

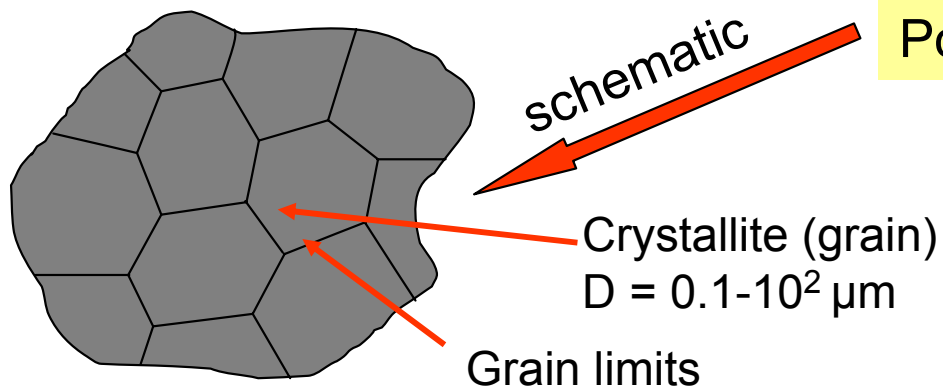
SOFT MAGNETIC NANOCRYSTALLINE/NANOSTRUCTURED MATERIALS PRODUCED BY MECHANICAL ALLOYING ROUTES



Ionel Chicinaș

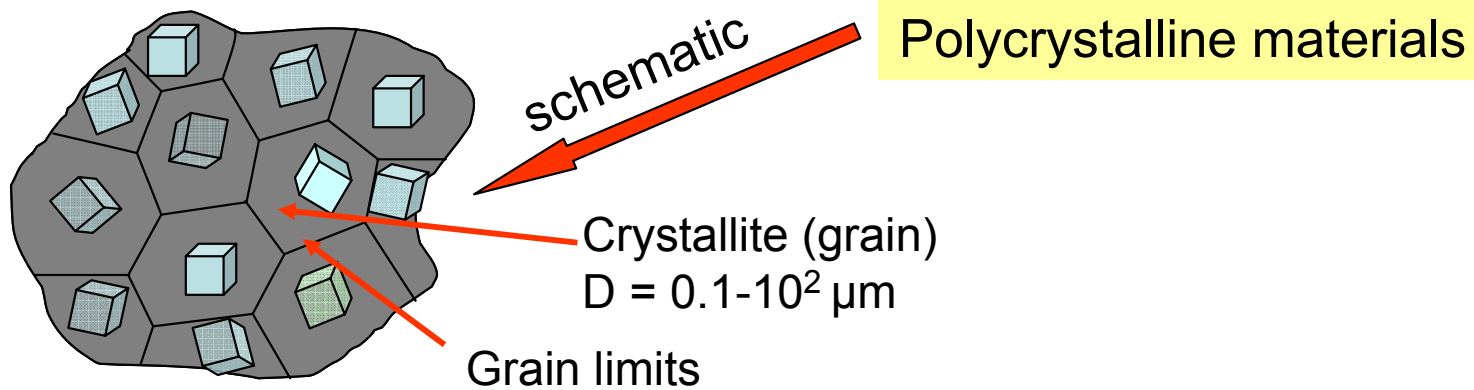
Department of Materials Science and Technology,
Technical University of Cluj-Napoca, Romania

What are Nanocrystalline Materials ?

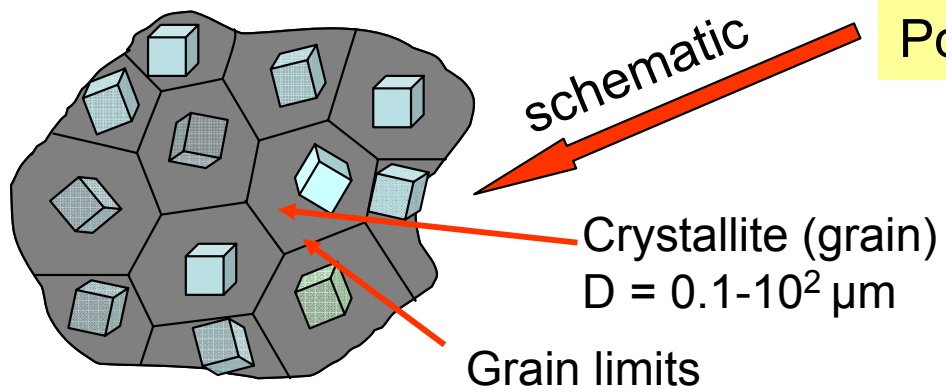


Polycrystalline materials

What are Nanocrystalline Materials ?

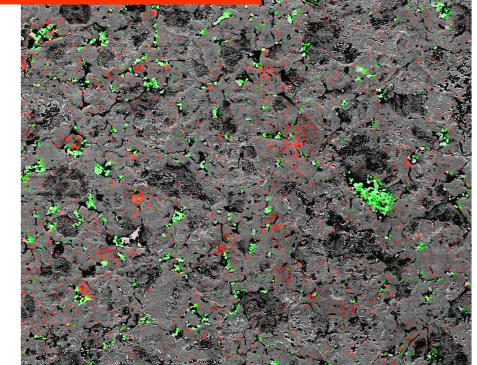
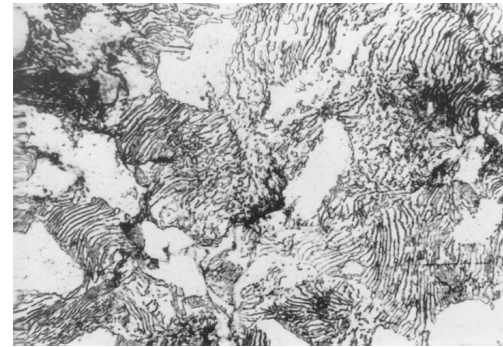


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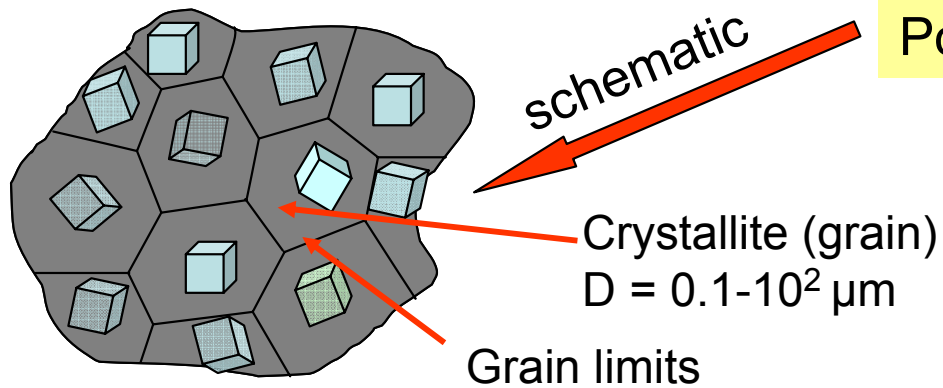


Polycrystalline materials

Real images

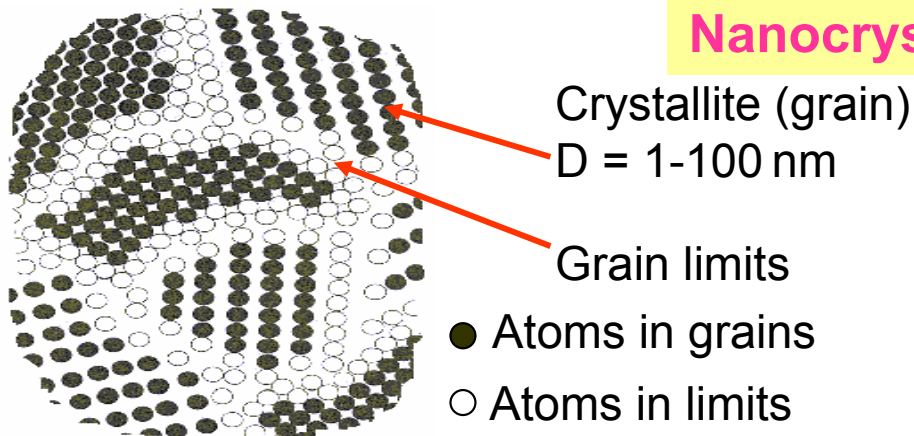
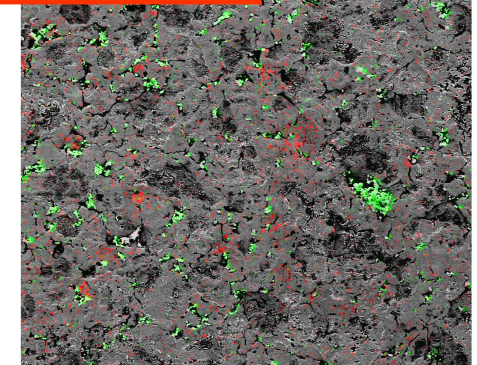
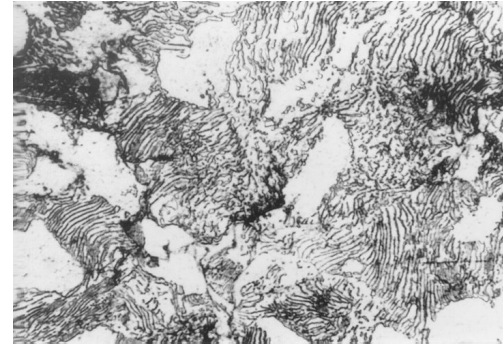


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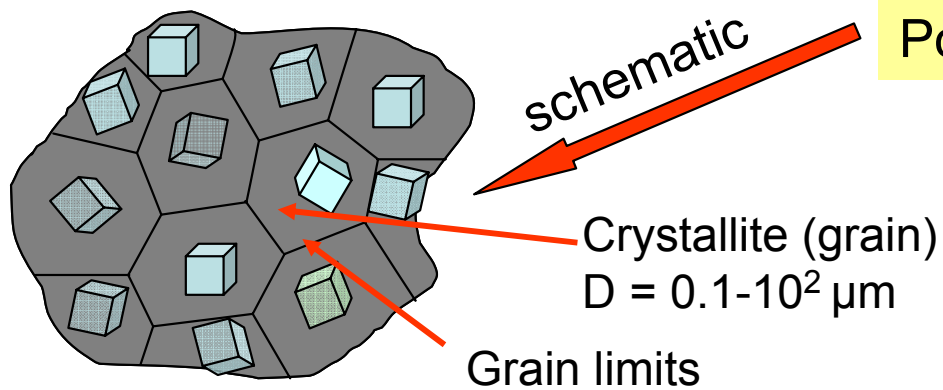


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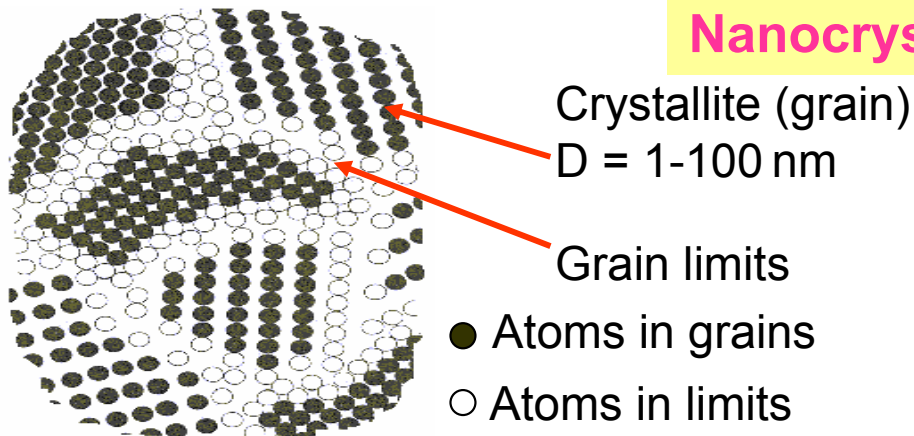
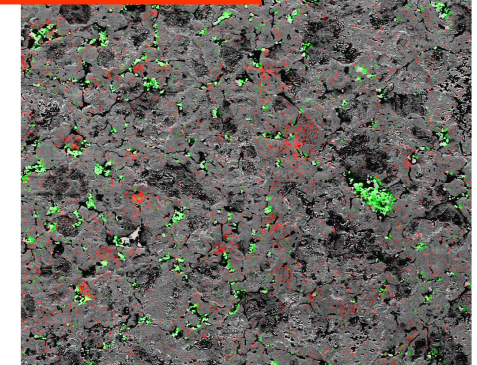
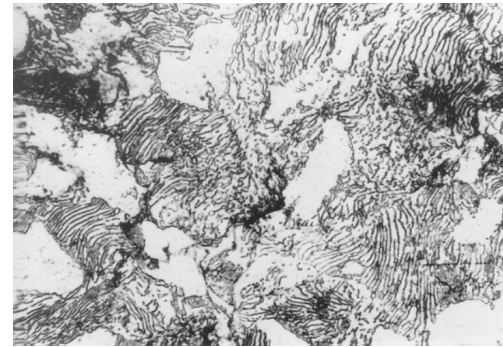


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Polycrystalline materials

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Nanocrystalline materials

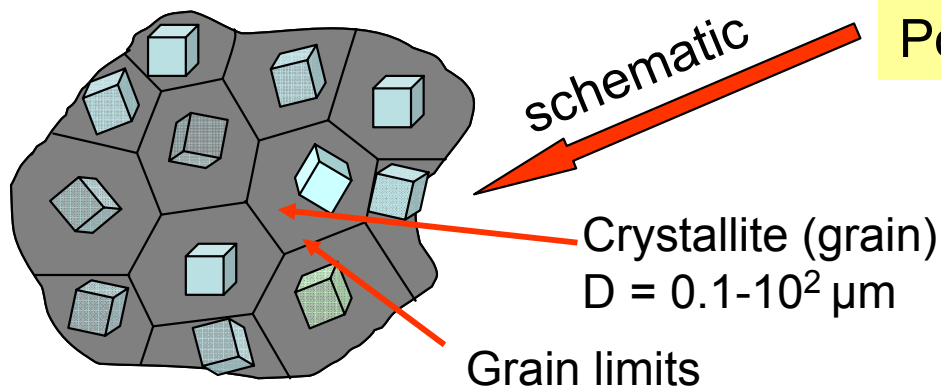
Fraction of atoms in limits

$$F = \frac{3 \Delta}{D}$$

Grain limit thickness

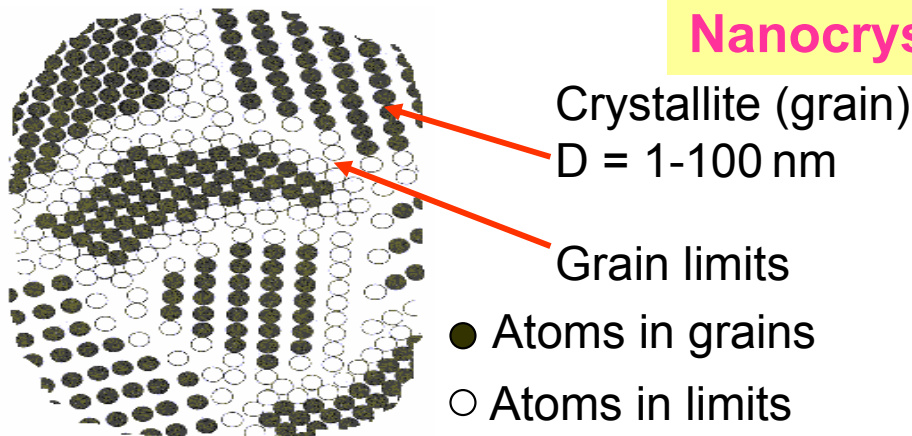
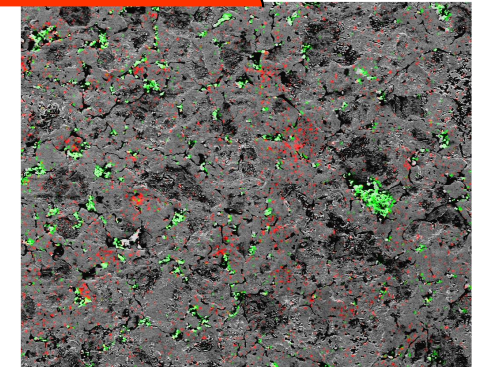
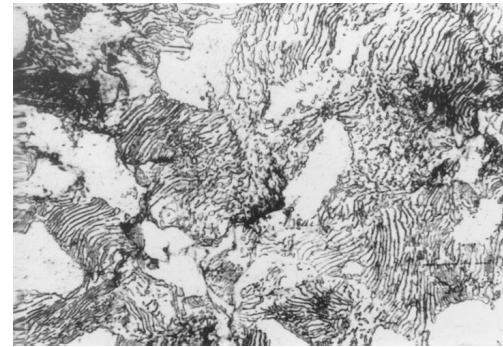
Crystallite size

What are Nanocrystalline Materials ?



Polycrystalline materials

Real images



Nanocrystalline materials

Fraction of atoms in limits

$$F = \frac{3 \Delta}{D}$$

Grain limit thickness

Crystallite size

Examples:

$D = 5 \text{ nm} \rightarrow F = 50\%$

$D = 10 \text{ nm} \rightarrow F = 30\%$

$D = 100 \text{ nm} \rightarrow F = 3\%$

Why are important Nanocrystalline Materials ?
What really means the Nanocrystalline Materials ?
When a Material is really Nano?

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What really means the Nanocrystalline Materials ?
When a Material is Nano?

For example: Coercive field H_C

depend on

intrinsic properties (anisotropy)

structure (grain size, stresses, inclusions, etc.)

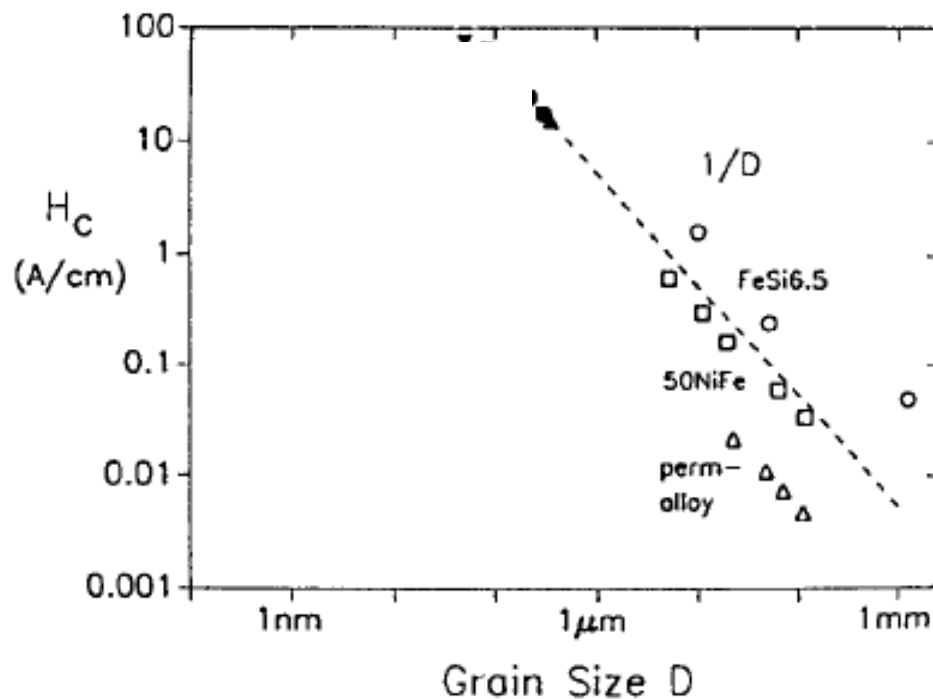
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Polycrystalline materials

H_C $\nearrow$ when D $\searrow$ and

$$H_C \sim 1/D$$

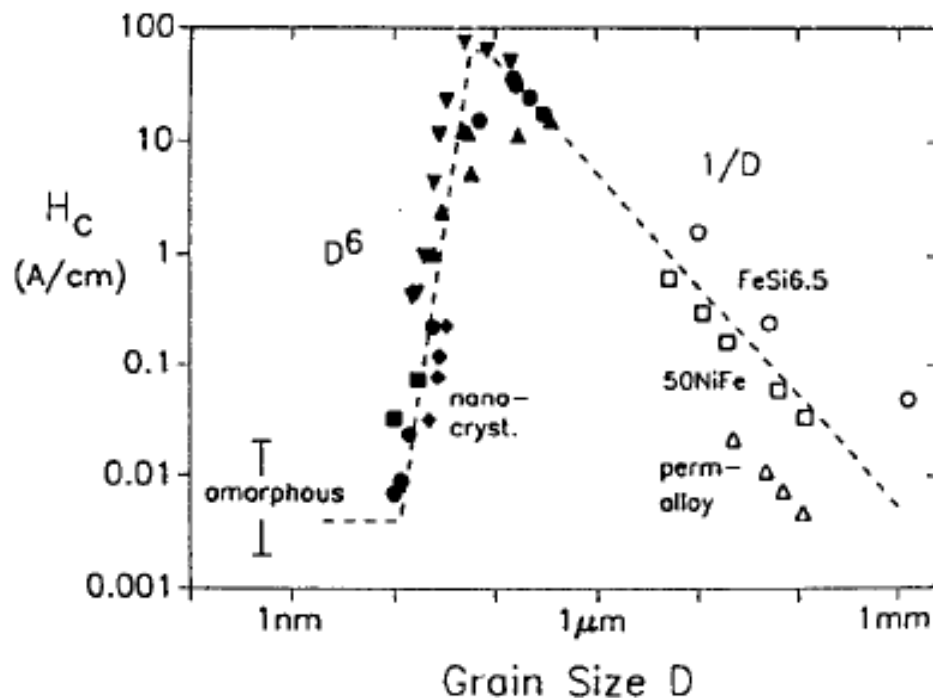
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Nanocrystalline materials

H_C $\nearrow$ when D $\searrow$ and

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G. Herzer, Scripta Metall et Mater., 33 (1995) 1741-1756.

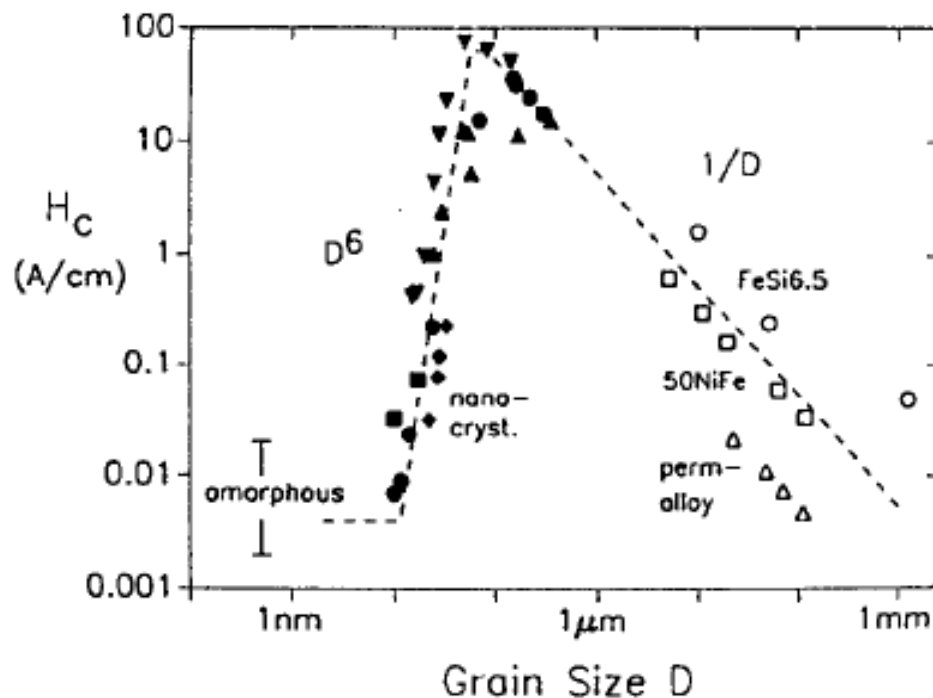
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A Material is Nanocrystalline when its Crystallite Size is lower then the Interaction Length of the considered Property!

G. Herzer, Scripta Metall et Mater., 33 (1995) 1741-1756.

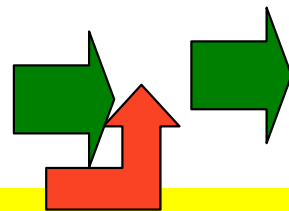
Nanocrystalline/nanostructured ($d < 100 \text{ nm}$) materials can be produced starting from:

- vapours - inert gas condensation, sputtering, plasma processing, CVD
- liquid - electrodeposition, rapid solidification
- solid - *mechanical alloying, mecanosynthese*, severe plastic deformation, spark erosion

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Mechanical alloying



Nanocrystalline/nanostructured magnetic materials

**annealing modifies
the structure and the microstructure**

Mechanical routes for producing nanocrystalline powders

What is mechanical alloying?

Mechanical routes for producing nanocrystalline powders

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Usually, we make alloys by melting together the components

Mechanical alloying (MA) involves the synthesis of materials in solid state by high-energy ball milling

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Elemental Powders Mixture



Milling in high energy ball mill

- Particles and grains are fractured
- Defects introduced in particles
- Temperature rise - diffusion

New phase

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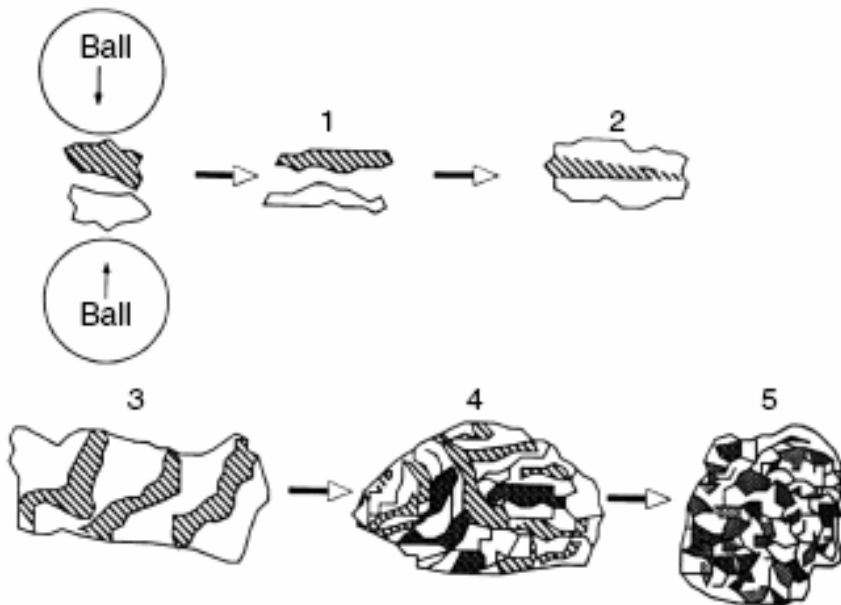
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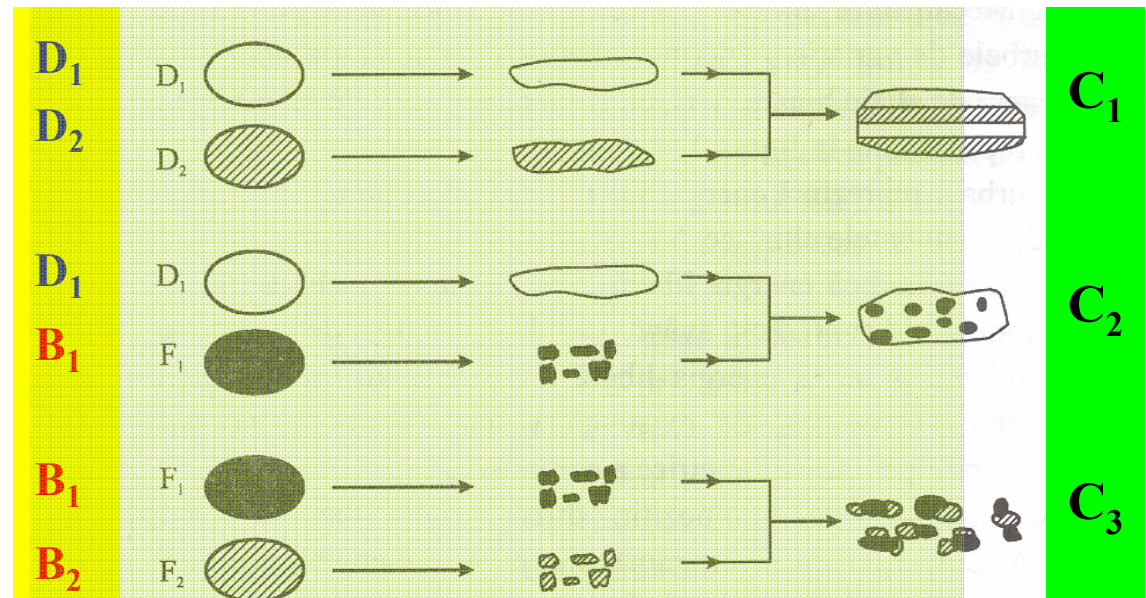
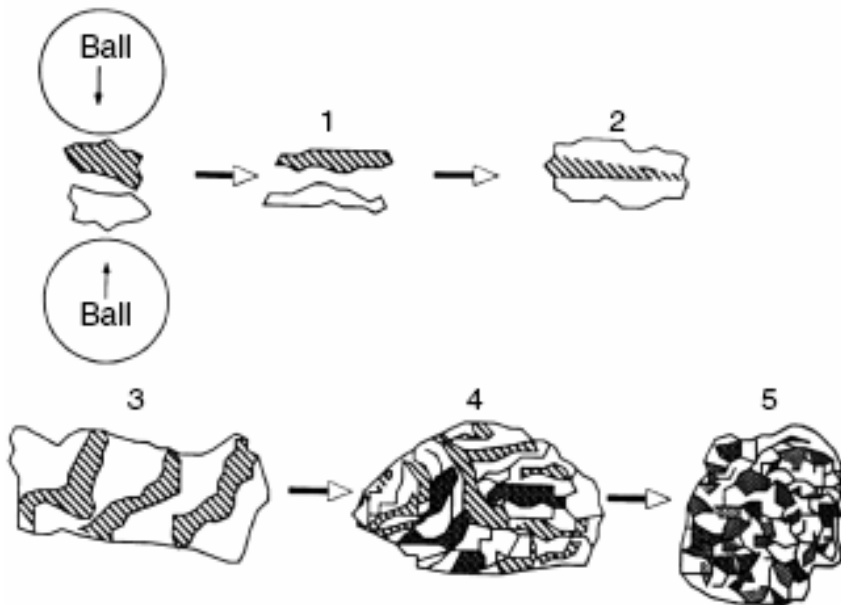
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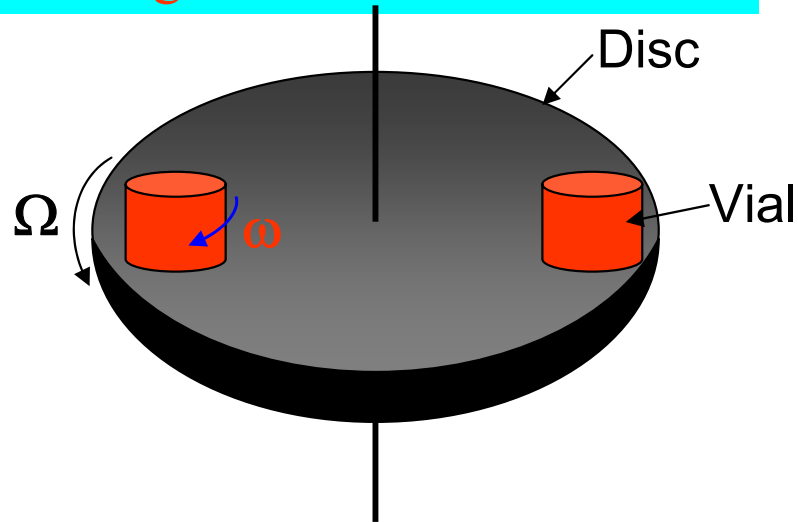
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Mechanical routes for producing nanocrystalline powders

Mechanical alloying (MA) involves the synthesis of materials by high-energy ball milling - **PROCESS**



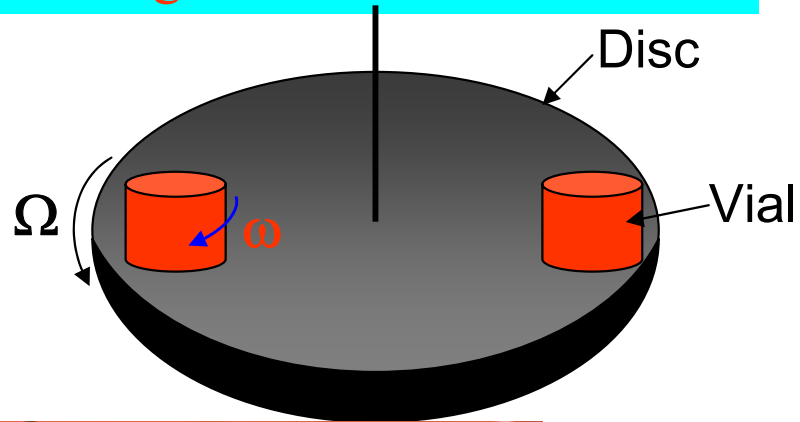
Mechanical milling (MM) refers to the process of milling pure metals or compounds without solid state reaction

$\Omega \gg \omega \rightarrow$ shock mode process (SMP)

$\Omega \ll \omega \rightarrow$ friction mode process (FMP)

Mechanical routes for producing nanocrystalline powders

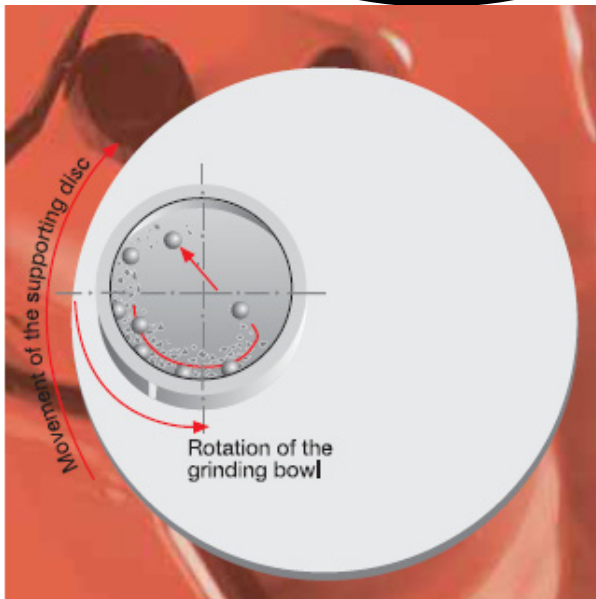
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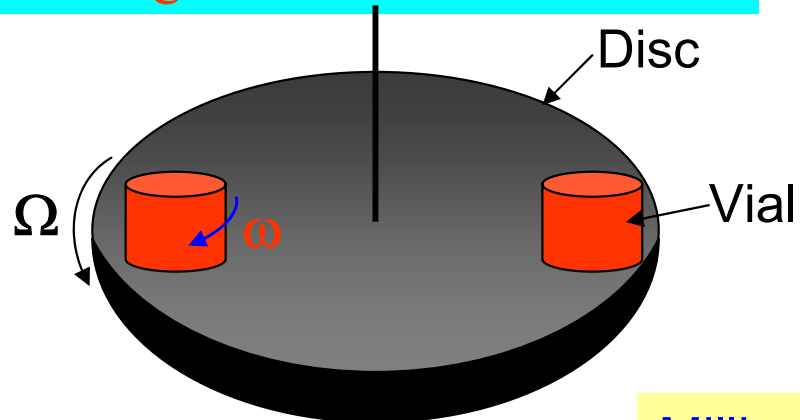
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working principle

Mechanical routes for producing nanocrystalline powders

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Milling:

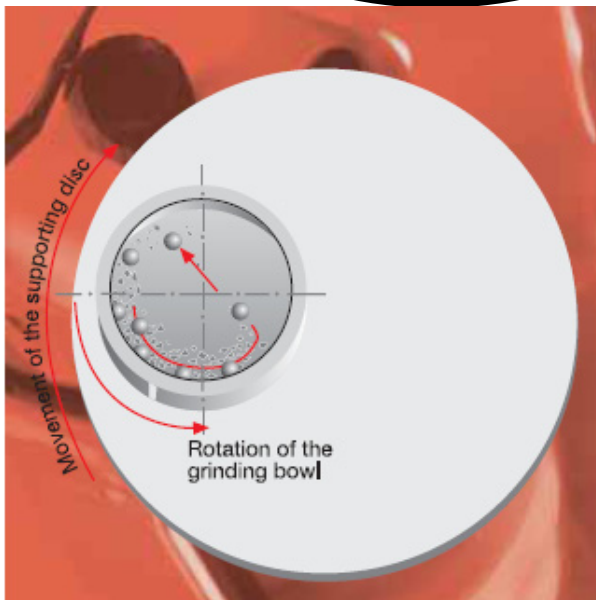
Dry milling
Wet milling
Cryomilling

Three groups of parameters were identified, depending on:

factors related to material or materials mixture subjected to milling.

Factors depending upon the milling equipment, including the milling bodies

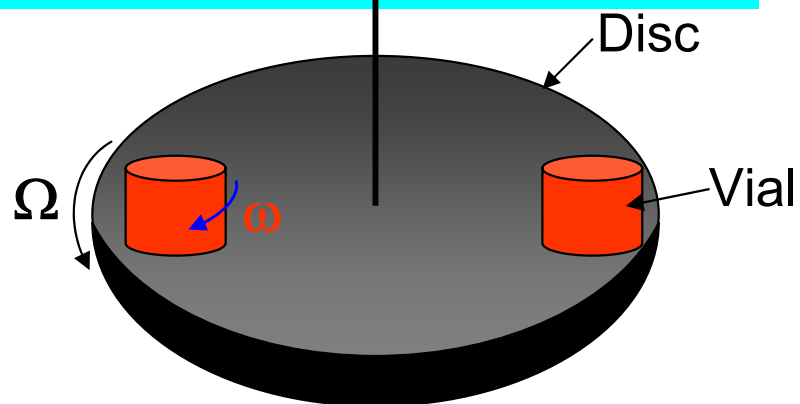
Factors depending upon processing



working principle

Mechanical routes for producing nanocrystalline powders

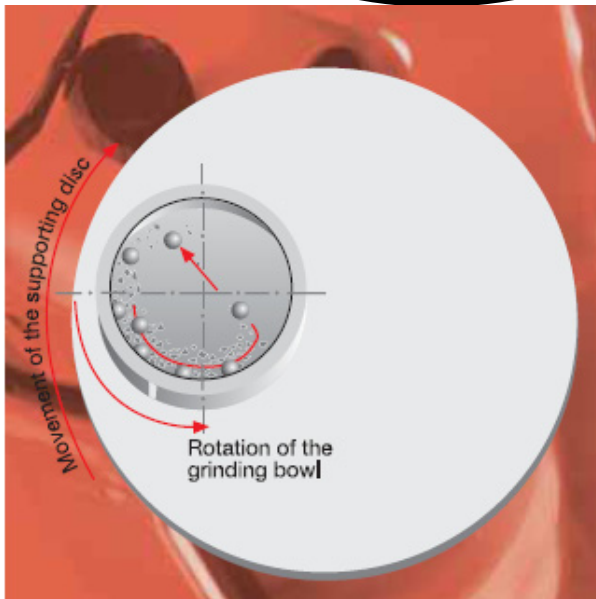
Mechanical alloying (MA) involves the synthesis of materials by high-energy ball milling - **Equipments**



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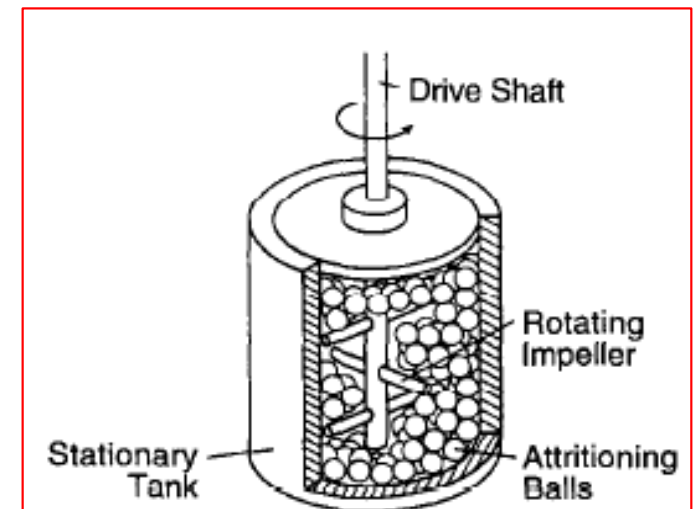
$\Omega \ll \omega \rightarrow$ friction mode process (FMP)



working principle



pulverisette 5 with 4 grinding bowl fasteners



Mechanical Alloying and Annealing Combining (MAAC) - What is this technique?

MA



Generally, synthesis of new material by MA needs a long time



Annealing the mixture milled



What's happening if we **STOP** the milling process **before the mechanical alloying finishing** and then we make an **annealing**?

V. Pop, O. Isnard and I. Chicinas, J. Alloys and Comp., **361** (2003), p.144-152.

Mechanical Alloying and Annealing Combining (MAAC) - What is this technique?

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What's happening if we **STOP** the milling
process **before the mechanical alloying**
finishing and then we make an **annealing**?

It is `possible to improve (finishing) the solid
state reaction of compound/alloy forming!

MAAC – can reduce the synthesis time!

Reactive milling (RM) Mechanochemistry (MC) (dry or wet MM)

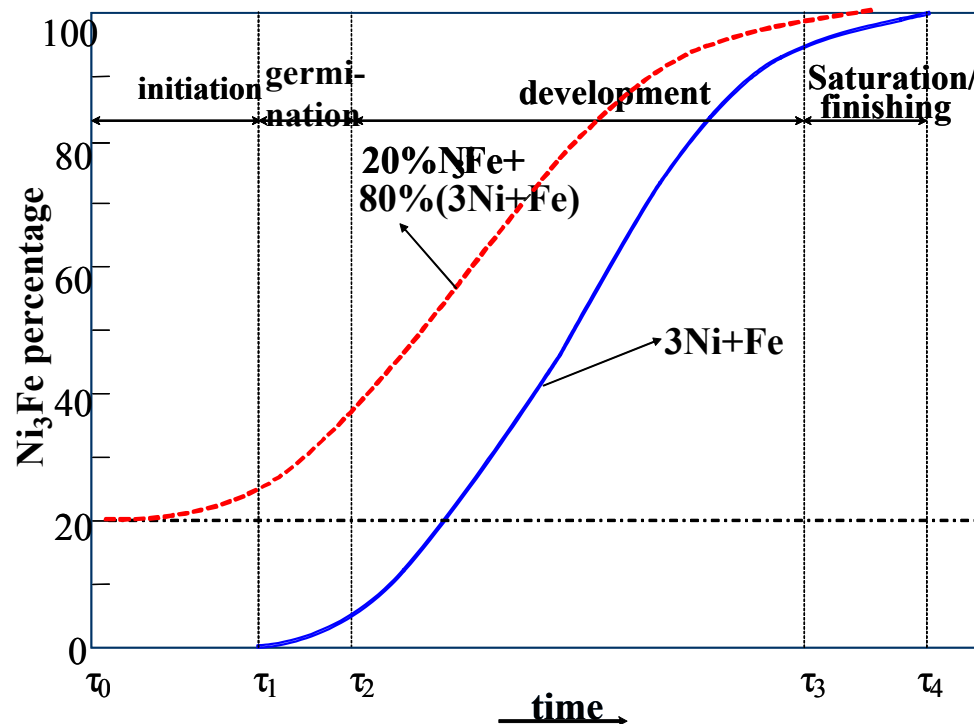
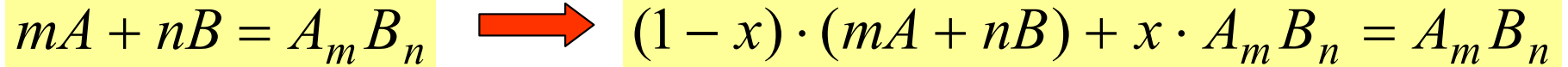
The MC consists of:

- a. reduction of the grain size below a certain value
- b. the subsequent chemical reaction towards the equilibrium phase composition under the milling conditions.

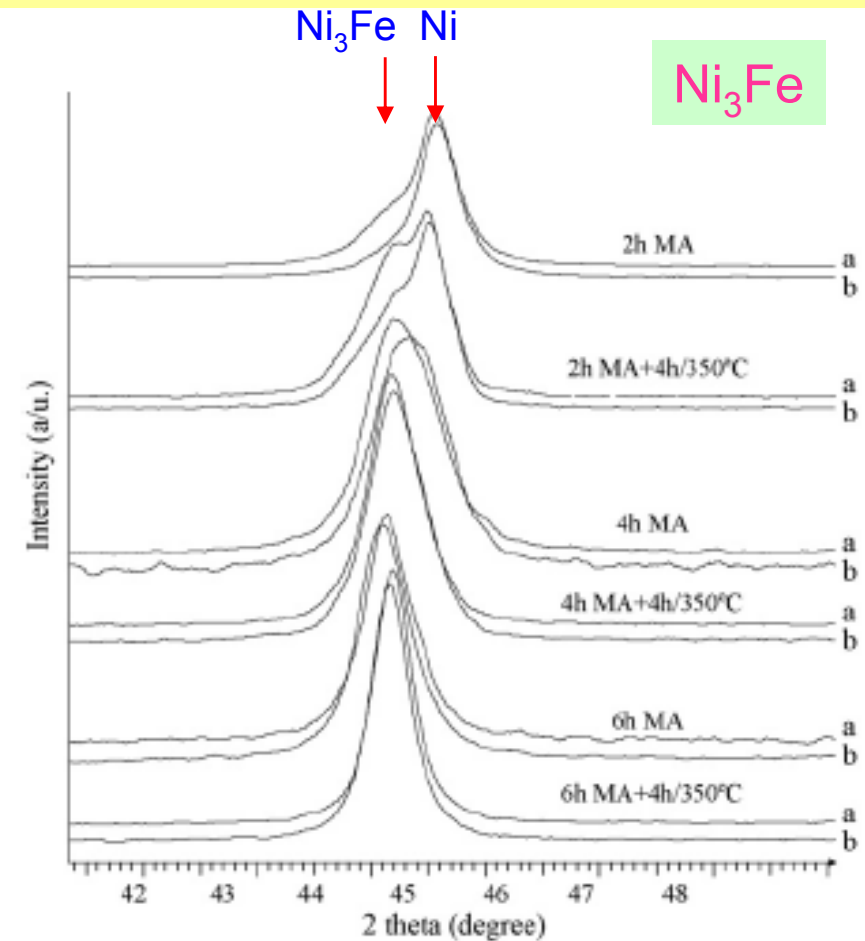
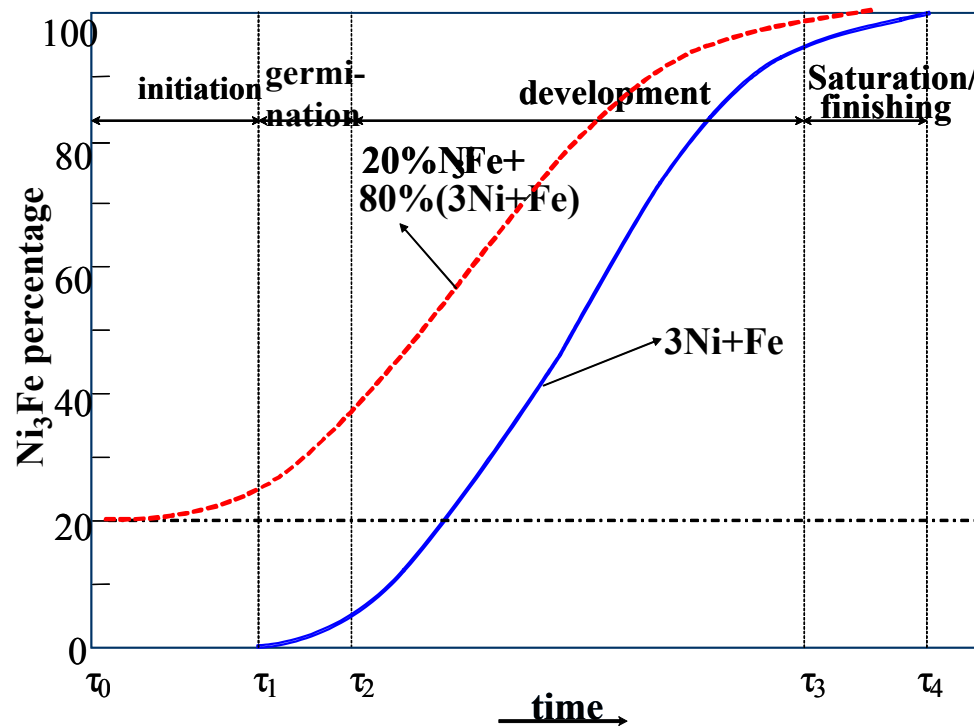
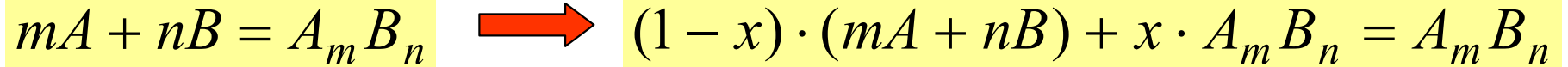


(it is applied for oxides, chlorides, sulphurs, etc.)

Mechanical Alloying in the Presence of Nanocrystalline Germs of the same Product

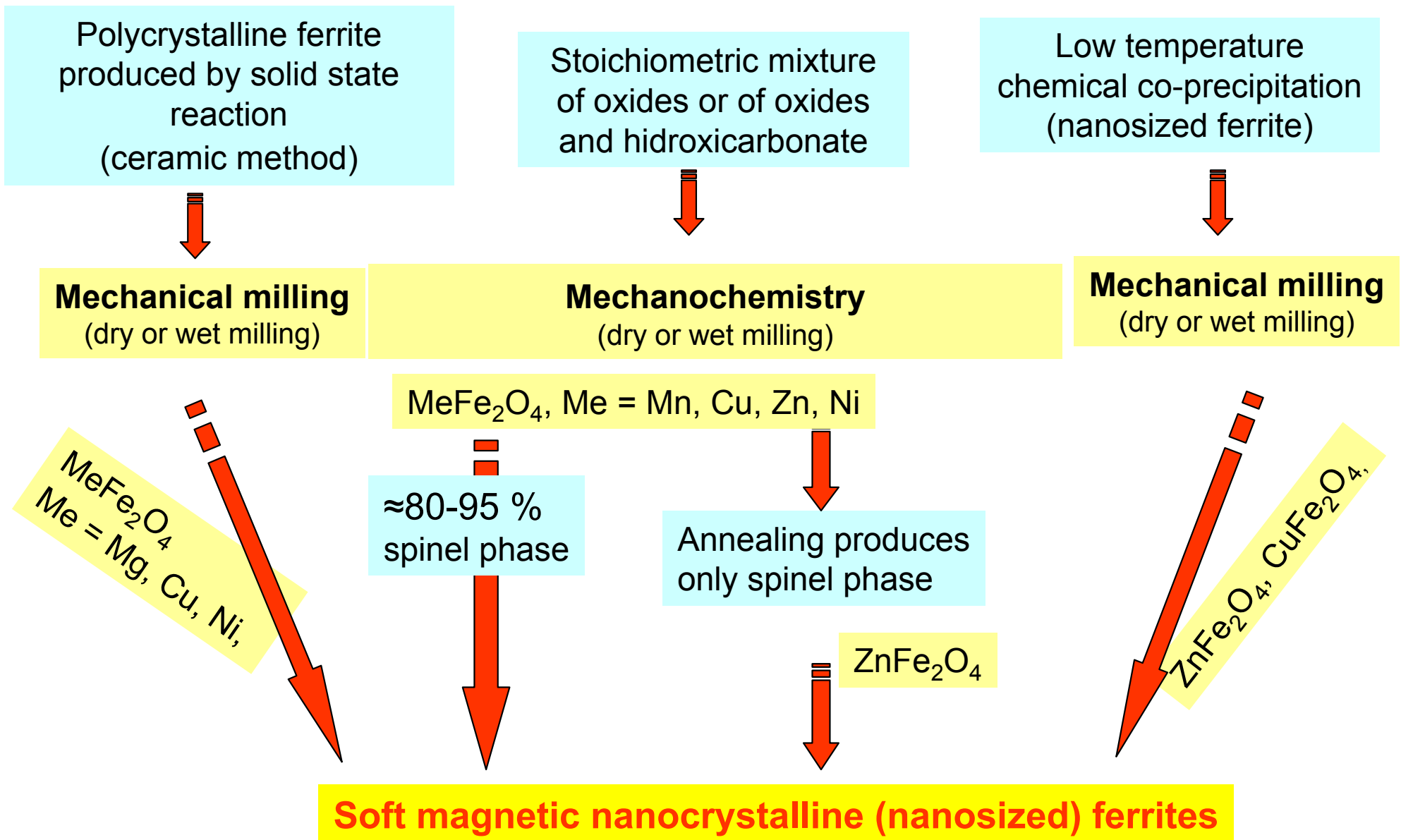


Mechanical Alloying in the Presence of Nanocrystalline Germs of the same Product



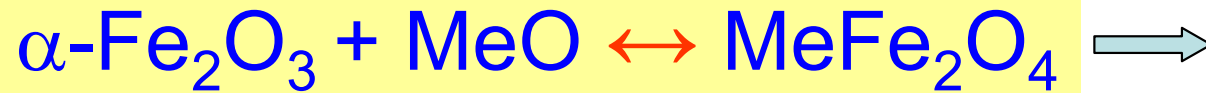
Z. Sparchez, I. Chicinas, O. Isnard, V. Pop, F. Popa, J. Alloys and Compounds, **434–435** (2007) 485–488

Mechanical routes for producing of ferrites

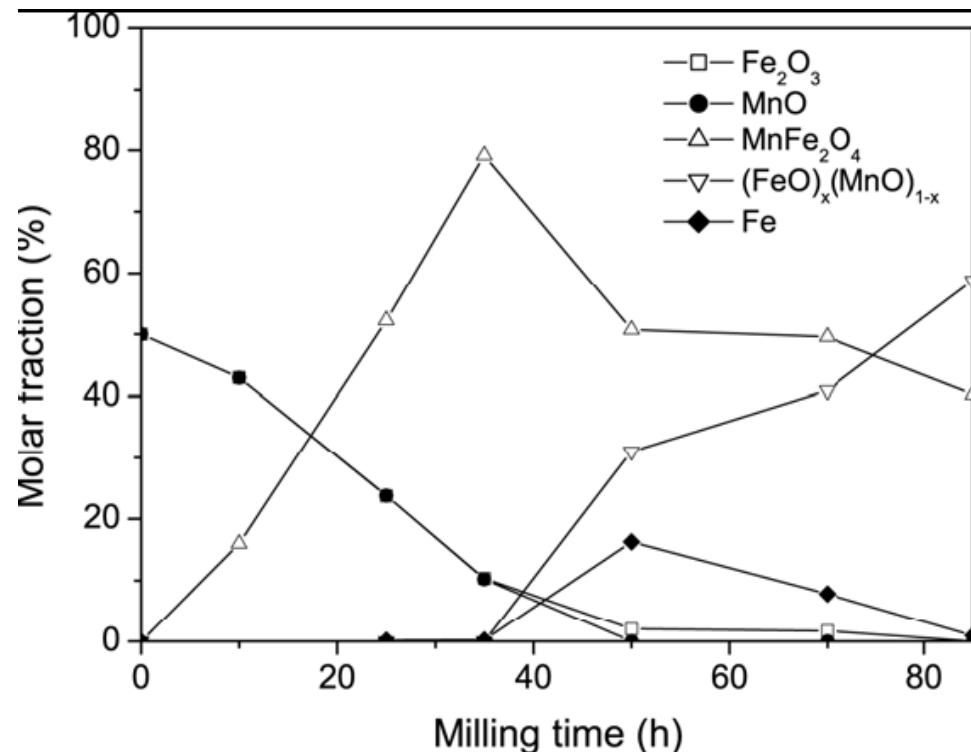


Structural properties, phase composition

Partial reversibility during milling of the reaction:



The particles contain several related Fe–Me–O phases



Milling in closed vial:
 $\alpha\text{-Fe}_2\text{O}_3$ is reduced at Fe_3O_4

Milling in open vial:
neither reduction of Fe^{3+} were detected

Particle size is generally
reduced under 10 nm

G.F. Goya, H.R. Rechenberg, J. Phys: Condens. Mater., **10** (1998) 11829-11840

G.F. Goya, H.R. Rechenberg, J.Z. Jiang, J. Appl. Phys. **84** (1998) 1101-1108

F. Padella et al. Mater. Chem. Phys. **90** (2005) 172-177

Magnetic behaviour of mechanosynthesized ferrites

The magnetic properties are associated with

the canted spin configuration in small particles

the non-equilibrium cation redistribution resulting in a decrease of the number of magnetic $\text{Fe}^{3+}(\text{A})\text{-O}^{2-}\text{-Fe}^{3+}(\text{B})$ linkages

Magnetisation does not saturate even in an applied field of 9 T
Ms decrease with milling time as a result of spin canting effect

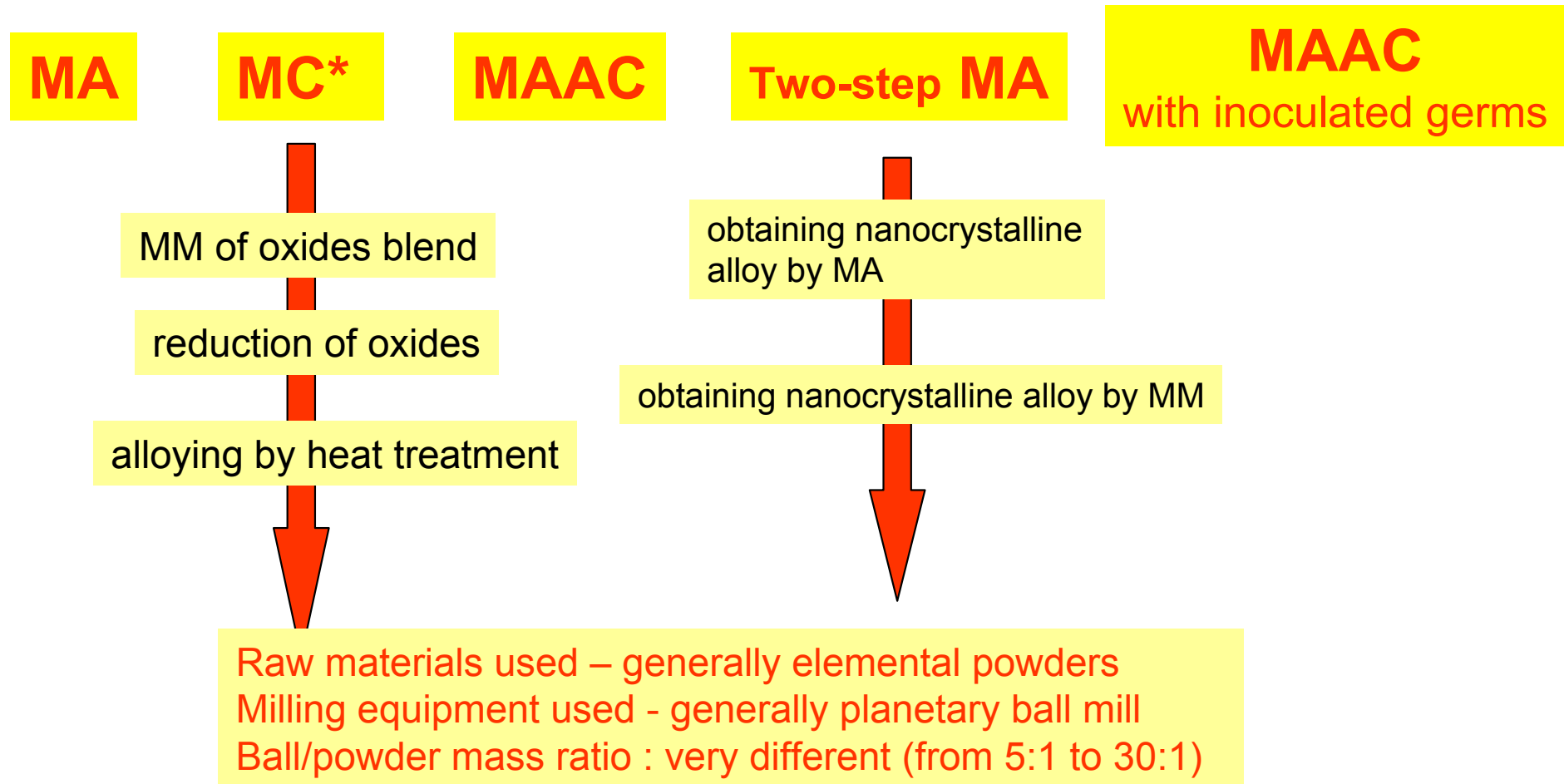
The hysteresis loop is not symmetrical about the origin and is shifted to the left



ΔH_C which increases with increasing the milling time

Coexistence of both ferrimagnetic and superparamagnetic phase

Mechanical routes used for producing SMA

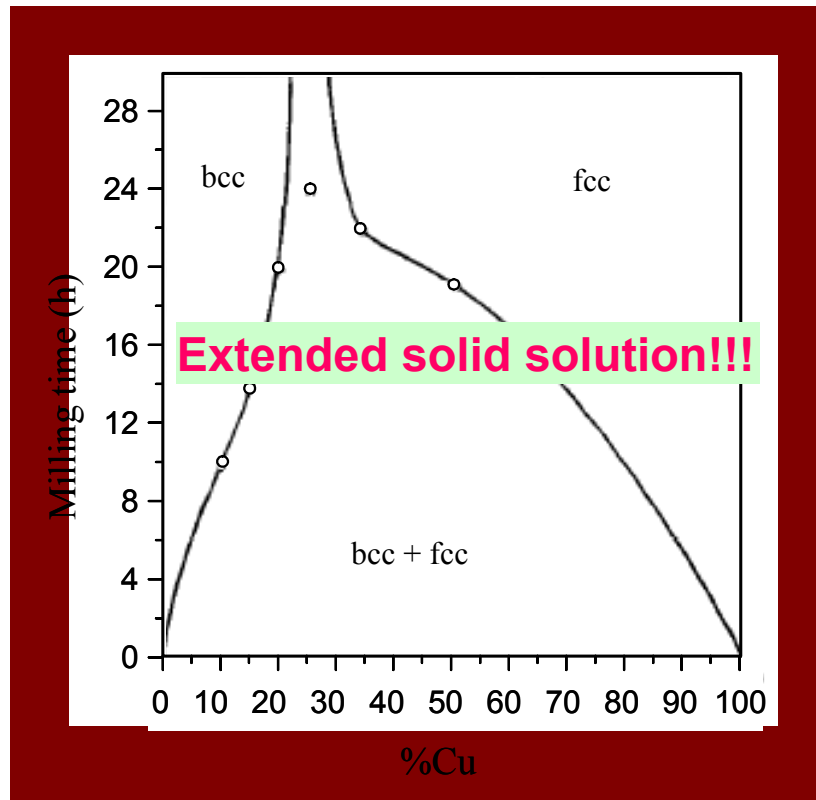


Soft Magnetic Nanocrystalline Powders

*X.Y. Qin, S.H. Cheong, J.S. Lee, Mater. Sci. Eng., **A 363** (2003) 62

Fe-Cu powders obtained by MA

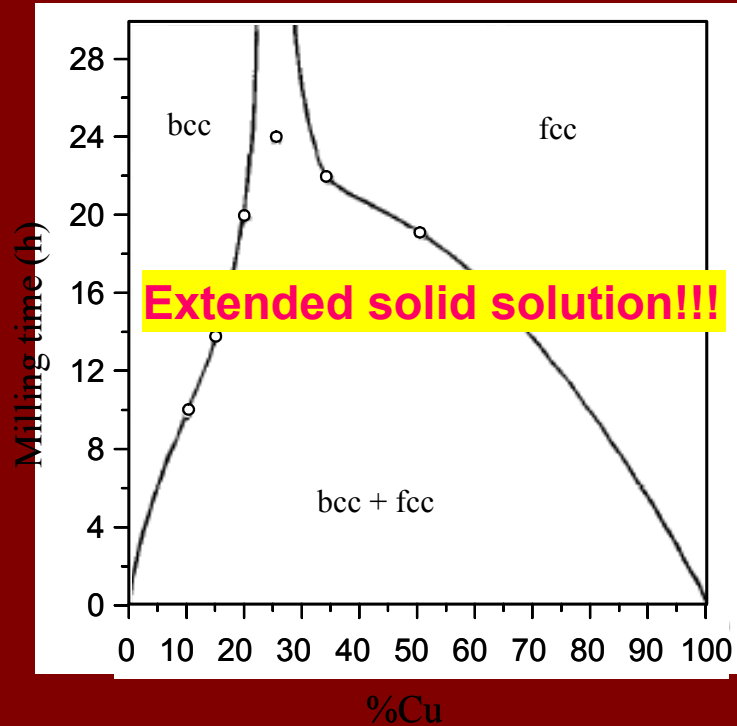
Milling map of mechanically alloyed Fe-Cu system



B. Majumdar et al., J. Alloys Comp. **248**, 192 (1997)

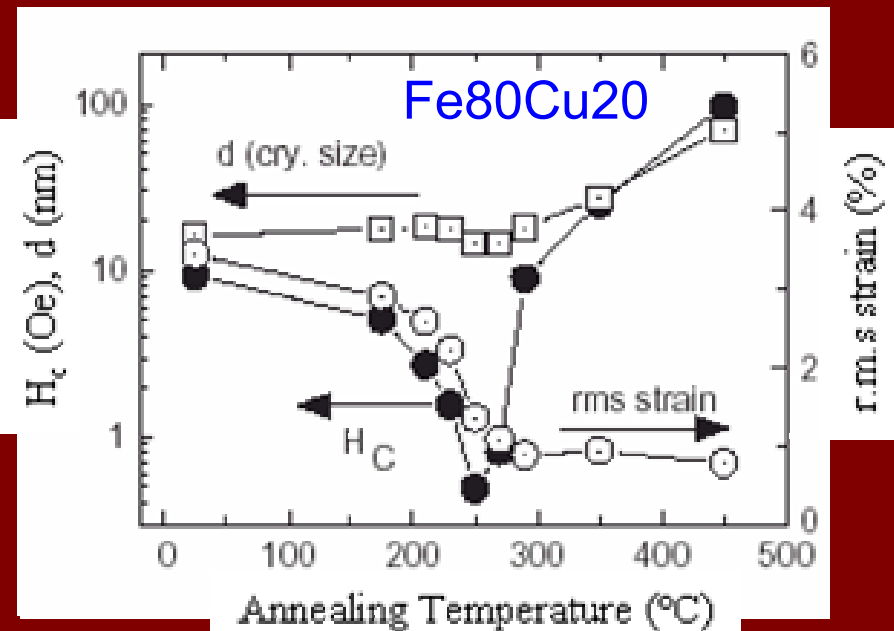
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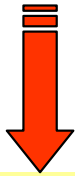
Interesting magnetic properties



R.B. Schwarz, T.D. Shen, U. Harms, T. Lollo, J. Magn. Magn. Mater. **283**, 223 (2004).

Ni-Fe and Ni-Fe-X-(Y) systems

Why Ni-Fe and Ni-Fe-X-(Y) systems?

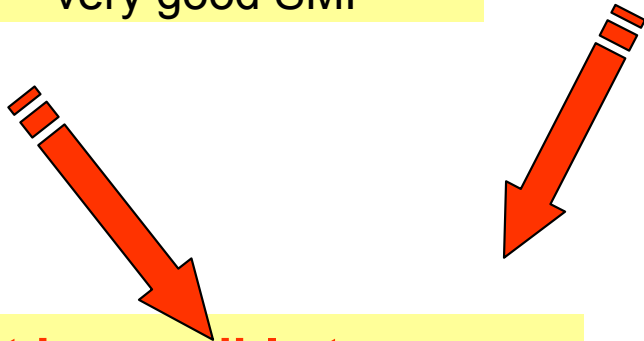


Polycrystalline Ni-Fe and Ni-Fe-X alloys have very good SMP

Why mechanical alloying techniques?



Nanocrystalline materials have very good SMP



It is possible to combine the properties of Ni-Fe and Ni-Fe-X-(Y) systems with the properties of nanocrystalline state

Ni-Fe and Ni-Fe-X-(Y) systems

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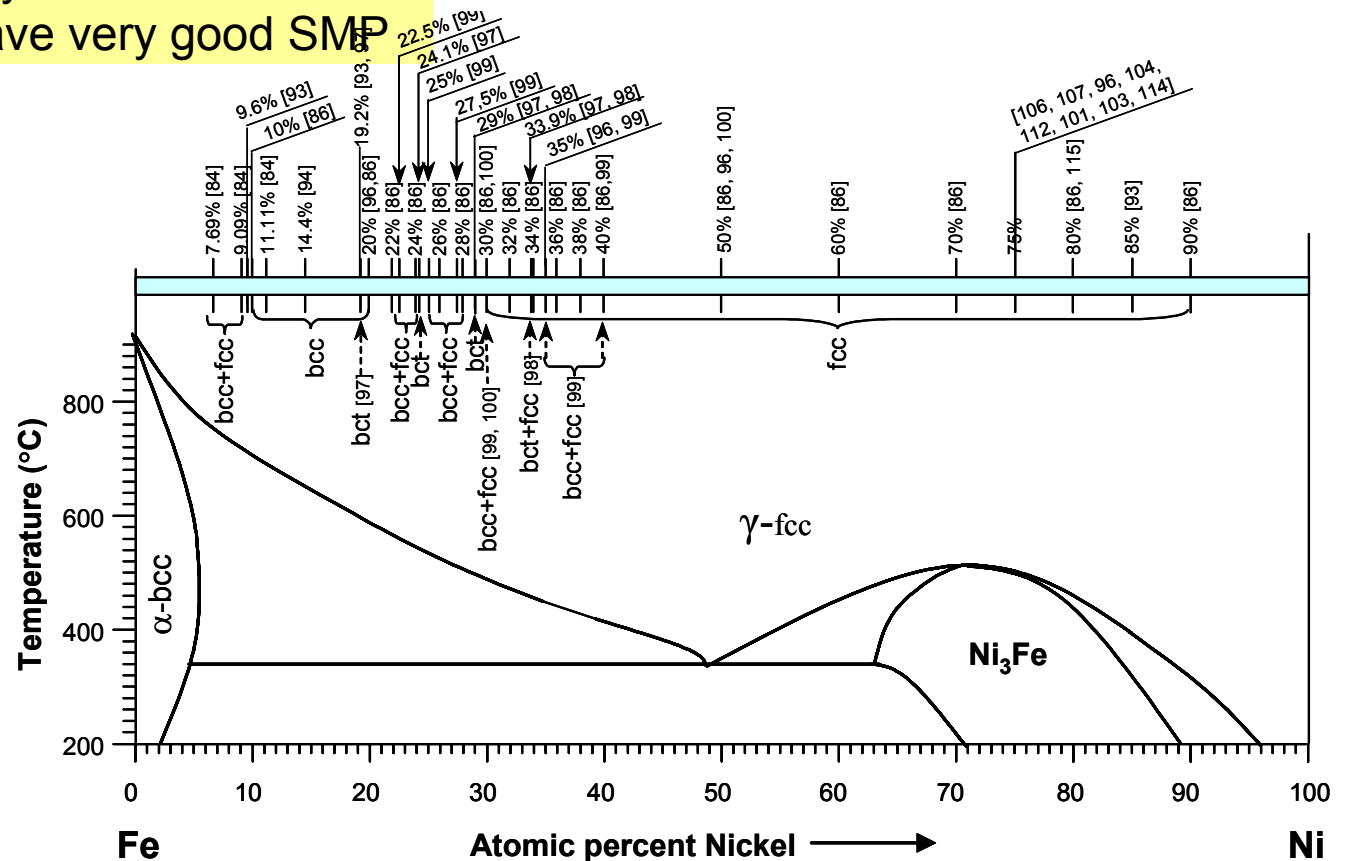
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Nanocrystalline materials have very good SMP

SMC powders produced by MA



V. Pop, I. Chicinaș, J. Optoelectron. Adv. Mater. **9** (2007), 1478-1491

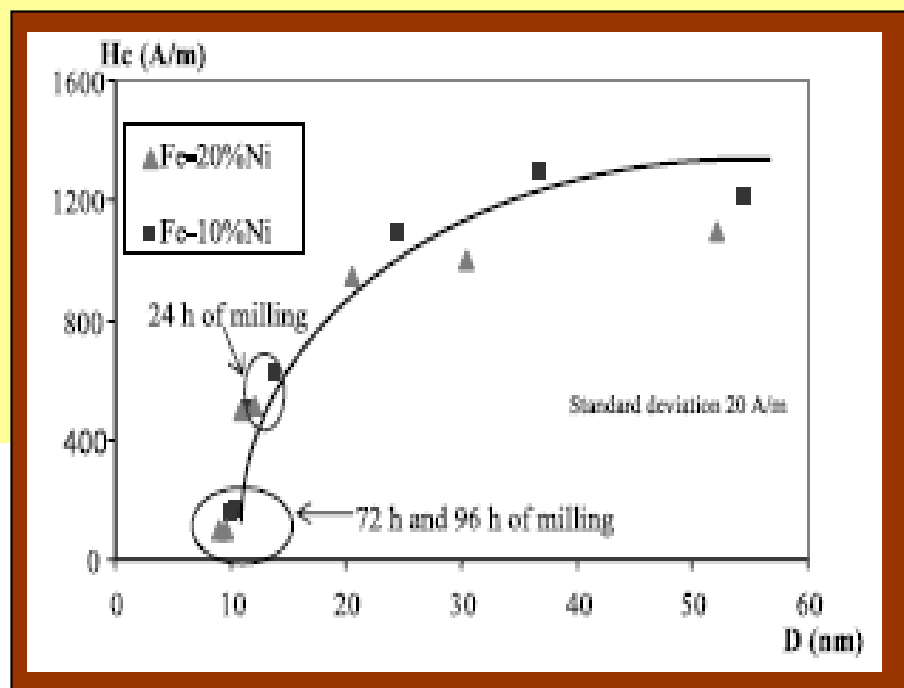
Properties depending of milling conditions

It has been proved that the milling performed in the friction mode (FMP) leads to the formation of alloys exhibiting a soft magnetic behaviour. However, magnetisation is not affected by the mode used

R. Hamzaoui, O. Elkedim, E. Gaffet, J. Mater. Sci., **39** (2004) 5139

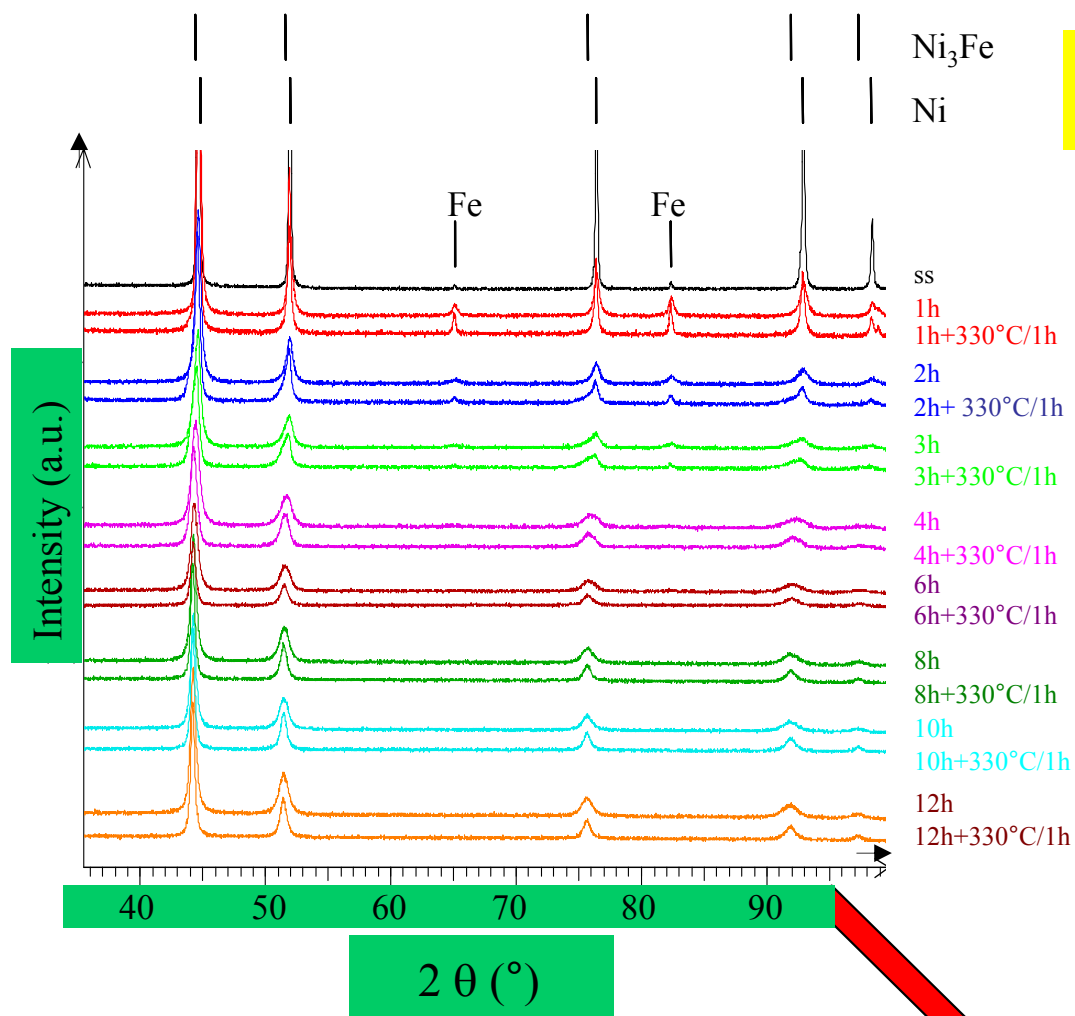
In high-energy ball milling process the fcc solid solution $\gamma(\text{Fe},\text{Ni})$ in alloys $\text{Fe}_{65}\text{Ni}_{35}$ was formed after 36 hours, while in the low-energy milling process the Fe lines disappeared after 400 hours of milling.

E. Jartych, J.K. Żurawicz, D. Oleszak, M. Pękała, J. Magn. Magn. Mater. **208** (2000) 221



A strong decrease of the coercive field versus crystallite size appears especially for crystallite size smaller than 20 nm

R. Hamzaoui, O. Elkedim, N. Fenineche, E. Gaffet, J. Craven, Mater. Sci. Eng. A 360 (2003) 299-305



- Ni_3Fe phase formation
- the first order internal stresses

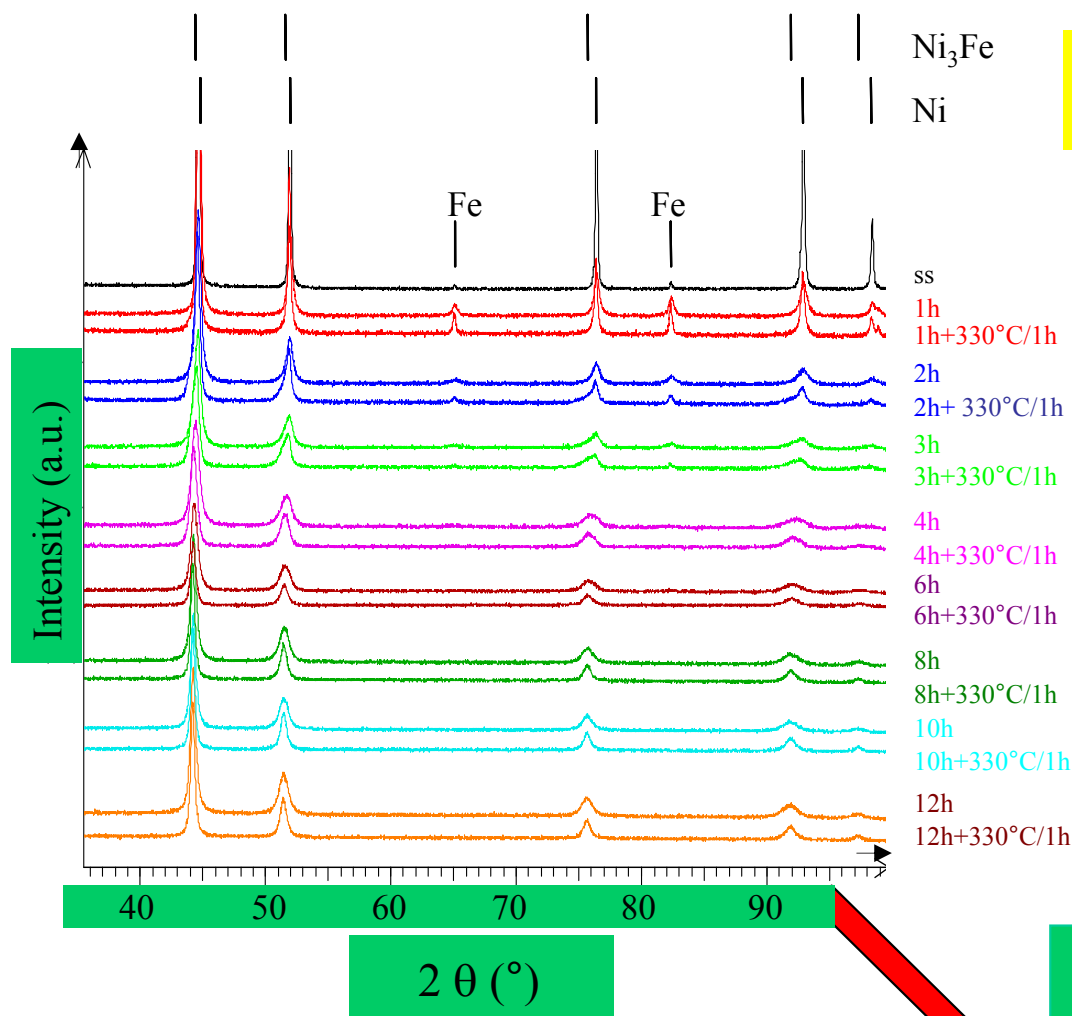
peaks shift to LOWER 2θ angles

peaks shift to HIGHER 2θ angles

relaxation of the first order internal stresses

the second order internal stresses
Crystallite size reduction

broadening of the diffraction peaks



- **Ni₃Fe** phase formation
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peaks shift to **LOWER** 2 θ angles

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relaxation of the first order internal stresses

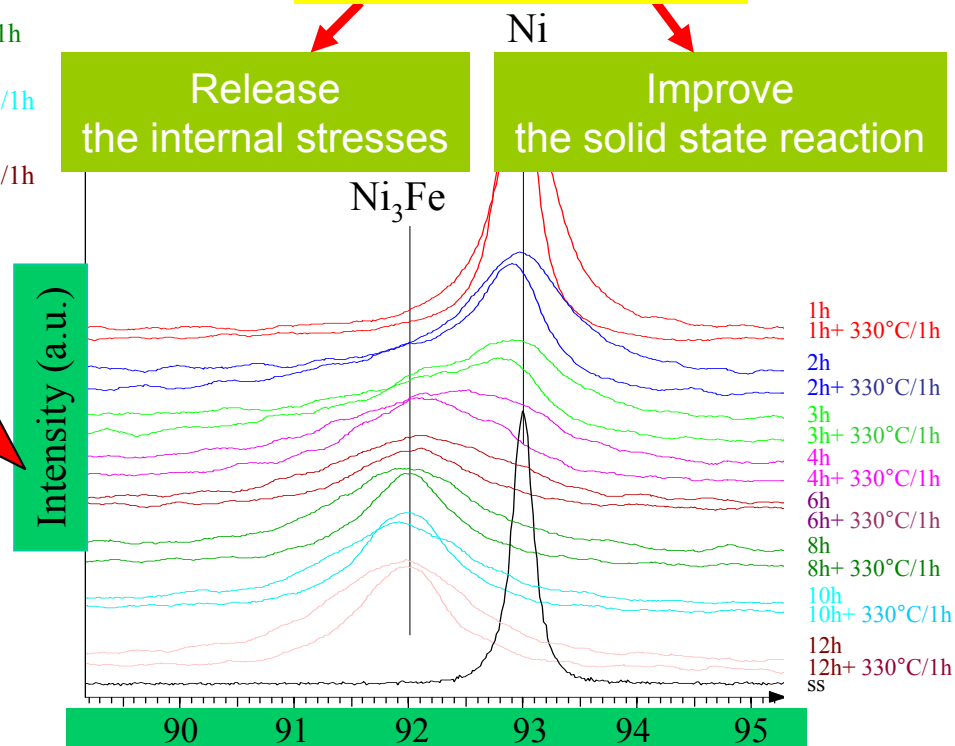
Annealing effect

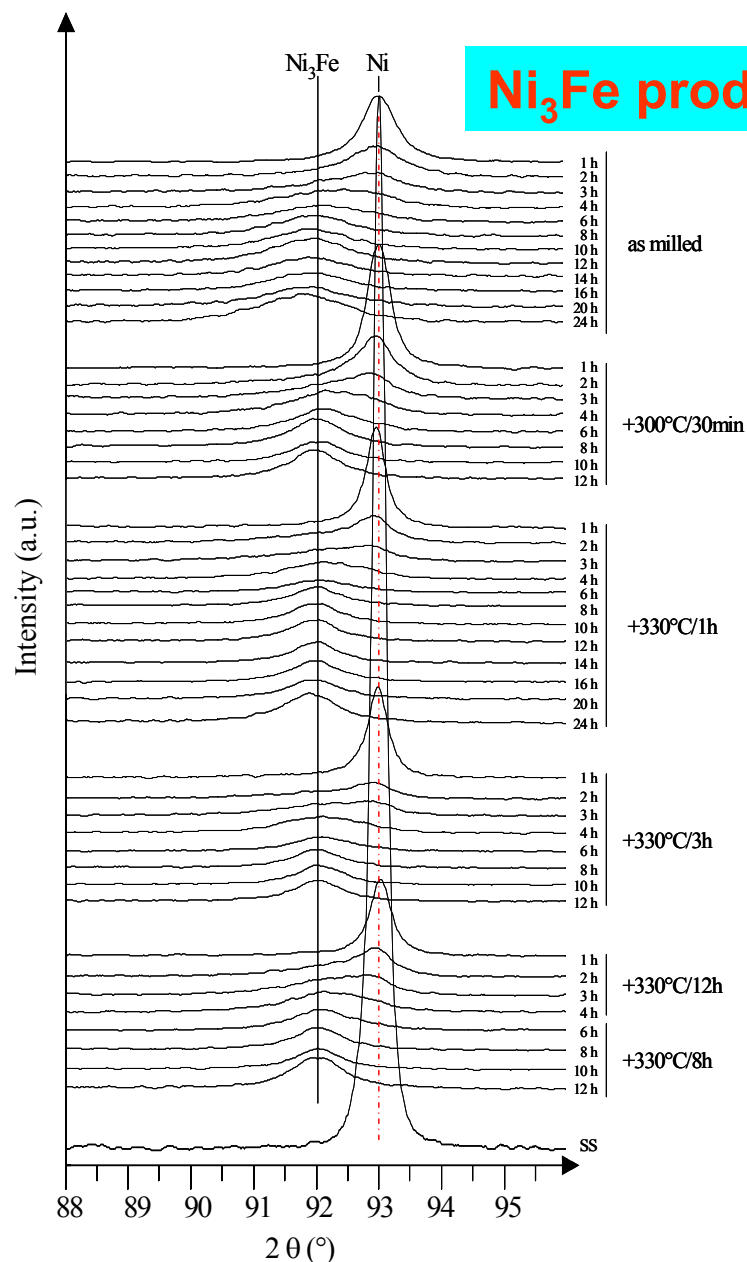
Release
the internal stresses

Improve
the solid state reaction

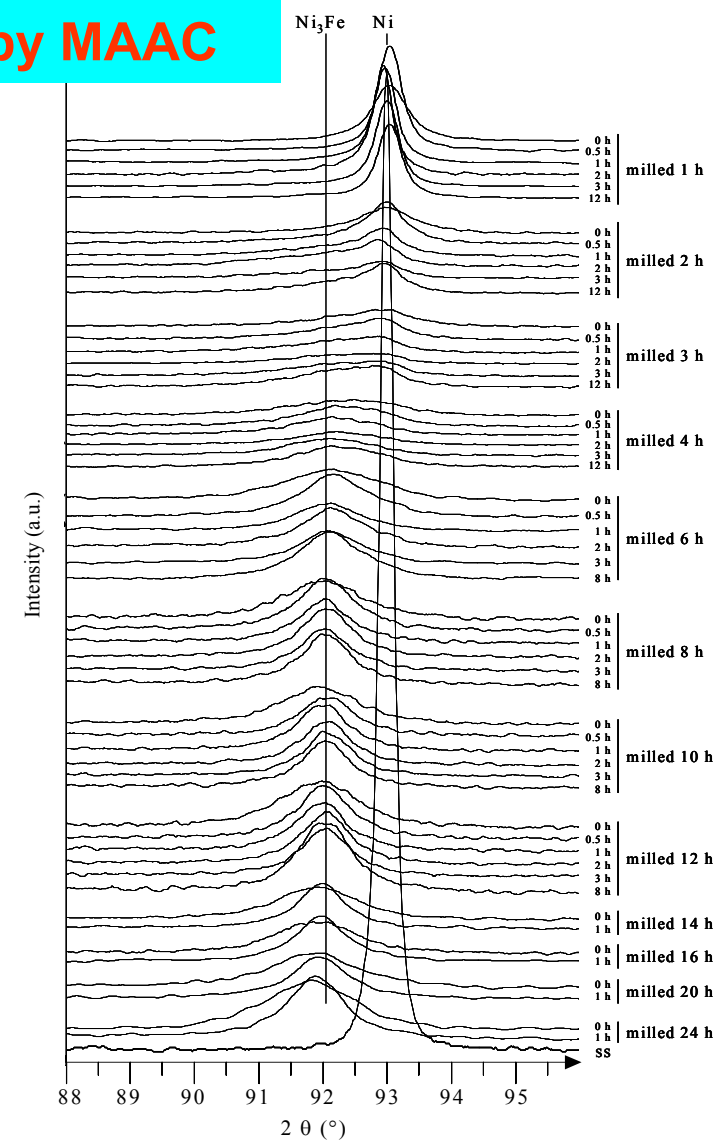
the **second order** internal stresses
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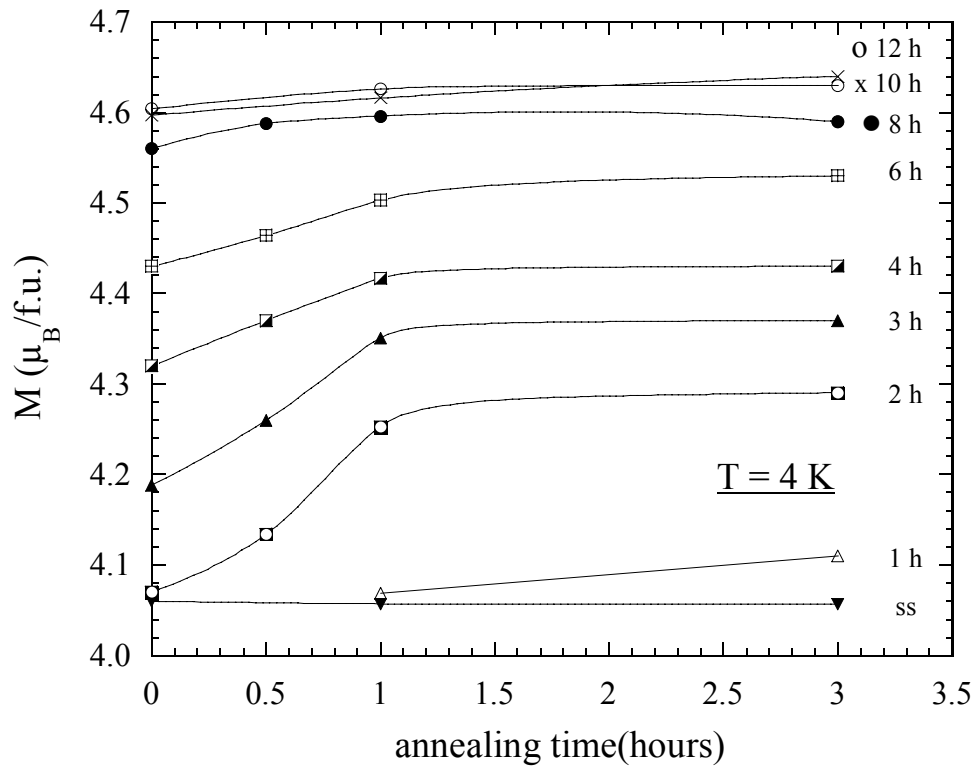


One annealing time - Different milling time



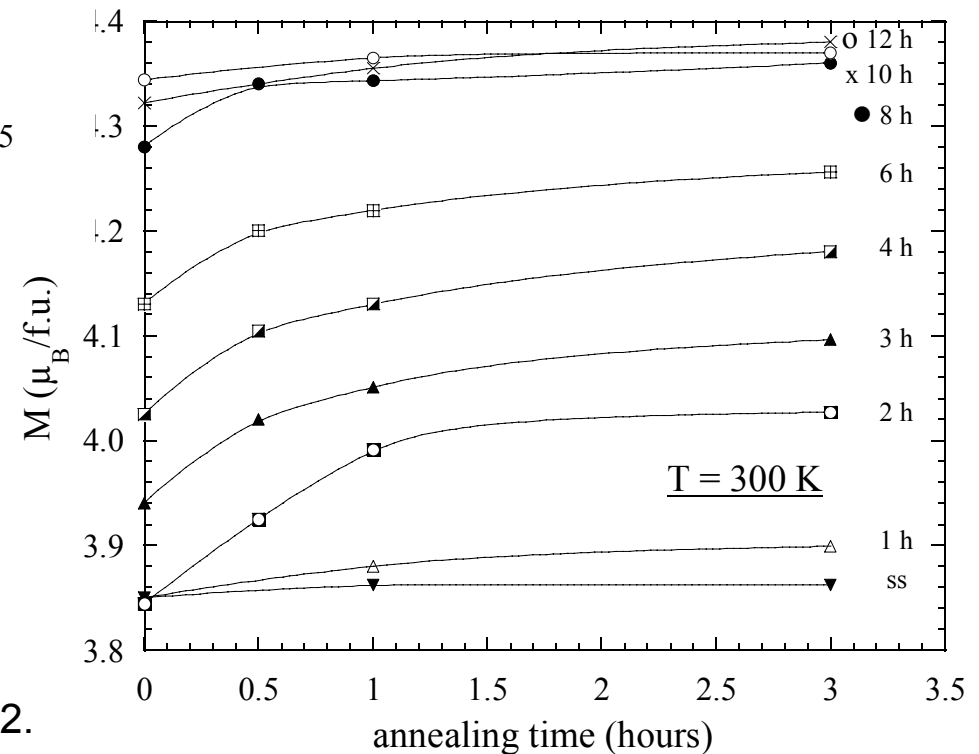
One milling time - Different annealing time

Mean grain size : 15 ± 2 nm , after 32 h milling

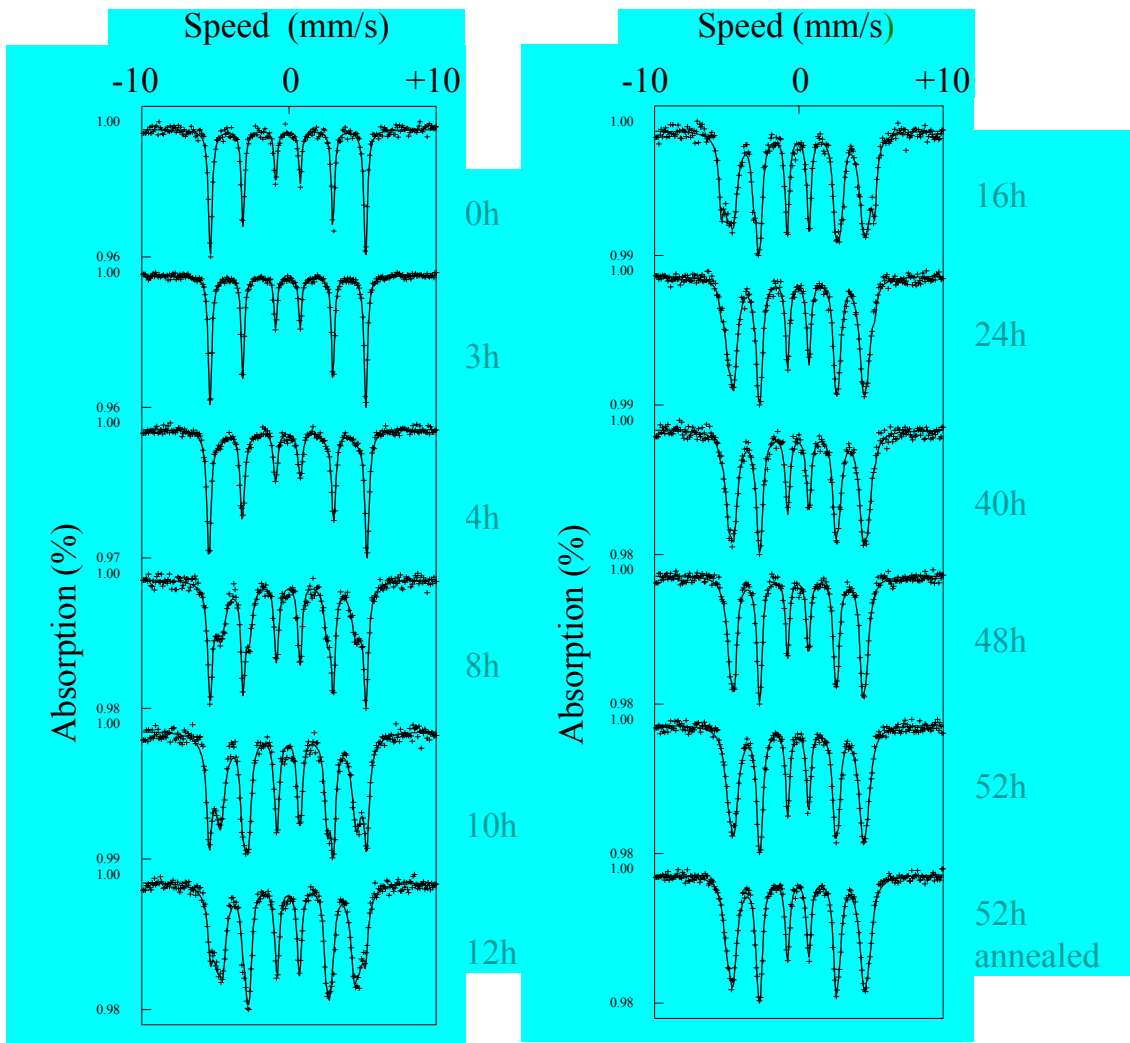


Ni₃Fe produced by MAAC

Influence of the milling and annealing conditions on the M_s



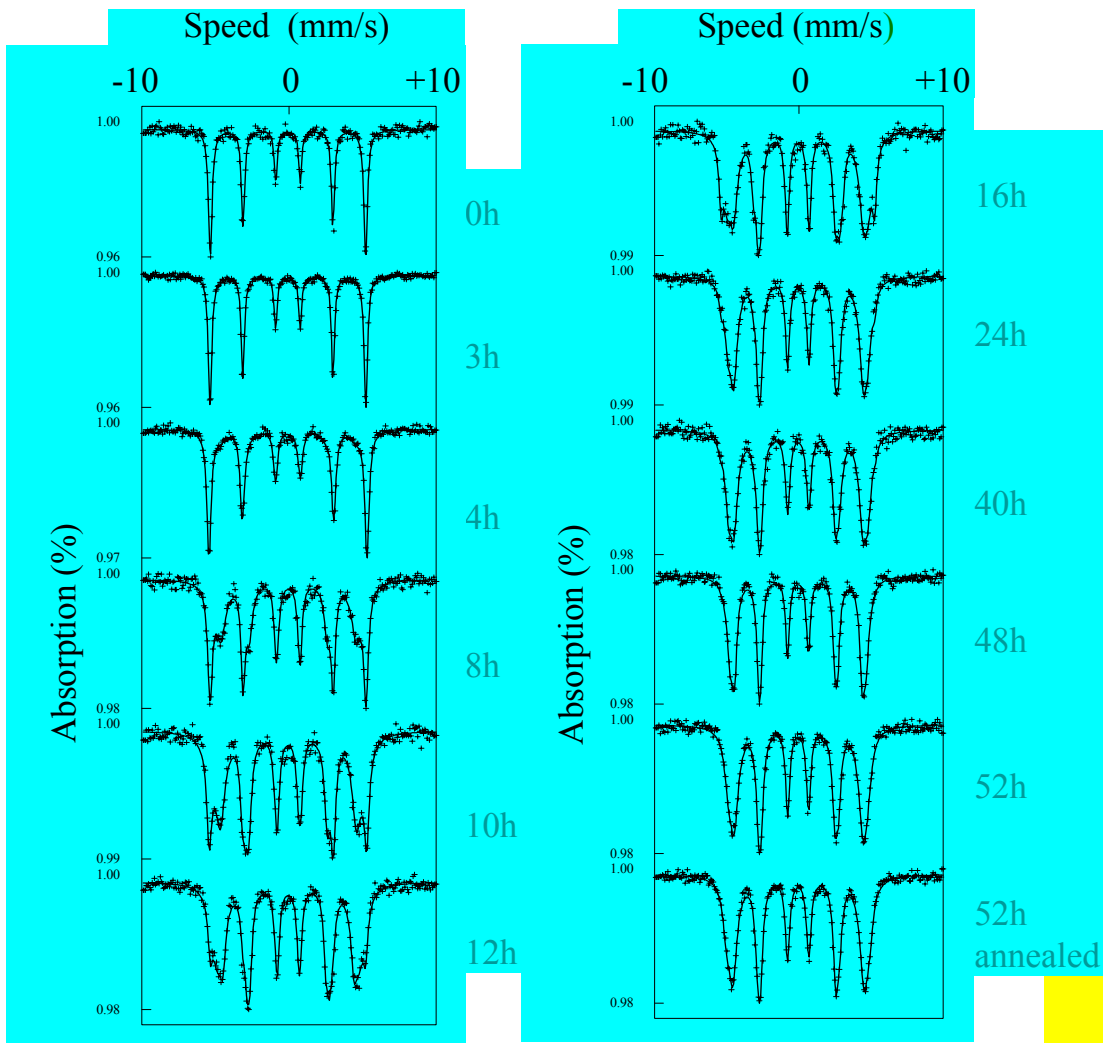
V. Pop, O. Isnard and I. Chichinas,
J. Alloys and Comp., **361** (2003), p.144-152.



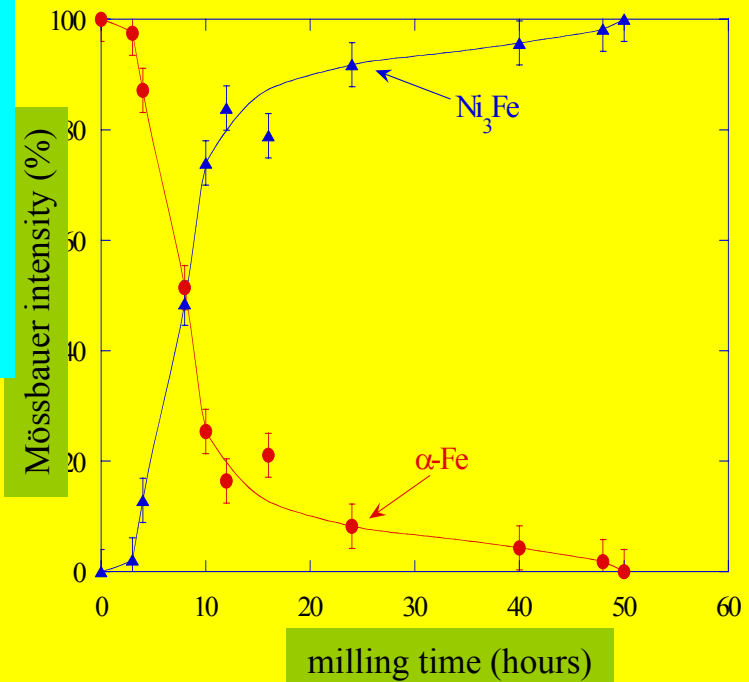
Mössbauer spectrometry

Ni_3Fe powders

I. Chicinas, V. Pop, O. Isnard, J.M. Le Breton and J. Juraszek, J. Alloys and Compounds 352 (2003), p. 34-40



Mössbauer spectrometry Ni_3Fe powders



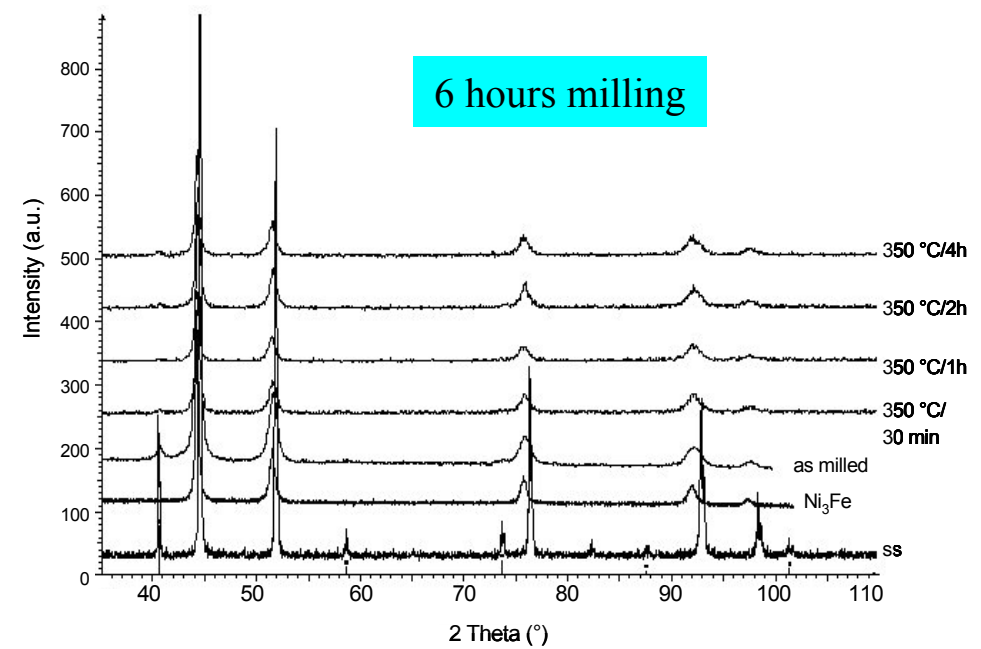
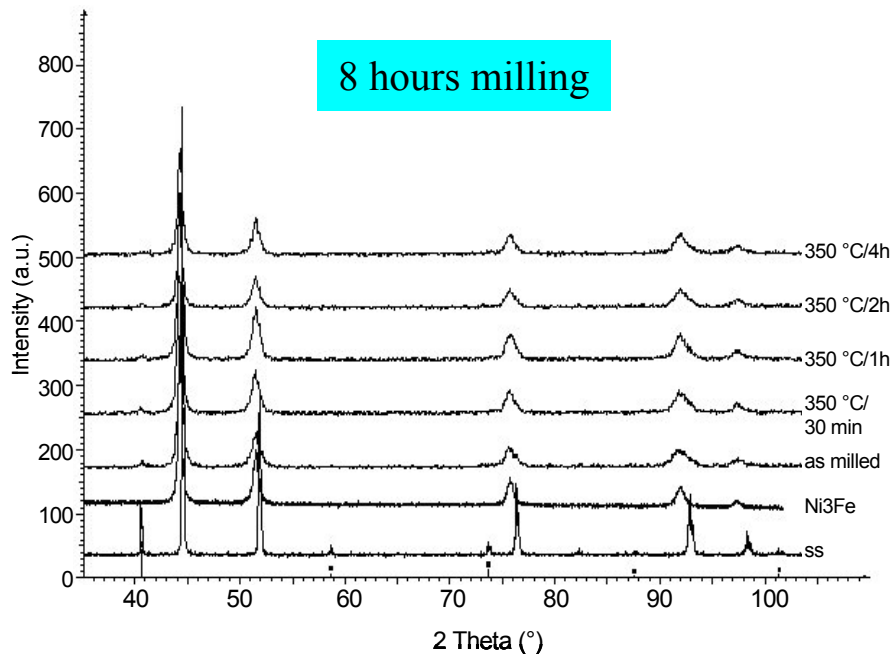
I. Chicinas, V. Pop, O. Isnard, J.M. Le Breton and J. Juraszek, J. Alloys and Compounds 352 (2003), p. 34-40

Nanocrystalline soft magnetic powders from Fe-Ni-X-(Y) systems

$\text{FeNi}_{3x}\text{Ag}_{1-x}$, $\text{Ni}_{50}\text{Al}_{50-x}\text{Fe}_x$, $\text{Fe}_{49}\text{Ni}_{46}\text{Mo}_5$, $\text{Fe}_{42}\text{Ni}_{40}\text{B}_{18}$,
 $\text{Ni-15\%Fe-5\%Mo}$ and $\text{Ni-16\%Fe-5\%Mo}$ (wt%), $\text{Ni-14\%Fe-5\%Cu-4\%Mo}$ and others

Supermalloy synthesis by MAAC:

- 8 hours milling
- different annealing conditions.



$$d = \frac{k \cdot \lambda}{\beta_{\frac{1}{2}} \cdot \cos \theta}$$

$\beta_{\frac{1}{2}}$ - FWHM



d = { 11 nm - 16 h milling and annealing at 350 °C for 2 hours
in order to remove second order internal stresses

I. Chicinas, O. Isnard, V. Pop, J. Mater. Sci. **39** (2004), p. 5305-5308

O. Isnard, V. Pop, I. Chicinas, J. Magn. Magn. Mater. **290-291** (2005), p. 1535-1538.

Alliage 77Ni14Fe5Cu4Mo % massique

Analyse thermomagnétique

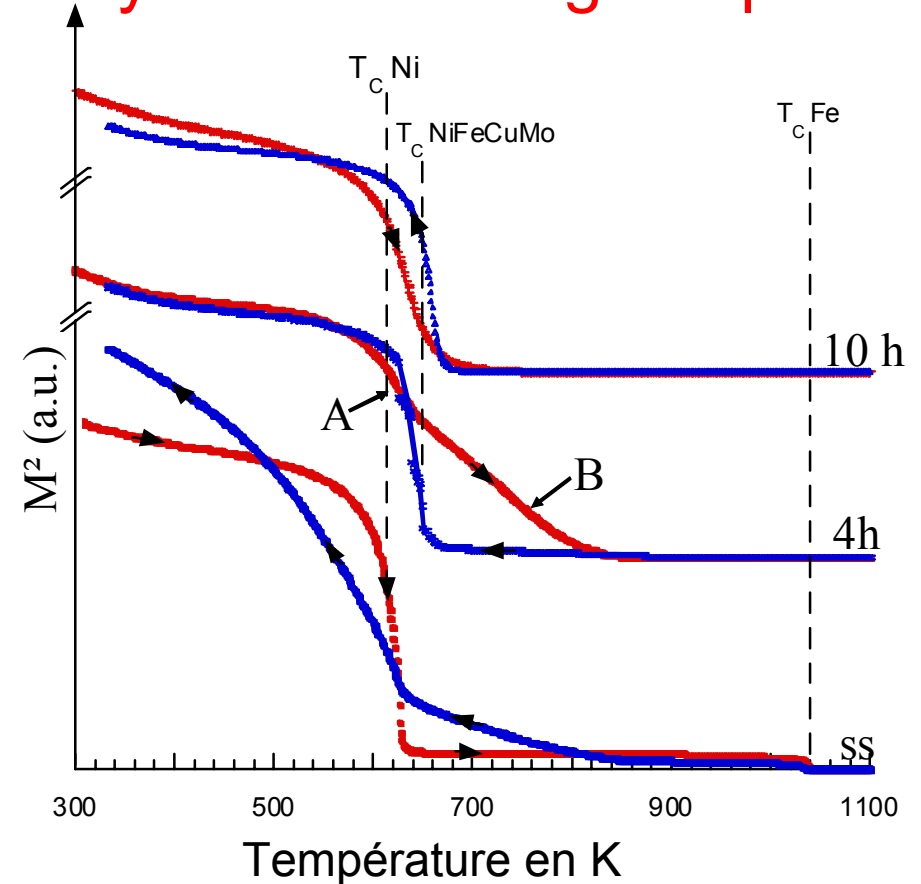
10h : seule la T_c de l'alliage est observée
le traitement thermique homogénéise

4h : -Chauffage changement de pente
au point A correspond à T_c de
NiFeCuMo obtenu par broyage

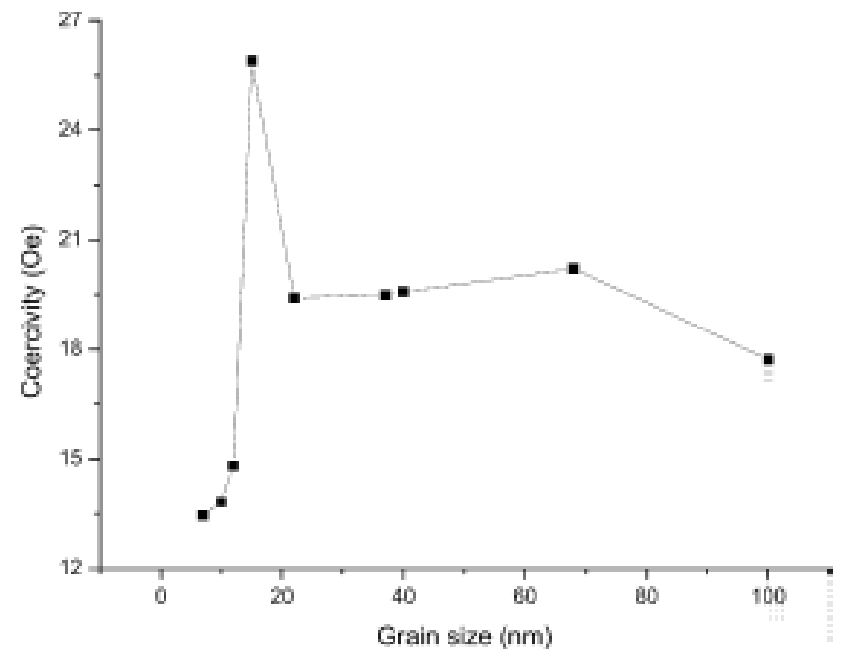
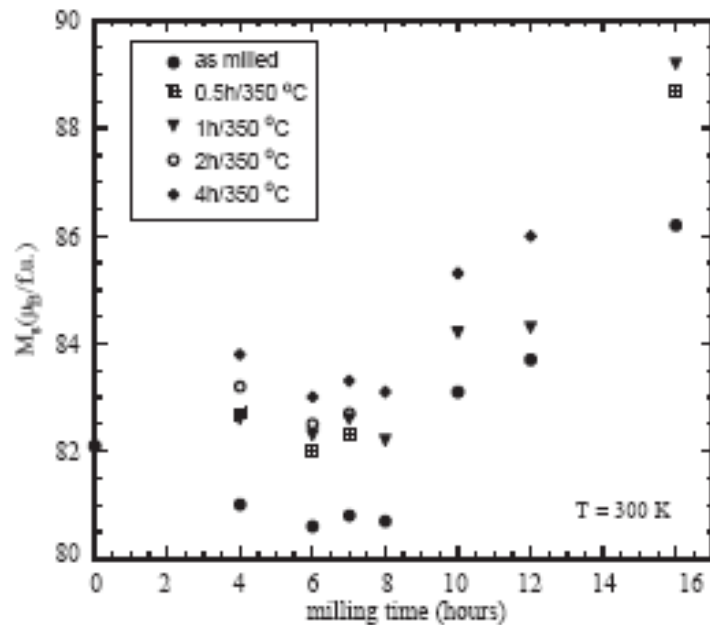
-Formation progressive de l'alliage
par chauffage (région B)
Large domaine de composition

-Refroidissement une seule T_c détectée
alliage formé dans le volume

SS : Mélange de départ T_c de Ni et Fe



F. Popa, O. Isnard, I. Chichinas, V. Pop, J. Magn. Magn. Mater., 316 (2007) e900–e903

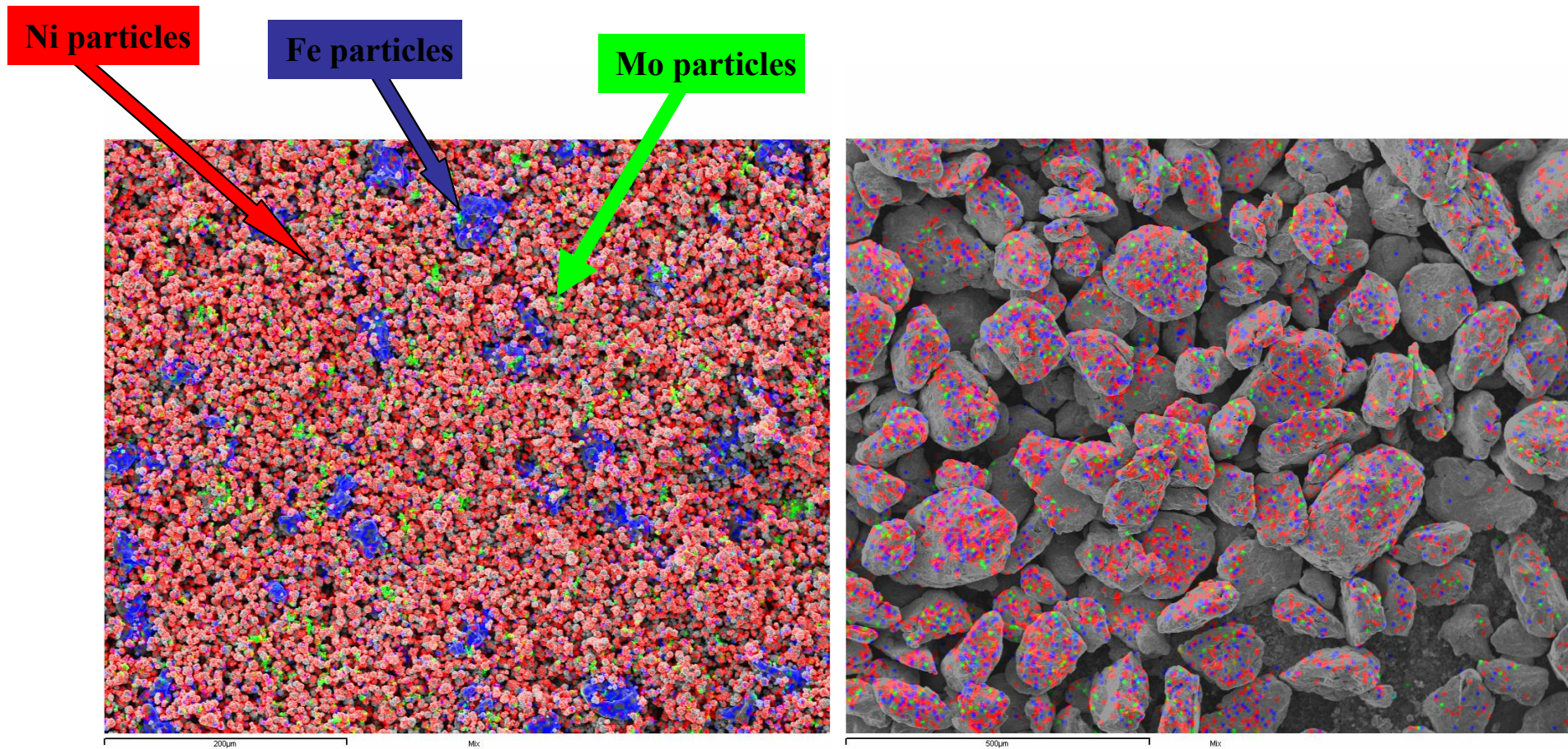


the mechanical alloying process occurs in two steps
an intermediate amorphous or poorly crystalline phase, (Ni,Fe)–Mo type.

The high coercivity before 10 h of milling is attributed to strong pinning of domain walls of the interaction domains at the grain boundaries.

O. Isnard, V. Pop, I. Chicinaş,
J. Magn. Magn. Mater. **290-291** (2005) 1535

Y. Shen, H.H. Hng, J.T. Oh,
J. Alloys Comp. **379** (2003) 266-271.



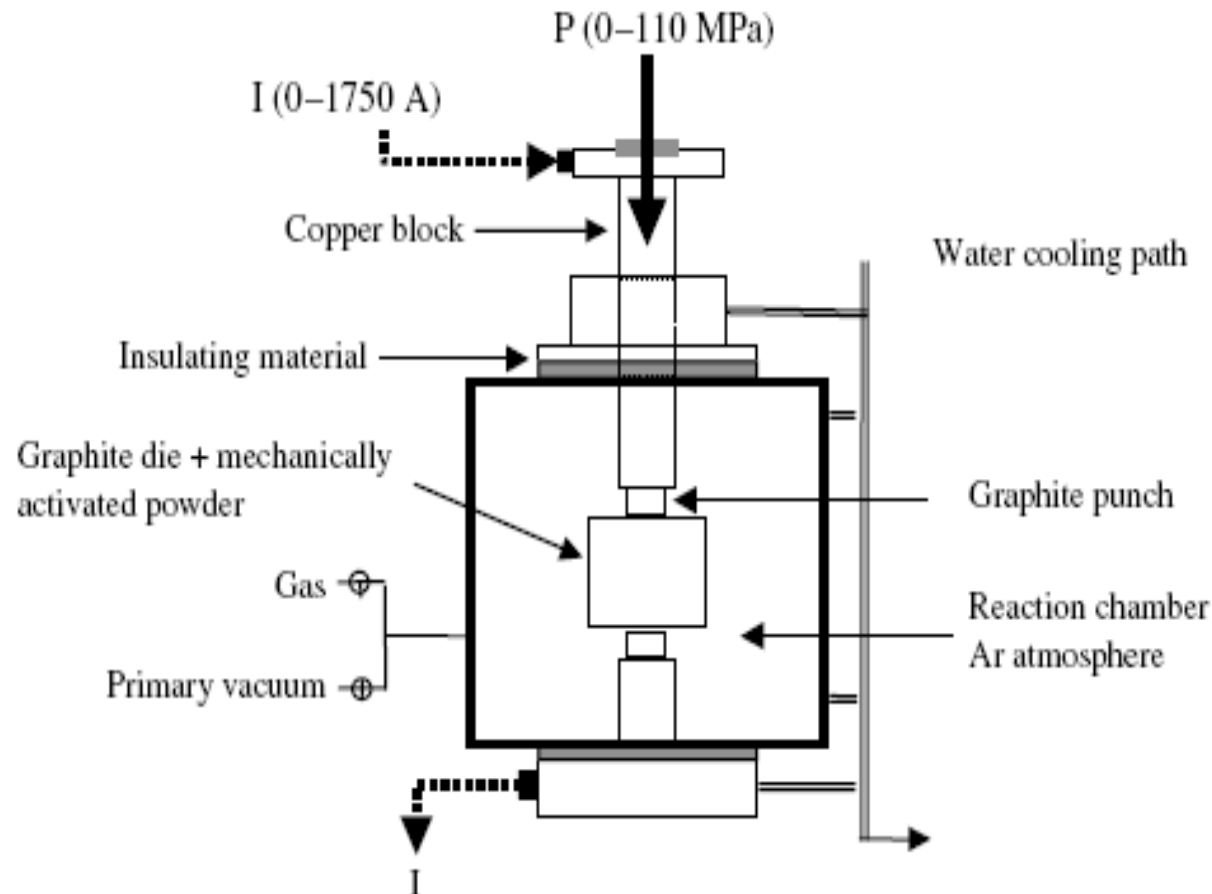
The Ni, Fe and Mo maps on starting sample (0 hours milling) and on the 12 hours milled sample. It can observe the chemical homogeneity of the Superalloy powders obtained by mechanical alloying and the particles morphology, too.

Methods to produce from the nanocrystalline powders a nanocrystalline compact

FAPAS

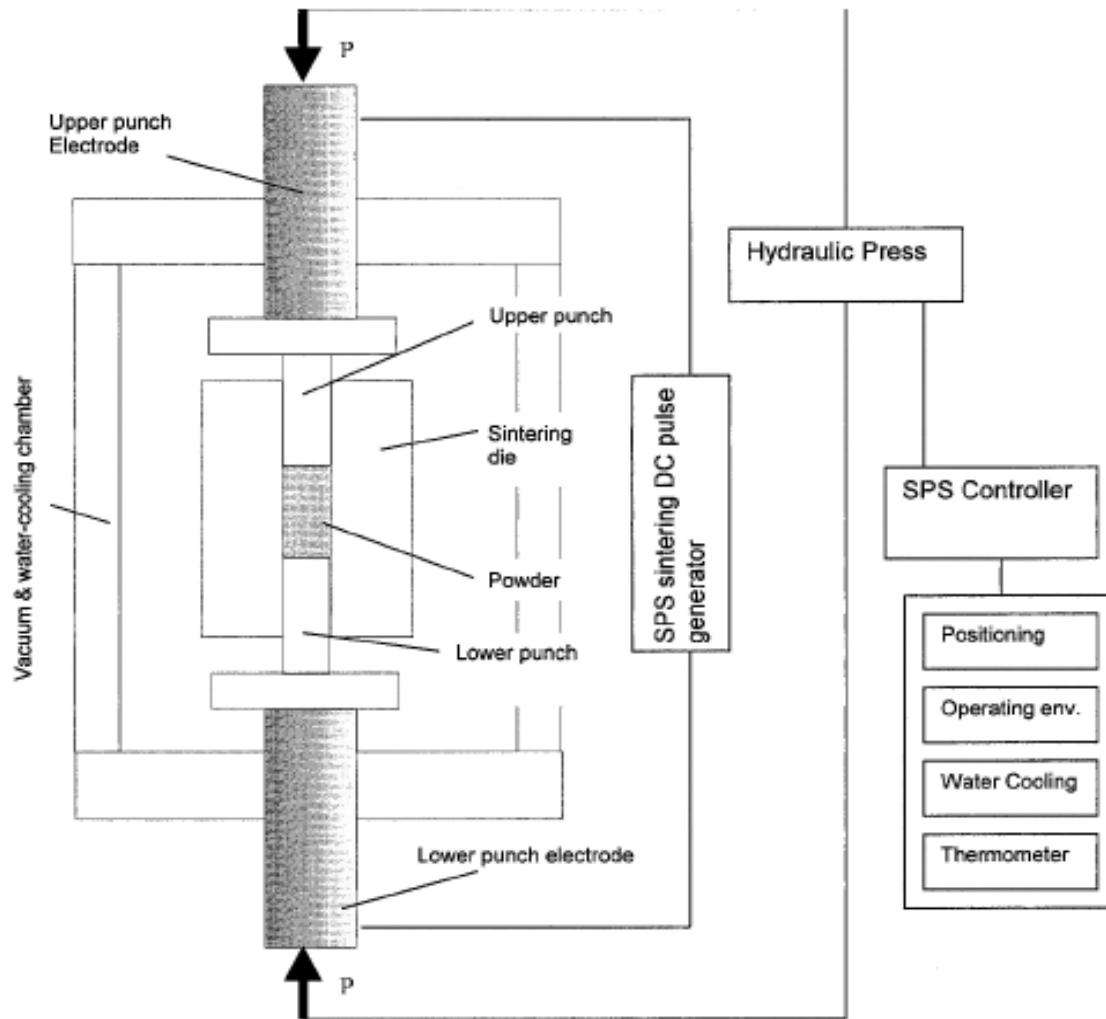
Field activated pressure assisted sintering. Compared to a classical sintering process under pressure, a current is applied in order to assist the sintering.

A current exhibiting a high intensity (up to 8,000 A) under low voltage (10 V) is applied.



E. Gaffet, G. Le Caër, Mechanical Processing for Nanomaterials, in Encyclopaedia of Nanoscience and Nanotechnology, vol.X, Ed. by H.S. Nalwa, American Sci. Publishers (2004).

Methods to produce from the nanocrystalline powders a a nanocrystalline compact



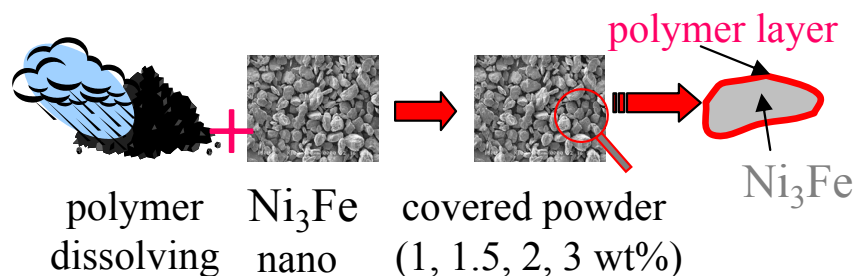
Spark plasma sintering

A process leading to bulk materials by a sintering step using pulse electric discharge. Due to the high intensity of the current, plasma may occur between the various powder grains.

V. Mamedov, Powder Metallurgy 2002 Vol. 45 No. 4, 322-327

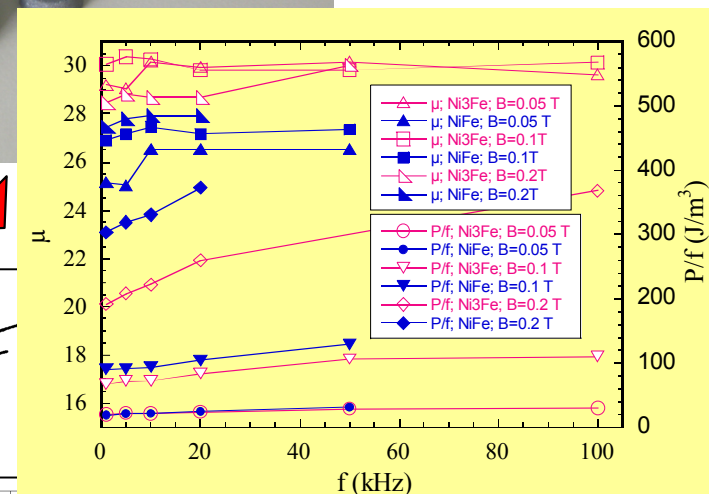
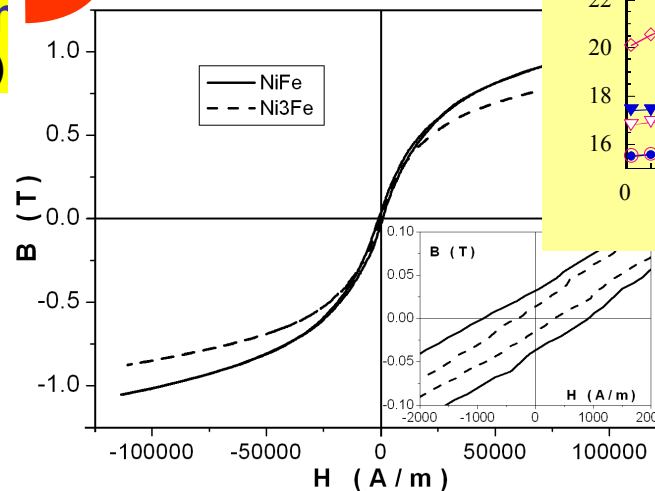
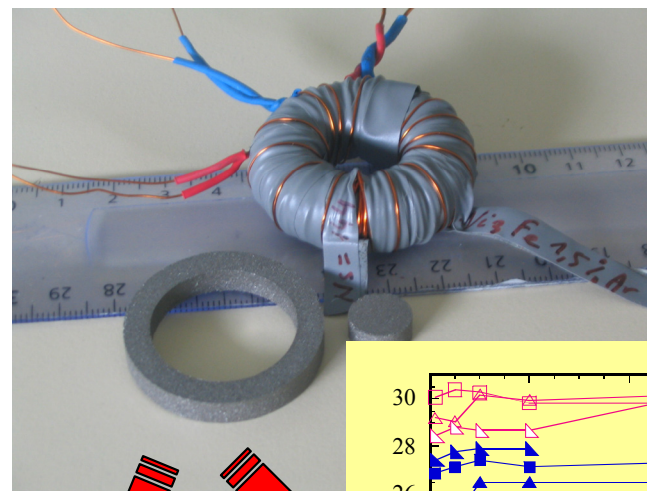
Soft magnetic nanocrystalline composites

Composites Production



Die pressed
(600 - 800 MPa)

Polymerisation
(60 min., 180 °C)



I. Chicinaș, O. Isnard, O. Geoffroy, V. Pop, J. Magn. Magn. Mater. **310** (2007), 2474-2476

Conclusions

The possibility of producing chemical transformations through mechanical energy has been extensively demonstrated in metallic as well as in oxide systems

The nanocrystalline/nanosized powders obtained by different mechanical routes exhibit very interesting properties, some from them different from those of bulk materials

Thank you for your attention!