

# Soft nanocrystalline alloys (Melt Spun)

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## 1 Presentation

Nanocrystalline magnetic soft alloys were patented in 1987 [Yos 88] and can be seen as an extension of amorphous magnetic soft alloys, introduced towards 1970. Their intrinsic extremely high magnetic permeability coupled with a low production cost allow to use them for a wide range of applications.

Different families exist with Typical composition (atomic) :

- \*  $\text{Fe}_{73.5}\text{Cu}_1\text{Nb}_3\text{Si}_{15.5}\text{B}_7$  (**Finemet** by Hitachi Metals, **Vitroperm** by Vacuumschmelze GmbH, † **Nanophy** by Imphy Alloys)
- \*  $\text{Fe}(\text{Co})_{86}\text{Zr}_7\text{B}_6\text{Cu}_1$  († **Nanoperm** by Alps Electric Co.)
- \*  $(\text{Fe}_{1-x}\text{Co}_x)_{88}\text{Hf}_7\text{B}_4\text{Cu}_1$  : **Hitperm**

## 2 Elaboration and crystallographic structure

The elaboration is made of two stages :

- \* **First stage** : Elaboration of an amorphous precursor :

- ➔ glass formers are needed (B, Hf...)
- ➔ It is necessary to achieve very high cooling rate to prevent crystallisation (cf on fig 1 : route AB instead of route AC) :

$$\frac{dT}{dt} > 10^6 \text{ K / s}$$

- ➔ Different technical processes exist :

- \* Splat cooling (Not industrial) : compression of a liquid drop between two copper disks.
- \* Projection on a rotative cooled copper wheel (Industrial) :
  - Melt spinning for ribbons of several millimetres width
  - Planar flow casting for ribbons of several centimetres width (until 20 cm)

- \* **Second stage** : Nanocrystallisation annealing ( $\approx$  One hour,  $T_{\text{anneal}} \approx 500 \text{ }^\circ\text{C}$ )

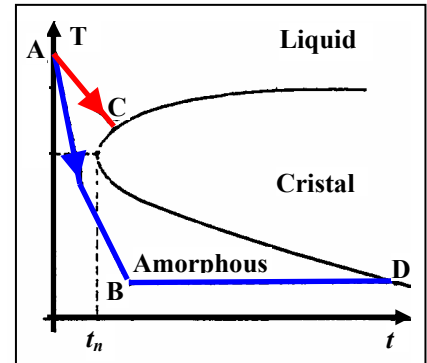


Fig. 1 : Temperature-duration-Transformation rate diagram

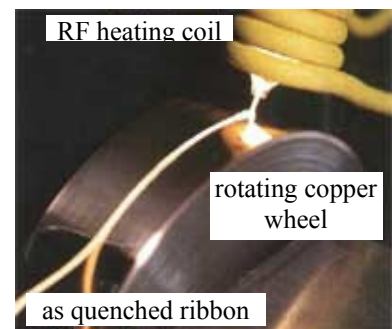


Fig. 2 a : melt spinning Process

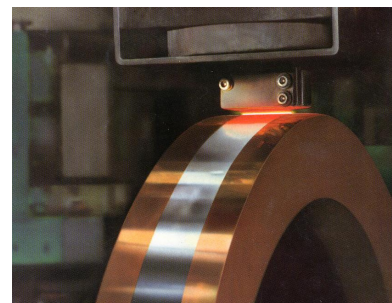


Fig. 2 b : Planar flow casting

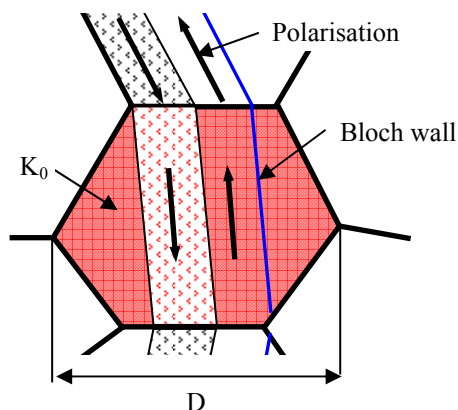


Fig. 3a : domain walls in classical crystalline alloys ( $e_w \approx 3 L \ll D$ )

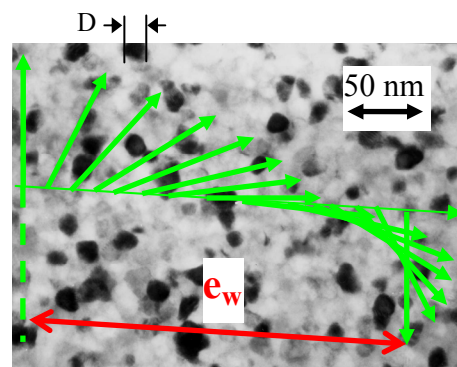


Fig. 3b : Microstructure of a Nanophy sample (Imphy Alloy). Superimposed, extension of a domain wall (thickness  $e_w \approx 3 L \gg D$ )

- ➔ Rapid diffusion of Cu initiates local nucleation of crystalline FeSi (Finemet) or Fe (Nanoperm) with random crystallisation directions.
- ➔ Slow diffusion of Nb (Finemet) or Zr (Nanoperm) inhibs growth of crystallites : typical size  $D \approx 10-20$  nm

➔ Atypical resulting crystalline structure (cf fig 3) :

Coexistence of a soft magnetic nanocrystalline phase (Fe or FeSi) with a residual amorphous phase.  
volumic crystalline fraction  $f \approx 70\%$

### 3 Magnetic Properties

\* Amorphous phase ensures continuity of magnetic exchanges interactions between nanograins :

- ➔ from a magnetic point of view, ribbon = continuous medium
- ➔ extension of a Domain-Wall upon a great number of grains ( $e_w \gg D$ , cf. Figure 3b)
- ➔ At the scale of the DW, anisotropy  $K_{eff}$  much smaller than the crystallographic one  $K_0$  due to averaging.

\* In addition : very low magnetostriction (cf. fig.7) :  
 $\lambda_s(f=70\%) \approx 10^{-6}$

➔ Coercivity  $\searrow\searrow$  ( $H_c < 1$  A/m)  
Permeability  $\nearrow\nearrow$  ( $\mu_r > 10^5$ )

#### Quantitative description : Random Anisotropy Model

Magnetic independent entity = Correlated Volume of side  $L$  (magnetic correlation length) (cf. fig. 4).

The effective anisotropy  $K_{eff}$  is driven by the random magnetocrystalline contribution  $K_a$ . Noticing  $A$  the exchange stiffness, one obtains :

$$L = \sqrt{A K_{eff}}$$

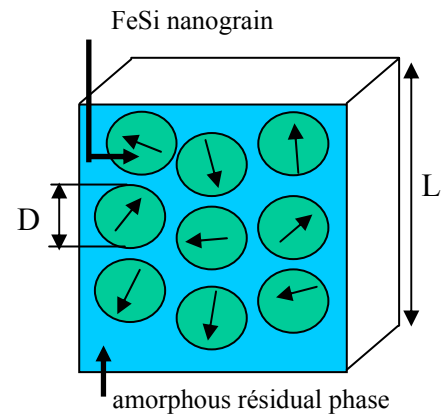
$$K_{eff} = K_a = \sqrt{\langle K^2 \rangle} = K_0 / \sqrt{n} \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} K_{eff} \approx K_0^4 A^{-3} f^{-2} D^6 \quad (1)$$

$$n = f (L/D)^3$$

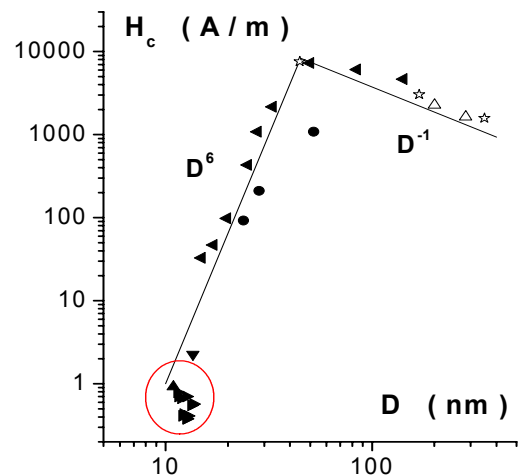
$H_c \approx K_{eff} \approx D^6$  (cf. Fig.5)

#### ➔ Related property :

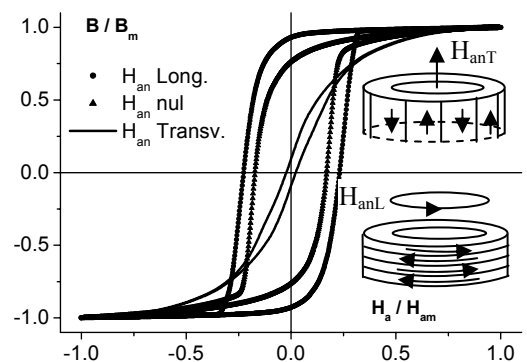
Due to vanishing anisotropies, possibility to tailor the shape of the hysteretic loop by means of induced anisotropy



**Fig. 4 : Magnetic correlated volume  $L^3$  comprising  $n = f(L/D)^3$  nanograins. Arrows feature the distribution of magnetization easy axes due to random cristallization**



**Fig. 5 : Evolution of the coercivity with the grain size. The  $D^{-1}$  dependency corresponds to classical alloys ( $e_w \ll D$ , see fig.3a). The circle denotes the region where magnetoelastic effects have to be considered**



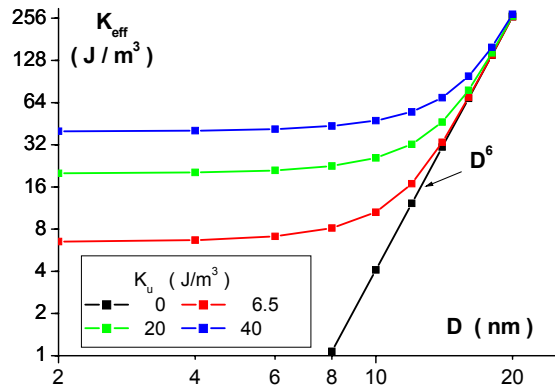
**Fig. 6 : different shapes of the hysteretic loop (round, flat, rectangular) obtained applying a magnetic field during annealing**

applying stress or magnetic field during crystallisation annealing (cf fig. 6) [ALV 05]

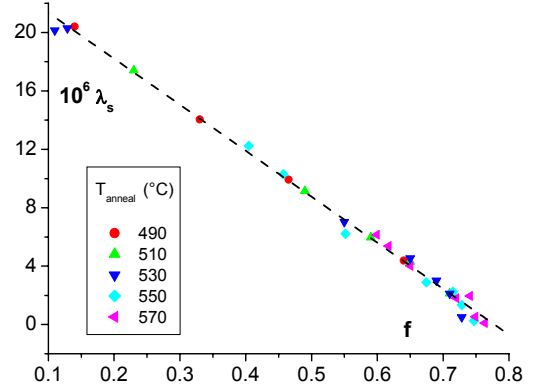
#### 4 Magnetostriction and Magnetoelastic effects :

For little grain sizes ( $D \approx 10$  nm), deviation from the  $D^6$  law occurs (cf. fig.5, circle) : in this region, MagnetoElastic effects give a significant contribution  $K_{me}$  to  $K_{eff}$ , leading instead of (1) to [SUS 98] :

$$K_{eff}^2 = K_{me}^2 + K_a^2 = K_{me}^2 + K_0^2 A^{-3/2} f^{-1} D^3 K_{eff}^{-3/2} \quad (2)$$



**Fig. 7 : Modelisation of  $K_{eff}$  as a function of grains size for different values of  $K_u$  ( $A = 10^{-11}$  J/m,  $f=1$ ,  $K_0 = 8000$  J/m<sup>3</sup>)**



**Fig. 8 : evolution of  $\lambda_s$  (measured by SAMR method) as a function of cristalline fraction  $f$  (samples Nanophy)**

Figure 7 illustrates the competition between  $K_{me}$  and  $K_a$ . It is so expected that for little grain sizes  $H_c$  is controlled by the magnetostriction coeff.  $\lambda_s$ .

Measurements show that  $\lambda_s$  linearly depends on crystalline fraction  $f$  (cf. fig. 8) with, as a first approximation, the typical behaviour

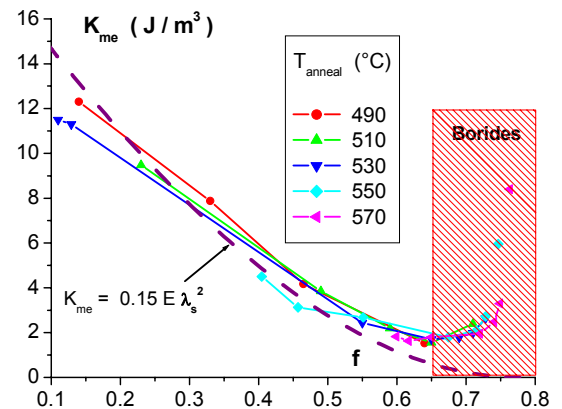
$$\lambda_s = f \lambda_c + (1-f) \lambda_a$$

$\lambda_c, \lambda_a =$  magnetostriction of crystalline and amorphous phases<sup>1</sup>.

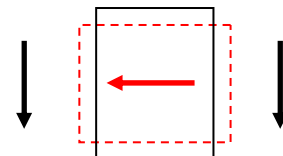
Starting from  $H_c, D, f$ , measurements,  $K_{me}$  is obtained from (2) and can be compared to  $\lambda_s$  measurements. With  $E =$  Young Modulus, it is experimentally obtained (cf. fig. 9)

$$K_{me} = \alpha E \lambda_s^2 \quad \alpha = 0,15$$

The  $\lambda_s^2$  dependency indicates that the source of stress is internal. Simple scaling argument explains that the source of Magnetoelastic frustration does not lie at the interface nanograin / amorphous but at the scale of the CV itself. According to quantitative modelisation [GEO 06], a reasonable scheme is that frustration occurs when the magnetization reverses in the CV : its shape (in black on Fig. 9) is imposed by the magnetization of the surrounding medium (black arrows), even when its own



**Fig. 9 : Evolution of  $K_{me}$  obtained from  $H_c$  measurements following (2) on Nanophy samples Comparison with a fit  $\approx E \lambda_s^2$ .**



**Fig. 10 : Schematic view of ME frustration occurring in CV at magnetisation reversal**

<sup>1</sup> An accurate modelisation has to take into account the  $f$  dependance of  $\lambda_a$  due to change in the amorphous phase composition and the contribution of surface magnetostriction to  $\lambda_c$  in the little grain sizes range [SLA 98], [NAN 01], [SZU 02]

magnetization (red arrow) would promote the red shape (dash line).

## 5 Additional properties

- \* Ribbon thickness  $\approx 20 \mu\text{m}$
  - \* Electrical resistivity  $\rho \approx 140 \cdot 10^{-8} \Omega$
- } → Nanocrystalline alloys = good candidates for medium frequencies applications

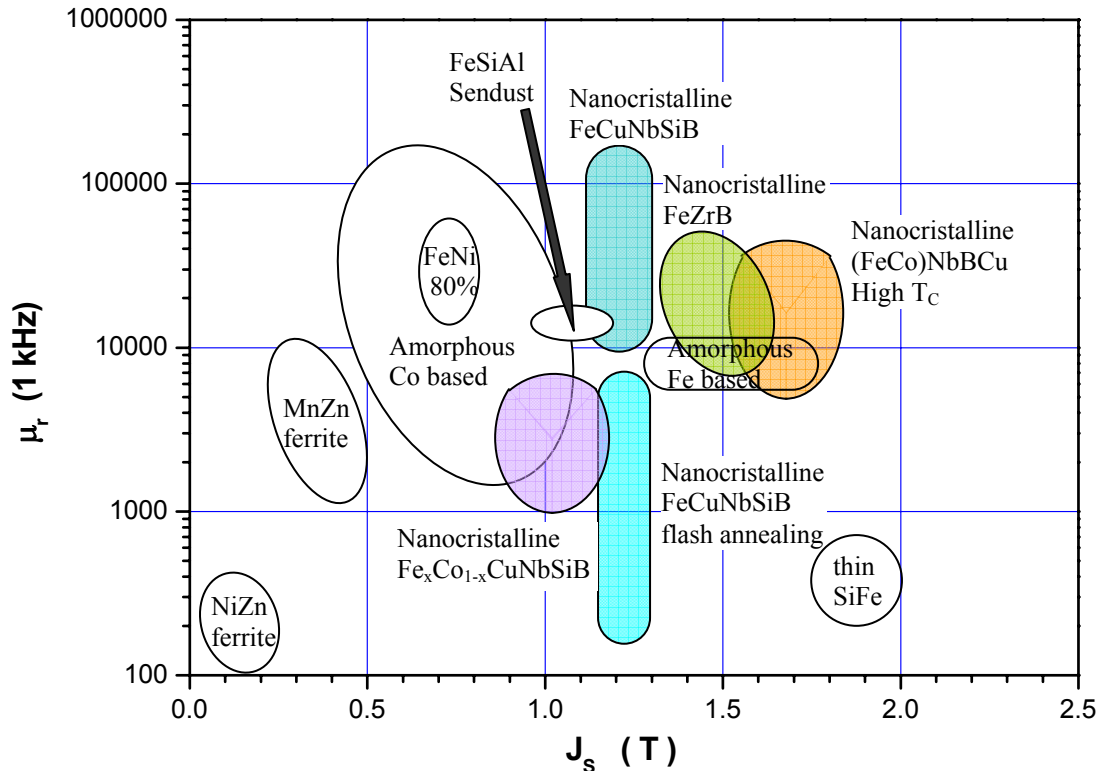


Fig. 11 : general view of soft magnetic materials for medium frequency applications [WAE 06]

- \* Magnetisation Saturation :  
 $J_s \approx 1,25 \text{ T}$  (Finemet)  $J_s \approx 1.7 \text{ T}$  (Nanoperm) [SUS 91]
- \* Operating Temperature  
 $\approx 150 \text{ }^\circ\text{C}$  limited by the Curie Temperature of the residual amorphous phase  $T_{Cam}$  (cf. Fig. 12)
  - ➔ Enhancement of  $T_{Cam}$  by partial substitution of Fe by Co in Finemet or Nanoperm (➔ Hitperm) [WIL 99], [MIT 04], [GER 06]

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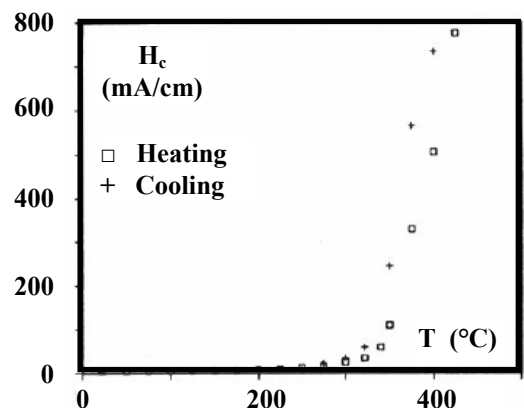


Fig. 12 : Coercivity of Finemet (annealed 1h 540 °C) as a function of temperature measurement [Her 89]

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