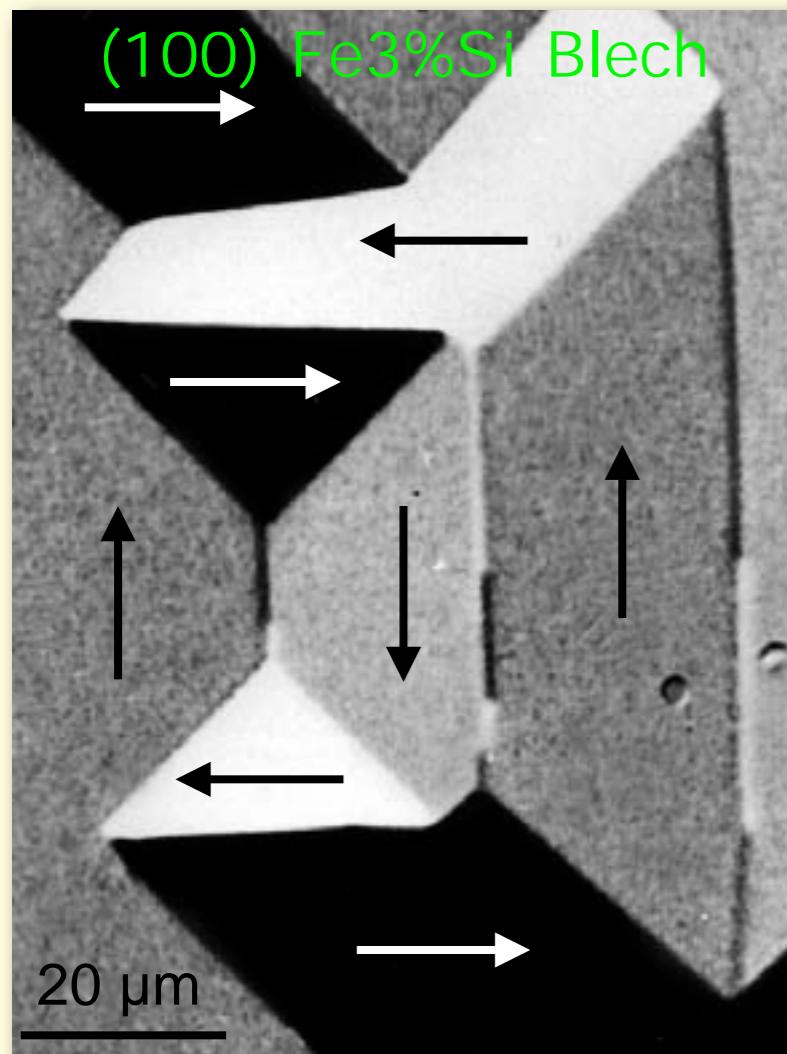
Linear birefringence

- if sample is illuminated perpendicular to magnetization vector ($k \perp m$), the light wave can only propagate in two linearly polarized modes of orthogonal pol. direction
- one plane is along m , the other perpendicular to m
- due to the magnetization, both plane modes feel different refraction indices
 - both modes propagate with different velocities
 - modes are shifted in phase
 - after leaving the sample they unify to elliptical wave
 - linear magnetic birefringence (Voigt effect)
- requires compensator due to ellipticity



Kerr-, Voigt- und Gradient Effects

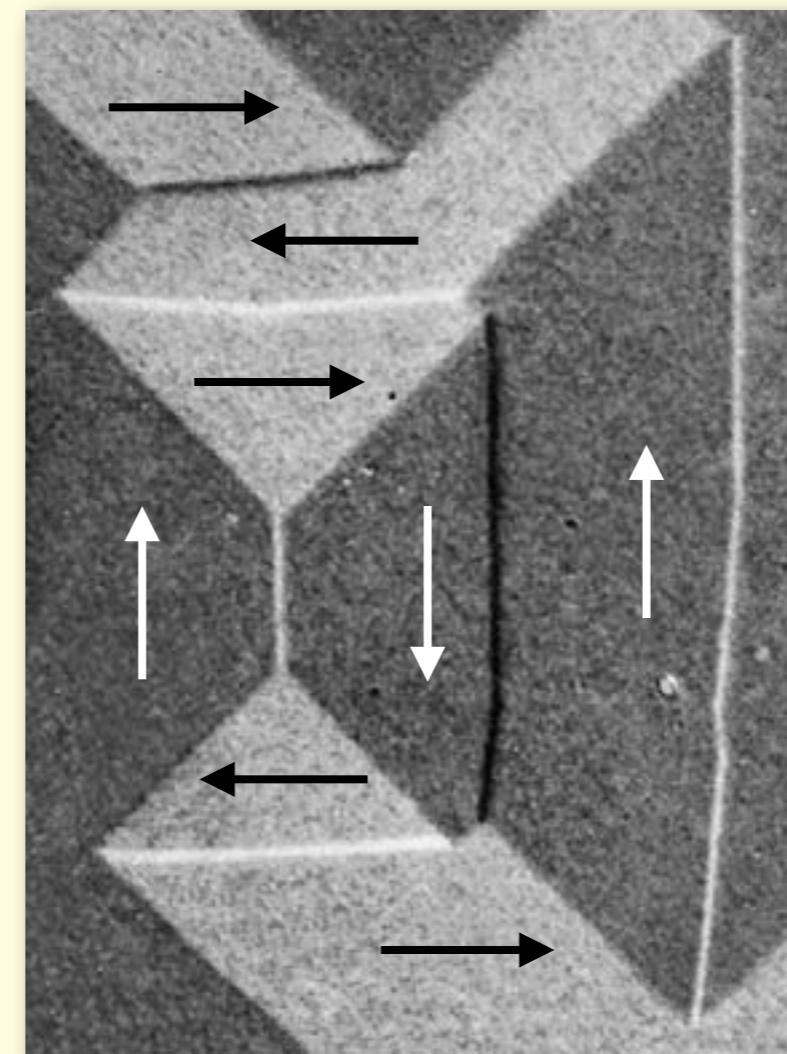
Kerr Effect



|| polarizer

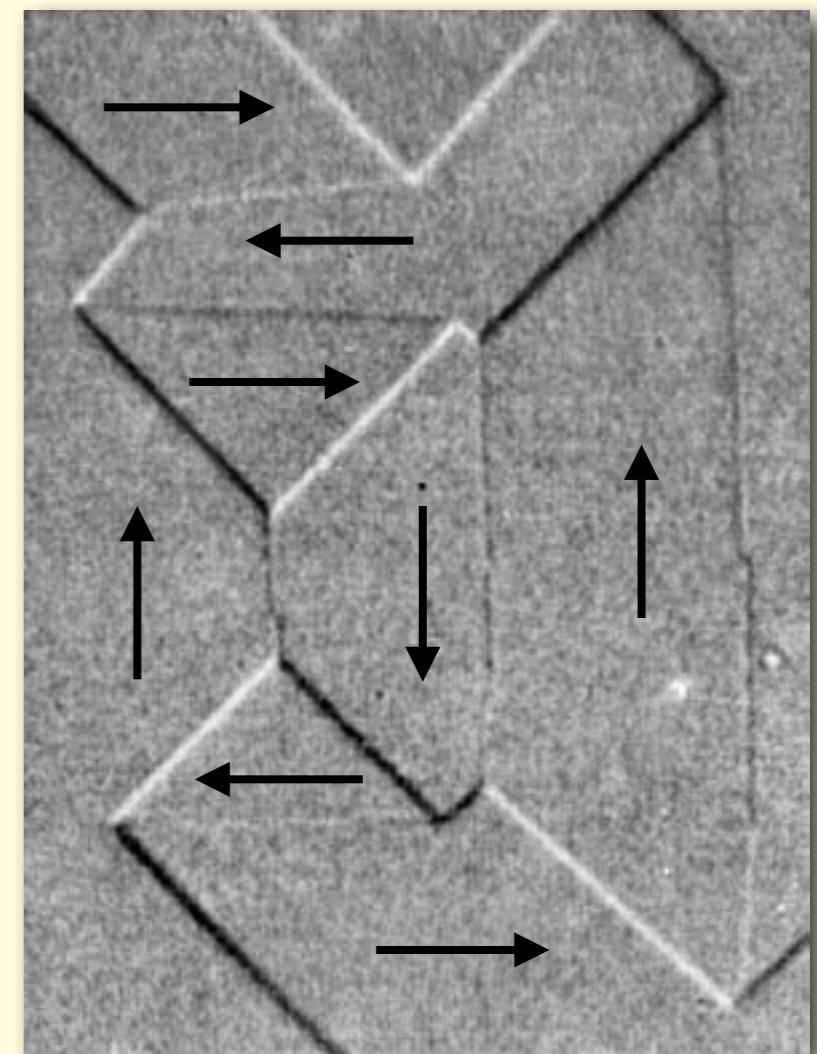
oblique incidence

Voigt and Gradient Effect



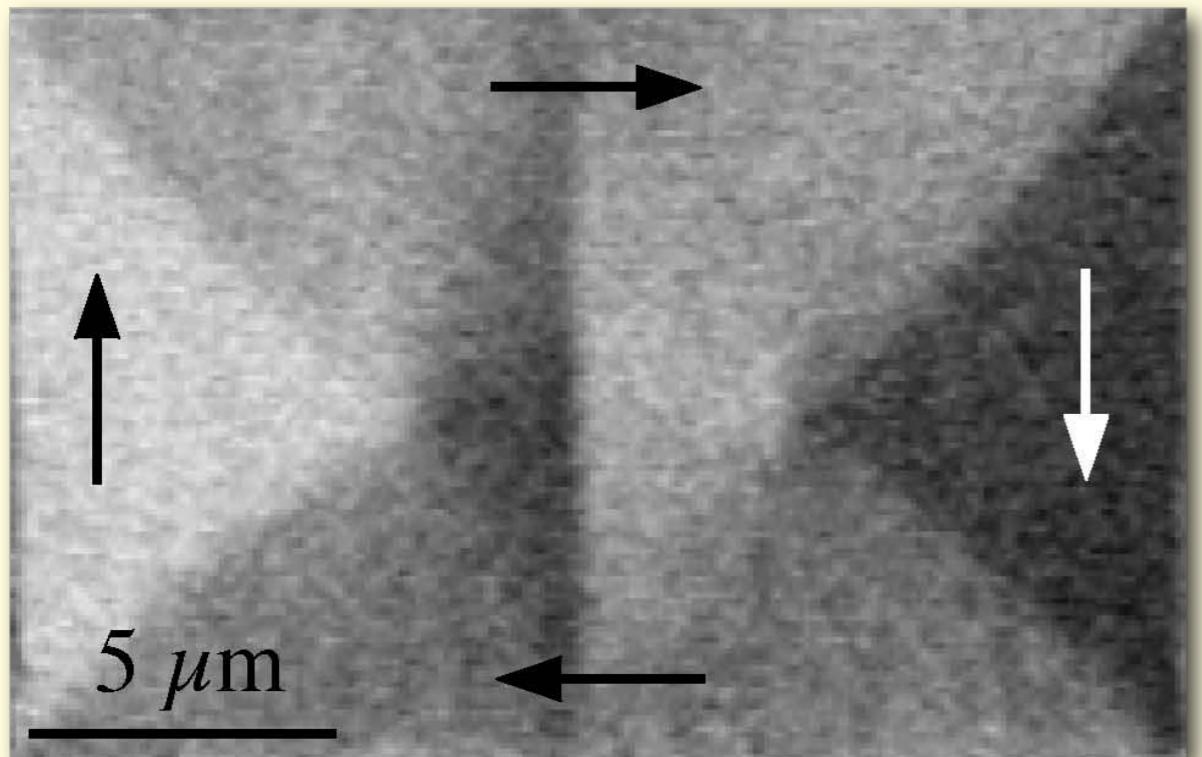
 polarizer

perpendicular incidence,
compensator



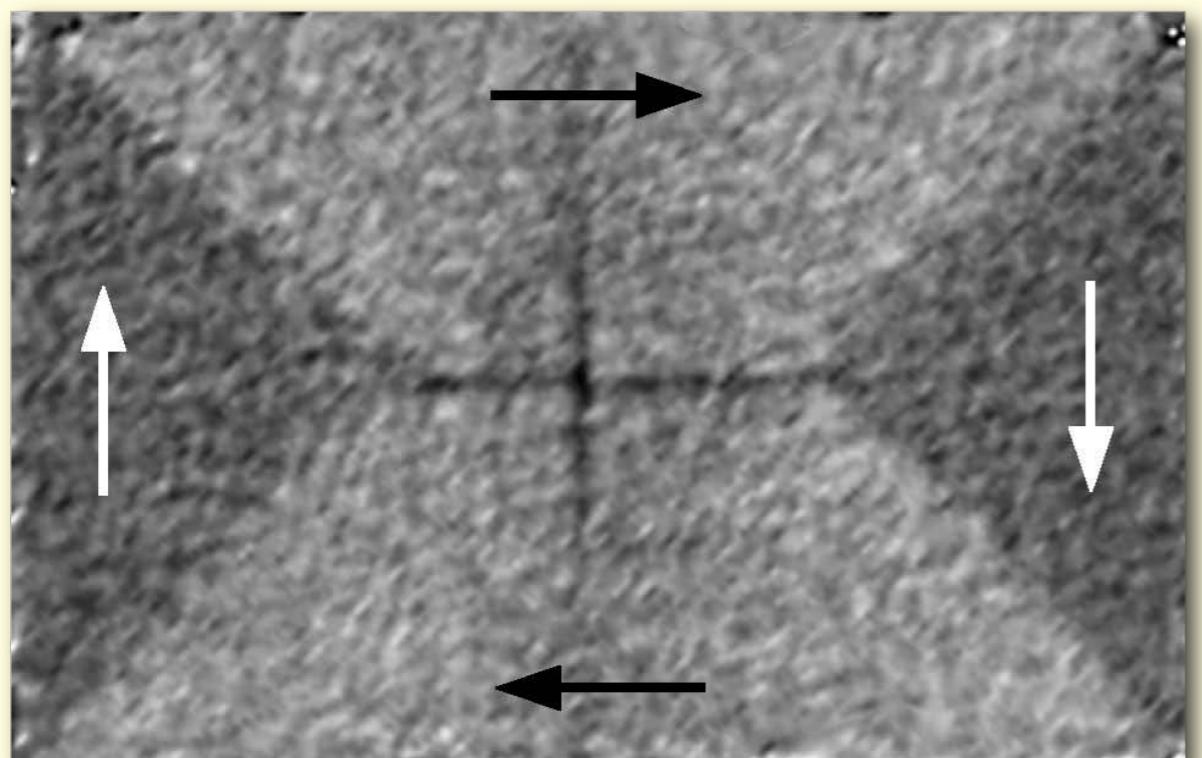
|| polarizer

Kerr-, Voigt- und Gradient Effects



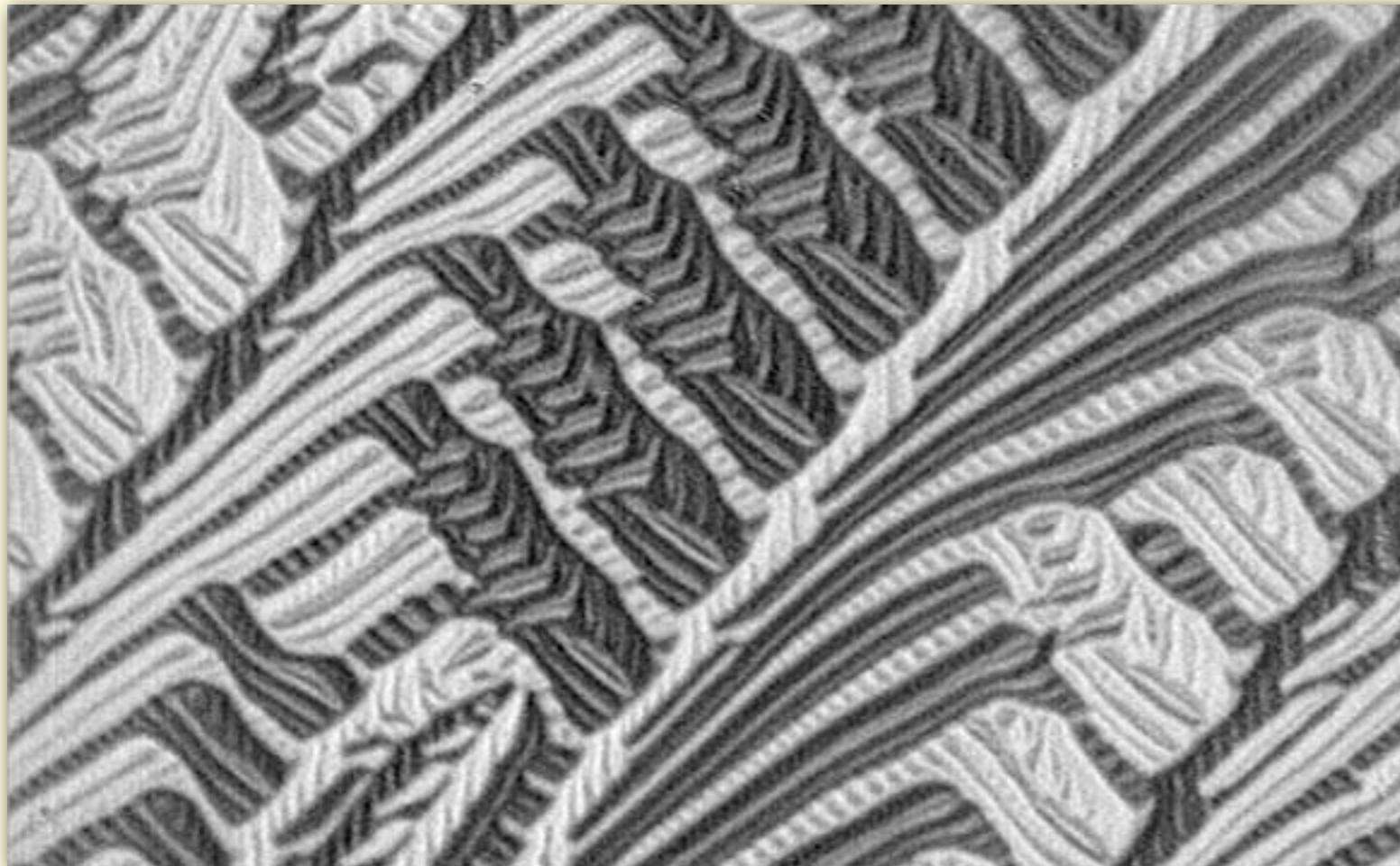
Kerr Effect

crosstie wall in
NiFe-film (50 nm thick)



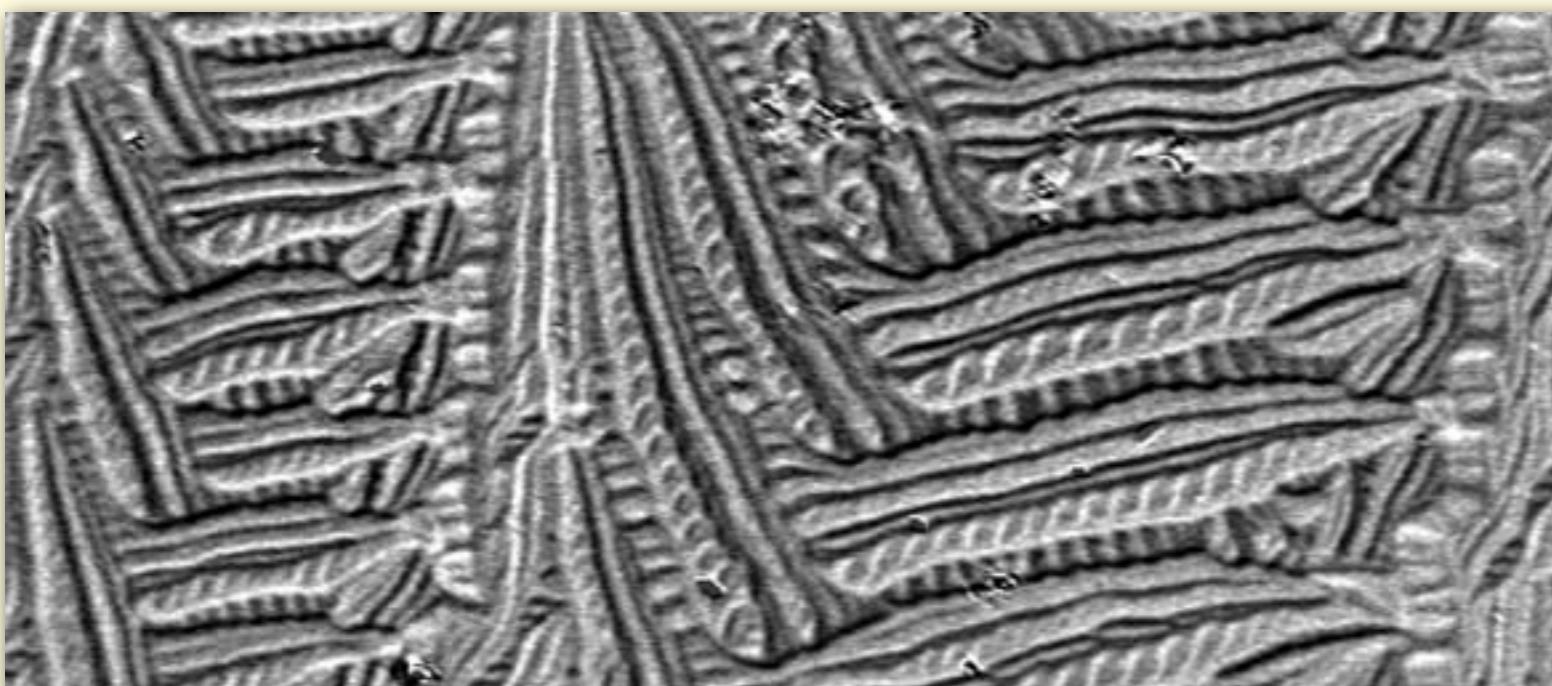
Voigt- and
Gradient-Effect

Application of Gradient effect



FeSi (111) surface

Kerr-
contrast



Gradient-
Contrast

10 μm